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56TH CONGRESS, HOUSE OF REPRESENTATIVES. DOCUMENT 2d Session. No. 530.

DEPARTMENT OF THE INTERIOR

WATER-SUPPLY

AND

IRRIGATION PAPERS

OF THE

UNITED STATES GEOLOGICAL SURVEY

No. 46

RECONNAISSANCES OF KERN AND YUBA RIVERS, CALIFORNIA.-Olmsted and Manson

> WASHINGTON GOVERNMENT PRINTING OFFICE 1901

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UNITED STATES GEOLOGICAL SURVEY

CHARLES D. WALCOTT, DIRECTOR

PHYSICAL CHARACTERISTICS OF KERN RIVER, CALIFORNIA

ΒY

FRANK H OLMSTED

AND

RECONNAISSANCE OF YUBA RIVER, CALIFORNIA

ΒY

MARSDEN MANSON



WASHINGTON GOVERNMENT PRINTING OFFICE 1901

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LETTER OF TRANSMITTAL.

DEPARTMENT OF THE INTERIOR, UNITED STATES GEOLOGICAL SURVEY, DIVISION OF HYDROGRAPHY, Washington, D. C., March 6, 1901.

SIR: I have the honor to transmit herewith two manuscripts for publication together in the series of papers upon water supply and irrigation.

The first manuscript is by Mr. Frank H. Olmsted, a civil engineer of southern California, and relates to the physical characteristics of the catchment area of Kern River, California. In this paper the author describes the drainage basin and estimates the amount of water coming from it and the power available from a complete utilization of the various portions of the stream. He also discusses the utilization of this power in pumping for irrigation.

The ultimate development of a considerable portion of the arid region depends not only upon complete storage and control of the streams, but upon the largest possible use of the power which may be generated in the upper or steeper portions of the channel and transmitted electrically out upon the plains, to be used in bringing to the surface the moisture which has sunk below the reach of the roots of the plants. By this means the area of cultivation can be greatly extended; and, as shown by Mr. Olmsted, the cost of pumping this water and applying it to the soil may, under favorable conditions, be less than that of obtaining a supply by gravity.

In earlier pamphlets of this series of Water-Supply Papers the utilization of wind power for this purpose has been discussed, the efficiency of the windmill has been described, and the advantages due to the small cost and independent construction of each mill have been shown. Where, however, it is practicable to obtain electric power at small cost, pumping plants operated by electricity can be widely distributed and may have certain advantages over the windmill. It is therefore important, in any discussion of the method of utilizing the water resources, to bring to public attention the possible developments along this line.

The second manuscript presented herewith has been prepared by Dr. Marsden Manson, and relates to Yuba River, a tributary of the Sacramento. Dr. Manson discusses the physical conditions and storage possibilities of this stream, bringing out particularly the importance of preserving the forest cover on the upper catchment basin,

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and, if possible, increasing this by artificial means; and shows by estimates the possible increase of available water through complete afforestation of the area. The relation of forests to river flow is believed to be of great importance, and is a matter upon which precise data are needed. It is hoped that as the systematic river measurements continue it will be possible to state more and more definitely the precise relation which the forest cover bears to the behavior of the stream.

The protection of the forests by the creation of reservations and the conservation of the waters through reservoirs constructed within these various reservations are of such vital importance to the utilization of the arid lands of the West, both by direct irrigation and by the creation of power for pumping water, that all matters pertaining to these subjects have interest to the citizens of the country as the great landowners.

It is for these reasons that these manuscripts are presented as contributions to a larger knowledge of the subject.

Very respectfully,

F. H. NEWELL, Hydrographer in Charge.

Hon. CHARLES D. WALCOTT, Director United States Geological Survey.

PHYSICAL CHARACTERISTICS OF KERN RIVER, CALIFORNIA, WITH SPECIAL REFERENCE TO ELECTRIC POWER DEVELOPMENT.

By FRANK H. OLMSTED.

INTRODUCTION.

The development of southern California has been retarded by three factors which are still operative: (1) Distance from the world's markets and commercial centers; (2) shortage of water; (3) lack of cheap fuel and power. Volumes might be written in regard to the relation which the development of water in southern California bears to the progress of the people, but broadly stated it may be said that the real development of this section will be defined and limited by the amount of water available for irrigation from San Diego to Santa Barbara and from San Pedro to the desert on the east. Regarding cheap fuel and power, neither Los Angeles, the commercial center of this section, nor any other place in southern California has had it. and even now, when it is reasonable to suppose that the local oil industry is at its best, the price of oil is approaching \$1 a barrel of 42 gallons; or, expressed differently, the cost of oil as fuel is equal to bituminous coal at \$4 a ton. During the last five years Los Angeles has had an industrial awakening corresponding to this decrease in the cost of fuel from \$7 or \$8 a ton to \$4 a ton.

During the first year of its advent in the Los Angeles market the cost of oil ranged between 0.40 and 1 a barrel. Most of the users of coal at that time found it economical to change their grates to oil burners, but since 1896 the tendency of the oil market has been upward, until now the cost of oil is 0.75 to 1 a barrel. At 1.50 a barrel oil as fuel is no cheaper than Gallup coal at 7 a ton, except that usually the oil feeder is arranged so as not to require an attendant, thus saving the wages of a stoker. In carload lots, the cost of Wellington bituminous coals is about 1 a ton more than the Eastern lignites; and, limited as the output has been, at present it virtually

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controls the Los Angeles market. During at least half of the year the demand in Los Angeles is so near the greatest available supply that outside orders for coal are not sought. The oil supply has contributed to the industrial advancement of southern California, and there are many reasons for believing that with cheap electric power



FIG. 1.-Map showing minor drainage basins of upper Kern River.

the manufactures and industries of southern California in general, and of the city of Los Angeles in particular, would quickly respond, and that their growth would be upon a safer foundation and a broader basis. The future outlook does not, however, warrant the hope for much better fuel rates, even with the construction of the

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INTRODUCTION.

Salt Lake Railroad assured; but there is good reason to expect cheaper power, and if this expectation is realized, the greater part of the power must come from Kern River.

PHYSICAL FEATURES.

Kern River rises on the western slope of the Sierra Nevada, the greatest mountain range in the United States. For a distance of 100 miles the average elevation of this crest line is more than 11,000 feet above the sea, and so great is the run-off that within the first 15 miles of its course the river receives 80 per cent of its total summer flow at the mouth of its canyon 100 miles away. The drainage area of the stream above the latter point is 2,349.3 square miles. Fig. 1 is a map showing the distribution of this drainage area, the minor drainage basins being outlined and their respective areas given. The following tables give the names and the respective areas of these minor drainage basins:

Areas of minor drainage basins of North Fork of Kern River.

Squ	are miles.
Headwaters	318.5
Whitney Creek	53.8
Small Creek	28.0
Ninemile Creek	7.5
Menache Creek	25.0
Trout Meadow Creek	25.5
Harris Creek	57.5
Tibbetts Creek	30.0
Brush Creek	49.5
Sa'mon Creek	31.0
Corral and other creeks	75.0
Little Kern River	142.5
Needles Creek	17.5
Clark Creek	26.0
Jackson Creek	27.5
Wade Creek	39.5
Tobias and other creeks	57.0
Bull Run Creek	28.7
Tilly Creek	30.0
Total to innetion of South Fork	1 070 0

Areas of minor drainage basins of South Fork of Kern River.

Squ	are miles.
Headwaters	165.0
Fish Creek	51.8
Middle tributaries	335.0
Lower tributaries from north	65.0
Lower tributaries from south	388.0

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Drainage areas of Kern River.

	Squ	are miles.
North Fork		1,070.0
South Fork		1,004.8
Tributaries from north side after junction		84.5
Tributaries from south side after junction		190.0
Total		-2,349.3

The length of Kern River from King River summit, on its main fork, to the mouth of the canyon above Bakersfield is 118 miles. The channel is in granite, and, with the exception of a few drops in the lower reaches of the stream, the grades are fairly uniform. In



the 62 miles above Kernville the stream falls 5,600 feet, and in the 48 miles below Kernville it falls about 2,100 feet. A view of the river near Kernville is shown in Pl. I, and a profile of the stream in fig. 2. Fig. 3 is a view of a mountain valley in the basin of the river.

The South Fork of the stream, which rises just south of Cirque Peak, is 83 miles long to its junction with the North (or main) Fork at Isabella. The main range of the Sierra Nevada drops off rapidly just south of Cirque Peak, which may account in a large measure for the comparatively small flow of the South Fork. This branch of Kern River possesses one decided advantage over the other branch,

[NO. 46.



VIEW OF KERN RIVER NEAR KERNVILLE.

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and over most California streams, in that it has a succession of particularly fine reservoir sites along a channel otherwise distinguished by reaches of rapid descent. A profile of the South Fork is shown in fig. 4.

The entire flow of Kern River is utilized for irrigation in the



FIG. 3. -- View of mountain valley in Kern River Basin.

southern end of San Joaquin Valley, and were it not for the great evaporation losses from the Buena Vista Lake reservoir the system could be called effective. The power of the stream, which, with one small exception, is available in large units, wastes itself upon the marbled bowlders and granite bed rock of the canyon, and suggests



an encouraging field for immediate investigation. The need of power in the agricultural valleys of California was never so apparent as now, after a series of dry years, when the ordinary flow of the streams has diminished to the extent of eliminating much hitherto valuable land, which of course precludes further development along gravity lines. Power applied to the pumping of water from the gravel beds which underlie most of the California streams where they debouch from their canyons at once solves the difficulty; and where the water plane is not far below the surface this method of irrigation

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FIG. 5.-Map showing points of stream measurements.

is in many ways more convenient and perhaps not more expensive than the ordinary canal.

VOLUME.

From daily measurements continued through a series of years the run-off of Kern River Basin is well established, though the precipita

U. S. GEOLOGICAL SURVEY

WATER-SUPPLY PAPER NO. 46 PL. II



VIEW OF GAGING STATION ON NORTH FORK OF KERN RIVER

OLMSTED.]

VOLUME.

tion and the local discharges in the watershed are still in question. Mr. Henry Hawgood, Mem. Inst. of C. E., who has made a careful study of the physical conditions existing in the watershed of Kern River, more particularly in that of the North Fork, has estimated the annual precipitation for the North Fork above Isabella at 25.4 inches, with a run-off of 12.5 inches. This would give a mean annual flow of the North Fork of 982 second-feet. Mr. Hawgood estimates the rainfall of the entire basin at 23 inches, and the mean run-off at 7.8 inches. On this last assumption the mean discharge of Kern River at its mouth would be 1,350 second-feet. As a fact, however, for the last five years (1895–1899)—a period of exceptional drought in the basin—the stream has had a mean annual discharge at First Point of Measurement, near Bakersfield (see map, Pl. III), of 864 second-feet, or 64 per cent of the normal assumed by Mr. Hawgood.

In June, 1900, stream measurements made by the writer above Kern Lake, about 90 miles above First Point of Measurement, showed that, when considered with measurements made at the latter place and making a time allowance for the distance between, the discharge of the upper part of the stream was 99 per cent of that of the lower part. The loss in volume in the passage of 939 second-feet of water (the amount flowing in the river just above Kern Lake on June 27, 1900) from Kern Lake to Bakersfield can not be stated accurately, but in the lower reaches of the stream, from Isabella to Bakersfield, where the conditions are similar, the loss when the flow was 1,333 second-feet was determined by the writer to be 3.21 second-feet to the mile. On this basis, on June 27, 1900, the flow of the North Fork just above Kern Lake was equal to 83 per cent of the flow of Kern River at First Point of Measurement. Fig. 5 is a map showing the points where stream measurements were made, and the following table gives the dates of the measurements and the discharge in second-feet, the numbers in the table corresponding to the numbers on the map.

Location.	Date.	Discharge.	Location.	Date.	Discharge.
$\begin{array}{c} 1 \\ 2 \\ 3 \\ 3 \\ 4 \\ 5 \\ 6 \\ 7 \\ 8 \\ 9 \\ 10 \\ 11 \\ 12 \\ 13 \\ 14 \\ 15 \\ \end{array}$	1900. (First Point of Measure- ment.) June 19 do June 20 June 21 June 22 do June 23 do June 23 do June 23 do June 24 June 24 June 25 do	$\begin{array}{c} Secft.\\ \hline 1.31\\ 14.18\\ 1,333.17\\ 2.30\\ 0.32\\ 3.45\\ 2.92\\ 5.07\\ 5.74\\ 4.26\\ 81.00\\ 1,154.90\\ 8.45\end{array}$	16 17 18 20 21 22 23 24 25 26 27 28 29 30	1900. June 25. June 29. June 25. June 27. do. do. June 28. June 29. do. do. June 30. June 30. July 2. do. July 3. do.	$\begin{array}{c} Secft.\\ 2.87\\ 1.80\\ 4.87\\ 939.60\\ 39.11\\ 4.72\\ 3.667\\ Dry.\\ 1.04\\ 8.222\\ 4.05\\ 2.38\\ 11.05\\ 1.96\\ 7.31\\ \end{array}$

Discharge measurements of Kern River and tributaries at points shown on map (fig. 5).

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Since September, 1893, the Kern County Land Company has made careful daily measurements of the flow of Kern River at First Point of Measurement. At Rio Bravo ranch, in sec. 11, T. 29 S., R. 29 E., M. D. M., $8\frac{1}{4}$ miles above First Point of Measurement, the flow of the river has been measured for many years by the State engineer of California. It is estimated by Mr. James, chief engineer of the Kern County Land Company, that there is a loss of 50 second-feet between these gaging stations. The accompanying tables give the monthly discharge of the river at Rio Bravo ranch for the years 1878–1884, inclusive, and at First Point of Measurement for the years 1893–1900, inclusive. On page 22 is a comparative table of the estimated daily discharge of the river during 1900 at First Point of Measurement and just below Tobias Creek, which is 17 miles above the mouth of the South Fork of Kern River and about 2 miles above the mouth of Salmon Creek, and enters the North Fork from the east.

On pages 22 and 23 is a table of miscellaneous discharge measurements of Kern River and its tributaries, and on the latter page are tables of rainfall at three places in Kern River Basin.

	Discharge in second-feet.				Run-off.	
Month.	Maxi- mum.	Mini- mum.	Mean.	Total in acre-feet.	Depth in inches.	Second- feet per square mile.
1878. November December			$\begin{array}{c} 400\\ 350 \end{array}$	23,802 21,521	$0.19 \\ .17$	$\begin{array}{c} 0.17\\ .15\end{array}$
1879. January February March April May July July August September October	$\substack{\begin{array}{c} 686\\ 745\\ 659\\ 1,054\\ 1,231\\ 1,290\\ 865\\ 387\\ 174\\ 210 \end{array}}$	$389 \\ 466 \\ 510 \\ 661 \\ 680 \\ 812 \\ 386 \\ 168 \\ 146 \\ 145 $	$\begin{array}{c} 462\\ 591\\ 552\\ 764\\ 927\\ 927\\ 535\\ 266\\ 171\\ 182 \end{array}$	$\begin{array}{c} 28,407\\ 32,823\\ 33,941\\ 45,461\\ 56,999\\ 57,778\\ 32,895\\ 16,356\\ 10,176\\ 11,191 \end{array}$	$\begin{array}{c} .23\\ .26\\ .28\\ .37\\ .46\\ .47\\ .26\\ .13\\ .08\\ .09\end{array}$	$ \begin{array}{r} 20 \\ 25 \\ 24 \\ 33 \\ 40 \\ 42 \\ 23 \\ 111 \\ 07 \\ .08 \\ \end{array} $
Season	1,231	145	514	371, 350	2.99	. 22
November December	325 650	$\frac{184}{280}$	261 356	$\frac{15,531}{21,890}$. 12 . 17	$\begin{array}{c} .11\\ .15\end{array}$
1880. January February March April June July August September October Season	$\begin{array}{r} 410\\ 380\\ 385\\ 3,320\\ 3,560\\ 4,070\\ 3,140\\ 1,500\\ 846\\ 794\\ \hline \end{array}$	$\begin{array}{r} 315\\ 315\\ 349\\ 395\\ 1, 615\\ 2, 740\\ 1, 550\\ 840\\ 710\\ 722\\ \hline 184\end{array}$	$\begin{array}{r} 354\\ 370\\ 389\\ 1,557\\ 2,659\\ 3,317\\ 2,196\\ 1,060\\ 767\\ 758\\ \hline \end{array}$	$\begin{array}{c} 21,767\\ 21,282\\ 23,919\\ 92,648\\ 163,496\\ 197,376\\ 135,027\\ 65,177\\ 45,640\\ 46,608\\ \hline \end{array}$	$\begin{array}{r} .17\\ .17\\ .20\\ .73\\ 1.31\\ 1.58\\ 1.08\\ .52\\ .37\\ .37\\ .37\\ \end{array}$	$\begin{array}{c} .15\\ .16\\ .17\\ .66\\ 1.14\\ 1.42\\ .94\\ .45\\ .33\\ .32\\ \hline 50\end{array}$
Season	4,070	10±				. 30

Estimated monthly discharge of Kern River at Rio Bravo ranch.



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Estimated monthly discharge of Kern River at Rio Bravo ranch-Continued.

	Dischar	ge in secc	ond-feet.		Run-off.	
Month.	Maxi- mum.	Mini- mum.	Mean.	Total in acre-feet.	Depth in inches.	Second- feet per square mile.
1880. November December	$\substack{830\\1,480}$	695 790	$\begin{array}{c} 767\\ 1,063\end{array}$	$45,640 \\ 65,361$	$\substack{\begin{array}{c} 0.37\\.52 \end{array}}$	$\substack{\begin{array}{c} 0.33\\ .45\end{array}}$
January February March April May June July August September October	$\begin{array}{c} 1, 640\\ 2, 970\\ 2, 100\\ 2, 612\\ 2, 710\\ 2, 390\\ 1, 520\\ 1, 200\\ 420\\ 360\\ \end{array}$	$\begin{array}{r} 950 \\ 1,430 \\ 1,400 \\ 2,100 \\ 2,060 \\ 1,475 \\ 710 \\ 420 \\ 320 \\ 310 \end{array}$	$\begin{array}{c} 1,078\\ 1,073\\ 1,570\\ 2,288\\ 2,362\\ 1,890\\ 1,126\\ 627\\ 361\\ 333 \end{array}$	$\begin{array}{c} 66,284\\ 98,471\\ 96,535\\ 136,145\\ 145,110\\ 112,462\\ 69,235\\ 38,552\\ 21,481\\ 20,475 \end{array}$	52.79.771.091.16.90.55.31.17.16	.46 .76 .67 .98 1.01 .81 .48 .27 .15 .14
Season	2,970	310	1,263	915, 751	7.31	.54
November December	$\begin{array}{c} 360\\ 410 \end{array}$	300 320	337 350	$20,053 \\ 21,521$	$\substack{.16\\.17}$	$\substack{.14\\.15}$
1882. January February March April May June July August September October	380 510 1,260 1,670 2,000 1,990 1,110	$310 \\ 360 \\ 440 \\ 920 \\ 1, 420 \\ 900 \\ 450 \\$	$\begin{array}{c} 335\\ 395\\ 600\\ 1,174\\ 1,670\\ 1,306\\ 726\\ 330\\ 330\\ 330\\ 330\end{array}$	$\begin{array}{c} 20,598\\ 21,937\\ 36,893\\ 69,858\\ 102,684\\ 77,712\\ 44,640\\ a20,291\\ a19,636\\ a20,291 \end{array}$	$ \begin{array}{r} .16\\ .18\\ .30\\ .56\\ .82\\ .62\\ .36\\ .16\\ .16\\ .16 \end{array} $	$\begin{array}{c} .14\\ .17\\ .26\\ .50\\ .71\\ .56\\ .31\\ .14\\ .14\\ .14\end{array}$
Season	2,000	300	655	476,114	3.81	. 28
November December			- 280 280	$a 16, 661 \\ a 17, 217$.13 .14	.12 .12
1883. January. February March April May June July August September October			$\begin{array}{c} 280\\ 350\\ 700\\ 1,170\\ 1,410\\ 1,170\\ 940\\ 470\\ 350\\ 280\end{array}$	$\begin{array}{c} a 17, 217\\ a 19, 438\\ a 43, 041\\ a 69, 620\\ a 86, 698\\ a 69, 620\\ a 57, 798\\ a 28, 899\\ a 20, 826\\ a 17, 217\end{array}$.14 .16 .35 .56 .69 .56 .46 .23 .17 .14	$\begin{array}{c} .12\\ .15\\ .30\\ .50\\ .60\\ .50\\ .40\\ .20\\ .15\\ .12\end{array}$
Season			638	464, 252	3.73	. 27
November December			200 200	$a{11,901 \atop a 12,298}$	$\begin{array}{c} .10\\ .10\end{array}$. 09 . 09
1884. January March April May June July August September October			$\begin{array}{c} 350 \\ 470 \\ 940 \\ 5,860 \\ 9,380 \\ 5,860 \\ 2,350 \\ 940 \\ 470 \end{array}$	$\begin{array}{c} a21,521\\ a27,084\\ a57,798\\ a117,818\\ a360,317\\ a558,148\\ a360,317\\ a144,496\\ a55,934\\ a28,899 \end{array}$	$\begin{array}{c} .17\\ .22\\ .46\\ .89\\ 2.90\\ 4.46\\ 2.90\\ 1.15\\ .45\\ .23\end{array}$	$\begin{array}{c} .15\\ .20\\ .40\\ .80\\ 2.50\\ 4.00\\ 2.50\\ 1.00\\ .40\\ .20\end{array}$
Season			2,422	a1,756,481	14.03	1.03

a Estimated from fragmentary records by State engineer.

Estimated monthly discharge of Kern River at First Point of Measurement.

[Drainage area used in previous reports, 2,345 square miles.]

	Discharge in second-feet.				Run	Run-off.	
Month.	Maxi- mum.	Mini- mum.	Mean.	Total in acre-feet.	Depth in inches.	Second- feet per square mile.	
1893. October November December	554 559 590	.517 .467 .430	$534 \\ 518 \\ 516$	$32,861 \\ 30,827 \\ 31,757$	$\begin{array}{r} 0.26\\.24\\.25\end{array}$	0.23 .22 .22	
1894. January February March April June June July August September October November December	$\begin{array}{c} 741\\ 1,114\\ 1,443\\ 1,892\\ 2,208\\ 1,719\\ 1,051\\ 549\\ 3&82\\ 3&68\\ 805 \end{array}$	5626047621,2091,228871400256172224230234	$\begin{array}{c} 661\\ 717\\ 1,001\\ 1,495\\ 1,607\\ 1,085\\ 700\\ 335\\ 248\\ 279\\ 244\\ 470\end{array}$	$\begin{array}{c} 40,644\\ 39,817\\ 61,541\\ 88,952\\ 98,798\\ 64,557\\ 43,036\\ 20,565\\ 14,756\\ 17,178\\ 14,500\\ 28,908 \end{array}$	$\begin{array}{c} .32\\ .32\\ .65\\ .71\\ .79\\ .51\\ .34\\ .16\\ .12\\ .14\\ .11\\ .23\end{array}$	$\begin{array}{c} .28\\ .30\\ .43\\ .64\\ .69\\ .46\\ .30\\ .14\\ .11\\ .12\\ .10\\ .20\\ \end{array}$	
The year	2,208	172	737	533, 252	4.40	. 31	
1895. January February. March April May June July August September October November December	$\begin{array}{c} 1,616\\ 4,762\\ 3,004\\ 3,897\\ 5,384\\ 3,721\\ 2,063\\ 1,073\\ 676\\ 612\\ 436\\ 447\end{array}$	$\begin{array}{r} 473\\675\\987\\1,911\\3,100\\2,174\\867\\354\\290\\276\\308\\368\\368\end{array}$	$\begin{array}{c} 809\\ 1,252\\ 1,374\\ 2,724\\ 4,369\\ 2,906\\ 1,482\\ 629\\ 344\\ 327\\ 346\\ 403\end{array}$	$\begin{array}{r} 49,762\\ 69,536\\ 84,437\\ 162,076\\ 268,608\\ 172,919\\ 91,113\\ 38,665\\ 20,469\\ 20,106\\ 20,588\\ 24,779\end{array}$	$\begin{array}{r} .40\\ .55\\ .67\\ 1.29\\ 2.14\\ 1.37\\ .73\\ 1.31\\ .17\\ .16\\ .17\\ .20\end{array}$	$\begin{array}{c} .34\\ .53\\ .59\\ 1.16\\ 1.86\\ 1.24\\ .63\\ .27\\ .15\\ .14\\ .15\\ .17\end{array}$	
The year	5,384	276	1,413	1,023,058	8.16	. 60	
1896. January February March April June June June September October November December	$\begin{array}{c} 3,101\\ 798\\ 2,089\\ 1,263\\ 3,370\\ 3,611\\ 2,210\\ 741\\ 473\\ 425\\ 416\\ 426\end{array}$	$\begin{array}{c} 377\\ 559\\ 652\\ 766\\ 934\\ 1,244\\ 741\\ 353\\ 234\\ 223\\ 288\\ 313\end{array}$	$\begin{array}{r} 747\\ 617\\ 951\\ 972\\ 1,401\\ 2,456\\ 1,316\\ 486\\ 304\\ 267\\ 355\\ 347\end{array}$	$\begin{array}{c} 45,931\\ 35,489\\ 58,475\\ 57,838\\ 86,144\\ 146,142\\ 82,762\\ 29,883\\ 18,089\\ 16,417\\ 21,124\\ 21,336\end{array}$	$\begin{array}{r} .37\\ .28\\ .47\\ .46\\ .69\\ 1.17\\ .66\\ .24\\ .14\\ .13\\ .17\\ .17\end{array}$	$\begin{array}{c} .32\\ .26\\ .41\\ .41\\ .60\\ 1.05\\ .57\\ .21\\ .13\\ .13\\ .15\\ .15\end{array}$	
The year	3,611	223	854	619, 630	4.95	. 36	
1897. January February March April June June July August September October November December	$\begin{array}{c} 832\\ 2,306\\ 2,044\\ 4,410\\ 5,342\\ 4,352\\ 1,536\\ 671\\ 363\\ 441\\ 477\\ 1,023\end{array}$	$\begin{matrix} 305 \\ 516 \\ 688 \\ 1,094 \\ 4,054 \\ 1,289 \\ 644 \\ 338 \\ 260 \\ 278 \\ 289 \\ 327 \end{matrix}$	$\begin{array}{c} 373\\ 809\\ 923\\ 2,914\\ 4,580\\ 2,309\\ 1,006\\ 469\\ 295\\ 340\\ 355\\ 422\end{array}$	$\begin{array}{c} 22,935\\ 44,930\\ 56,753\\ 173,395\\ 281,613\\ 137,395\\ 61,857\\ 28,838\\ 17,554\\ 20,906\\ 21,124\\ 25,948 \end{array}$	$\begin{array}{c} .18\\ .36\\ .45\\ 1.38\\ 2.25\\ 1.09\\ .49\\ .23\\ .14\\ .17\\ .17\\ .21\\ \end{array}$	$\begin{array}{c} .16\\ .35\\ .39\\ 1.24\\ 1.95\\ .98\\ .43\\ .20\\ .13\\ .15\\ .15\\ .18\\ \end{array}$	
The year	5,342	260	1,234	893, 248	7.12	. 53	

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Estimated monthla	y discharge of	f Kern River at	First Point of	f Measurement-Cont'd.
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	Dischar	Discharge in second-feet.			Run	ŀoff.
Month.	Maxi- mum.	Mini- mum.	Mean.	Total in acre-feet.	Depth in inches.	Second- feet per square mile.
1898.						
January	400	311	363	22,320	0.17	0.15
February	923	316	434	· 24, 103	.20	. 19
March	485	304	388	23,857	.20	. 17
April	1,342	371	735	42,247	. 00 26	. ƏU 21
Iuno	686	394	551	32 786	26	- 23
July	416	127	244	15,003	. 12	.10
August	142	86	120	7,378	. 06	. 05
September	294	80	116	6,902	. 06	. 05
October	232	127	160	9,838	.08	.07
November	188	136	166	9,877	.08	. 07
December	314	147	199	12,236	.09	. 08
The year	1,342	80	348	251, 743	2.01	. 15
1899.						
January	361	182	263	16,172	.13	. 11
February	365	258	302	16,772	.14	. 13
March	4,932	247	590	36,278	. 29	. 20
April	1,107	576	890	$\frac{100}{51}$.40	. 00
May	2,230	809	1 331	79,200	63	.50
July	894	229	489	30.057	.24	. 21
August	240	99	156	9,592	. 08	. 07
September	117	89	105	6,257	.05	. 04
October	229	86	160	9,838	.08	.07
November	385	183	221	13,151	.10	. 09
December	781	182	277	17,032	1.36	1.18
The year	4,932	86	468	338, 829	3.94	. 29
1900.						
January	1,048	266	362	22,259	.17	. 15
February	329	238	280	15,550	. 12	. 12
March Appell	502	307	413	20, 394	.21	. 18
Mow	1 969	440	1 111	68 312	- 22	
June	1.878	841	1,283	76.344	.61	.55
July	850	202	392	24,103	. 20	. 17
August	217	101	144	8,854	.07	.06
September	270	106	166	9,878	. 08	. 07
October	186	137	160	9,838	. 08	. 07
November	1,339	161	349	20,767	. 17	. 15
December	445	288	313	22,934	. 18	, 16
The year	1,969	101	459	332, 319	2.65	. 20

Thirteen-year mean of the discharge of Kern River, as compiled from the foregoing records of the State engineering department and the United States Geological Survey.

Season and year.	Discharge.		
1878-1879 1879-1880 1880-1881 1880-1881 1881-1882 1882-1883 1883-1884 1895 1896 1896 1897 1897 1898 1899 1900 Thirteen-year mean	$\begin{array}{r} Secft.\\ 514\\ 1,169\\ 655\\ 638\\ 2,422\\ 737\\ 1,413\\ 854\\ 1,234\\ 348\\ 468\\ 459\\ \hline 936\\ \end{array}$	$\begin{array}{c} Acre-fect.\\ 371, 350\\ 850, 361\\ 915, 751\\ 476, 114\\ 464, 252\\ 1, 756, 481\\ 533, 252\\ 1, 023, 058\\ 619, 630\\ 8993, 248\\ 251, 743\\ 338, 829\\ 332, 319\\ \hline 678, 953\\ \end{array}$	

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	July.		Aug	ust.	Septe	mber.	Oeto	ber.
Day.	First Point of Measure- ment.	Just be- low Tobias Creek.	First Point of Measure- ment.	Just be- low Tobias Creek.	First Point of Measure- ment.	Just be- low Tobias Creek.	First Point of Measure- ment.	Just be- low Tobias Creek.
1	Secft.	Secft.		$\begin{array}{c} Secft.\\ 334.00\\ 338.00\\ 306.20\\ 225.90\\ 224.38\\ 230.62\\ 225.90\\ 224.438\\ 2230.062\\ 225.90\\ 224.34\\ 225.90\\ 225.90\\ 224.34\\ 225.36\\ 226.00\\ 224.34\\ 225.38\\ 226.580\\ 226.580\\ 201.50\\$	$\begin{array}{c} Secft.\\ 108.31\\ 115.71\\ 108.31\\ 115.71\\ 131.89\\ 147.24\\ 190.01\\ 159.17\\ 156.86\\ 241.22\\ 221.09\\ 212.66\\ 188.13\\ 175.33\\ 174.77\\ 170.70\\ 66\\ 155.33\\ 174.77\\ 170.66\\ 155.60\\ 151.98\\ 146.16\\ 138.63\\ 139.29\\ 142.05\\ 153.44\\ 153.44\\ 155.78\\ 141.31\\ 153.44\\ 155.78\\ 151.31\\ 147.22\\ \hline \end{array}$	$\begin{array}{c} Secft.\\ 212,80\\ 310,40\\ 308,00\\ 274,28\\ 275,00\\ 273,29\\ 246,400\\ 244,00\\ 244,00\\ 244,80\\ 232,66\\ 232,58\\ 232,46\\ 232,268$	Secft. 144.95 142.44 141.92 146.64 154.68 164.04 164.77 157.39 153.30 151.08 152.02 156.04 158.50 156.19 	Secft. 204. 32 205. 20 208. 16 204. 12 202. 80 202. 80 202. 40 200. 80 201. 20 202. 14 201. 66 201. 20 201. 20 201. 20 200. 40
Mean			144.10	222.00	166.45	228.91		

Estimated daily discharge of Kern River for 1900.

Miscellaneous discharge measurements of Kern River and its tributaries.

Date.	Stream.	Locality.	Hydrographer.	Eleva- tion.	Dis- charge.
1898. July 10	North Fork of Kern River.	"A" channel, above junction with	F. H. Olmsted	Feet.	Secft. 17.00
Do Do Do Do	do do do South Fork of Kern River.	"B" channel "C" channel "D" channel 700 feet above junc- tion with North	do do do do		$199,00 \\ 107,00 \\ 8,00 \\ 13,00$
July	North Fork of Kern River	Fork. At mouth	do		330.00
Do	South Fork of Kern River.	At engineers' old	do		18.00
Do Do	do do	Sec. 6, T. 22 S., R. 36 E. Menache Meadows	do		$ \begin{array}{r} 10.00 \\ 5.30 \end{array} $
Aug. 29	Kern River	First Point of Meas- urement.	do		115.60
1899. Sept.2	do	do	do		99.22
1900. June 19	Basin Creek	Rankin's ranch,	do		1.32
June 20	South Fork of Kern River.	Walkers Basin. 700 feet above junc-	do		14.18
D0	River.	Hooper's mill bridge.	do		1,333.17
June 22	Tobias Creek	At mouth	do	3 200	$2.92 \\ 18$
Do Do	Salmon Creek	Near mouth	do		3.45
June 23	South Needles Creek	At Needles Peak	do	4,550	5.82

Date.	Stream.	Locality.	Hydrographer.	Eleva- tion.	Dis- charge.
1900. June 23 Do June 24 June 25 Do Do Do	Clark Creek Jackson Creek Wade Creek North Needles Creek Little Kern River Tibbetts Creek Harris Creek Onemile Creek North Fork of Kern River. Whitney Creek	Dry Meadowsdo do 	F. H. Olmsted	Feet.	Secft. 5.19 5.74 5.07 4.26 81.00 2.87 8.45 4.87 1,154.90 4.72 29111
Do	Creek south of Bald Mountain. North Fork of Kern River.	800 feet above Kern Lake.	do	6,560	939.60
June 29 Do	River. Tibbetts Creek North Fork of Brush Creek.	At 8,300 feet elevation At 5,800 feet elevation	do do do	~ 000	1.80 1.04
June 30	North Fork of Kerne River.	Above North Fork. At new gaging sta- tion 4,000 feet above junction with South Fork.	do	ə, 600	8.22 825.25
Do July 2 July 3 July 3 Do	Sauth Fork of Kern River. Powers ditch Neils ditch Hooper's mill ditch.	At Horse Aleadows T.25 S., R.35 E Near head Isabella At gaging station on Kern River.	do do do do do do	7,700 2,920	$ \begin{array}{r} 4.05 \\ 11.05 \\ 2.38 \\ 1.96 \\ 7.31 \\ \end{array} $

Miscellaneous discharge measurements of Kern River and its tributaries-Cont'd.

Precipitation in Kern River Basin.

DAUNT.

[Observer, Mountain Home sawmill.]

Year.	Sept.	Oct.	Nov.	Dec.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.
1895–96 1896–97	0.00	0.60	0.40	1.95	11.91 	0.83	5.13	11.01	1.30	2.70	0.65	0.50

KERNVILLE,

[Observer, Stephen Barton, Isabella.]

Season.	Sept.	Oct.	Nov.	Dec.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Total.
1895-96 1896-97 1897-98 1898-99 1899-00 1900-01	$\begin{array}{c} 0.00\\ 0.15\\ 0.04\\ 0.00\\ 0.79 \end{array}$	$\begin{array}{c} 1.15\\ 0.38\\ 0.00\\ 0.78\\ 0.10 \end{array}$	$\begin{array}{c} 0.41 \\ 0.00 \\ 0.00 \\ 0.85 \\ 5.09 \end{array}$	$\begin{array}{c} 0.85 \\ 1.28 \\ 0.33 \\ 0.73 \\ 0.00 \end{array}$	$\begin{array}{c} 3.52\\ 3.40\\ 0.58\\ 1.95\\ 0.80\end{array}$	$\begin{array}{c} 0.00\\ 3.60\\ 0.99\\ 0.19\\ 0.53\end{array}$	$1.54 \\ 2.57 \\ 0.58 \\ 1.89 \\ 0.58$	$\begin{array}{c} 0.86\\ 0.10\\ T.\\ 0.28\\ 0.52\end{array}$	$\begin{array}{c} 0.00\\ 0.00\\ 0.54\\ 0.25\\ 0.90 \end{array}$	$\begin{array}{c} 0.\ 20 \\ 0.\ 00 \\ 0.\ 00 \\ 0.\ 45 \\ 0.\ 00 \end{array}$	$\begin{array}{c} 2.25 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \end{array}$	$\begin{array}{c} 0.05 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \end{array}$	$12.08 \\ 4.50 \\ 5.38 \\ 5.69$

MOUNT BRECKENRIDGE,

[Observer, G. Otterman.]

Season.	Sept.	Oct.	Nov.	Dec.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.
1896-97 1897-98	0.00	0.00	2.20	4.30	2.00	4.67	7.72	0.00	0.40	0.10	0.00	0.00
1898–99					1.67	0.94						

The rain gage at Daunt is at the Mountain Home sawmill, near the divide between Kern and Kaweah rivers, and at an elevation of 6,600 feet. Kernville is at an elevation of 2,600 feet, and Mount Breckenridge at an elevation of 6,750 feet.

From the diagram (fig. 6) showing synchronous discharge and temperature observations at First Point of Measurement for the months of April, May, and June, 1897—the particular season of the year when the factor of snow enters prominently into the regimen of the river we gather, by connecting the peak points of flow and temperature, that ordinarily it requires about forty-seven hours for the stream waters to pass from the snow line, about 100 miles up the river, to



tions at First Point of Measurement. Dotted lines are temperature curves; heavy lines are discharge curves.

First Point of Measurement. Under ordinary circumstances the melting of snow below the 7,000-foot contour would accompany a low gage, and the mean velocity would of course be relatively slow compared with a larger stream. The run-off of the heavy snows would start certainly not lower than the 8,500-foot contour, and invariably would be accompanied by a general breaking up of winter in the higher mountains, resulting in a high gage throughout the entire stream; from which we may infer that there is no marked difference in the time required for the passage of snow water between points as much as 30 miles apart to the canyon mouth. When the spring rise begins the mean velocity of the stream waters from the snow line, 60 miles
up, to First Point of Measurement must be about 1.90 feet per second. When the snow line reaches the 8,500-foot contour, 100 miles upstream, the flood velocity is approximately 3.1 feet per second. This 1.2-footper-second play in velocity between high and low snow water gage in the stream represents the only data available for estimating, even crudely, the velocity-slope relations during the remainder of the year.

POWER POSSIBILITIES.

Elevations and distances have been and still are to a certain extent assumptions, and were it not that the data in some form is in demand, it certainly would be desirable to possess more basic information of Kern River Basin before undertaking to even outline the power possibilities of the stream. The flood period of the year is May and June; the minimum flow occurs in September and October. During extremely dry years the flow at First Point of Measurement drops to 80 second-feet, with a probable mean for the month in which this occurs of, say, 100 second-feet.

In the reach between First Point of Measurement and Isabella the stream has been affected by losses from evaporation and seepage and by increment in flow due to the South Fork, Clear Creek, and other small tributaries. The net result of these plus and minus factors is estimated to be a loss between these points of 122 second-feet. Calling this loss 120 second-feet, and taking the minimum flow at First Point of Measurement (80 second-feet), we have, as the least flow of the river at the latter place, 200 second-feet. Between Isabella and First Point of Measurement the fall is about 1,900 feet, giving more than 42,000 theoretical horsepower. At Isabella the mean flow for the full year 1899 was 588 second-feet, for 1898 it was 469 second-feet, and for 1897 it was 1,353 second-feet. Below Isabella the topography on the right bank is not unfavorable for the construction of a large canal, but the immense bowlders which cover the southern and western sides of the Greenhorn Mountains, and which are constantly in transit down the slopes, are not an economical factor in canal construction.

Of the total flow of Kern River at First Point of Measurement 80 per cent passes Functions on the North Fork, or a point of equal elevation (7,050 feet) on the South Fork, which would be about midway between the lower end of Menache Meadows and the mouth of Fish Creek. The theoretical power possibilities of the stream below these places would be, then, about 500,000 horsepower, which, for a watershed of 2,349.3 square miles in an arid region, evidences the remarkable advantages of the stream, so far as grades and discharge are concerned, for electrical-power development.

The Kern River Company, which has been engaged for the last four years in securing rights of way (now approved by the Department of the Interior), and in arranging preliminaries incident to the construction of so large a plant, has as yet accomplished nothing in the way of actual building. A plan of the reservoir site of the company is shown in fig. 7. The diversion works of their power canal will be in



FIG. 7.—Plan of reservoir site of Kern River Company. Area, 1,121 acres; storage capacity, 42,000 acre-feet; height of dam, 72 feet.

the lower end of the town of Kernville, where the river forks. The West Fork is to be deepened so that during low stages this branch will gather all of the water of the river, and a low training wall, over which floods of the river will pass, will be built. The head gate will be 3,600 feet distant, on bed rock, and of solid masonry. The standard cross section of the canal for the first 10 miles is 25 feet wide at bottom, 7.5 feet depth of water, and on a grade of 1.058 feet to the mile. At a distance of $4\frac{1}{2}$ miles from the head gate the only considerable structure on the line is encountered—the bridge over Kern River. After passing that point the cross section of the canal is reduced and the grades are increased accordingly.

The plans of the company are based upon a minimum flow of Kern River past their diversion works of 400 second-feet. This, considering the storage proposed on Salmon Creek, which is described further on, is a conservative estimate for any ordinary series of years, but could not have been maintained in 1899-1900, although in nine out of ten years it easily could be increased to 500 second-feet. The plans are based on an available head at the wheels of 230 feet during extreme high water, with an additional head of 40 feet when the river is at its minimum stage. Mr. H. Hawgood, the chief engineer of the Kern River Company, has designed, as a generating unit, a water wheel of 1,500 horsepower, with an alternator of 1,030 kilowatts capacity. There are to be nine of these units-eight for daily service and one to be held in reserve. For the additional 40-foot head possible during low water, there will be a 750-horsepower wheel and one 550-kilowatt alternator. On this basis, at no time would there be supplied to the wheels less than 11,200 horsepower. The impulse type of wheel would give an efficiency of 80 per cent, the alternators an efficiency of 95 per cent, and the step-up transformers an efficiency of 98 per cent, thus delivering to the line 8,342 horsepower. Assuming 5 per cent average loss in transmission (a larger allowance than the 80-mile carriage of the Southern California Power Company's current indicates is necessary), there would be delivered at the Los Angeles power house 7,825 horsepower, and with 98 per cent efficiency in the step-down transformers there would be 5,720 kilowatts for daily distribution in the city. This delivery could be increased 50 per cent for an hour to take care of the maximum load, which occurs between the hours of 5 and 6 p.m. Speaking conservatively, and having in mind the ruling rates elsewhere on the Coast, this 7,668 horsepower should command 1¹/₃ cents per horsepower per hour. During the irrigating season of 1900 the municipality of Los Angeles paid 2.2 cents per horsepower per hour for power registered between the hours of 11 p. m. and 5 p. m., and 4.4 cents per horsepower per hour for power registered between the hours of 5 p. m. and 11 p. m. In large plants working eighteen hours a day, and with good bituminous coal at \$4 a ton, the cost of 1 horsepower per year would be \$85, and in small plants, where the attendance factor is relatively greater, the cost would be \$150. At the rate of $1\frac{1}{3}$ cents the cost of a horsepower per year of three hundred and thirteen working days is \$75. At this rate the gross annual revenue of the plant would be \$768,000.

The company's estimate of the cost of construction of the plant and lines for the transmission of the current to Los Angeles is, approximately, \$1,333,000. Using direct-connected motor and centrifugal pumps, with 30 feet depth of wheel pit and 20 feet additional lift, and assuming the duty of water to be 8 acres per miners' inch, 1.42 horsepower would irrigate 100 acres at the rate of, say, \$2.50 per acre per annum. This would be on the basis of a 50-foot lift and a rate of 2 cents per horsepower per hour for the current. The efficiency of pumping plants ranges from 20 to 68 per cent—frequently plants are condemned solely because of a lack of skillful assembling of the units.

Electric motive power possesses many advantages over either steam or gasoline plants for pumping water, and in actual cost of service it may be questioned whether it is not to be compared with many wellmanaged canal systems of the State. The Kern Land Company has twenty-five pumping plants in operation near Bakersfield, each delivering from 1,400 to 2,000 gallons a minute. These plants each consist of four wells in a line, sunk to a depth of 80 to 130 feet through strata of alluvial loam, clay, and water-bearing sand. The wells are cased with galvanized iron, 13 inches in diameter, No. 16 gage, perforated with vertical slits opened one-sixteenth of an inch. It was the practice of Mr. Lewis A. Hicks, the engineer in charge of this work, to land the casing in clay, and to perforate for all sand below a depth of 30 feet. Surface water was generally encountered at about 15 feet. In each plant the four wells are 6 feet apart on centers, and by experiment it was found that the flow from the four was generally a little more than double that from one. The total lift for most of these plants was about 35 feet.

After many experiments to determine the pump best suited to these conditions, a centrifugal pump, connected directly to the motor and working on a vertical rod, all thoroughly bolted to steel framework, was found to give the greatest efficiency and the least trouble in operation—one attendant looks after ten plants, and there have been months when the plants were in operation 98 per cent of the time. The farmers under the Kern Land Company's water supply are taxed 75 cents per acre-foot for irrigating water from these electrically driven pumping plants, and as the land requires 2 acre-feet annual irrigation the expense is \$1.50 per acre per year. It is not probable that the rate of $1\frac{1}{3}$ cents per horsepower per hour could be maintained in Antelope Valley or farther south in San Fernando Valley for irregular demand, but there is no good reason why a 2-cent rate could not be maintained by any of the Kern River companies.

The 68 per cent efficiency obtained in many of the Kern Land Company's plants deserves more than passing notice. In electrically driven pumping plants 55 per cent efficiency (reckoned from the meter consumption to the foot-pounds raised) is very good, but when this is raised to 68 per cent, the method employed to obtain this result merits a detailed description. The following is quoted from one of Mr. Hicks's reports:

The pumps are of the Pit type, provided with 10-inch outlet, automatic balance, heavy shaft, and runners of special curvature adapted to the speed and height of lift, and a delivery of 5 to 6 cubic feet per second. The bearings are provided with sight-feed oil cups, and the feed on the upper bearing is upward against the water with which the stuffing-gland chamber is filled. The chamber is provided with a gage glass to enable the attendant to note any leak through the packing. The pump is bolted to cast-iron pedestal set on a wooden base, and the steel angles which support the motor are attached to the same pedestal. The assembling of the pumps and frame was accomplished in the shops, and the completed unit was hauled to its destination and lowered into place on the floor of the pit, only requiring to be guyed to a perpendicular position in the anchor frame to be ready to receive the motor. The adjustment of the thrust of the pump can be altered so as to carry the entire weight of the motor and shafting or such portion of it as may be desirable. It has been found preferable to separate them with 100 to 200 pounds down thrust, as there is a tendency to bow out the shaft between bearings if it is thrown into compression with resulting vibration. The motor is provided with adjusting screws, so that its position in vertical or horizontal planes can be easily changed with a hand wrench. The pump, motor, and frame constitute a self-contained unit, so that any settlement of foundation does not





alter the relative position of either machine, and can be quickly rectified, should it occur, by guying the frame back to a vertical position. The motors used for this installation are the ordinary type of 30-horsepower inductive motor, equipped with special end shields to adapt them for vertical use. The oiling is accomplished by means of centrifugal force, which is utilized to lift the oil from the inside periphery of a revolving cup to the top of the bearings, whence it returns to the oil cups through oil grooves along the shaft. The motors are wound for a potential of 550 volts, and as the transformers at these points can be connected up to 605 volts, the effective heating overload is greatly reduced.

The Kern River Company's transmission line from the power station at the mouth of Clear Creek to Los Angeles would be 105 miles long, map measurement, and 108 miles when the vertical departures are considered. The line begins at an elevation of 2,450 feet, and its southern terminal at Los Angeles is 350 feet above the sea. A number of mountain ranges would be crossed, but a large proportion of the line would be over good ground, and it is believed that the highest elevation reached (6,500 feet, at Tehachapi) will offer no serious obstacles to a daily inspection of the pole line.

A reservoir on Salmon Creek, a tributary of Kern River, is planned by the Kern River Company for the storage of 47,000 acre-feet of water. About 20,000 acres can be made tributary to this intake, and it is hoped that with this catchment basin and the precipitation from an elevation of 7,700 feet on this divide the reservoir will supplement the flow of Kern River to 400 second-feet during the particular season of any year when the normal flow is below that figure. Fig. 8 is a cross section of the dam site on Salmon Creek. It is in a



FIG. 9.—Plan of reservoir site of Kern-Rand Electric Power Company. Area, 3,562 acres; storage capacity, 63,722 acre-feet; height of dam, 65 feet above stream bed.

granite canyon, with clean bed rock on bottom and sides. The width at the bottom is 125 feet between walls; the top width at the 75-foot level would be 390 feet. A rock-fill dam is estimated to require 26,000 cubic yards of material and to cost $\$80,000.^1$

The utilization of the higher reaches of Kern River for power purposes will certainly be accomplished in time, but for the present,

¹Reservoirs for Irrigation, Water Power, and Domestic Water Supply, by J. D. Schuyler.

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and with the disinclination of electrical engineers to recommend the transmission of power to distances greater than 100 miles, it is doubtful whether the market outside of Los Angeles will warrant the outlay; and the latter city is so far away from the upper river as



FIG. 10.—Plan of dam site of Kern-Rand Electric Power Company.

to preclude, for the present at least, supplying it with power from that source.

The Kern-Rand Electric Power Company, of Los Angeles, purposes to construct a rock-fill dam on the South Fork of Kern River, at Menache Meadows, and an initial power station near the upper end





some recent geological time Menache Meadows must have been an immense mountain A dam 65 lake. high feet would throw the water back 6 miles from the canyon mouth, in two arms 6 miles apart. A dam of that height would store 63,700 acrefeet of water at a mean depth of 18 There is no feet. question that in an ordinary year the drainage area tributary to the South Fork and above the Meadows (165 square miles) would furnish ample storage water for this reservoir, although it is probable that in a season like that of 1899-1900 there would be a short-There is no age. reliable data for determining the minimum precipitation in Menache Meadows, for generally the snows lie so deep over the mountains surrounding the basin to as make it impenevear.

capacity of the reservoir

the

trable during at least the colder half of the

Height above base of dam.	Surface area.	Capacity.
Feet. 10	$\begin{array}{c} Acres. \\ 22 \\ 146 \\ 812 \\ 1,865 \\ 2,599 \\ 3,254 \\ 3,814 \\ 4,420 \\ 5,830 \end{array}$	$\begin{array}{c} A cre-feet, \\ 110 \\ 954 \\ 4,563 \\ 18,827 \\ 40,732 \\ 39,885 \\ 105,236 \\ 146,419 \\ 248,852 \end{array}$

Capacity of Menache Meadows reservoir site.

Fig. 9 is a plan of the reservoir site of the Kern-Rand Electric Power Company in Menache Meadows, fig. 10 is a plan of the dam site, and figs. 11, 12, and 13 are details of the dam proposed. The material at the dam site is apparently hard granite, overlain with earth, sand, and gravel. The dam site is at an elevation of 8,200 feet above the sea, and consequently snow and frost prevail there during the winter months. There is no wagon road to the dam site, and the cost of making one would add very materially to the cost of the dam. The drainage area tributary to this reservoir being all above an elevation of 8,200 feet, naturally has the greater part of its precipitation in the form of snow. This makes the run-off an uncertain quantity, and leaves the proper height for the dam a difficult question to decide.

Taking all of these considerations into account, the engineers of the company were led to select a loose rock-fill dam faced with earth as the most economical and serviceable for the locality. On account of the possible action of frost, flatter slopes were given the rock faces than are absolutely necessary to make the dam heavy enough to resist the water pressure. So far as possible, the material found in the immediate vicinity of the dam will be used in its construction, and the outlet, gates, and connections have been designed so that all of their parts can easily be transported on mules over a steep yountain trail. The crest of the dam was fixed at 65 feet above the natural surface of the ground at the dam site. This height can, however, be increased to 95 feet, if it is found that a larger reservoir capacity could be supplied, at a proportionate increase in cost. It is proposed to excavate all of the rock required in the construction of the dam on the north side, forming a suitable wasteway in the solid rock, capable of discharging a stream of water 100 feet wide and 9 feet deep at a velocity of 6 feet per second—a volume of 5,400 cubic feet per second. As each foot rise of water over the bottom of the wasteway represents about 5,000 acre-feet, 9 feet rise of water in the wasteway would increase the volume in the reservoir to 45,000 acre-feet. This, in addition to the water running through the wasteway and outlet. would make more than 50,000 acre-feet, which, if it all came in twenty-four hours, would represent a run-off of about 54 inches. It

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is believed that a wasteway of this size would make the dam absolutely safe against any possibility of the water ever flowing over the top. The capacity of the reservoir with a dam 65 feet high, as now



FIG. 12.—Vertical section of tower for dam proposed by Kern-Rand Electric Power Company, showing arrangement of gates.

proposed, would be 63,700 acre-feet; and if the dam were raised hereafter to a height of 85 feet the capacity of the reservoir would be nearly trebled.

OLMSTED.]

It is proposed to take the water from the reservoir by means of a tunnel through the solid rock on the south side of the dam. The masonry or concrete tower (see figs. 11, 12, and 13) is designed as an inlet to this tunnel and to accommodate the placing of the gates in



FIG. 13.—Sectional elevation and plan of gate tower for dam proposed by Kern-Rand Electric Power Company.

the most simple and economical manner. The gates are so simple and so easily opened and closed that it has not been considered necessary to provide for their repair under a full head of water in the reservoir. Fig. 12, however, shows a simple and economical way of shutting off the water after it has fallen to an elevation of 8,260 feet, or 35 feet above the base of the dam. This would prevent the necessity of emptying the reservoir for the purpose of making repairs to the gates.

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Following are the estimates for three sizes of the dam proposed:

Estimate of cost of a 75-foot dam with slopes 1 to 1 and ³/₄ to 1.

Loose rock, 73,000 cubic yards; or 43,800 cubic yards solid	
at \$1.50	\$65,700.00
Earth, 55,870 cubic yards at \$0.25	13,967.50
Extra labor on 5,000 cubic yards laid by hand, at \$1	5,000.00
Tunnel, 350 feet at \$12	4,200.00
Tower, gates, and connections	15,000.00
Guide walls, etc., at wasteway	15,000.00
	118,867.50
Engineering and contingencies, 10 per cent	11,886.75
Total	130, 754, 25

Estimate of cost of 75-foot dam with slopes $1\frac{1}{2}$ to 1 and $\frac{3}{4}$ to 1.

Loose rock	91 000 cubic	vards: or 54 600	cubic vards solid

120000 room, or, or or, or or, or	
at \$1.50	\$81,900.00
Earth, 55,870 cubic yards at \$0.25	13,967.50
Extra labor on 6,000 cubic yards laid by hand, at \$1	6,000.00
Tunnel, 350 feet at \$12	4,200.00
Tower, gates, and connections	15,000.00
Guide walls, etc., at wasteway	15,000.00
	136,067.50
Engineering and contingencies, 10 per cent	13,606.75
Total	149,674.25

Estimate of cost of 95-foot dam with slopes 1 to 1 and ⁸/₄ to 1.

Loose rock, 110,000 cubic yards; or 66,000 cubic yards solid at	
\$1,50	\$99,000
Earth, 70,000 cubic yards at \$0.25.	17,500
Extra labor on 7,000 cubic yards, at \$1	7,000
Tunnel, 350 feet at \$12	4,200
Tower, gates, and connections, with bridge to tower	17,000
Guide walls. etc., at wasteway	20,000
	164,700
Engineering and contingencies, 10 per cent	16,470
Total	181, 170

The foregoing estimates are based on the supposition that the rock will be hard enough to stand vertically around the tower and that the tunnel will not need lining.

The transmission line from the power plant in sec. 14, T. 25 S., R.

35 E., M. D. M., to Randsburg, 43 miles distant, would be over as fine a country for a pole line as can well be found—easy slopes, virtually unimproved and without tree growth. With very few exceptions a wagon could be driven, without road work, along the transmission line from the power plant to Randsburg. The highest elevation reached on the pole line would be at Walkers Pass, 5,320 feet above sea level, and at that point the snow lasts only a few days and would never interfere with the regular patrol of the line.

The following is an approximate estimate of the cost of generating and transmitting electric current from the South Fork power house, for a delivery in Randsburg of 900 horsepower, with conduit and poleline capacity for 450 additional horsepower:

Estimate of cost of generating and transmitting electric current from South Fork power house to Randsburg.

Regulating gate 1,00 Riveted-steel pipe, 8,000 feet of 30-inch, gage No. 12, at \$2.70 21,60 Pipe work in canyon, 8,000 feet 10,00 Flume, 3,500 feet at \$3 10,50 Tunnel, 1,300 feet at \$10 13,00 Canal in earth, 3,000 feet, with concrete lining 6,75 Canal in rock, 1,594 feet at \$1.50 per foot run 2,36 Siphon, 1,000 feet at \$3 3,00 Penstock, 4,000 feet at \$4 16,00 Water wheels 6,00 Power houses, two, fireproof 6,00 Wire for transmitting current, 900 horsepower, delivered 43 13,00 miles 13,00 Telephone 2,00 Line poles (43 miles, 40 to the mile), and placing same 20,00 Distribution of current at Randsburg 5,00	00
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Distribution of current at Randsburg 5,00	00
	00
170, 2	41
Contingencies, 15 per cent	36
Total	77

A landslide has blocked the canyon and created a lake of about 40 acres area on the North Fork of Kern River just below the mouth of Whitney Creek and above the mouth of the Little Kern. This lake, known as Kern Lake, the California State engineering department, in its investigations of the Kern River drainage basin, has considered as a possible reservoir site. At the lower end of the lake the eliffs tower almost vertically above it to heights ranging from 2,000 to 3,000 feet, and estimates have been made for the blasting of large fragments into the dam site, forming a loose rock-fill dam. The capacity of the reservoir at the 220-foot level would be 46,000 acre-feet. The State

engineering department considered the possibility of paving the mass of rock thus thrown down to a uniform surface and covering it with asphalt. The width of the canyon at the site is only 100 feet at the bottom and 400 feet at a height of 230 feet above the stream bed. There would be no question about the ability of the drainage basin to fill the reservoir annually, and if it is possible to construct such a dam at this place the site probably would be of value for replenishing the late summer flow for power and irrigation.

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RECONNAISSANCE OF YUBA RIVER, CALIFORNIA.

By MARSDEN MANSON.

WATERSHED.

Yuba River is a tributary of Feather River, which it enters at Marysville, 30 miles above its mouth. It drains about 1,357 square miles of the western slope of the Sierra Nevada, comprising portions of Sierra, Nevada, Plumas, and Yuba counties. The extreme length of the watershed is about 60 miles, the extreme width 36 miles. In addition to the length given there are about 11 miles of channel in the valley between the foothills and Feather River. In size Yuba River is fourth in the Sacramento Valley. Its extreme low-water discharge is about 360 cubic feet per second,¹ its mean winter discharge 1,500 cubic feet per second, and its flood discharge 26,000 cubic feet per second.² For the lower 10 miles of its course in the foothills the river is greatly clogged with débris from hydraulic-mining camps (estimated at many million cubic yards), and is between levees which have been raised from year to year to meet the overflow caused by the filling up of the area between them. The channel of the river in the lower foothills has been filled with cobbles and gravel to a depth of more than 100 feet. (See Pl. IV, B.) From the foothills to the mouth of the river at Marysville the channel is over a surface of gravel, sand, and clay, recently built up from the mines above. The channels are irregular and change from winter to winter and sometimes during the summer. It is therefore impracticable to establish lowwater gaging stations which would serve for more than one summer and fall and which would be suitable for winter or flood-stage gagings.

¹This is not as small as the natural discharge would be. The large mining companies—the South Yuba Canal Company, the North Bloomfield Gravel and Mining Company, the Milton Excelsior Water and Mining Company, the Eureka Lake and Yuba Canal Company, and others store large volumes of water during the winter and spring months for use during periods of low water in the late summer and the early autumn.

² Extreme flood discharge estimated by Mr. Hubert Vischer, Asst. Engr., U. S. Engrs., at 125,000 cubic feet per second. H. R. Doc. No. 431, Fifty-sixth Congress, second session, p. 12.

The changes in the bottom and in the position of the channel are so great that the gagings at the flood stages of the river would be unsatisfactory, and if undertaken from boats would be highly dangerous, if not impossible.

The drainage basin is subdivided into five small basins, namely, North Fork, with a drainage area of 491.6 square miles; Middle Fork, with a drainage area of 218 square miles; South Fork, with a drainage area of 360 square miles; Deer Creek, with a drainage area of 89.6 square miles; and Dry Creek, with a drainage area of 105.5 square miles. In addition to these an area of 92.5 square miles drains into the main stream above the 100-foot contour. Dry Creek joins Yuba River from the north just as it leaves the foothills. The other streams unite in the mountains. The forks are perennial in flow, but the



FIG. 14.—Map of Yuba River, showing location of gaging stations.

discharge of the two creeks mentioned (Deer and Dry) becomes insignificant in the late summer and early autumn.

As they merge into the valley the Sierra foothills have an elevation of about 100 feet above tide. The watershed rises gently, in rounded and broken mountains, to the crest of the Sierra, which at the headwaters of the Yuba is at a mean elevation of about 8,200 feet, with peaks rising to a height of 9,100 feet. From Mount Lincoln—a peak common to the watersheds of Yuba, American, and Truckee rivers to a point about $2\frac{1}{2}$ miles northeast of Mount Webber, the summit of the Sierra divides the watershed of Yuba River from that of Truckee River, which discharges into Humboldt Basin. Farther north from Mount Webber there is a secondary crest which divides the watersheds of Yuba and Feather rivers, the watershed of the latter stream reaching farther east, to a less elevated divide in which the passes are lower than those of the easterly crest.

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A. HEAD OF SOUTH FORK OF YUBA RIVER AND LAKE SPAULDING.



B. YUBA RIVER IN THE FOOTHILLS.

TOPOGRAPHY.

The western and lower portions of the drainage area are composed of slates and kindred rock, very much eroded and merging into the gravel and alluvial deposits of the great valley of California. The upper portions of the basin are composed principally of lavas and granites, all deeply eroded, particularly the lavas. Some idea of the magnitude of the erosion may be obtained when it is considered that it has required at least 4,000 (possibly 6,000) cubic miles of denuded materials to fill the great valley of California to its present level, and that most of this has come from the Sierra Nevada.

A stratum of serpentine traverses the watershed of Yuba River in a direction generally parallel with the crest of the Sierra. It is intersected by the North Fork at Goodyears Bar, by the Middle Fork near Moores Flat, and by the South Fork just east of Washington, and leaves the drainage basin of the Yuba, passing near Towle Station on the Central Pacific Railroad. This stratum is generally softer and more easily eroded than adjoining strata, and through it the canyons of the various forks are upon lighter grades than immediately above and below, and they generally are wider. This softer material also controls the loci of longer and more deeply eroded tributaries, which afford approaches to the main canyons for roads and trails. This stratum is of further interest because it is the dividing line between the auriferous strata in the watershed. To the west of it the mines are more extensive, the occurrences of gold-bearing rock to the east being irregular and difficult to trace.

The middle and upper portions of the watersheds of the three forks differ materially. The North Fork rises in lavas which vary much in composition and hardness, but which generally afford a deep soil for timber and shrub growth. The Middle Fork rises in similar lavas and in granite. The mean elevation of the crest of the Sierra at the head of these forks is about 8,200 feet. The main and tributary streams fall rapidly, and their canyons head well up in the mountains. The sides of these canyons are covered with timber and brush, which, with the deep soil, retain the moisture and feed numerous perennial springs. (See Pl. V, A.) In the case of the North Fork this is particularly noticeable. The forests of its watershed make it a reliable and constant stream. The mean annual precipitation upon the watersheds of the North and Middle forks is about 54 inches. Warm rains on soft snow sometimes give a high flood run-off, but snow remains on the higher peaks until midsummer. Reservoir sites are not numerous; they will be mentioned later. The headwaters of the South Fork lie upon a broad granite surface, into which the streams have not cut deeply until the main stream reaches a point 16 miles from the summit, where it drops rapidly into a deeply eroded canyon. The eastern or upper edge of the drainage area has a mean elevation about the same as the other forks, but the 5,000-foot contour is about

20 miles to the westward. This broad surface has been denuded by glacial action, and the harder nature of the granite has not permitted a deep soil to form. The area is therefore less heavily timbered than the drainage areas of the other two forks, and its accessibility has caused it to suffer more severely from the ax of the lumberman. This topography gives a broader and more gently sloping surface than characterizes the headwaters of other Sierra Nevada streams. The surface is marked by nearly 100 glacial lakelets and valleys, affording many excellent reservoir sites which have been or are being utilized. This elevated watershed receives a mean annual precipitation of 60 inches, most of which is in the form of snow. The slow melting of the snow maintains the discharge of tributaries until June or July, which, with the natural and artificial reservoirs, makes the South Fork of the Yuba a highly valuable and reliable source of water supply.

NATURAL STORAGE OF WATER IN YUBA RIVER BASIN.

Precipitation upon the drainage basin of Yuba River is dependent upon the southerly or winter extension of the north temperate rain belt. During the summer months the more northerly position of this belt leaves California in the comparatively rainless region between the north temperate and equatorial rain belts. The rains and snows, therefore, fall from October to April, with little or no rainfall of moment from May to September, so that during the latter months the streams depend upon either natural or artificial storage. Natural storage is by snow and the slow run-off of water retained in afforested and brush-covered soils. On the South Fork artificial storage has reached a very effective stage. The precipitation ranges from 20 inches at Marysville, in the valley, to 70 inches at the summit of the Sierra.¹

Snow storage of water is depended on during the latter part of April and into July, the run-off until June being superabundant for all purposes, but in July it begins to fall below the necessities of dependent industries, and it remains below until the autumnal rains occur. Snow storage has been made a subject of extended observation by Mr. W. F. Englebright, chief engineer of the South Yuba Canal Company, through whose courtesy the writer has been enabled to prepare a most instructive diagram of the accumulation, depth, and rate of melting of snow at Lake Fordyce (fig. 15). This lake has an elevation of 6,500 feet above tide level, and is in a region over which the annual precipitation in rain and melted snow is 70 inches. Snow begins to accumulate late in November, and reaches its maximum depth in packed snow in March. During the winter months the lower readings on the gage rod following higher readings generally indicate a packing of the snow.

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¹These figures are taken from a map prepared, under the writer's direction, for the California Water and Forest Association, showing the drainage areas, the mean annual rainfall, and the distribution of forests throughout the State.



1. CANYON OF MIDDLE FORK OF YUBA RIVER.



B. MIDDLE FORK OF YUBA RIVER NEAR FREEMAN'S CROSSING.

MANSON.]

Melting begins in March and continues quite regularly until the middle of June or early July. Short storms during April and May cause offsets in the curve, which resumes a parallel line. A series of cold and heavy storms in April, 1896, caused the snow to last until July 5, while the clear, warm spring of 1897 caused it to disappear on June 7.

During the latter half of April, by means of daily reports by telephone, Mr. Englebright is enabled, through diagrams upon a larger scale, to approximate to within a few days the duration of the snow supply and the beginning of the draft on the reservoirs. Data and studies of this kind are very valuable, and suggest the importance of stations above the snow line as a means of determining the volume of snow storage available at different seasons and the ratio between the volume stored by snow and that stored by reservoirs. The discharge of the streams is maintained by snow during the spring and for half of





the summer months, and the volume and rate of the discharge can be foretold with reasonable accuracy by daily readings of gages properly located.

ARTIFICIAL STORAGE POSSIBILITIES.

The natural facilities for the storage of storm waters are particularly favorable in the upper third of the drainage basin of the South Fork. The demands for large volumes of water under high pressure to operate the mines in the middle and lower portions of that drainage basin and those on Bear and American rivers were met by the construction of large and expensive canals and storage reservoirs. Just above the great bend north of the head of Bear River and at the head of the steep canyon of the South Fork is a broad, flat, glacial valley which has been converted into a lake by the construction of a stone dam. This lake, known as Lake Spaulding and shown in Pl. IV, A, has a capacity of 270,000,000 cubic feet, and is the lower and controlling reservoir of a series embracing the available storage and supply above. This supply is derived from about 120 square miles, upon which the mean annual precipitation in rain and melted snow is about 5 feet. The following is a list of the storage reservoirs:

Name of reservoir.	Elevation.	Area.	Capacity.	Cost of dam.
Meadow Stirling White Rock Peak Lakes (three) Fordyce Lost River Fallcreek Lakes (six) Spaulding Summit Lake Bear Valley Total	Feet, 7,515 7,200 7,000 6,900 6,500 7,000 7,000 4,846 6,800 4,400	$\begin{array}{c} Acres.\\ 300\\ 100\\ 80\\ 150\\ 474\\ (a)\\ 171\\ 215\\ 400\\ 60\\ \hline 1,950\\ \end{array}$	$\begin{array}{c} Gallons.\\ 1,275,000,000\\ 340,000,000\\ 225,000,000\\ 1,275,000,000\\ 5,950,000,000\\ 1,020,000,000\\ 2,125,000,000\\ 1,020,000,000\\ 1,938,816,000\\ 145,411,200\\ b\ 14,409,227,200 \end{array}$	$\begin{array}{c} \$75.000\\ 20,000\\ 5,000\\ (a)\\ 300,000\\ (a)\\ (a)\\ 50,000\\ 30,000\\ 30,000\\ 30,000\\ 30,000\\ 478,000\\ \end{array}$

Storage reservoirs in Yuba River Basin.

a Records lost.

b1,921,230,293 cubic feet.

The aggregate area of these reservoirs is 3.05 square miles, and they are filled to an average depth of 22.5 feet, thus giving storage for about 12 per cent of the mean annual precipitation upon the tributary area, the remainder going to waste and to swell the floods which devastate the valley. It is possible, by raising the dams and enlarging the canals, to utilize a considerable additional portion of the precipitation. The conditions favorable to the conservation of water on the upper third of the drainage basin of the South Fork are far greater than in the lower two-thirds of that basin or in the basin of the other forks.

On the upper portion of Canyon Creek, a tributary of the South Fork, the Eureka Lake and Yuba Canal Company and the North Bloomfield Gravel and Mining Company have the following storage reservoirs:

Name of reser- voir.	Area.	Height.	Top length.	Baro- metric eleva- tion.	Catch · ment area.	Capacity.	Cost.
Bowman Sawmill Flat Shot Gun Lake. Island Lake Middle Lake Crooked Lake Fall Creek Jackson Lake Faucherie Lake Weaver Lake Eureka Lake Total	Acres. 500.0 80.6 26.2 48.8 11.2 10.3 8.1 20.0 90.0 83.5 337.3	$Feet. \\ 100.0 \\ 39.2 \\ 10.0 \\ 12.8 \\ 12.0 \\ 3.0 \\ 11.0 \\ \hline 5.0 \\ 21.0 \\ 21.8 \\ 68.2 \\ \hline e8.2$	Feet. 425	$\begin{array}{c} Feet. \\ 5,450 \\ 5,780 \\ 6,410 \\ 6,690 \\ 6,460 \\ 6,510 \\ 6,590 \\ 6,690 \\ 5,410 \\ 6,060 \\ \hline \\ 6,480 \\ \hline \end{array}$	Acres. 12,093	$\begin{array}{c} Cubic feet,\\ 930,000,000\\ 2,000,000\\ 3,423,816\\ 23,027,558\\ 2,305,800\\ 1,600,000\\ 2,906,630\\ \hline 15,000,000\\ 150,000,000\\ 661,000,006\\ \hline 1,849,354,804 \end{array}$	\$151,521 Total amount expended on these dams and reser- voirs, \$246,000. 8,000 35,000

Storage reservoirs on upper portion of Canyon Creek.

The drainage area tributary to these reservoirs is 28.4 square miles, and it receives a total precipitation during an average year of



A ENGLISH RESERVOIR ON MIDDLE FORK OF YUBA RIVER.



B SMALL DAM OF ENGLISH RESERVOIR.

4,589,481,600 cubic feet, 1,849,354,804 cubic feet of which is stored, or between one-third and one-half of the mean annual precipitation.

On the Middle Fork there are no reservoirs storing water at the present time. The only site of any importance is that of the Ruyard or English reservoir (see Pl. VI), which has not been in use since the failure of the dam in June, 1883. This site has a capacity of 650,000,000 cubic feet. Weaver Lake is on the watershed of the Middle Yuba, but its catchment area is not large enough to fill it, so it is supplied from the Eureka Lake and Yuba Canal Company's ditch from Canyon Creek, a tributary of the South Yuba, and is included in the foregoing list. At Milton there is a reservoir site with an estimated capacity of 28,000,000 cubic feet. The total storage capacity on the Middle Yuba may be considered to be 678,000,000 cubic feet.

On the North Fork are the dam and headworks of the Browns Vallev Irrigation District. (See Pl. VII.) The dam is a well-built crib structure, about 167 feet long on the crest, with a maximum height of 37 feet. The head gates are in concrete. For several miles above the dam the river bed is covered with gravel, sand, and cobbles on a grade slightly less than that of the original stream. This is a feature common to dams upon streams carrying mining débris. The dam thus acts as a retaining wall as well as an overflow weir. Leakage through the débris and dam is slight. The head gates open into a flume 5 feet by 7 feet, on a grade of 13 feet to the mile, and built to carry 300 second-feet of water. The greater portion of the water diverted is used to develop power at the Colgate and Browns Valley power stations of the Bay Counties Power Company, lessees of the Browns Valley Irrigation District rights. This power is transmitted to Marysville, Oroville, Wheatland, Nevada City, Grass Valley, and Sacramento. These plants are synchronized with one on the South Yuba, about 7 miles distant.

On the North Fork there are the following small lakes, which might be developed to an aggregate storage capacity of 500,000,000 cubic feet:

Name of lake.	Area.
Upper Sardine Lower Sardine	$\begin{array}{c} Acres, \\ 38.0 \\ 40.0 \\ 9.0 \\ 2.5 \\ 7.0 \\ 2.5 \\ 5.0 \\ 30.0 \\ 50.0 \\ 11.0 \\ 16.0 \\ 27.0 \\ 3.0 \end{array}$
Total	241.0

Reservoir sites on the North Fork.

Assuming that artificial storage on the North Fork and the Middle Fork could be developed to a capacity equal to that above the Lake Spaulding dam, there would then be in service an area of 6.8 square miles with water at an average depth of 26.4 feet, or 5,692,000,000 cubic feet. The mean annual precipitation in the drainage basin of Yuba River is 170,829,000,000 cubic feet. The total ultimate artificial storage is less than 3.3 per cent of this precipitation, and could hardly be recognized in a gaging of the total run-off. Moreover, in the storage of water for industrial purposes the uncertainty of the character of the seasonal rainfall makes it prudent and desirable to permit the reservoirs to fill during the earlier rains, and not leave the husbanding of a supply to possible succeeding rains. Hence it generally happens that when the heavy storms of the late winter and spring months occur the reservoirs are full and the flood wave passes down without being diminished by the reservoirs. This is also true to a limited extent of regions above the snow line, where the unmelted snow constitutes a reservoir of far greater capacity than ordinarily is obtained by building dams. It happens that when late warm rains or rapid melting of the snows occurs the reservoirs are already full, and consequently do not diminish the flood volume.

It would appear, therefore, that however useful artificial reservoirs are for domestic and industrial purposes they can not be relied upon, except under unusual conditions, to decrease the heights of late winter and spring floods, and we must look elsewhere for a solution of that problem.

COMPARISON OF LOW-WATER DISCHARGE FROM A TIMBERED AREA WITH THAT FROM A COMPARATIVELY TREELESS AREA.

On the south fork of the North Fork is a watershed area of 139 square miles, which was gaged on September 19, 1900, after three successive seasons of deficient rainfall, and gave a minimum run-off of 113 second-feet, or 0.8 second-foot per square mile. This area is well covered with timber and brush, and in 120 days it gives a minimum run-off of 1,441,152,000 cubic feet.

The drainage basin of the North Fork is more heavily timbered than the basins of the other forks, and consequently it has a deeper soil, and, although only one-tenth of the total drainage area, it furnishes 75 per cent of the low-water flow of the entire drainage basin above Parks Bar.

On the south fork above Lake Spaulding there is a watershed of 120 square miles, which has heretofore been described as comparatively barren of timber, the timbered areas which once existed having been denuded. (See Pl. VIII, A.) The run-off of this area is practically nothing for 120 days of the year, due to the absence of forests and



A. BROWNS VALLEY IRRIGATION DISTRICT DAM FROM ABOVE



B. BROWNS VALLEY IRRIGATION DISTRICT DAM FROM BELOW

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brush. If this area were afforested and gave a minimum run-off of 0.8 second-foot per square mile, the discharge would be 100 second-feet, equivalent to an effective storage capacity of 1,036,800,000 cubic feet. This minimum low-water discharge of 100 second-feet for 120 days is equivalent to more than half the storage capacity of all the reservoirs above Lake Spaulding dam, which aggregate 1,375,000,000 cubic feet. As the basis of this estimate is extreme low-water discharge, it may be assumed that by afforesting the watershed this costly and extensive system of reservoirs could safely be drawn upon for double their present capacity. As what is true of portions of the watershed is true of the watershed as a whole, aggregating as it does 1,357 square miles, the value of afforesting the area becomes apparent.

It appears to the writer that the solution of the problem of storage of flood waters is not the retention of a small percentage of the storm waters behind dams, but the application of storage over the entire watershed by the systematic protection and extension of forest-covered and brush-covered areas.

DISCHARGE MEASUREMENTS OF YUBA RIVER AND ITS TRIBUTARIES.

The accompanying tables of low-water discharge measurements of Yuba River and its forks are based upon observations and gagings



FIG. 16.—Curve showing relation of gage height to discharge of Yuba River.

made by Mr. H. D. H. Connick, under the direction of the writer, during the months of June, July, August, September, and October, 1900. The precipitation during the wet season preceding these gagings was about two-thirds to three-fourths of the mean annual rainfall. The precipitation during the two preceding wet seasons was still further below the normal.

The location of the gaging stations is shown on the map, fig. 14, page 40. The gagings were made with a large Price meter furnished by the United States Geological Survey. The usual method was pursued, namely, the cross section was divided into subsections of 5 feet each, and the velocities were observed for three minutes for each foot of depth. The integral of the discharges thus ascertained divided by the total cross-sectional area determined the mean velocity. The volumes thus determined for various stages were platted as a curve of discharge, using gage heights and discharges as ordinates, from which curve intermediate discharges were estimated to fill out the tables. For discharge curves, see figs. 16, 17, and 18.

Daily discharge of Yuba River at Parks Bar Bridge during the month of July, 1900.

Der	Gage 1	neight.	Mean	Area of Mean ve-		lean Area of Mean ve-		ahanaa
Day.	6 a.m.	6 p.m.	6 p.m. height. section. locity.	locity.	1015	charge.		
$\begin{array}{c} 1 \\ 2 \\ 3 \\ 4 \\ 5 \\ 5 \\ 6 \\ 7 \\ 8 \\ 9 \\ 9 \\ 9 \\ 10 \\ 11 \\ 12 \\ 13 \\ 14 \\ 14 \\ 15 \\ 15 \\ 15 \\ 16 \\ 17 \\ 18 \\ 19 \\ 20 \\ 21 \\ 22 \\ 23 \\ 24 \\ 24 \\ 25 \\ 26 \\ 23 \\ 24 \\ 25 \\ 26 \\ 27 \\ 28 \\ 29 \\ 30 \\ 31 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ $	$\begin{array}{c} Feet. \\ 2,90 \\ 3,10 \\ 2,60 \\ 2,70 \\ 2,60 \\ 2,70 \\ 2,60 \\ 2,70 \\ 2,60 \\ 2,70 \\ 2,70 \\ 2,70 \\ 2,70 \\ 2,50 \\ 2,50 \\ 2,50 \\ 2,50 \\ 2,50 \\ 2,50 \\ 2,40 \\ 2,40 \\ 2,40 \\ 2,50 \\ 2,50 \\ 2,40 \\ 2,40 \\ 2,50 \\ 2,50 \\ 2,50 \\ 2,40 \\ 2,40 \\ 2,50 \\ 2,50 \\ 2,50 \\ 2,50 \\ 2,50 \\ 2,50 \\ 2,40 \\ 2,50 \\ 2$	$\begin{array}{c} Feet,\\ 2,80\\ 2,90\\ 2,90\\ 2,70\\ 2,80\\ 2,70\\ 2,80\\ 2,70\\ 2,80\\ 2,70\\ 2,80\\ 2,50\\ 2,50\\ 2,50\\ 2,50\\ 2,50\\ 2,50\\ 2,40\\ 2,40\\ 2,30$	$\begin{array}{c} Feet.\\ 2.850\\ 3.005\\ 2.755\\ 2.860\\ 2.2755\\ 2.260\\ 2.2755\\ 2.260\\ 2.2755\\ 2.2455\\ 2.2455\\ 2.2455\\ 2.2455\\ 2.2455\\ 2.2455\\ 2.2455\\ 2.2455\\ 2.2455\\ 2.2455\\ 2.2455\\ 2.2455\\ 2.2555\\ 2.2455\\ 2.255\\$	Square feet. 	Feet per second.	$\begin{array}{c} Second.\\ feet,\\ 970,0\\ 1,020,0\\ 1,020,0\\ 890,0\\ 890,0\\ 850,0\\ 850,0\\ 850,0\\ 850,0\\ 775$	$\begin{array}{c} Cubic feet per\\ 2! hours.\\ 83, 808, 006\\ 88, 128, 000\\ 95, 040, 000\\ 69, 984, 000\\ 76, 896, 000\\ 76, 896, 000\\ 73, 440, 000\\ 73, 440, 000\\ 73, 440, 000\\ 73, 440, 000\\ 73, 440, 000\\ 66, 960, 000\\ 65, 900, 000\\ 57, 024, 000\\ 57, 025, 280\\ 57, 024, 000\\ 50, 112, 000\\ 50, 10, 00\\ 50, $	
Total			••••••				1,955,059,000	



A. SECOND-GROWTH FOREST DESTROYED BY FIRE.



B. HEAD OF SOUTH YUBA CANAL COMPANY'S DITCH.

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Daily discharge of Yuba River at Parks Bar Bridge during the month of August, 1900.

Day.	Gage 6 a. m.	height. 6 p. m.	Mean gage height.	Area of section.	Mean ve- locity.	Dis	charge.
$\begin{array}{c} 1 \\ 2 \\ 2 \\ 3 \\ 4 \\ 5 \\ 6 \\ 7 \\ 8 \\ 9 \\ 10 \\ 11 \\ 12 \\ 13 \\ 14 \\ 15 \\ 16 \\ 17 \\ 18 \\ 19 \\ 20 \\ 21 \\ 22 \\ 23 \\ 21 \\ 22 \\ 23 \\ 24 \\ 23 \\ 24 \\ 25 \\ 26 \\ 27 \\ 27 \\ 27 \\ 28 \\ 29 \\ 29 \\ 29 \\ 29 \\ 29 \\ 29 \\ 29$	$\begin{array}{c} Feet. \\ 2:30 \\ 2:20 \\ 2:20 \\ 2:20 \\ 2:20 \\ 2:30 \\ 2:30 \\ 2:30 \\ 2:30 \\ 2:30 \\ 2:20 \\ 2:20 \\ 2:20 \\ 2:20 \\ 2:10 \\ 2:20 \\ 2:10 \\ 2:30 \\ 2:30 \\ 2:30 \\ 2:30 \\ 2:30 \\ 2:30 \\ 2:30 \\ 2:30 \\ 2:30 \\ 2:30 \\ 2:30 \\ 2:30 \\ 2:30 \\ 2:30 \\ 2:20 \\ 2$	$\begin{array}{c} Feet. \\ 2,30 \\ 2,20 \\ 2,20 \\ 2,20 \\ 2,20 \\ 2,20 \\ 2,20 \\ 2,20 \\ 2,20 \\ 2,20 \\ 2,20 \\ 2,20 \\ 2,20 \\ 2,20 \\ 2,30 \\ 2,20 \\ 2$	$\begin{array}{c} Feet, \\ 2, 30, \\ 2, 25, \\ 2, 20,$	Sq. ft.	<i>Ft.persec.</i> 3.54 3.59 3.49	$\begin{array}{c} Secft.\\ 545.0\\ 510.0\\ 480.0\\ 480.0\\ 480.0\\ 536.8\\ 571.2\\ 510.0\\ 440.0\\ 440.0\\ 440.0\\ 440.0\\ 510.0\\ 535.0\\ 440.0\\ 440.0\\ 440.0\\ 510.0\\ 558.0\\ 0\\ 510.0\\ 558.0\\ 0\\ 510.0\\ 558.0\\ 0\\ 510.0\\ 510.0\\ 558.0\\ 0\\ 510.0\\ 545.0\\ 0\\ 545.0\\ 0\\ 545.0\\ 0\\ 545.0\\ 0\\ 545.0\\ 0\\ 545.0\\ 0\\ 545.0\\ 0\\ 545.0\\ 0\\ 545.0\\ 0\\ 545.0\\ 0\\ 545.0\\ 0\\ 545.0\\ 0\\ 545.0\\ 0\\ 545.0\\ 0\\ 545.0\\ 0\\ 545.0\\ 0\\ 545.0\\ 0\\ 0\\ 545.0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0$	$\begin{array}{c} Cu. ft. per 2t.\\ hrs.\\ 47, 085, 000\\ 44, 064, 000\\ 41, 472, 000\\ 41, 472, 000\\ 41, 472, 000\\ 41, 472, 000\\ 41, 472, 000\\ 41, 472, 000\\ 41, 472, 000\\ 41, 472, 000\\ 38, 016, 000\\ 38, 016, 000\\ 38, 016, 000\\ 41, 472, 000\\ 38, 016, 000\\ 41, 472, 000\\ 38, 016, 000\\ 41, 472, 000\\ 38, 016, 000\\ 41, 064, 000\\ 44, 064, 000\\ 44, 064, 000\\ 44, 064, 000\\ 44, 064, 000\\ 44, 064, 000\\ 44, 064, 000\\ 44, 064, 000\\ 44, 064, 000\\ 44, 064, 000\\ 44, 064, 000\\ 44, 064, 000\\ 44, 066, 000\\ 44, 066, 000\\ 44, 066, 000\\ 44, 066, 000\\ 44, 066, 000\\ 44, 066, 000\\ 44, 066, 000\\ 44, 066, 000\\ 38, 016, 000\\ 34, 560, 000\\ 34, 560, 000\\ 38, 016, 000\\ $
Total							1,286,151,520

Daily discharge of Yuba River at Parks Bar Bridge during the month of September, 1900.

Day.	Gage 1	height.	Mean gage height	Area of section.	Mean ve- locity.	Dis	charge.
1	$\begin{array}{c} Feet. \\ \$ 10 \\ $ 10 \\ $$	$\begin{array}{c} Feet.\\ 2.10\\ 2.10\\ 2.10\\ 2.10\\ 2.20\\ 2.20\\ 2.20\\ 2.20\\ 2.20\\ 2.20\\ 2.20\\ 2.20\\ 2.20\\ 2.20\\ 2.20\\ 2.20\\ 2.20\\ 2.10\\ 2.20\\ 2.20\\ 2.10\\ 2.20\\ 2.20\\ 2.10\\ 2.20\\ 2.10\\ 2.00$	$ \begin{array}{c} Feet. \\ 2.10 \\ 2.10 \\ 2.10 \\ 2.10 \\ 2.10 \\ 2.20 \\ 2.20 \\ 2.25 \\ 2.40 \\ 2.25 \\ 2.40 \\ 2.25 \\ 2.40 \\ 2.25 \\ 2.40 \\ 2.20 \\ 2.15 \\ 2.20 \\ 2.20 \\ 2.15 \\ 2.20 \\ 2.20 \\ 2.10 \\ 2.00 \\ $	Sq. ft.	Ft. per sec.	$\begin{array}{c} Secft.\\ 400.0\\ 400.0\\ 400.0\\ 400.0\\ 410.0\\ 515.0\\ 470.0\\ 470.0\\ 470.0\\ 470.0\\ 410.0\\ 400.0\\ 510.0\\ 620.0\\ 510.0\\ 620.0\\ 510.0\\ 620.0\\ 470.0\\ 470.0\\ 470.0\\ 470.0\\ 470.0\\ 470.0\\ 470.0\\ 470.0\\ 470.0\\ 470.0\\ 860.0\\ 360.0\\$	$\begin{array}{c} Cu. ft. per 24.\\ hrs.\\ 34, 560, 000\\ 34, 560, 000\\ 34, 560, 000\\ 38, 016, 000\\ 38, 016, 000\\ 453, 568, 000\\ 47, 088, 000\\ 40, 608, 000\\ 40, 608, 000\\ 40, 608, 000\\ 40, 608, 000\\ 40, 608, 000\\ 44, 064, 000\\ 53, 568, 000\\ 44, 064, 000\\ 53, 568, 000\\ 44, 064, 000\\ 53, 568, 000\\ 44, 064, 000\\ 53, 568, 000\\ 44, 064, 000\\ 53, 568, 000\\ 44, 064, 000\\ 34, 560, 000\\ 34, 560, 000\\ 34, 560, 000\\ 34, 560, 000\\ 31, 104, 000\\$

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	Gage height.		Mean	D	
Day.	6 a. m.	6 p. m.	height.	Discharge.	
1	$\begin{matrix} Fcet. \\ 2.00 \\ 2.80 \\ 3.20 \\ 4.60 \\ 4.20 \\ 3.70 \\ 3.50 \\ 3.50 \\ 3.50 \\ 3.40 \\ 3.40 \\ \end{matrix}$	Feet. 2.00 2.00 4.90 4.60 4.00 3.60 3.50 3.40 3.40 3.40 3.40	$\begin{matrix} Feet. \\ 2.00 \\ 2.00 \\ 3.10 \\ 4.05 \\ 4.60 \\ 4.10 \\ 3.65 \\ 3.50 \\ 3.45 \\ 3.50 \\ 3.40 \\ 3.50 \\ 3.40 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\$	$\begin{array}{c} Secft.\\ 360\\ 360\\ 1,200\\ 2,140\\ 2,720\\ 1,730\\ 1,595\\ 1,595\\ 1,595\\ 1,540\\ 1,480\\ 1,595\\ 1,480\\ \end{array}$	$\begin{array}{c} Cu. ft. per 24\\ hrs.\\ 31, 104, 000\\ 31, 104, 000\\ 103, 650, 000\\ 184, 896, 000\\ 235, 008, 000\\ 190, 080, 000\\ 149, 472, 000\\ 137, 808, 000\\ 137, 808, 000\\ 137, 808, 000\\ 137, 808, 000\\ 127, 872, 000\\ 137, 808, 000\\ 127, 872,$

Daily discharge of Yuba River at Parks Bar Bridge during the month of October, 1900.

NOTE.—On the evening of October 4 gage No.1 was washed out. All subsequent readings were made on gage No. 2. Equation: Gage No. 2+2.2=gage No. 1. Thus: 2.7+2.2=4.9, gage height.

Daily discharge of North Fork of Yuba River at Yuba Power Company's dam during the month of July, 1900.

Day.	Gage height.		Mean	Area of	Mean ve-	Discharge	
	6 a. m.	6 p. m.	height.	section.	locity.	Discharge.	
1	Feet. 2.07 2.06	Feet. 2.07	Feet. 2.07	Sq. ft.	Ft. per sec.	Secft. 630.0	Cu.ft.per 24 hrs 54,432,000
3 4	2.05 2.05 2.05	$2.05 \\ 2.00$	2.00 2.05 2.03	203.1	2.98	606.0 610.0	52,358,400 52,704,000
5 6 7	$2.00 \\ 1.95 \\ 2.00$	$2.00 \\ 2.00 \\ 2.00 \\ 2.00$	$2.00 \\ 1.98 \\ 2.00$	196.4	2.88	595.0 566.8 595.0	51,408,000 48,971,520 51,408,000
8 9	1.95 1.90 1.95	1.95 1.85 1.85	1.95 1.88 1.83			560.0 520.0 400.0	48,384,000 44,928,000 42,226,000
$ \begin{array}{c} 10\\ 11\\ 12\\ 12\\ 12 \end{array} $	$1.80 \\ 1.80 \\ 1.75 \\ 1.75$	1.80 1.80 1.75	$1.80 \\ 1.75 \\ 1.75$			470.0 440.0	42, 350, 000 40, 608, 000 38, 016, 000
13 14. 15	$ \begin{array}{r} 1.75 \\ 1.75 \\ 1.75 \\ 1.75 \\ \end{array} $	$ \begin{array}{r} 1.45 \\ 1.75 \\ 1.75 \\ 1.75 \end{array} $	$ \begin{array}{r} 1.75 \\ 1.75 \\ 1.75 \\ 1.75 \\ \end{array} $			$440.0 \\ 440.0 \\ 440.0$	38,016,000 38,016,000 38,016,000
16 17 18	$ \begin{array}{r} 1.75 \\ 1.70 \\ 1.70 \end{array} $	$ \begin{array}{r} 1.75 \\ 1.70 \\ 1.70 \\ 1.70 \\ \end{array} $	$ \begin{array}{r} 1.75 \\ 1.70 \\ 1.70 \\ 1.70 \\ \end{array} $	160.3 157.0	2.73 2.66	$440.0 \\ 437.7 \\ 418.7$	38,016,000 37,817,280 36,175,680
19. 20. 91	1.70 1.65 1.65	1.70 1.65 1.65	1.70 1.65 1.65			410.0 380.0 380.0	35.424,000 32,832,000 32,832,000
23 23	1.65 1.65 1.70	1.00 1.70 1.70 1.70	1.63 1.68 1.70			400.0 410.0	35, 352, 000 34, 560, 000 35, 424, 000
24 25 26	$ \begin{array}{c} 1.40 \\ 1.65 \\ 1.65 \end{array} $	$ \begin{array}{r} 1.65 \\ 1.65 \\ 1.65 \end{array} $	$1.68 \\ 1.65 \\ 1.65$			400.0 380.0 380.0	34,560,000 32,832,000 32,832,000
27 28 	$ \begin{array}{r} 1.65 \\ 1.60 \\ 1.60 \end{array} $	$ \begin{array}{r} 1.65 \\ 1.60 \\ 1$	$ \begin{array}{r} 1.65 \\ 1.60 \\ 1$	158.5	2.31	$ 366.1 \\ 350.0 \\ 371.4 $	31, 631, 040 30, 240, 000 32, 088, 960
30. 31.	$ 1.60 \\ 1.60 \\ 1.60 $	$1.60 \\ 1.60 \\ 1.60$	1.60 1.60 1.60	159.1	2.28	350.0 363.9	30,240,000 31,440,960
Total							1.232,548,840

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Deer	Gage	height.	Mean	Area of	Mean	Dia	ah an sa
Day.	6 a.m.	6 p.m.	gage height.	section.	velocity.	DIS	charge.
$\begin{array}{c} 1 \\ 2 \\ 3 \\ 4 \\ - \\ 5 \\ - \\ - \\ - \\ - \\ - \\ - \\ - \\ -$	$\begin{array}{c} Fee t. \\ 1, 60 \\ 1, 55 \\ 1, 50 \\ 1, 50 \\ 1, 50 \\ 1, 50 \\ 1, 49 \\ 1, 49 \\ 1, 47 \\$	$\begin{array}{c} Feet. \\ 1.60 \\ 1.55 \\ 1$	$\begin{array}{c} Feet. \\ 1, 60 \\ 1, 55 \\ 1, 50 \\ 1, 50 \\ 1, 50 \\ 1, 50 \\ 1, 49 \\ 1, 49 \\ 1, 47 \\$	Sq. ft.	Ft. per sec.	$\begin{array}{c} Secft.\\ 350.0\\ 320.0\\$	$\begin{array}{c} Cu, ft. per 24\\ hrs. \\ 30, 240, 000\\ 27, 648, 000\\ 27, 648, 000\\ 27, 648, 000\\ 27, 648, 000\\ 27, 648, 000\\ 27, 648, 000\\ 27, 648, 000\\ 27, 648, 000\\ 27, 648, 000\\ 27, 648, 000\\ 27, 648, 000\\ 27, 648, 000\\ 27, 648, 000\\ 27, 648, 000\\ 27, 648, 000\\ 27, 648, 000\\ 27, 648, 000\\ 27, 648, 000\\ 27, 648, 000\\ 25, 920, 000\\ $
Total							814 971 520

Daily discharge of North Fork of Yuba River at Yuba Power Company's dam during the month of August, 1900.

Daily discharge of North Fork of Yuba River at Yuba Power Company's dam during the month of September, 1900.

Dav	Gage height.		Mean	Di	sahango
Day.	6 a. m.	6 p. m.	height.	Di	SCHALES.
1 2 3 4 5 5 6 7 8 9 10 11 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30	$\begin{array}{c} Feet. \\ 1.46 \\ 1.46 \\ 1.46 \\ 1.48 \\ 1.49 \\ 1.49 \\ 1.49 \\ 1.47 \\ 1.47 \\ 1.47 \\ 1.47 \\ 1.46 \\ 1.55 \\ 1.55 \\ 1.55 \\ 1.55 \\ 1.49 \\ 1.48 \\ 1.45 \\ 1.44 \\ 1.44 \\ 1.44 \\ 1.45 \\ 1.47 \\ 1.47 \\ 1.47 \\ 1.47 \\ 1.46 \\ 1.45 \\ 1.47 \\ 1.47 \\ 1.46 \\ 1.45 \\ 1.47 \\ 1.46 \\ 1.45 \\ 1.47 \\ 1.46 \\ 1.45 \\ 1.47 \\ 1.46 \\ 1.45 \\ 1.47 \\ 1.46 \\ 1.45 \\ 1.47 \\ 1.46 \\ 1.45 \\ 1.47 \\ 1.46 \\ 1.45 \\ 1.47 \\ 1.46 \\ 1.45 \\ 1.47 \\ 1.46 \\ 1.45 \\ 1.47 \\ 1.46 \\ 1.47 \\ 1.46 \\ 1.45 \\ 1.47 \\ 1.46 \\ 1.45 \\ 1.47 \\ 1.46 \\ 1.47 \\ 1.46 \\ 1.47 \\ 1.46 \\ 1.47 \\ 1.46 \\ 1.47 \\ 1.46 \\ 1.47 \\ 1.46 \\ 1.47 \\ 1.46 \\ 1.47 \\ 1.47 \\ 1.46 \\ 1.47 \\ 1.47 \\ 1.46 \\ 1.47 \\ 1.47 \\ 1.46 \\ 1.47 \\ 1.47 \\ 1.46 \\ 1.47 \\ 1.47 \\ 1.46 \\ 1.47 \\ 1.47 \\ 1.46 \\ 1.47 \\ 1.47 \\ 1.46 \\ 1.47 \\ 1.47 \\ 1.46 \\ 1.47 \\ 1.47 \\ 1.46 \\ 1.47 \\ 1.47 \\ 1.46 \\ 1.47 \\ 1.47 \\ 1.46 \\ 1.47 \\ 1.47 \\ 1.46 \\ 1.47 \\ 1.47 \\ 1.46 \\ 1.47 \\ 1.47 \\ 1.46 \\ 1.47 \\ 1.47 \\ 1.46 \\ 1.47 \\ 1.47 \\ 1.46 \\ 1.47 \\ 1.47 \\ 1.46 \\ 1.47 \\ 1.46 \\ 1.47 \\ 1.47 \\ 1.46 \\ 1.47 \\ 1.46 \\ 1.47 \\ 1.47 \\ 1.46 \\ 1.47 \\ 1.46 \\ 1.47 \\ 1.47 \\ 1.46 \\ 1.47 \\ 1.47 \\ 1.46 \\ 1.47 \\ 1.46 \\ 1.47 \\ 1.46 \\ 1.47 \\ 1.47 \\ 1.46 \\ 1.47 \\ 1.47 \\ 1.46 \\ 1.47 \\ 1.47 \\ 1.46 \\ 1.47 \\ 1.47 \\ 1.46 \\ 1.47 \\ 1.47 \\ 1.46 \\ 1.47 \\ 1.47 \\ 1.46 \\ 1.47 \\ 1.47 \\ 1.46 \\ 1.47 \\ 1.47 \\ 1.46 \\ 1.47 \\ 1.47 \\ 1.46 \\ 1.47 \\ 1.47 \\ 1.46 \\ 1.47 \\ 1.47 \\ 1.46 \\ 1.47 \\ 1.47 \\ 1.46 \\ 1.47 \\ 1.47 \\ 1.46 \\ 1.47 \\ 1.47 \\ 1.46 \\ 1.47 \\ 1.47 \\ 1.46 \\ 1.47 \\ 1.47 \\ 1.46 \\ 1.47 \\ 1.47 \\ 1.46 \\ 1.47 \\ 1.47 \\ 1.47 \\ 1.46 \\ 1.47 \\ 1.47 \\ 1.47 \\ 1.47 \\ 1.47 \\ 1.46 \\ 1.47 \\ 1.47 \\ 1.47 \\ 1.47 \\ 1.47 \\ 1.47 \\ 1.48 \\ 1.47 \\ 1.48 \\ 1.47 \\ 1.48 \\ 1.47 \\ 1.48 \\ 1.47 \\ 1.48 \\ 1.47 \\ 1.48 \\ 1.47 \\ 1.48 \\ 1.47 \\ 1.48 \\ 1.47 \\ 1.48 \\ 1.47 \\ 1.48 \\ 1.47 \\ 1.48 \\ 1.47 \\ 1.48 \\ 1.48 \\ 1.47 \\ 1.48 \\ 1$	$\begin{array}{c} Feet. \\ 1.46 \\ 1.46 \\ 1.45 \\ 1.47 \\ 1.49 \\ 1.50 \\ 1.50 \\ 1.49 \\ 1.48 \\ 1.48 \\ 1.49 \\ 1.60 \\ 1.50 \\ 1.60 \\ 1.50 \\ 1.60 \\ 1.49 \\ 1.48 \\ 1.48 \\ 1.48 \\ 1.45 \\ 1.45 \\ 1.45 \\ 1.45 \\ 1.46 \\ 1$	$\begin{array}{c} Feet. \\ 1.46 \\ 1.46 \\ 1.46 \\ 1.47 \\ 1.50 \\ 1.50 \\ 1.50 \\ 1.49 \\ 1.50 \\ 1.49 \\ 1.49 \\ 1.47 \\ 1.48 \\ 1.49 \\ 1.53 \\ 1.50 \\ 1.49 \\ 1.47 \\ 1.47 \\ 1.47 \\ 1.47 \\ 1.47 \\ 1.47 \\ 1.48 \\ 1$	$\begin{array}{c} Secft.\\ 270\\ 270\\ 270\\ 280\\ 945\\ 300\\ 295\\ 295\\ 280\\ 295\\ 280\\ 295\\ 310\\ 355\\ 310\\ 330\\ 295\\ 280\\ 280\\ 280\\ 280\\ 280\\ 280\\ 280\\ 280$	$\begin{array}{c} Cu. ft. per 24 hrs. \\ 23, 328, 000 \\ 23, 328, 000 \\ 23, 328, 000 \\ 24, 92, 000 \\ 25, 448, 000 \\ 25, 920, 000 \\ 25, 448, 000 \\ 25, 488, 000 \\ 25, 488, 000 \\ 25, 488, 000 \\ 24, 192, 000 \\ 24, 492, 000 \\ 25, 488, 000 \\ 25, 488, 000 \\ 25, 488, 000 \\ 25, 488, 000 \\ 25, 488, 000 \\ 25, 488, 000 \\ 25, 920, 000 \\ 25, 920, 000 \\ 25, 920, 000 \\ 24, 192, 000 \\ 24, 192, 000 \\ 24, 192, 000 \\ 23, 328, 000 \\ 22, 982, 400 \\ 22, 982, 400 \\ 22, 982, 400 \\ 22, 982, 400 \\ 22, 982, 400 \\ 22, 982, 400 \\ 22, 982, 400 \\ 22, 982, 400 \\ 22, 982, 400 \\ 22, 982, 400 \\ 22, 982, 400 \\ 24, 192, 000 \\ 24, 192,$
Total					710, 830, 800





FIG. 17.—Curve showing relation of gage height to discharge of North Fork of Yuba River.

FIG. 18.—Curve showing relation of gage height to discharge of Middle Fork of Yuba River.

Daily discharge of North Fork of Yuba River at Yuba Power Company's dam during the month of October, 1900.

Dav	Gage height.		Mean	Dischause	
Day.	6 a. m.	6 p. m.	height.	LASCHAFGE.	
1	Feet. 1.46 1.48 1.99 2.68 2.12 1.81 1.70 1.67 1.64 1.60 1.64 1.65	$Feet. \\ 1.47 \\ 1.50 \\ 2.40 \\ 2.15 \\ 2.70 \\ 1.95 \\ 1.80 \\ 1.68 \\ 1.75 \\ 1.71 \\ 1.70 \\ 1.68 \\$	$\begin{matrix} Feet. \\ 1.47 \\ 1.49 \\ 2.19 \\ 2.04 \\ 2.69 \\ 2.03 \\ 1.80 \\ 1.69 \\ 1.71 \\ 1.68 \\ 1.65 \\ 1.67 \\ 1.67 \\ \hline \end{matrix}$	$\begin{array}{c} Secft.\\ -280\\ -295\\ -720\\ -610\\ 1.080\\ -610\\ 470\\ 405\\ 410\\ -400\\ -350\\ -390\\ -390\\$	$\begin{array}{c} Cu.\ ft.\ per\ 2h\ lns.\\ 24,\ 192,\ 000\\ 25,\ 488,\ 000\\ 62,\ 208,\ 000\\ 93,\ 312,\ 000\\ 93,\ 312,\ 000\\ 40,\ 608,\ 000\\ 35,\ 704,\ 000\\ 35,\ 424,\ 000\\ 34,\ 992,\ 000\\ 35,\ 424,\ 000\\ 35,\ 424,\ 000\\ 35,\ 424,\ 000\\ 35,\ 424,\ 000\\ 35,\ 424,\ 000\\ 35,\ 600,\ 000\\ 33,\ 696,\ 000\\ 33,\ 696,\ 000\\ \hline \hline \ 556,\ 416,\ 000\\ \hline \end{array}$

[NO. 46.

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Dar	Gage	height.	Mean	Area of	Mean ve-	Dis	charge
Day.	6 a. m.	6 p. m.	height.	section.	locity.	1015	charge.
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\begin{array}{c} 6 \text{ a. m.} \\ \hline \\ $	$\begin{array}{c} 6 \text{ p. m.} \\ \hline \\ \hline \\ Feet. \\ \hline \\ \hline \\ 2.60 \\ 2.40 \\ 2.45 \\ 2.40 \\ 2.40 \\ 2.40 \\ 2.40 \\ 2.40 \\ 2.40 \\ 2.40 \\ 2.30 \\ 2.20 \\ 2.20 \\ 2.20 \\ 2.20 \\ 2.20 \\ 2.40 \\ 2.45 \\ 2.40 \\ 2.45 \\ 2.40 \\ 2.45 \\ 2.40 \\ 2.45 \\ 2.40 \\ 2.45 \\ 2.40 \\ 2.35 \\ 2.40 \\ 2.35 \\ 2.40 \\ 2.35 \\ 2.40 \\ 2.35 \\ 2.40 \\ 2.35 \\ 2.40 \\ 2.35 \\ 2.40 \\ 2.35 \\ 2.40 \\ 2.35 \\ 2.40 \\ 2.35 \\ 2.20 \\$	height. Feet. 40 2.355 2.243 2.255 2.255 2.244 2.255 2.255 2.244 2.255 2.255 2.244 2.2555 2.255 2.2	Sq. ft. 63.0 59.9 58.1 	Ft. per sec. 3.03 3.00 3.18 2.58 	$\begin{array}{c} Secft.\\ 190, 8\\ 189, 0\\ 179, 9\\ 184, 9\\ 150, 0\\ 150, 0\\ 161, 7\\ 150, 0\\ 123, 0\\ 120, 0\\ 120, 0\\ 120, 0\\ 120, 0\\ 120, 0\\ 120, 0\\ 120, 0\\ 120, 0\\ 120, 0\\ 120, 0\\ 120, 0\\ 100, 0\\ 100, 0\\ 100, 0\\ 100, 0\\ 110, 0\\ 110, 0\\ 110, 0\\ 119, 0\\ 119, 0\\ 119, 0\\ 119, 0\\ 119, 0\\ 119, 0\\ 119, 0\\ 119, 0\\ 119, 0\\ 110, 0\\ 100, 2\\ 90, 0\\ 80, 0\\ \end{array}$	$\begin{array}{c} Cu, ft, per 24\\ hrs.\\ hrs.\\ 16, 485, 120\\ 15, 329, 600\\ 15, 543, 360\\ 15, 575, 360\\ 15, 975, 360\\ 12, 960, 000\\ 12, 960, 000\\ 13, 970, 880\\ 12, 960, 000\\ 10, 810, 000\\ 10, 868, 000\\ 10, 368, 000\\ 10, 368, 000\\ 10, 368, 000\\ 8, 640, 000\\ 8, 640, 000\\ 8, 640, 000\\ 8, 640, 000\\ 9, 504, 000\\ 9, 504, 000\\ 9, 504, 000\\ 10, 281, 600\\ 10, 281, 600\\ 10, 281, 600\\ 10, 281, 600\\ 9, 504, 000\\ 9, 504, 000\\ 10, 281, 600\\ 10, 281, 600\\ 9, 504, 000\\ 10, 281, 600\\ 10, 281, 600\\ 9, 504, 000\\ 10, 281, 600\\ 9, 504, 000\\ 9, 504, 000\\ 10, 281, 600\\ 9, 504, 000\\ 10, 281, 600\\ 9, 504, 000\\ 10, 281, 600\\ 9, 504, 000\\ 10, 281, 600\\ 9, 504, 000\\ 10, 281, 600\\ 9, 504, 000\\ 10, 281, 600\\ 9, 504, 000\\ 10, 281, 600\\ 9, 504, 000\\ 10, 281, 600\\ 1$
Total							341, 898, 400

Daily discharge of Middle Fork of Yuba River at Freeman's bridge during the month of July, 1900.

Daily discharge of Middle Fork of Yuba River at Freeman's bridge during the month of August, 1900.

Dag	Gage height.		Mean Area of		Mean ve-	Discharge	
Day.	6 a.m.	6 p. m.	height.	section.	locity.	Dis	charge.
$\begin{array}{c} 1 \\ 2 \\ 3 \\ 3 \\ 4 \\ 4 \\ 5 \\ 6 \\ 7 \\ 8 \\ 9 \\ 9 \\ 10 \\ 11 \\ 12 \\ 13 \\ 14 \\ 15 \\ 16 \\ 17 \\ 13 \\ 14 \\ 15 \\ 16 \\ 17 \\ 12 \\ 20 \\ 21 \\ 22 \\ 23 \\ 24 \\ 24 \\ 22 \\ 23 \\ 24 \\ 24$	$\begin{array}{c} Feet. \\ 2.20 \\ 2.15 \\ 2$	$\begin{array}{c} \textit{Feeet.}\\ 2.20\\ 2.15\\ $	Feet. 2.20 2.18 2.15 2.15 2.15 2.15 2.15 2.15 2.15 2.15	Sq.ft.	<i>Ft. per sec.</i>	$\begin{array}{c} Sec. ft.\\ 80.0\\ 79.0\\ 75.0\\ 7$	$\begin{array}{c} Cu.,ft. per 24\\ hrs.\\ hrs.\\ 6,912,000\\ 6,825,600\\ 6,480,000\\ 6,048,000$
Total							192, 530, 304

Dev	Gage height.		Mean	Area of	Mean ve-	Discharge.	
Day.	6 a. m.	6 p. m.	height.	section.	locity.	Discharge.	
1	$\begin{array}{c} Feet. \\ 2.10 \\ 2.00 \\ 2.05 \\ 2.05 \\ 2.05 \\ 2.05 \\ 2.05 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.015 \\ 2.15 \\ 2.15 \\ 2.10 \\ 2.20 \\ 2.00 \\ $	$\begin{array}{c} Feet. \\ 2.100 \\ 2.05 \\ 2.000 \\ 2.05 \\ 2.05 \\ 2.05 \\ 2.05 \\ 2.05 \\ 2.05 \\ 2.05 \\ 2.05 \\ 2.05 \\ 2.05 \\ 2.20 \\ 2.15 \\ 2.15 \\ 2.15 \\ 2.15 \\ 2.10 \\ 2.00 \\$	$\begin{array}{c} Feet. \\ 2 & 10 \\ 2 & 00 \\ 2 & 00 \\ 2 & 05 \\ 2 & 05 \\ 2 & 05 \\ 2 & 05 \\ 2 & 00 \\ 2 & 05 \\ 2 & 00 \\ 0 & 0 \\ 0 &$	Sq. ft.	<i>Ft. per sec.</i>	$\begin{array}{c} Secff. \\ 70.0 \\ 60.0 \\ 60.0 \\ 65.0 \\ 65.0 \\ 65.0 \\ 65.0 \\ 65.0 \\ 65.0 \\ 65.0 \\ 65.0 \\ 65.0 \\ 60.0 \\ 80.0 \\ 75.0 \\ 90.0 \\ 80.0 \\ 75.0 \\ 75.0 \\ 75.0 \\ 75.0 \\ 60.0$	$\begin{array}{c} Cu. ft. per 24\\ hrs. \\ 6,048,000\\ 5,875,000\\ 5,184,000\\ 5,875,000\\ 5,184,000\\ 5,616,000\\ 5,616,000\\ 5,616,000\\ 5,616,000\\ 5,616,000\\ 5,616,000\\ 5,616,000\\ 5,616,000\\ 6,912,000\\ 6,912,000\\ 6,912,000\\ 6,912,000\\ 6,912,000\\ 6,912,000\\ 6,912,000\\ 5,184,000\\ 5,1$
10141							110, 101, 000

Daily discharge of Middle Fork of Yuba River at Freeman's bridge during the month of September, 1900.

Discharge of Middle Fork of Yuba River at Freeman's bridge during the month of October, 1900.

Dev	Gage height.		Mean	Discharge	
Day.	6 a. m.	6 p. m.	height.	101.	scharge.
1 2 3 4 5 5 6 7 7 8 8 9 9 9 10 11 11 12 12 13	$\begin{array}{c} Feet. \\ 2.00 \\ 2.05 \\ 2.45 \\ 2.40 \\ 3.00 \\ 2.00 \\ 2.45 \\ 2.30 \\ 2.15 \\ 2.00 \\ 2.00 \\ 2.00 \end{array}$	$\begin{array}{c} Feet. \\ 2.00 \\ 2.45 \\ 2.50 \\ 3.00 \\ 2.55 \\ 2.35 \\ 2.20 \\ 2.20 \\ 2.20 \\ 2.15 \\ 2.15 \\ 2.00 \end{array}$	$\begin{array}{c} Feet.\\ 2.00\\ 2.00\\ 2.45\\ 2.45\\ 3.00\\ 2.25\\ 2.45\\ 2.25\\ 2.20\\ 2.17\\ 2.08\\ 2.08\\ 2.00\\ \end{array}$	$\begin{array}{c} Secft.\\ 60\\ 00\\ 130\\ 130\\ 360\\ 90\\ 120\\ 90\\ 80\\ 78\\ 68\\ 68\\ 68\\ 60\\ \end{array}$	$\begin{array}{c} Cu.\ ft.\ per\ 24\ hrs.\\ 5, 184,000\\ 5, 184,000\\ 11,232,000\\ 11,232,000\\ 21,104,000\\ 7,776,000\\ 10,368,000\\ 7,776,000\\ 6,912,000\\ 6,739,200\\ 5,875,000\\ 5,875,000\\ 5,184,000\\ 5,184,000\\ \end{array}$
Total					110, 441, 200

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DEPARTMENT OF THE INTERIOR

WATER-SUPPLY

AND

IRRIGATION PAPERS

OF THE

UNITED STATES GEOLOGICAL SUBVEY

No. 47

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EPCIMEN

OPERATIONS AT RIVER STATIONS, 1900 .- PART I

WASHINGTON GOVERNMENT PRINTING OFFICE 1901

IRRIGATION REPORTS.

The following list contains titles and brief descriptions of the principal reports relating to water supply and irrigation prepared by the United States Geological Survey since 1890:

1890.

First Annual Report of the United States Irrigation Survey, 1890; octavo, 123 pp.

Printed as Part II, Irrigation, of the Tenth Annual Report of the United States Geological Survey, 1888-89. Contains a statement of the origin of the Irrigation Survey, a preliminary report on the organization and prosecution of the survey of the arid lands for purposes of irrigation, and report of work done during 1890.

1891.

Second Annual Report of the United States Irrigation Survey, 1891; octavo, 395 pp.

Published as Part II, Irrigation, of the Eleventh Annual Report of the United States Geological Survey, 1889-90. Contains a description of the hydrography of the arid region and of the engineering operations carried on by the Irrigation Survey during 1890; also the statement of the Director of the Survey to the House Committee on Irrigation, and other papers, including a bibliography of irrigation literature. Illustrated by 29 plates and 4 figures.

Third Annual Report of the United States Irrigation Survey, 1891; octavo, 576 pp.

Printed as Part II of the Twelfth Annual Report of the United States Geological Survey, 1890-91. Contains "Report upon the location and survey of reservoir sites during the fiscal year ended June 30, 1891," by A. H. Thompson; "Hydrography of the arid regions," by F. H. Newell; "Irrigation in India," by Herbert M. Wilson. Illustrated by 93 plates and 100 figures.

Bulletins of the Eleventh Census of the United States upon irrigation, prepared by F. H. Newell; quarto.

No. 35, Irrigation in Arizona; No. 60, Irrigation in New Mexico; No. 85, Irrigation in Utah; No. 107, Irrigation in Wyoming; No. 153, Irrigation in Montana; No. 157, Irrigation in Idaho; No. 163, Irrigation in Nevada; No. 178, Irrigation in Oregon; No. 193, Artesian wells for irrigation; No. 198, Irrigation in Washington.

1892.

Irrigation of western United States, by F. H. Newell; extra census bulletin No. 23, September 9, 1892; quarto, 22 pp.

Contains tabulations showing the total number, average size, etc., of irrighted holdings, the total area and average size of irrighted farms in the subhumid regions, the percentage of number of farms irrighted, character of crops, value of irrighted lands, the average cost of irrightion, the investment and profits, together with a résumé of the water supply and a description of irrightion by artesian wells. Illustrated by colored maps showing the location and relative extent of the irrighted areas.

1893.

Thirteenth Annual Report of the United States Geological Survey, 1891–92, Part III, Irrigation, 1893; octavo, 486 pp.

Consists of three papers: "Water supply for irrigation," by F. H. Newell; "American irrigation engineering" and "Engineering results of the Irrigation Survey," by Herbert M. Wilson; "Construction of topographic maps and selection and survey of reservoir sites," by A. H. Thompson. Illustrated by 77 plates and 119 figures.

A geological reconnoissance in central Washington, by Israel Cook Russell, 1893; octavo, 108 pp., 15 plates. Bulletin No. 108 of the United States Geological Survey; price, 15 cents.

Contains a description of the examination of the geologic structure in and adjacent to the drainage basin of Yakima River and the great plains of the Columbia to the east of this area, with special reference to the occurrence of artesian waters.

1894.

Report on agriculture by irrigation in the western part of the United States at the Eleventh Census, 1890, by F. H. Newell, 1894; quarto, 283 pp.

Consists of a general description of the condition of irrigation in the United States, the area irrigated, cost of works, their value and profits; also describes the water supply, tha value of water, of artesian wells, reservoirs, and other details; then takes up each State and Territory in order, giving a general description of the condition of agriculture by irrigation, and discusses the physical conditions and local peculiarities in each county.

Fourteenth Annual Report of the United States Geological Survey, 1892–93, in two parts; Part II, Accompanying papers, 1894; octavo, 597 pp.

Contains papers on "Potable waters of the eastern United States," by W J McGee; "Natural mineral waters of the United States," by A. C. Peale; and "Results of stream measurements," by F. H. Newell. Illustrated by maps and diagrams.

(Continued on third page of cover.)

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DEPARTMENT OF THE INTERIOR

WATER-SUPPLY

AND

IRRIGATION PAPERS

OF THE

UNITED STATES GEOLOGICAL SURVEY

No. 47



WASHINGTON GOVERNMENT PRINTING OFFICE 1901

OPERATIONS AT RIVER STATIONS, 1900

A REPORT OF THE

DIVISION OF HYDROGRAPHY

OF THE

UNITED STATES GEOLOGICAL SURVEY

PART I



WASHINGTON GOVERNMENT PRINTING OFFICE 1901

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LETTER OF TRANSMITTAL.

DEPARTMENT OF THE INTERIOR, UNITED STATES GEOLOGICAL SURVEY, DIVISION OF HYDROGRAPHY, Washington, D. C., March 1, 1901.

SIR: I have the honor to transmit herewith a manuscript giving the results of operations at various river stations in 1900, and request that it be published in the series of Water-Supply and Irrigation Papers. In order to comply with the law limiting these papers to 100 pages, it is necessary to divide the material. This has been done n a general geographic basis, following the precedent of Water-Supply Papers Nos. 35 to 39, relating to similar operations for the

year 1899. In the first paper are introductory remarks and the data relating to New England and Eastern streams. The succeeding papers take up in order the rivers flowing into the Atlantic Ocean, then those tributary to the Ohio and Mississippi rivers, the Great Lakes, Missouri River and the Rio Grande, the interior basin, and finally those flowing into the Pacific Ocean, from north to south, ending with the data relating to the streams of southern California.

The general conclusions drawn from the operations at the river stations, together with diagrams, maps, and illustrations, are being prepared for publication in Part IV of the Twenty-second Annual Report, this being designed to be in form and substance similar to preceding volumes known as Part IV of the Eighteenth to the Twentyfirst Annual Reports.

Very respectfully,

F. H. NEWELL, Hydrographer in Charge.

Hon. CHARLES D. WALCOTT, Director United States Geological Survey.

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OPERATIONS AT RIVER STATIONS, 1900. PART I.

INTRODUCTION.

The following pages contain descriptions of the river stations maintained during 1900 by the United States Geological Survey, together with details of the average daily height of the water and results of measurements of discharge. The rating tables constructed from the latter and applicable in general for the calendar year will be given at the end of the publication. Similar facts have been printed for the year 1899 in Water-Supply Papers Nos. 35 to 39, inclusive, and a general description of the method of publication has been given on page 9 of Paper No. 35.

ACKNOWLEDGMENTS.

Most of the measurements herewith presented have been obtained through local hydrographers, a comparatively small part of the work having been conducted directly from the office of the Geological Survey at Washington. Acknowledgment is therefore due to these persons individually. Thanks should also be extended to individuals and corporations who have cooperated in various ways—by furnishing readings of the heights of water, by assisting in transportation, etc. The following list gives the names of the resident hydrographers or persons cooperating, arranged alphabetically by States:

California: J. B. Lippincott, civil engineer, Los Angeles.

Colorado: A. L. Fellows, civil engineer, Denver.

Georgia and Alabama: Prof. B. M. Hall, civil engineer, Atlanta; Prof. W. S. Yeates, State geologist, Atlanta; and Prof. Eugene A. Smith, State geologist, Tuscaloosa.

Idaho: N. S. Dils, civil engineer. Caldwell.

Kansas: W. G. Russell, Russell.

Maryland: Prof. W. B. Clark, State geologist, Baltimore.

Montana: Prof. Samuel Fortier, Bozeman; Prof. Fred D. Smith, Missoula.

Nebraska: Prof. O. V. P. Stout, State University, Lincoln, assisted by Adna Dobson and Glenn E. Smith.

Nevada: L. H. Taylor, civil engineer, Golconda.

New Mexico: P. E. Harroun, civil engineer, Albuquerque.

North and South Carolina: Prof. J. A. Holmes, State geologist, Chapel Hill, North Carolina, assisted by E. W. Myers.

Texas: Prof. Thomas U. Taylor, State University Utah: Prof. George L. Swendsen, Logan, Virginia and West Virginia: Prof. D. C. Humphreys, Washington and Lee University, Lexington, Virginia.

Washington: Sydney Arnold, civil engineer, North Yakima; William J. Ware, civil engineer, Port Angeles.

Wyoming: A. J. Parshall, civil engineer, Cheyenne.

In a number of instances related data have been inserted, such as results of computation of daily flow at milldams made by local engineers and data of river heights obtained from the United States Weather Bureau or the Corps of Engineers, United States Army. Reference to these facts, mainly unpublished, has been or will be made in other publications of this Survey, and they are therefore placed in consecutive order for convenience of reference.

The methods of measuring the discharge of various streams and of preparing the computations have been described on pages 18 to 30 of the Nineteenth Annual Report, Part IV, and on pages 20 to 22 of the Twentieth Annual Report, Part IV.

METHOD OF USING STREAM GAGINGS FOR THE COMPUTATION OF WATER POWER.¹

One of the objects of the gagings which are made by the United States Geological Survey is to assist engineers in the estimation of available power on the larger streams of the United States. In an article by John W. Hays in the Manufacturers Record of January 10, 1901, there is given a description of the use which he has made of the daily records published by the Survey. The suggestions made by Mr. Hays are of such general interest that they are given herewith.

Speaking generally, to determine the power available on any stream it is necessary to know the fall and the flow. The fall can easily be determined by an engineer, but the flow of many of our streams is still very uncertain. Usually, an engineer, after obtaining all available data of the stream being studied and also of the neighboring streams, must rely largely upon his judgment to determine maximum and minimum flows and the power that can economically be developed. Often the only basis of estimate is the knowledge of what some other stream has been doing within a limited period, or a comparison with some power on the same stream. When it is remembered that during extreme low water a variation in level of only a few inches may affect the quantity of water passing as much as 100 per cent, it will be seen how misleading may be a single gage or float measurement, even when reinforced by the assurance of casual observers that "the river is as low as it ever gets." Yet it is upon such data that many estimates of prospective power have been made, mills built, and machinery installed, only to have the first dry season show conclusively that the estimates were greatly in error. Then has followed the raising of the dam for storage, which has rarely met expectations, and, after many

¹ Report of H. A. Pressey.

shut-downs, the inevitable steam auxiliary comes, and with it regret, on the part of the owners, that hydraulic development was attempted.

The method described by Mr. Hays in the article referred to has been used in computations made from time to time of the available power of the Potomac and other streams, and found to be reliable and convenient. Mr. Hays illustrates the method by quoting the record of Deep River, in North Carolina, as published by the Geological Survey. The various stages of that river for 1899, as read on the gage of the Survey, are given in the following table:

	Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1.		2.03	4.58	6.91	7.12	2.99	2.84	1.52	4.54	0.85	0.83	12.74	2.77
2		3.21	5.00	6.25	4.70	2.85	2.61	1.36	4.36	. 79	. 78	5.86	1.85
3.		3.41	6.78	6.39	4.52	2.56	3.45	1.34	3.46	. 75	. 88	4.23	1.83
4		3.27	7.06	13.25	5.16	2.51	3.13	1.18	3.08	. 91	. 79	3.48	2.19
ð	• • • • • • • • • • • • • • • • • • •	2.79	16.40	14.43	8.64	2.29	2.49	4.20	1.46	. 73	. 87	3.04	2.15
ő		10.97	20.48	15.77	6.18	2.25	1.95	2.42	1.20	.71	7.20	2.74	1.49
6	•••••	10.27	23.21	10.07	0.40	2.41 0.05	1.00	9 11	4. 04	.89	0.49	2.24	1.27
0		9.10	20.00	10.03	15 04	6.00	1.49	2 10	4.11	1.19	0.70	1.91	1.19
ð		5 59	18 70	7 39	8 28	4 43	2.55	2 10	3 37	1.10	3.96	1.00	1.11
1		4.99	12 26	5 05	6 16	3 85	3 23	1 79	1 39	2 10	3 19	89	4 03
2		5.83	7.19	4.41	5.40	5.89	4.72	1.67	1.41	2.55	1.97	1.09	5.95
3		6.07	6.98	4.67	4.86	7.99	3.78	1.34	1.25	2.04	1.72	1.02	4.69
4		9.79	6.06	3.91	4.48	9.23	3.40	1.19	1.21	4.86	1.59	1.09	3.39
5		13.07	5.10	21.19	3.76	5.99	2.56	1.09	1.29	1.96	1.31	. 96	2.35
.6		8,61	6.76	22.51	3.98	4.46	2.42	1.28	1.31	1.04	1.17	. 98	1.39
7		7.91	16.20	16:21	4.10	3.97	2.40	. 90	1.17	. 93	1.27	1.08	1.34
8	· · · · · · · · · · · · · · · · · · ·	6.93	21.26	9,99	4.04	3.75	1.68	1.14	1.09	. 84	1.04	1.26	1.47
.9		5.99	19.34	14.69	3.54	3.69	1.58	1.11	1.25	. 87	1.06	1.14	1.39
Q	· · · · · · · · · · · · · · · · · · ·	4.73	15.30	15.31	3.32	3.05	1.49	1.02	. 88	1.71	1.12	1.02	. 63
1		3.15	9.92	9.02	3.40	2.89	1.50	1.02	. 74	1.99	. 97	. 98	1.27
14		0.00	9.00	6.10	2.10	2.01	1.41	1.02	. 10	1,49	. 90	1.10	1.13
10 M		3.00	7 02	5 49	9.06	9.85	1.11	1.19	. 90	1.14	.01	1.00	1.07
5		3 25	6 24	4 01	2 07	2 75	1.55	$1.11 \\ 1.52$	1.06	2 34	. 00	1.04	1.19
8		3 27	6.92	4 41	5 60	2 51	1.57	1.67	84	1 53	. 01	1.32	1 10
7		3.54	12.94	4.14	5.54	2.25	1.71	5.19	1.00	1.35	1.01	1.92	1.07
8.		3.19	18.22	7.07	4.46	2.02	2.15	4.35	. 96	1.09	. 98	1.83	. 95
9		2.55		11.65	3.50	1.91	1.68	3.77	1.20	1.17	. 94	3.78	1.03
0		2.21		10.31	3.04	2.54	1.60	2.11	1.22	1.04	. 89	2.84	. 97
31	*****************	3.23		8.44		2.96		6.28	. 89		1.13		1.03

Daily gage height, in feet, of Deep River at Moncure, North Carolina, for 1899.

As will be seen from an inspection of the foregoing table, the records kept by the Geological Survey show the stage of water of each stream measured on each day of the year, and the rating table, which is computed from numerous measurements, shows the quantity of water passing at each reading of the gage. These data may most conveniently be applied by developing a table as follows:

In the first column arrange in order all graduations of the gage rod from the lowest to the highest. In the succeeding columns write opposite each gage height the following: (a) The number of days during the year on which the gage read that particular height; (b) the equivalent volume in second-feet; (c) the effective head; (d) the equivalent gross horsepower; (e) the number of days during the year on which power would have been lessened by low water and by high water, respectively. By way of illustration: The gage read 1.6 feet on 17 days, equivalent to a volume of 380 second-feet, an effective head of 46.4 feet, and a gross horsepower of 2,004, which would be lessened on 121 days by deficient water and on 227 days by high water in the tailrace. If the gage readings at Moncure station from the records of the year 1899 be thus assembled and the variation of the effective head be noted, there results the following table:

Table showing method of determining the daily available horsepower of a stream from records kept by the United States Geological Survey, using the gage heights of Deep River at Moncure, North Carolina, for the year 1899 as a basis.

Gage	Number of days during year 1899 that gage stood at respec- tive heights.	Equiva- lent	Equiva- lent	Equiva- lent gross	Number whic cated been	er of da h powe l would diminis	ays on r indi- have hed.	Ratio o total a	f diminu unnual p	ution to bower.
Inght.		volume.	head.	horse- power.	By low water.	By high water.	Total.	Low water.	High water.	Total.
$\begin{array}{c} reet, \\ 0, 6 \\ \ldots \\ 0, 8 \\ \ldots \\ 1, 0 \\ \ldots \\ 1, 2 \\ \ldots \\ 1, 4 \\ \ldots \\ 1, 8 \\ \ldots \\ 2, 0 \\ \ldots \\ 2, 2 \\ \ldots \\ 2, 4 \\ \ldots \\ 2, 6 \\ \ldots \\ 2, 8 \\ \ldots \\ 3, 0 \\ \ldots \\ 3, 2 \\ \ldots \\ \ldots \\ 3, 2 \\ \ldots \\$	$1 \\ 37 \\ 48 \\ 27 \\ 18 \\ 17 \\ 9 \\ 13 \\ 8 \\ 9 \\ 9 \\ 10 \\ 10 \\ 11$	$\begin{array}{c} sec7t.\\ 210\\ 230\\ 250\\ 330\\ 380\\ 440\\ 500\\ 560\\ 630\\ 715\\ 805\\ 900\\ 1,070\end{array}$	$\begin{array}{c} recc.\\ 47.4\\ 47.2\\ 447.0\\ 46.8\\ 46.6\\ 46.4\\ 46.2\\ 46.0\\ 45.8\\ 45.6\\ 45.4\\ 45.2\\ 45.2\\ 445.0\\ 44.8\end{array}$	$\begin{array}{c} 1,128\\ 1,232\\ 1,335\\ 1,544\\ 1,747\\ 2,004\\ 2,260\\ 2,530\\ 2,839\\ 3,192\\ 3,600\\ 4,050\\ 4,050\\ 4,500\\ 5,379\end{array}$	$\begin{array}{c} 0 \\ 1 \\ 28 \\ 76 \\ 103 \\ 121 \\ 138 \\ 147 \\ 160 \\ 168 \\ 177 \\ 186 \\ 196 \\ 206 \end{array}$	$\begin{array}{c} 364\\ 337\\ 289\\ 262\\ 244\\ 227\\ 218\\ 205\\ 197\\ 188\\ 179\\ 169\\ 159\\ 159\\ 148\end{array}$	364 338 317 338 347 348 356 3552 356 355 3555 3555 3554	$\begin{array}{c} 1.25\\ -0.000\\ -010\\ -022\\ -045\\ -065\\ -095\\ -125\\ -155\\ -189\\ -217\\ -250\\ -270\\ -300\\ -350\end{array}$	$\begin{array}{c} rer \ et. \\ 0.077 \\ 0.075 \\ 0.072 \\ 0.065 \\ 0.058 \\ 0.055 \\ 0.055 \\ 0.055 \\ 0.055 \\ 0.050 \\ 0.050 \\ 0.040 \end{array}$	$\begin{array}{c} rer cl.\\ 0.07\\ .08\\ .09\\ .11\\ .13\\ .15\\ .18\\ .21\\ .24\\ .27\\ .30\\ .32\\ .34\\ .39\end{array}$
3.4 3.6 3.8 4.0 4.2 4.4 4.6 4.8	13 3 7 8 3 7 8 3	$\begin{array}{c} 1,240\\ 1,410\\ 1,580\\ 1,750\\ 1,940\\ 2,130\\ 2,320\\ 2,510\\ \end{array}$	$\begin{array}{c} 44.6 \\ 44.4 \\ 44.2 \\ 44.0 \\ 43.8 \\ 43.6 \\ 43.4 \\ 43.2 \end{array}$	$\begin{array}{c} 6,154\\ 6,926\\ 7,735\\ 8,536\\ 9,417\\ 10,289\\ 11,094\\ 11,197\end{array}$	$\begin{array}{c} 217\\ 230\\ 233\\ 240\\ 248\\ 251\\ 258\\ 266\end{array}$	$ \begin{array}{r} 135 \\ 132 \\ 125 \\ 117 \\ 114 \\ 107 \\ 99 \\ 96 \\ 96 \end{array} $	352 361 358 357 361 358 357	$\begin{array}{r} .390 \\ .415 \\ .430 \\ .450 \\ .470 \\ .490 \\ .510 \end{array}$. 036 . 035 . 035 . 035 . 035 . 035 . 033 . 030	.43 .45 .46 .48 .50 .52 .54
$\begin{array}{c} 5.0 \\ 5.5 \\ 5.5 \\ 6.0 \\ 6.5 \\ 7.0 \\ 7.5 \\ 8.0 \\ 7.5 \\ 8.5 \\ 9.0 \\ 11.0 \\ 12.0 \\ 13.0 \\ 13.0 \\ 14.0 \\ 15.0 \\ 20.0 \\ 22.0 \\ 0 \\ 25.0 \\ \end{array}$	$\begin{array}{c} 9 \\ 9 \\ 6 \\ 12 \\ 6 \\ 13 \\ 1 \\ 5 \\ 3 \\ 4 \\ 2 \\ 5 \\ 1 \\ 2 \\ 4 \\ 3 \\ 11 \\ 7 \\ 2 \end{array}$	$\begin{array}{c} 2,700\\ 3,175\\ 3,650\\ 4,125\\ 4,600\\ 5,100\\ 5,600\\ 6,100\\ 9,100\\ 7,600\\ 9,600\\ 10,600\\ 10,600\\ 11,600\\ 12,600\\ 12,600\\ 23,580\end{array}$	$\begin{array}{c} 43.0\\ 42.5\\ 42.5\\ 42.0\\ 41.5\\ 41.0\\ 40.5\\ 39.0\\ 38.5\\ 38.0\\ 37.0\\ 36.0\\ 35.0\\ 35.0\\ 33.0\\ 23.0\\ 23.0\\ \end{array}$	$\begin{array}{c} 12,900\\ 14,960\\ 16,800\\ 19,000\\ 20,500\\ 22,923\\ 24,880\\ 26,741\\ 28,587\\ 30,338\\ 32,072\\ 35,335\\ 38,386\\ 41,195\\ 48,792\\ 46,200\\ 56,000\\ 61,640\\ \end{array}$	209 278 284 294 302 315 316 321 324 335 335 335 335 338 338 338 338 338 338	$\begin{array}{c} 87\\ 81\\ 693\\ 633\\ 509\\ 449\\ 441\\ 411\\ 375\\ 330\\ 299\\ 27\\ 335\\ 200\\ 99\\ 2\\ 0\\ 0\end{array}$				
	365									-

An inspection of the foregoing table will show to what extent any power plant which might have been installed at this place would have been affected by variations in the flow of the river during the year 1899, the number of days on which the power would have been diminished by high and low water, respectively, and the exact amount of such diminution. For instance, the power would have varied from 1,128 horsepower gross at extreme low water to 61,640 horsepower gross at extreme high water. There would have been but one day on which 1,232 horsepower gross could not have been realized, about two hundred days on which 5,000 horsepower gross could not have been realized, and two hundred and fifty days on which 10,000

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horsepower gross could not have been realized. All of these figures are for continuous power, night and day. Should it be desired to concentrate flow into day service by night storage, which is practicable at Moncure, the installation for horsepower should be doubled. For instance, 10,000 horsepower gross would have been realized on one hundred days, and the power would have fallen below that amount on two hundred days.

It should be noted that the foregoing figures are based on a head of 47 feet normal, with which head little inconvenience would be experienced from high water, the maximum flood for the year being about 25 feet, and on only nine days did the water in the tailrace rise above 15 feet and on thirty days above 10 feet. But the physical conditions indicate a development of the power under two separate heads, which would be affected by flood water to a somewhat greater degree, as will be seen from an inspection of the table. Having accurate knowledge of the periods of decreased head and partial gate, it is possible to determine the capacity of the wheels for any required installation.

Should steam auxiliary be required, the table affords the data necessary to determine the exact proportion of steam power. For example, suppose it is desired to install a plant of 3,600 horsepower for night and day service, during what proportion of the year will steam power be required, and what proportion of the total power desired should be steam power? The following table shows the way of arriving at the answer. From the table on page 12 it will be seen that during one day of the year the available water power is 1,128 horsepower; so that to insure 3,600 horsepower every day in the year it will be necessary to install a steam plant of 2,472 horsepower. During twenty-seven days of the year the available water power is 1,232 horsepower, and on those days 2,268 horsepower of steam will be required, and so on, as shown in the table.

Table showing number of days and amount of steam power required during the year 1899 to develop daily 3,600 horsepower on Deep River at Moncure, North Carolina.

Number of days on which water power of the various amounts was available.	Water power available.	Steam power required.
$1 \\ 27 \\ 48 \\ 27 \\ 18 \\ 17 \\ 9 \\ 13 \\ 8 \\ 9 \\ 9 \\ 9 \\ 9$	$\begin{array}{c} \textit{Horsepower.} \\ 1, 128 \\ 1, 232 \\ 1, 335 \\ 1, 544 \\ 1, 724 \\ 1, 995 \\ 2, 260 \\ 2, 530 \\ 2, 839 \\ 3, 192 \\ 3, 600 \end{array}$	$\begin{array}{c} \textit{Horsepower.} \\ 2,472 \\ 2,268 \\ 2,265 \\ 2,056 \\ 1,876 \\ 1,665 \\ 1,340 \\ 1,070 \\ 1,070 \\ 761 \\ 408 \\ 0 \end{array}$

Summarizing, the total horsepower days $(3,600 \times 365)$ are 1,314,000; the total steam horsepower days are 325,743, or nearly 25 per cent, and steam power would have been required on 177 days of the year 1899.

For conciseness, the factors of wheel efficiency and partial gate are not considered in this estimate. A fair rating of the power of Deep River at this place would be 1,500 horsepower continuous, or 3,000 horsepower for day flow only, on a basis of thirty days' deficiency by reason of the dry season and thirty days' deficiency when the head would be decreased 10 per cent or more by flood water in the tailrace.

In the article referred to Mr. Hays also shows, basing his computations upon the Geological Survey records, that while in ordinary seasons, from the run-off of a drainage area of 12 square miles on Broad River we may expect 1 horsepower per foot of fall of the stream, it will require the run-off from a drainage area of 60 square miles to furnish 1 horsepower per foot of fall on Neuse River, 45 square miles on Cape Fear, Tar, Deep, and Haw rivers, 30 square miles on Roanoke River, 20 square miles on Yadkin River, 15 square miles on lower Catawba River, and 12 square miles on upper Catawba and French Broad rivers.

As the number of stations on any one stream is necessarily limited, it becomes desirable to apply the data obtained at one point to other points on the same stream. This may be done by determining the relative drainage areas. It should be noted, however, that the efficiency of a stream increases as the headwaters are approached. During the dry season of 1897 Yadkin River had nearly 331 per cent greater efficiency at Salisbury than at Norwood, and the Catawba had nearly 20 per cent greater efficiency at the Catawba station, near Hickory, North Carolina, than it had at Rockhill, South Carolina. Neuse River has the lowest efficiency of any stream in North Carolina, its drainage area lying wholly in the eastern section of the State, where the geological formation is not conducive to perennial springs, and during the dry season of 1897 the run-off for that river at Selma, North Carolina, was only 15 per cent of that of Broad River at Gaffney, South Carolina, for the same drainage area. The drainage area of the latter stream lies wholly in the mountains; that of the former stream lies in the lowlands. In the year 1897 the maximum flood of the Neuse was 105 times its minimum flow, while the maximum flood of the Broad was only 24 times its minimum flow. These two streams are excellent illustrations of the effect of physical conditions on the efficiency of flow, and the physical conditions are almost invariably such as to give greater efficiency as the headwaters are approached.

A knowledge of the greatest flood volume of a stream is most essential in the construction of hydraulic works. Experience has shown that the failure of dams may in nearly every case be attributed to lack of sufficient knowledge of the floods which they will be required to withstand. In this respect also streams are very dissimilar. For instance: The maximum flood of the Roanoke in 1897 (gage height of 28 feet at Neal, North Carolina) was about 7 second-feet per square mile. In the same year Tar River gave a flood discharge of 6 secondfeet, Neuse River a flood discharge of 7 second-feet, Cape Fear River 8 second-feet, Yadkin River' 10 second-feet, and Broad River 13 second-feet, while the Catawba developed a flood of 26 second-feet to the square mile. The greatest flood ever recorded on the Cape Fear at Fayetteville, North Carolina, was a gage height of 58 feet above low water and a discharge of only 13 second-feet per square mile, or half that of the Catawba in 1897.

MEASUREMENT OF SEDIMENT.¹

The following method has been employed for measuring the amount of sediment held in suspension by streams in Arizona: By means of a small bottle attached to a hollow rod, samples were taken from various parts of the stream and collected in a bucket. After thorough mixing, the water in the bucket represented as nearly as possible the average condition of the water flowing in the stream. A measured quantity of this water, usually 100 cubic centimeters, was placed in a tubular graduate of glass divided into cubic centimeters. Ordinarily this was allowed twenty-four hours to settle, but if longer time was required for thorough settlement, it was allowed. The clear liquid was then decanted and rejected, leaving a small quantity of water with the sediment in the bottom. If the amount of sediment was inconsiderable, another sample was added, taken on the day following that on which the first sample was procured, and after settlement it was decanted in like manner, the process being repeated from day to day until a sufficient quantity of sediment had accumulated to make a reading on the scale of the glass graduate. Under ordinary conditions, when the stream was not in flood, it sometimes required thirty days to accumulate samples which would show 2 or 3 cubic centimeters of sediment, but at times of flood a large quantity of sediment was sometimes obtained from a single sample of 100 cubic centimeters, in which case the quantity of sediment was ascertained by reading, and a new determination was started on the following day. The total quantity of sediment obtained from the samples or series of samples was divided by the quantity of water used in the accumulation, and a ratio was thus established which was applied to the total volume flowing in the river.

It was found that the mud obtained from these samples was of a very thin consistency and contracted greatly upon being dried. To determine the amount of this contraction for Gila River water a number of laboratory tests were made. The residue was dried at 100° C., and the dried material was weighed, its specific gravity also being determined. As might be expected, the results of these tests were by

¹ Report of A. P. Davis.

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no means uniform, but the mean of the tests made indicated about one part of dry matter to five parts of mud, which factor has been used in reducing observations of this kind. In other words, it is assumed that after complete settlement the mud in the bottom of the water sample consists of one part of solid matter and four parts of water.

The foregoing method requires very little skill and time, and the apparatus used is extremely simple. The error of the determinations lies mainly in the assumption of the factor used in reducing the mud to solid matter, and it is probably considerable.

Another method which is now undergoing test is as follows: Samples of water are obtained in the manner already described, and a measured quantity is poured upon an ordinary filter paper in a funnel and is filtered as in the chemical laboratory. If the residue is inconsiderable the process is repeated until a measurable quantity of sediment is obtained, which is dried and afterwards is weighed. The reduction is made in the same way as in the first method, that is, the quantity of water used is to the sediment obtained as the quantity of water flowing in the stream is to the quantity of silt carried in suspension.

This method, to be used with any considerable degree of accuracy, requires the use of a pair of delicate scales. The error of the determination consists partly in the errors of observations, which would be greater than by the first method, unless great skill is employed in the filtering and weighing of the sediment, but chiefly in determining or assuming the specific gravity of the silt obtained, as it is volume and not weight that ordinarily is required. It is believed, however, that where the necessary instruments and skill are available it is much more accurate than the first method.

The method of estimating the turbidity by measurement of opacity is inaccurate in any country where the water is stained to any considerable degree by leaves and roots with which it comes in contact. This is clearly shown by the writer's experience on sluggish rivers in Nicaragua, notably the San Francisco and Deseado rivers. On the latter stream it was sometimes desired to gage the river in the absence of the electric recording apparatus, but attempts to do this showed that it was impossible to observe the revolutions of the meter more than 6 inches beneath the surface of the stream, owing to the opacity of the water. At the same time sediment samples were settled and accumulated for sixty days without yielding any measurable quantity of solid matter, showing that the water was free from sediment, the dense opacity being caused entirely by vegetable stains produced by the leaves, roots, and bark of the dense tropical vegetation with which it came in contact. However, vegetable stains and sediment are seldom found in considerable degree in the same water, for only sluggish waters remain long enough in contact with vegetation to become colored, and these carry but little sediment, so that in most

cases opacity observations can profitably be used by carefully noting the true cause of the opacity.

Mr. Allen Hazen, member American Society of Civil Engineers, after reading the foregoing description, made the following comments:

Of course the aggregate amount of sediment carried by a stream, considered with reference to its tendency to fill a reservoir, is very different from the average amount of sediment carried by the water from a waterworks standpoint. In the first case, the maximum amount of sediment occurs, generally speaking, at times of maximum discharge, and, for most streams with which 1 am familiar, so large a percentage of the sediment as to be practically the whole of it would be carried by the water in floods occupying but a few days in each year. The average amount of sediment in the water taken for waterworks purposes, on the other hand, represents the average of the amounts in substantially equal volumes of water taken from the stream each day in the year. In comparing different streams with one another, I think it would make a great difference which method was used.

The statements regarding the colors of the waters in Nicaragua are of great interest. Of course color is an element of disturbance in any optical method of measuring turbidity. Computations and experiments conducted by Mr. Whipple and myself show, however, that water with a color which will be tolerated as a municipal supply, or which is capable of being decolorized at a reasonable cost, is not so highly colored as to affect the turbidity reading to a notable extent. The most deeply colored waters with which I have had experience have not much exceeded 2.00 on the platinum scale. The waters from Nicaragua referred to must have had colors many times deeper than this, and it would be very interesting to have accurate determinations of their colors made.

Mr. George W. Fuller, associate member of the American Society of Civil Engineers, made the following comments upon the methods described:

The determination of turbidity is a very important matter in connection with various water problems. Various methods are practiced for its determination, and thus far no standard method obtains. Apparently the "standard silica solution" is going to accomplish a great deal in this direction. Careful studies of this method are now being made at New Orleans, and the results are very promising. Messrs. Whipple and Jackson first described the standard silica solution method in the "Technology Quarterly," Vol. XII, No. 4.

The method used by Mr. Davis in Arizona was tried by myself at Louisville for several months, side by side with gravimetric determinations. It was found that the individual results were quite variable, although for the purpose for which he used them the method is probably much more satisfactory than under the conditions to which it was put in getting an accurate record of the rapidly changing Ohio River water.

The second method mentioned by Mr. Davis strikes me as a more satisfactory one, when reasonable facilities are available for carrying it out. It does not appear to me that it is so much the specific gravity of the sediment as the percentage of voids as actually found in the bottom of the reservoirs, that would materially affect the correctness of the estimates as to volume. This method has been used for a great many years on the Missouri and Mississippi rivers, and is described in the European text-books on water analysis. With coarse-grained turbidity it seems to work very well, and, all things considered, I presume that as a laboratory method it is entitled to high rating.

With the Ohio River water, which contains a considerable percentage of very

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fine clay, this method was not found to be practicable, as the clay would pass through a dozen or more thicknesses of the finest filter paper, to say nothing of the length of time necessary for filtering the clay. On that work it was the practice to determine the total residue on evaporation of the water as collected, and then of the filtrate after passing the water through a Pasteur filter. The suspended matter could then be obtained by the difference, and the results were quite satisfactory when the amount of sediment was not too low. There is a slight error in this procedure, due to the Pasteur filter sometimes absorbing and sometimes giving off dissolved substances. Taking everything into consideration, the standard silica solution seems to be the more practicable procedure at present for routine work, especially when used with a diaphanometer (see Technology Quarterly, Vol. XII, No. 2). At New Orleans this method is being depended upon very largely, although the weight of suspended matter is being determined by the same method as at Cincinnati, as frequently as time allows, in order to establish the ratio between the silica turbidity and the weight of suspended matter.

There are, of course, many instances where turbidity and dissolved color are both present in the same water. As a general proposition, however, this does not seem to be true, as the very highly turbid waters below the glacial drift formation do not generally contain much color. Strictly speaking, however, such a statement would apply only to large rivers, and not to very small streams, which are influenced by swamps. On the other hand, those streams for the most part on the drift or in the neighborhood of swamps, and which are highly colored, do not, as a rule, contain sufficient turbidity to justify any elaborate records of the suspended matter.

In future years the amount of dissolved vegetable matter giving color to a water is bound to be a factor. Information upon this subject is very desirable. As suggested by Mr. Hazen, it is likely that this matter could best be handled in the field by a graduated color scale on glass, the different tints or depths of color to be obtained progressively by the use of different shades of color, or different thicknesses of glass, as found most expedient.

TESTS TO DETERMINE THE ACCURACY OF DISCHARGE MEAS-UREMENTS OF NEW YORK STATE CANALS AND FEEDERS.¹

During the summer of 1900 the State of New York undertook investigations to determine the flow, seepage, and evaporation of its canals. The work was under the immediate supervision of Mr. E. Kuichling, member American Society of Civil Engineers. Careful measurements were made by means of floats and current meters at various points on the Erie Canal and its branches. After completing the work it was thought wise to investigate the methods and determine the accuracy of the measurements taken. These special experiments were made under the direction of Prof. G. S. Williams, in charge of the hydraulic laboratory at Cornell University, assisted by the writer, by Mr. W. P. Boright, civil engineer, and by members of the senior class in experimental hydraulics at the university. Float and meter measurements were made in the flume at the hydraulic laboratory, and the results were compared to determine the variation between the two methods of measurement. It is thought that a brief description of the general method applied and of the results obtained will be of interest to engineers.

The movement of water in canals and feeders is quite different from that of a natural stream. This difference is due mainly to lockage and to irregular feed from one section to another, which cause rapid fluctuations of the surface level and of the velocity—in some cases the surface level dropped several inches in a few seconds and the velocity increased from 25 to 50 per cent. The disturbance of the water at a given place may be due either to lockage or to feed at one or both ends of the section. The water that is needed in a lower level should be passed through a culvert. Ordinarily, however, it is passed through the lock by opening one or more valves in the gates. In some cases four such valves are opened at once for a few minutes, but as a rule only one is opened for a longer time. It will readily be seen, then, that when a boat is passing in or out of a section which is being gaged, or is entering or leaving short adjacent sections, the water in that section is in a very disturbed condition. The length of time required for it to return to a normal condition after one of these disturbances, depends to some extent on the velocity of the water. The greater the velocity, the quicker it will return to normal condition: for very low velocities it requires hours to quiet down. In one case, with a steady gage, it was impossible to obtain a single gaging (which required only five minutes) in a whole day. It will readily be seen that, to be of any value, discharge measurements under such conditions must be made quickly. Even when the surface did not fluctuate the work was often stopped by one or more boats passing the place of measurement. Instantaneous measurements of discharge and a continuous record of surface fluctuations at the point of measurement are desirable. This was approximated by making a rod gaging in from four to ten minutes and reading the surface fluctuations every thirty to sixty seconds.

Two instruments were used to measure the velocity, viz, float rods and current meter. The float rods used were 1.90 inches in diameter, of wood, and weighted at the lower end with iron pipe and lead of the same diameter, so as to float upright. By adjusting the weight at the lower end the immersed length of the rod may bear any ratio to the depth of the water in which it floats. If the immersed length is equal to the depth, the speed or velocity of the rod is very nearly that of the average velocity of the water in the vertical plane in which the rod moves. On account of the action of the wind on the part of the rod which projected above the surface of the water, that part of the rod was limited in length to about 8 inches. Extensions of the rod were used when the depth required them.

In this work it was not possible to have the depth of immersion of the rods more than about 90 per cent of the depth of the water, on account of inequalities in the bottoms and sides of the canals. Neither was it advisable to have rods of many lengths, on account of the labor required to transport them from place to place. Rods of three lengths were carried, viz, 18, 40, and 80 inches, which, with a set of extensions to use on either the 40-inch or the 80-inch rods, gave five lengths. From these were selected those that could be used with the greatest depth of immersion and which would not project more than 8 inches out of the water. The discharge of the channel was computed from a number of gagings made very rapidly, when the surface fluctuated little, with different depths of immersion. It is very desirable that results obtained in this way should be tested by comparing them with results obtained under the same conditions by a more accurate method of measurement.

Two kinds of tests were made: (1) Rod discharge by one party with rod discharge by the other party, and rod discharge with meter discharge, made on the canals and feeders under actual conditions; and (2) rod discharge and meter discharge with discharge over standard weir, made in the hydraulic laboratory of Cornell University.

The discharge of the Erie Canal at Rochester was measured simultaneously with rods by two parties, and was again measured simultaneously with rods by one party and with meter by another party. At Lockport a similar comparison of rod discharge with meter discharge was made. Similar comparisons of rod discharge with rod discharge and of rod discharge with meter discharge were made on the Black River Canal at Boonville and on the Glens Falls feeder at Glens Falls. A comparison of the rod measurements of one party with the simultaneous rod measurements of the other party will show the error in measuring the loss of water between stations, and a comparison of the meter measurements made on the canals with the meter measurements made in the hydraulic laboratory at Cornell will serve to tie together the two sets of tests.

The common method of measuring discharge with a current meter, by observing the velocity at many points in a cross section, could not be used in this work because it required too much time. Two more rapid methods were used, viz, the six-tenths method and the integrating method. The former method consists in making a single observation in each vertical at a distance from the surface equal to six-tenths of the depth of the water. It generally gives, as do the float rods, the mean velocity in a vertical in one observation. The integrating method is more rapid than the six-tenths method, but it is not so accurate. It consists in moving the meter from the bottom to the surface and from the surface to the bottom several times while it is being carried from one side of the channel to the other. In this work the integrating method was only used as a check on the results obtained by the six-tenths method.

The current meter has a small revolving wheel with a rate of motion proportional to the velocity of the water in which it is held. Being small, one observation with this wheel gives the mean velocity for only a few square inches, and it is necessary to hold it in several places in a vertical in order to get the mean velocity in that vertical, while the float rods give the mean velocity in a vertical at one observation. The meter will give the velocity at any point in the depth; the rods will give the mean velocity only. The meter can also be used where the rods can not, and it is a less expensive method of measuring discharge.

The laboratory tests cover a range of velocities of 0.25, 0.50, 1, and 1.50 feet per second for channel depths of 7.5, 8.3, and 9 feet, and 0.5, 1, 1.50, and 2 feet per second for a channel depth of 6 feet. Two depths of immersion were used with each velocity, viz, 75 per cent and 90 per cent. Every velocity, depth of channel, and depth of immersion found in the field work could not be duplicated in the laboratory tests, so that the foregoing range covers only the most important cases. The laboratory experiments were made in the same way as the field experiments, using the same lengths of run and the same distance from the point of starting the floats to the upper chain.

The conditions of the flow were not quite the same in the field tests as in the laboratory tests. The Lockport comparison was made in a rock cut, with nearly vertical rough rock sides and a rough bottom. The meter section was 62.5 feet wide, 8.5 to 9 feet deep, and about 700 feet above the point where the rod measurements were made. The section where the rod discharge was measured was 65 feet wide and 8.5 to 10 feet deep. There was undisturbed flow for at least a half mile on each side of the place of measurement. The Rochester comparisons were made on the Rochester Aqueduct, which has very smooth and nearly vertical sides. The width was 43 feet, the depth 7.5 feet. The flow was undisturbed for a half mile above the point of measurement, but there was a very sharp curve less than 100 feet below the place where the rods were used. The Boonville comparisons were made in an earth cut with side slopes varying so as to make a gradual transition from the flat bottom to the top. The surface width was 43 feet, the greatest depth 7.7 feet. There was unobstructed flow for a quarter of a mile above the point of measurement and for a half mile below it. The sections where the Glens Falls comparisons were made have nearly vertical sides. The width is 32 feet, the greatest depth 6 feet. There is a bend in the feeder about 100 feet above the upper section, and another bend about 1,000 feet below the lower section. The meter section was between the rodmeasuring sections, 75 to 100 feet distant from them.

The Cornell University canal has vertical sides of concrete and a concrete bottom. One side is at present roughened somewhat on account of the lining being cut out in places preparatory to its repair. The canal is 16 feet wide, 10 feet deep, and 415 feet long, with a standard sharp-crested weir, and with gates at the upper end for admitting water and at the lower end for controlling the depth of water in the canal, and with piezometers and gages for measuring accurately the head on the weir and the depth of water in the canal. The discharge of the weir is known for any head on it, so that a simple measurement of the head gives the discharge of the canal. The discharge can then be measured with rods or current meter and compared with the weir discharge, and thus the error by the rods or meter be determined. The weir is 220 feet above the point where the rod measurements were made, and 15 feet below it are baffleboards for quieting the water. About 70 feet below the meter section is a bulkhead, and at the side of it are two rectangular gates. During the experiments the water passed out of the canal through two horizontal slits in the bulkhead, used to secure velocity in all of the water section. At the higher velocities some water passed out under one of these gates. The width of the Cornell channel was only from one-fourth to one-half that of the channels in which the field comparisons were made. At Cornell the water was probably moving in a more disturbed condition than in the canals and feeders. The retarding effect of bottom and sides was less in the former channel than in the latter, and the depth of water and the area of the channel were measured with greater accuracy at Cornell than on the canals.

The results of the field comparisons are given in the following table:

Place.	Date.	V'r.	V"r.	Vm.	Q′r.	Q″r.	Q <mark>m</mark> .	${f Q'r}_{{f Q''r}}$ in Q'r.	Q'r- Qm in Q'r.	Q"r- Qm in Q"r.
Lockport Rochester Do Do Boonville Do Glens Falls Do	1900. Sept.14 Sept.20 Sept.21 do Sept.25 do do do do do do do	Feet. 	$\begin{array}{c} Feet. \\ 1.440 \\ .704 \\ .884 \\ .889 \\ .899 \\ .813 \\ .850 \\ .836 \\ .690 \\ .640 \end{array}$	Feet. 1.531 .736 .929 .939 1.079 1.111	Cu. ft. per sec. 297.82 227.22 164.73 149.66	$\begin{array}{c} Cu.\ ft.\\ per\ sec.\\ 805.70\\ 235.12\\ 302.04\\ 301.35\\ 307.08\\ 227.51\\ 238.81\\ 233.54\\ 172.77\\ 158.57 \end{array}$	Cu. ft. per sec. 799.85 251.57 310.83 317.54 228.66 234.70 161.50 155.23	Per ct. 1.41 13 4.88 5.92	Per ct.	$\begin{array}{c} Per \ ct. \\ +0.73 \\ -7.00 \\ \hline \\ -3.14 \\ -3.46 \\ \hline \\ +4.25 \\49 \\ +6.52 \\ +2.11 \end{array}$

Results of field comparisons.

V'r = mean velocity found by party No. 1, with rods.

V''r=mean velocity found by party No. 2, with rods.

Vm=mean velocity found with meter, using six-tenths method.

Q'r =discharge found by party No. 1, with rods.

Q''r=discharge found by party No. 2, with rods.

Qm =discharge found with meter, using six-tenths method.

In the Lockport and Glens Falls comparisons the meter was suspended from a bridge by means of an insulated wire. In the Rochester and Boonville comparisons it was suspended from a boat by means of the same wire. The conditions were very good during the Lockport comparisons. There was very little wind, the surface did not fluctuate, there was a good measurable velocity in all parts of the cross sections, and no curve near to disturb the direct flow of the water. The meter discharge will be seen to agree closely with the rod discharge. The conditions were not so good in the Rochester comparisons. The lower gaging station was too near a curve in the canal. The time of run of the individual rods at the same point differs by a considerable amount, much more than at the upper station. On the afternoon of September 20 the surface did not fluctuate much, but rain interfered somewhat with the work. The meter discharge for that day is 7 per cent greater than the corresponding rod discharge. The next day, September 21, the surface fluctuated somewhat, but not more than while much of the regular gaging work was being done. The rod discharge measurements for that day differ by 1.41 per cent, and the average meter discharge is larger than the rod discharge by 3.3 per cent.

At Boonville the conditions were all good. The rod discharges agree closely, as does one of the meter measurements with the corresponding rod measurement.

The Glens Falls comparisons are not very good—the upper gaging station was too near a curve, and there was a strong probability of leakage from the feeder between the points where the rod measurements were made. There was no leakage visible on the surface, but the point where the measurements were made is only a short distance below the portion of the feeder which is noted for its large leakage, so that there probably was some leakage here, although it does not show on the surface.

For the reasons stated we believe that the results of the Glens Falls comparisons should be given little weight, and that those at Rochester should be given only half the weight of those at Lockport and Boonville.

		F	lod gaging	rs in cana	1.		
Date.	Referred	Depth of	Immersio	on, 75 per nt.	Immersion, 90 per cent.		
	tostand- ard weir.	water.	Veloc- ity.	Dis- charge.	Veloc- ity.	Dis- charge.	
1900. October 24 Do Do Do October 26 Do October 27 Do Do October 27	$\begin{array}{c} Cu.ft.\\ per sec.\\ 214.6\\ 140.5\\ 71.7\\ 38.2\\ 178.6\\ 125.3\\ 61.3\\ 30.9\\ 196.4\\ 132.4\\ 132.4\\ 132.4\\ 132.4\\ 31.1\\ 50.3\\ 198.3\\ 125.3\\ 65.3\\ 31.1\\ \end{array}$	$\begin{array}{c} Feet. \\ 9.36 \\ 9.25 \\ 9.34 \\ 8.81 \\ 7.55 \\ 7.55 \\ 7.47 \\ 7.38 \\ 6.16 \\ 6.30 \\ 6.23 \\ 5.85 \\ 8.37 \\ 8.39 \\ 8.37 \\ 8.26 \end{array}$	$\begin{array}{c} Ft. per\\ sec.\\ 1, 42\\ -, 96\\ .28\\ 1, 51\\ 1, 08\\ .27\\ 2, 07\\ 1, 35\\ .95\\ .56\\ .56\\ .56\\ .54\\ .96\\ .61\\ .25\\ \end{array}$	$\begin{array}{c} Cu.ft.\\ per sec.\\ 213.8\\ 143.0\\ 73.5\\ 39.1\\ 183.1\\ 131.0\\ 63.7\\ 31.6\\ 204.7\\ 136.7\\ 95.4\\ 52.2\\ 204.9\\ 129.1\\ 68.8\\ 33.1\\ \end{array}$	$Ft. per \\ sec. \\ \hline \\ 0.95 \\ .48 \\ .27 \\ 1.53 \\ 1.06 \\ .52 \\ .26 \\ 2.04 \\ 1.34 \\ .94 \\ .55 \\ 1.51 \\ \hline \\ .55 \\ .24 \\ \hline \\ \end{array}$	$\begin{array}{c} Cu.ft.\\ per sec.\\ \hline \\ 141.0\\ 71.4\\ 38.6\\ 184.8\\ 128.3\\ 62.5\\ 30.3\\ 202.4\\ 135.8\\ 94.5\\ 51.6\\ 202.4\\ \hline \\ 67.3\\ 32.1\\ \hline \end{array}$	

Results of experiments at Cornell hydraulic laboratory.¹

¹A recomputation of this data gave results slightly different from those contained in this report.

Results of experiments at Cornell hydraulic laboratory-Continued.

	Current-meter gagings in canal.													
	Re-		SI	nall	Price r	neter (N	o. 363).	Small o	Pric rdin	e m ary	eter (1 metho	Jo.351), d.		
Date.	ferred to stand- ard	Dep of wate	pth of si ter. n		enths hod.	Integ: met	Integrating method.		7tica	1.	Graj	phical.		
	weir.		Ve it	loc- y.	Dis- charge	Veloc- ity.	Dis- charge.	Veloc- ity.	Di chai	s- ge.	Veloc- ity.	Dis- charge.		
1900. October 24 Do Do October 26 Do	$\begin{array}{c} Cu. ft.\\ per sec.\\ 216.1\\ 140.5\\ 71.7\\ 38.3\\ 178.6\\ 125.8\\ 61.3\\ 31.2\\ 196.4\\ 132.4\\ 91.1\\ 132.4\\ 91.1\\ 132.5\\ 31.2\\ 25.3\\ 65.3\\ 31.2\\ 31.2 \end{array}$	Fee 9. 9. 9. 9. 7. 7. 7. 7. 6. 6. 6. 8. 8. 8. 8. 8. 8.	$\begin{array}{cccc} Ft \\ t. & s \\ 377 \\ 344 \\ 587 \\ 667 \\ 664 \\ 588 \\ 566 \\ 288 \\ 400 \\ 322 \\ 001 \\ 457 \\ 511 \\ 511 \\ 48 \\ 46 \end{array}$	$\begin{array}{c} . per \\ ec. \\ 1.47 \\99 \\28 \\ 1.49 \\52 \\52 \\52 \\99 \\ 1.32 \\94 \\54 \\ 1.51 \\95 \\50 \\24 \end{array}$	$\begin{array}{c} Cu.ft.\\ persec\\ 223.0\\ 148.5\\ 73.2\\ 40.1\\ 184.1\\ 128.9\\ 63.8\\ 31.5\\ 201.4\\ 136.0\\ 95.7\\ 52.7\\ 206.5\\ 130.0\\ 67.7\\ 32.7 \end{array}$	$\begin{array}{c} Ft. per \\ sec. \\ 1.43 \\ .98 \\ .48 \\ .31 \\ 1.52 \\ 1.08 \\ .52 \\ .31 \\ 2.03 \\ 1.34 \\ .92 \\ .56 \\ 1.55 \\ 1.00 \\ .49 \\ .32 \end{array}$	$\begin{array}{c} Cu. ft.\\ per sec.\\ 217.5\\ 148.1\\ 72.7\\ 44.4\\ 187.8\\ 131.7\\ 63.8\\ 38.1\\ 205.4\\ 138.1\\ 93.8\\ 241.2\\ 211.7\\ 137.3\\ 67.1\\ 43.4 \end{array}$	$\begin{array}{c ccccc} Ft. per & Cu.ft.\\ sec. & per sec\\ 1.45 & 220.4\\ .95 & 143.1\\ .48 & 71.5\\ .24 & 23.3\\ 1.41 & 174.7\\ .98 & 120.3\\ .50 & 61.3\\ .23 & 28.1\\ 1.86 & 188.2\\ 1.20 & 123.8\\ .82 & 83.9\\ .48 & 46.5\\ 1.38 & 187.8\\ .84 & 114.5\\ .44 & 60.5\\ .19 & 25.2\\ \end{array}$		ft. sec. 0.4 3.1 1.5 3.3 4.7 0.8 1.5 3.8 1.5 3.8 3.9 3.5 7.8 4.5 5.2 3.5 7.8 4.5 5.2	$\begin{array}{c} Ft.per\\sec.\\1.44\\.95\\.48\\.255\\.43\\1.00\\.50\\.24\\1.90\\1.24\\1.90\\1.24\\.86\\.49\\1.44\\.86\\.45\\.21\\\end{array}$	$\begin{array}{c} Cu.ft.\\ per sec.\\ 219.0\\ 143.2\\ 72.1\\ 35.5\\ 176.2\\ 123.1\\ 60.7\\ 29.2\\ 192.1\\ 127.3\\ 87.3\\ 87.3\\ 195.8\\ 87.3\\ 117.3\\ 61.0\\ 28.9\\ \end{array}$		
		Error in discharge computed by different methods when re- ferred to standard weir.												
	Thus		Rod r	neas ents	ure-		Met	er measurements.						
Date.	locity at meter station.		mmon	r- Immer-		Six-1 me	tenths thod.	Inf		0	ndi '	Ordi- nary method		
		si pe:		sion per		si t. pe	on, 90 er cent.	Analyt- ical.	Graph ical.	grat n- metl	ing hod.	me	ary ethod.	com- puted from ve- locity curves.
1900. October 24 Do Do October 26 Do Do Do Do Do Do Do Do Do Do Do October 31 Do October 29 November 1	Ft.pers 1. 1. 1. 1. 1. 1. 1. 1. 1. 1.	sec. F 41 93 48 227 44 02 50 26 94 28 89 52 45 92 48 23	$\begin{array}{c} er \ cen \\ +3.6 \\ -1.74 \\ -2.56 \\ -2.44 \\ -2.57 \\ -4.55 \\ -3.94 \\ -3.94 \\ -4.25 \\ -3.94 \\ -4.35 \\ -3.6 \\ -3.6 \\ -3.6 \\ -5.14 \\ -6.14 \end{array}$	$\begin{array}{c c} cent. \\ \hline Per \ cent \\ 3. 64 \\ \hline \\ 1. 74 \\ 2. 56 \\ 4. 25 \\ 2. 57 \\ -1. 02 \\ 2. 57 \\ -3. 51 \\ 4. 55 \\ -2. 40 \\ 1. 93 \\ 2. 24 \\ +2. 01 \\ 4. 23 \\ -3. 04 \\ 2. 32 \\ 4. 75 \\ -3. 74 \\ -2. 62 \\ 3. 36 \\ -2. 11 \\ 3. 05 \\ -2. 88 \\ 6. 14 \\ -3. 16 \end{array}$		$\begin{array}{c} Per \ cent. \\ -4.11 \\ -6.13 \\ -2.08 \\ -6.00 \\ -3.09 \\ -2.76 \\ -4.84 \\ -1.46 \\ -3.18 \\ -5.32 \\ -5.92 \\ -3.71 \\ -3.75 \\81 \\ -2.47 \end{array}$	$\begin{array}{c} Per \ cen \\ -3.1 \\ -5.7 \\ -2.0 \\ -4.6 \\ -2.8 \\ -4.0 \\ -1.6 \\ -2.5 \\ -2.5 \\ -4.7 \\ -4.1 \\ -3.7 \\ -2.8 \\ -4.0 \end{array}$	$\begin{array}{c} t. \ Per \ c \\ 77 \ -16 \\ 70 \ -36 \\ 88 \ -36 \\ 86 \ -11 \\ 96 \ -36 \\ 86 \ -11 \\ 96 \ -36 \\ 86 \ -36 \ -36 \\ 86 \ -36 \ -36 \\ 86 \ -36 \ -36 \\ 86 \ -36 \ -36 \\ 86 \ -36$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		$\begin{array}{c} \cdot \ cent. \\ -1.97 \\ -1.84 \\ -2.17 \\ -2.17 \\ -3.60 \\ -2.17 \\ -3.60 \\ -0.08 \\ -10.00 \\ -4.14 \\ -6.49 \\ -7.67 \\ -7.67 \\ -5.28 \\ -8.60 \\ -7.44 \\ -19.34 \end{array}$	$\begin{array}{c} Per \ cent. \\ -1.13 \\ -1.94 \\64 \\ +7.02 \\ +1.34 \\ +1.75 \\ +.90 \\ +6.41 \\ +2.20 \\ +3.84 \\ +4.08 \\ +5.72 \\ +1.22 \\ +6.41 \\ +6.62 \\ +7.57 \end{array}$		

NOTE.—Minus sign indicates that the discharge is greater than that by standard weir; plus sign indicates that it is less than that by standard weir.

Referring to the Rochester comparisons, it must not be inferred that because the rod discharges found by the two parties on September 21 agree closely, and the meter and rod discharges of the 20th differ by 7 per cent of the rod discharge, that this difference is all due to the meter. At least half of it is chargeable to the rod measurement. The two sets of velocity readings given by the meter on the 20th agree closely; there is nothing about them that will account for this large difference. The time of run of the rods, however, differs by a considerable amount, as already stated. The rodmeasuring party was hindered by the rain and by the refusal of one of the men to work in the rain.

The results of the experiment work are given in the foregoing tables. The method of procedure was to open the head gates until the head on the weir was such as to give the desired discharge; then the slits in the bulkhead and the height of the gates at the lower end of the canal were adjusted so as to give the desired depth of water in the canal. As soon as the flow of water became steady, three parties began measuring the discharge of the canal, one with rods and two with current meters. Two lots of rods were used, one lot of 75 per cent depth of immersion, the other lot of 90 per cent depth of immersion; the former rods were lettered, the latter rods were numbered, so that they could easily be recognized as they passed under each wire. One of the current-meter parties measured the discharge in the ordinary way; the other party used the six-tenths and the integrating methods, and after completing their measurements they assisted the rod-measuring party, four stop watches being then employed and the number of rods observed in a given time being nearly The rod work was continued until the other meter party doubled. completed its measurement. During the experiment a gage giving the head on the weir and two gages giving the depth of water in the canal and the slope of the water surface, respectively, were read every 30 seconds. As a check on the weir gages and canal gage readings other readings were taken with a hook gage several times during the experiment. The length of run of the rods, or the distance between the chains was as follows: 25 feet for the 2-foot velocity, with a starting distance of 10 feet; 20 feet for the 1-foot and the 1.5-foot velocities, with a 10-foot starting run; 10 feet for the 0.5-foot velocity, with a 10-foot starting run; and 7 feet for the 0.25-foot velocity, with an 8-foot starting run. The number of rod observations made in an experiment varied from 50 to 150. The observations of each rod-discharge experiment were platted, using the distance from the side of the canal as abscissa and the time of run as ordinate, and a mean time curve was drawn. The mean time was found from this curve. and from that the mean velocity, which multiplied by the cross-sectional area gave the discharge.

In the six-tenths method the meter was held with its center at sixtenths of the depth from the surface, and, successively, at 1, 3, 7, 9, 13, and 15 feet from one side of the canal, and the revolutions in two consecutive periods of 50 seconds each were counted from the indications of an electric buzzer. The meter was then held at the same distances from the other side of the canal, and the revolutions in two consecutive 50-second periods were counted as before. These observations gave four measurements of velocity, covering a period of 50 seconds each, in these six verticals, at six-tenths of the depth below the surface. These points were platted, using the distance from the side of the canal as abscissa'and the revolutions in 100 seconds as ordinate, and a mean curve was drawn. The mean number of revolutions for the whole cross section was computed from this curve and converted into mean velocity by the use of a rating table. The discharge was then found by multiplying the mean velocity by the cross-sectional area. The discharge was also found, analytically, without platting the points and drawing a mean curve. The difference between the weir discharge and the meter discharge, expressed in per cent, as found by these two processes, is given in the table on page 24. As a rule, the discharge found by using the curve is more accurate than that found without it.

In the integrating method the meter was moved in the following way: Its center started at 0.5 foot from the bottom and 1 foot from the side of the canal, and passed slowly to the surface at 4.5 feet from the side, then to 0.5 foot from the bottom and 8 feet from the side; then to the surface at 11.5 feet from the side, then to 0.5 foot from the bottom and 15 feet from the side. The time at the beginning and end of this operation was noted, and the revolutions of the meter wheel were counted, as indicated by the buzzer. The meter was then carried back over the same path at about the same speed, the time of passage being noted and the revolutions of the meter wheel counted as before. The discharge was computed by dividing the sum of the revolutions of the meter wheel in the passage across the canal and back again by the corresponding time, converting this into velocity and multiplying by the cross-sectional area.

In the ordinary method the meter was held by a rod at five points in the same six verticals in which the other meter was held, and the number of revolutions of the meter wheel, in single periods of 60 seconds each, were read from a recorder. The points in the verticals were usually 1³/₄ inches, 1 foot, and 2 feet from the bottom, the surface, and at one other point between the two. The recorder indicated only complete revolutions, while with the buzzer quarters of a revolution could be recognized. The mean velocity shown by the observations with this meter has been computed in two ways: (1) The mean number of revolutions per second of the meter wheel while being moved from one side of the canal to the other, at the five depths of immersion, have been computed and platted and a curve drawn through them, from which the mean number of revolutions per second for the whole cross section has been found, and this converted into mean velocity by the use of the rating table; and (2) the mean velocity has been computed by using with these observations the observations obtained at the same time with the other meter, using the six-tenths method, the mean revolutions per second at the different depths being converted
into velocity and platted on a large scale, the velocity at six-tenths the depth being platted therewith and a mean velocity curve drawn among the points (not necessarily connecting them), from which the mean velocity for the whole cross section was found. The discharge found from the mean velocity computed in the latter way is given in the table on page 24, also the velocity found by the ordinary method.

Meter No. 351 used in the ordinary way did not work well on November 1. The wheel did not turn continuously for the small velocity 0.229 foot per second, but would stop for a few seconds and then start again. The other meter (No. 363) worked much better for the same velocity. The rating tables, however, indicate that the latter meter will measure a smaller velocity than the former. It should be said that the rating table for meter No. 351, which was used to convert revolutions into velocity, is for the meter suspended by a cable and not held by a rod. There was not sufficient time to rate it on a rod before making the computations.

In the table on pages 23 and 24 two values of depths are given; the one in the third column on page 23 is the mean depth for the 40 feet of distance passed over by the rods, the other (third column, top of page 24) is the mean depth at the meter station, and is for a distance of 15 feet. Two values of discharge of the standard weir are given for each experiment, the one in the second column being the average for the period during which discharge was measured by rods and meter, using the ordinary method; the other being for the period during which the discharge was measured by meter, using the six-tenths and integrating methods.

It will be seen from the table on pages 23 and 24 that the rod discharge and the meter discharge for the six-tenths method and for the integrating method are greater than the weir discharge, and that the meter discharge by the ordinary method is less than the weir dis-The sign used is that of the correction to be applied to the charge. meter or rod discharge to obtain the standard weir discharge. The rod discharge for 90-per cent rod immersion is on an average about 2 per cent greater than the weir discharge, and the rod discharge for 75-per cent rod immersion and the meter discharge by the six-tenths method are each on an average 3.5 per cent greater than the weir discharge. The variation from the weir discharge, which we will call the error, is in each case slightly greater for the lower velocities than for the higher velocities. The extreme percentage difference between any discharge and the mean of all the corresponding discharges is about 2.6 per cent. The error in the discharge as found with the current meter, using the ordinary method, is seen to increase as the velocity decreases, and the error in the meter discharge as found by the integrating method is seen to also increase as the velocity decreases. It also increases as the speed at which the meter is carried through the water increases. This we know must be the case, since the velocity indicated by the meter is the resultant of the velocity of the water

and the velocity of the meter as it is moved through the water. When the velocity of the water is small, doubling the speed of the meter will nearly double the indicated velocity. In the following table is given the speed, in feet per second, of the meter, also the percentage of difference between the true velocity and the velocity as found by the integrating method. For a given speed of meter, the error is seen to be greater for the low velocities than for the higher, and for any given velocity of water the error increases with the speed of the meter.

Table showing effect of change of speed of meter in the integrating method, computed from experiments at Cornell University.

Date.	Depth of water.	(S) Speed of meter, inte- grating method.	(V) True ve- locity.	(V ₁) Velocity by integrating method.	$\frac{V-V_1}{V}$
1900	Feet	Ft per sec	Et ner sec	Et per sec	Porcont
October 24	9.460	0.118	1.409	1 429	-142
Do	9.374	142	. 932	982	- 5 36
Do	9 338	164	477	485	- 1.68
Do	8 918	107	265	308	
October 96	7 673	137	1 444	1 519	5 20
Do	7 640	135	1 018	1 079	- 5.00
October 97	7 589	149	509	599	2 00
Do	7 557	199	.00%	. 022	0.00
Do	6 979	. 120	1 040	0.00	
D0	0.210	. 100	1.940	2.000 1.000	4.04
D0	0.399	.104	1.200	1.558	4.29
Do	6.319	. 188	. 893	. 920	-3.02
Do	6.005	. 142	. 515	. 555	- 7.77
October 29	8.476	. 151	. 478	. 492	-29.29
October 31	8.470	. 293	1.454	1.552	- 6.74
Do	8.508	. 258	. 915	1.002	- 9.51
November 1	8.455	.185	. 229	. 319	-39.30
November 29	8.476	. 301	. 478	. 572	-19.67

CONCLUSIONS.

Assuming that the discharge given for the Cornell University weir is correct, the greatest percentage error in discharge when measured with rods of 90 per cent depth of immersion is 3.74 per cent. The range of percentage errors, omitting that on November 27 for velocity, 0.255 foot per second, is 4 per cent, the mean error for all depths and velocities is 2 per cent, and the greatest variation from this mean is 2.5 per cent. The greatest percentage error in the discharge when measured with rods of 75 per cent depth of immersion is 6.14 per cent. The range of these percentage errors, omitting that on November 24 for the velocity of 1.409 feet per second, is 4.4 per cent. The mean error for all depths and velocities is 3.5 per cent, and the greatest departure from this mean is 2.6 per cent. The greatest percentage error in the discharge as found with the current meter, using the sixtenths method, is 5.7 per cent, and the range of these percentage errors is 4.7 per cent. The mean percentage error for all depths and velocities is 3.5 per cent, and the greatest departure from this mean is 2.6 per cent.

From these facts we may conclude (1) that a discharge measure-

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ment of a canal or feeder may be in error 6 per cent when its mean velocity is small, but that, as a rule, the error will not be more than 3.5 per cent, and (2) that a measurement of loss from a section, which is mainly the difference between two simultaneous discharge measurements, may be in error 4.7 per cent—the largest difference that can be obtained by subtracting any two of the percentage errors in the third, fourth, and sixth columns of the table on page 24, except the two just mentioned, and it is very unlikely that this worst combination of errors will ever occur; but it is quite likely that the errors made by the two parties will be about the same in magnitude and have the same sign, in which case the measured percolation is nearly free from error. The average error in the measured percolation is probably not more than 2 per cent, and does not depend on the correctness of the standard weir discharge.

Of no little interest and importance is the fact, brought out by these comparisons and accuracy tests, that the current meter will give quickly and with a high degree of accuracy the discharge of canals and feeders or other channels of rectangular and trapezoidal cross section with fairly smooth bottoms.

The general subject of the relative accuracies of the various methods of measuring stream flow should be more thoroughly investigated, and it is hoped that more light will be thrown upon obscure points in river hydraulics and some improvements be suggested in the methods of measuring the flow of streams.

MEASUREMENTS AT RIVER STATIONS.

KENNEBEC RIVER AT WATERVILLE, MAINE.

This river was described by Prof. Dwight Porter in the Nineteenth Annual Report, Part IV, pages 65 to 84. Tables of its daily discharge from 1892 to 1898 will be found in Water-Supply Paper No. 27, pages 11 to 14; and similar data for 1898 and 1899 will be found in Water-Supply Paper No. 35, pages 25 and 26. The figures for the latter year, however (April to December, inclusive), were not computed with the same degree of accuracy as were those for former years, and since the publication of Water-Supply Paper No. 35 they have been recomputed, and the revised figures for the year 1899 and those for the year 1900 are presented herewith.

The computations for this station include the figuring of the discharge over the dam, through the waste gates and waste weirs, and through the various wheels of the Hollingsworth and Whitney mills. The Sunday flow at times, especially at low stages of the river, is found to be irregular, as the mill at Waterville is sometimes operated Saturday nights, drawing the water from the pond, so that on Sunday there is no flow except that due to leakage. During the dry season there is usually less water passing on Sundays than on week days, for at many of the mills on the river the dams are closed in order to allow the ponds to fill.

Daily discharge, in second-feet, of Kennebec River at Waterville, Maine, for 1899.

100			1 (10		
L	rainage	area,	4,410 S	quare	miles. J

												and the second second
Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1	2,529 2,202 2,274 2,159 2,452 2,4451 1,739 2,4451 1,739 2,451 2,4451 1,739 2,451 2,440 2,3866 2,4404 2,4468 2,448 2	2,458 2,198 2,187 2,163 1,580 2,507 2,173 2,071 2,071 2,071 2,057 2,141 2,244 2,348 1,964 2,348 1,844 2,392 2,277	3,382 3,047 3,333 3,324 1,963 3,331 3,563 3,563 3,563 3,563 3,563 3,563 3,562 3,428 3,552 3,428 3,352 3,552 3,552 3,552 3,552 3,552 3,552 3,552 3,552 3,552 3,5555 3,555 3,5555 3,5555 3,5555 3,55555 3,55555 3,55555555	$\begin{array}{c} 6, 411\\ 6, 214\\ 6, 160\\ 6, 017\\ 6, 207\\ 6, 227\\ 6, 433\\ 7, 541\\ 9, 650\\ 9, 405\\ 11, 181\\ 19, 700\\ 23, 106\\ 38, 826\\ 30, 532\\ 30, 312\\ 30, 312\\ \end{array}$	41, 756 39, 665 36, 589 30, 942 30, 531 30, 125 22, 132 20, 229 18, 697 19, 643 14, 886 15, 009 17, 307 15, 073	$\begin{array}{c} 13,044\\ 12,790\\ 10,647\\ 11,673\\ 12,264\\ 11,123\\ 12,264\\ 12,506\\ 10,738\\ 12,506\\ 10,738\\ 6,039\\ 7,030\\ 6,739\\ 7,557\\ 5,913\\ 6,807\end{array}$	$\begin{array}{c} 6,115\\ 5,024\\ 5,363\\ 3,178\\ 5,258\\ 5,258\\ 5,120\\ 5,076\\ 5,3936\\ 5,142\\ 5,123\\ 5,142\\ 5,120\\ 5,976\\ 5,142\\ 5,100\\ 5,978\\ 4,866\\ 5,100\\ 5,978\\ 4,043\\ 4,862\\ 5,232\\ 4,866\\ 5,232\\ 4,043\\ 4,866\\ 5,232\\ 4,866\\ 5,232\\ 4,043\\ 4,866\\ 5,232\\ 4,045\\ 4,866\\ 5,232\\ 4,045\\ 4,866\\ 5,232\\ 4,045\\ 4,866\\ 5,232\\ 4,045\\ 4,866\\ 5,232\\ 4,045\\ 4,866\\ 5,232\\ 4,045\\ 4,866\\ 5,232\\ 4,045\\ 4,866\\ 5,232\\ 4,045\\ 4,866\\ 5,232\\ 4,045\\ 4,866\\ 5,232\\ 4,045\\ 4,866\\ 5,232\\ 4,045\\ 4,866\\ 5,232\\ 4,045\\ 4,866\\ 5,232\\ 4,045\\ 4,866\\ 5,232\\ 4,045\\ 4,866\\ 5,232\\ 4,045\\ 4,866\\ 5,232\\ 4,045\\ 4,866\\ 5,232\\ 4,102\\ 4$	$\begin{array}{c} 4,809\\ 3,594\\ 4,442\\ 4,199\\ 4,498\\ 4,415\\ 5,195\\ 4,388\\ 4,101\\ 3,954\\ 4,101\\ 3,954\\ 3,538\\ 3,213\\ 3,954\\ 3,538\\ 3,213\\ 3,007\\ 3,331\\ 3,007\\ 3,332\\ 3,332\\ 3,333\\ 3,$	$\begin{array}{c} 1,623\\2,010\\567\\1,612\\2,082\\2,070\\2,082\\2,070\\2,352\\2,067\\2,340\\2,377\\1,261\\1,208\\1,218\\1$	$\begin{array}{c} 1,443\\ 1,665\\ 1,415\\ 1,969\\ 1,476\\ 1,476\\ 1,476\\ 1,215\\ 940\\ 774\\ 1,784\\ 1,968\\ 1,391\\ 1,391\\ 1,378\\ 1,307\\ 1,378\\ 1,667\\ 1,367\\$	$\begin{array}{c} 1,390\\ 2,819\\ 4,093\\ 4,093\\ 3,327\\ 3,327\\ 3,106\\ 2,633\\ 2,119\\ 1,698\\ 1,970\\ 2,053\\ 1,488\\ 1,9707\\ 2,053\\ 1,823\\ 1,739\end{array}$	$\begin{array}{c} 1,456\\1,441\\747\\2,913\\3,567\\3,196\\2,015\\2,070\\1,737\\1,160\\2,022\\5,223\\4,410\\4,621\\1,861\\2,695\end{array}$
19 20 21 22 23 24 25 26 27 28 29 30 31	$\begin{array}{c} 2, 434\\ 2, 434\\ 2, 629\\ 2, 440\\ 2, 709\\ 2, 154\\ 2, 435\\ 2, 453\\ 2, 454\\ 1, 245\\ 2, 513\\ 2, 453\\ 2, 453\\ \end{array}$	2,198 2,915 2,734 2,744 2,451 2,745 2,929 1,420 3,039 3,362	$\begin{array}{c} 3,320\\ 3,320\\ 3,080\\ 2,778\\ 2,771\\ 2,837\\ 2,770\\ 2,030\\ 2,786\\ 2,740\\ 2,998\\ 3,962\\ 6,820\\ \end{array}$	$\begin{array}{c} 37,096\\ 41,565\\ 34,540\\ 30,286\\ 39,550\\ 45,724\\ 41,739\\ 43,139\\ 45,795\\ 39,943\\ 41,584\\ 39,300\\ \end{array}$	$\begin{array}{c} 15,071\\ 15,684\\ 16,262\\ 18,287\\ 17,271\\ 15,900\\ 15,925\\ 11,480\\ 12,567\\ 12,303\\ 13,064\\ 13,035\\ 12,823\\ \end{array}$	7,290 6,483 7,101 7,317 7,319 7,516 5,673 7,301 7,315 6,880 7,038 6,445	$\begin{array}{c} 4,948\\ 4,880\\ 5,499\\ 6,367\\ 5,688\\ 6,509\\ 5,837\\ 5,916\\ 5,502\\ 5,649\\ 4,170\\ 2,500\\ 4,087\\ \end{array}$	$\begin{array}{c} 2, 643\\ 2, 643\\ 1, 242\\ 2, 748\\ 3, 377\\ 2, 956\\ 2, 534\\ 2, 180\\ 2, 180\\ 2, 288\\ 2, 203\\ 2, 065\\ 2, 354\\ \end{array}$	$\begin{array}{c} 2,005\\ 2,362\\ 2,362\\ 2,006\\ 2,351\\ 2,348\\ 1,073\\ 2,031\\ 1,761\\ 1,466\\ 2,046\\ 1,951\\ 2,091\\ \end{array}$	$\begin{array}{c} 1,096\\ 1,096\\ 1,377\\ 1,120\\ \hline \\ 1,408\\ 1,334\\ 1,04\\ 995\\ 1,149\\ 1,21\\ 406\\ 1,104\\ 1,086\\ \hline \end{array}$	$\begin{array}{c} 1,718\\ 2,317\\ 1,748\\ 2,085\\ 2,085\\ 2,028\\ \hline 1,413\\ 1,743\\ 1,744\\ \hline \\ \hline \\ \hline \end{array}$	2,027 2,611 1,878 2,340 2,617 2,068 2,323 2,330 1,821 1,474
Mean _	2,357	2,363	3,218	24,006	21,303	8,821	5,077	3,302	1,854	1,274	2,252	2,741

Daily discharge, in second-feet, of Kennebec River at Waterville, Maine, for 1900.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
Day. 1 2 3 5 6 7 8 9 10 11 12 13 14 15 16 17 18 20 21 22 23 24 25 26 37	$\begin{array}{c} 1,463\\1,565\\1,604\\1,565\\1,604\\1,493\\1,452\\2,060\\1,998\\1,751\\1,714\\1,998\\1,751\\1,714\\1,798\\1,751\\1,748\\2,060\\1,712\\2,060\\4,045\\3,748\\3,697\\3,684\\3,697\end{array}$	$\begin{array}{c} 7,117\\ 3,606\\ 3,628\\ \hline 3,628\\ \hline 3,166\\ 3,158\\ 3,628\\ \hline 3,188\\ 3,303\\ 2,925\\ 3,114\\ 1,615\\ 2,933\\ 12,148\\ 15,073\\ 12,148\\ 15,073\\ 11,998\\ 5,711\\ 5,973\\ 11,998\\ 5,871\\ 7,090\\ 6,978\\ 5,871\\ 13,387\\ 13,3$	$\begin{array}{c} 11447\\ \hline \\ 15,408\\ 9,653\\ 9,654\\ 6,240\\ 9,323\\ 4,913\\ 4,927\\ 4,927\\ 4,927\\ 4,927\\ 4,927\\ 4,932\\ 4,913\\ 7,479\\ 9,323\\ 10,511\\ 10,514\\ 9,792\\ 20,538\\ 12,542\\ 12,442\\ 11,361\\ 10,742\\ 9,792\\ 9,420\\ 5,922\\ 12,442\\ 11,361\\ 10,742\\ 9,792\\ 9,420\\ 5,922\\ 12,442\\ 11,361\\ 10,742\\ 9,792\\ 9,420\\ 5,922\\ 12,442\\ 11,361\\ 10,742\\ 9,792\\ 9,420\\ 5,922\\ 12,442\\ 11,361\\ 10,742\\ 9,792\\ 9,420\\ 5,922\\ 12,442\\ 12$	A pr. 8, 702 8, 531 9, 3387 15, 927 15, 927 17, 050 25, 327 26, 429 35, 155 15, 927 16, 927 17, 050 25, 327 26, 429 35, 155 180 14, 93 19, 93 26, 541 180 14, 93 26, 554 180 180 180 180 180 180 180 180	22, 830 227, 905 28, 823 52, 268 48, 843 39, 551 28, 889 33, 551 28, 889 23, 551 28, 889 23, 551 28, 889 23, 551 28, 628 25, 241 20, 804 18, 378 22, 945 31, 845 40, 225 48, 400 25, 403 23, 333 21, 682 18, 907 17, 467	$\begin{array}{c} 12,115\\12,782\\15,730\\25,091\\14,088\\12,792\\10,950\\10,495\\10,048\\12,792\\10,049\\10,495\\10,048\\9,661\\10,168\\7,707\\9,141\\7,256\\7,808\\7,808\\7,808\\7,808\\5,866\\6,402\\6,651\\5,806\\5,015\\6,669\\5,066\\5,806\\\end{array}$	$\begin{array}{c} 5 \\ 4 \\ 8 \\ 4 \\ 8 \\ 232 \\ 7 \\ 5 \\ 27 \\ 5 \\ 27 \\ 5 \\ 27 \\ 5 \\ 27 \\ 5 \\ 27 \\ 5 \\ 27 \\ 5 \\ 27 \\ 5 \\ 27 \\ 5 \\ 27 \\ 5 \\ 27 \\ 5 \\ 5 \\ 7 \\ 5 \\ 5 \\ 7 \\ 5 \\ 5 \\ 5 \\ $	$\begin{array}{c} 4.02,\\ 4.910\\ 5.525\\ 5.601\\ 4.431\\ 5.358\\ 4.758\\ 4.$	4,238 3,180 2,905 2,995 2,955	$\begin{array}{c} 2,859\\ 3,337\\ 3,134\\ 2,876\\ 2,565\\ 2,565\\ 2,565\\ 3,477\\ 3,477\\ 3,175\\ 3,715\\ 3,715\\ 3,715\\ 3,715\\ 3,903\\ 3,993\\ 4,190\\ 3,720\\ 2,590\\ 3,720\\ 2,304\\ 4,190\\ 3,720\\ 4,190\\ 4,$	$\begin{array}{c} 2,307\\ 2,357\\ 2,2357\\ 2,2932\\ 1,660\\ 2,260\\ 1,604\\ 1,630\\ 3,819\\ 17,580\\ 11,521\\ 13,301\\ 10,314\\ 5,859\\ 4,8776\\ 8,564\\ 5,709\\ 5,215\\ 8,107\\ 6,553\\ 5,799\\ 5,215\\ 8,107\\ 6,360\\ 0,886\\ 7,886\\ 7,886\\ 7,030\\ 7,886\\ 7,030\\ 7,320\\ 1,232\\ 1,$	$\begin{matrix} 1 \\ 5 \\ 6, 540 \\ 4, 304 \\ 6, 146 \\ 5, 968 \\ 4, 641 \\ 4, 558 \\ 4, 641 \\ 4, 586 \\ 4, 641 \\ 4, 586 \\ 3, 595 \\ 3, 851 \\ 4, 078 \\ 4, 101 \\ 3, 588 \\ 3, 998 \\ 4, 106 \\ 3, 595 \\ 3, 881 \\ 3, 799 \\ 4, 106 \\ 4, 311 \\ 8, 88 \\ 3, 196 \\ 4, 408 \\ 3, 196 \\ 4, 408 \\ 3, 196 \\ 4, 408 \\ 3, 196 \\ 4, 408 \\ 3, 196 \\ 4, 408 \\ 3, 196 \\ 4, 408 \\ 3, 196 \\ 4, 408 \\ 3, 196 \\ 4, 408 \\ 3, 196 \\ 4, 408 \\ 3, 196 \\ 4, 408 \\ 3, 196 \\ 4, 408 \\ 3, 196 \\ 4, 408 \\ 3, 196 \\ 4, 108 \\ 4, 108 \\ 3, 196 \\ 4, 108 \\ 3, 196 \\ 4, 108 \\ 3, 196 \\ 4, 108 \\ 3, 196 \\ 4, 108 \\ 3, 196 \\ 4, 108 \\ 1, 196 \\ 1$
28 29 30 31	$ \begin{array}{r} 3,007 \\ 6,851 \\ 4,311 \\ 5,399 \end{array} $	18,375	8,604 8,391 8,410 8,498	23,905 21,793 14,688	$15,469 \\ 19,171 \\ 16,301 \\ 14,113$	7,679 7,189 9,043	4,872 2,344 4,231 3,725	$3,501 \\ 3,629 \\ 3,147 \\ 3,454$	2,568 3,169 2,197	1,520 2,902 2,623 2,338	5,214 6,660	4,299 4,035 2,468 4,050
Mean .	2,384	9,050	9,153	28,473	28,272	10,033	5,791	4,173	2,807	3,065	6,376	4,096

MAINE.

COBBOSSEECONTEE RIVER AT RESERVOIR DAM NEAR AUGUSTA, MAINE.

This river is described in the Nineteenth Annual Report, Part IV, pages 79 and 80. The record of the discharge measurements from 1890 to 1899, inclusive, will be found in Water-Supply Paper No. 35, pages 28 to 33. The following measurements of daily discharge for 1900 were furnished by Mr. Alexander H. Twombly, engineer of the Forest Paper Company, of Yarmouthville, Maine. The measurements are made at the reservoir dam, where the discharge of the river is controlled by gates, except during flood stages. The gates are closed on Sundays and no water is allowed to pass. The great Cobbosseecontee dam furnishes a supplementary supply to the reservoir below, and water is occasionally drawn from it.

Daily discharge, in second-feet, of Cobbosseecontee River at upper dam near Augusta, Maine, for 1900.

	Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1		130	220	815	776	300	300	(a)	260	260	230	180	220
2		130	220	1,463	495	300	300	280	260	(a)	220	165	(<i>a</i>)
3		130	220	2,316	417	300	(<i>a</i>)	280	260	260	190	140	220
4		125	(a)	2,055	656	413	300	(a)	260	260	175	(a)	220
5		125	220	1,911	977	803	280	280	(a)	240	175	130	220
6		125	220	1,622	907	934	280	280	260	240	150	130	220
- X		\cdot (a)	220	1,481	1,087	831	280	280	260	240	(a)	130	220
8		130	220	1,290	1,379	606	280	(a)	260	240	160	130	220
10		100	220	1,100	1,000	400	280	280	200	(a)	1/0	200	(α)
11		100	(0)	1,100	1,04%	249	(0)	200	200	240	100	4.20	440
19		- 00	220	1 116	1,207	200	280	280	(a)	210	220	220	240
12		90	220	1,037	1 297	(a)	280	280	260	235	220	220	240
14		(a)	2.194	999	1,297	300	280	280	260	230	(a)	220	230
15		100	1.573	999	1.297	300	280	(a)	260	230	220	220	230
$\overline{16}$		95	1.283	999	1.213	300	280	280	260	(a)	220	220	(a)
17		90	856	1.615	1,105	300	(a)	280	260	250	220	220	240
18		90	562	1,611	1,072	300	280	280	260	250	220	(a)	240
19		90	425	1,473	1.260	300	280	280	(a)	250	220	220	240
20		90	294	1,518	1,380	585	280	280	260	250	220	220	240
21	•	(a)	270	1,811	1,338	704	280	280	275	245	(a)	220	240
22		140	270	1,662	1,260	998	280	<i>(a)</i>	275	250	220	220	240
23	· · · · · · · · · · · · · · · · · · ·	160	270	1,517	1,223	1,325	280	280	275	(a)	220	220	(a)
24 0*		200	270	1,472	1,223	1,422	(<i>a</i>)	280	275	250	220	220	240
20 00		200	(<i>a</i>)	1,334	1,182	1,301	280	270	275	250	220	(α)	(<i>a</i>)
20 97		200	004 669	1,289	869	1,016	280	260	(<i>a</i>)	250	220	220	240
64 98		(a)	776	1,200	010 977	400	280	200	210	200	220	220	240
40 20		(0)	110	1,200 1 105			280	200	210	240	(a)	220	240
20 20		220		1,105	300	300	280	(a)	20	200	220	220	240
31		220		925	000	300	400	260	260	(a)	200	14140	210
-1				0640		500		200	200		200		240
	Mean .	136	508	1,365	1,044	562	282	276	264	245	206	199	232

Dittintes our out and square miles	[]	Drainage area	, 230 square	miles.	1
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a Water shut back on Sunday when under control.

ANDROSCOGGIN RIVER AT RUMFORD FALLS, MAINE.

This river receives the drainage from the Rangeley and other lakes near the border line between Maine and New Hampshire. It flows in a southerly and southeasterly direction, descending with rapid fall, and is one of the most valuable streams in New England for waterpower purposes. It is described in the Nineteenth Annual Report, Part IV, pages 84 to 97. Figures of daily discharge will be found in Water-Supply Papers No. 27, pages 14 to 16, and No. 35, page 28; also 32

in the Twentieth Annual Report, Part IV, pages 67 to 69. Figures of monthly discharge for the year 1899 will be found in the Twenty-first Annual Report, Part IV, page 57.

The following table of the daily discharge of Androscoggin River for the year 1900 has been furnished by Mr. Charles A. Mixer, resident engineer of the Rumford Falls Power Company, who states that notable features of the discharge of the river for that year (1900) are the high maximum discharge and the high average for February. There is no previous record or recollection of thaws or rains in that section during that month, but in February, 1900, there were two such periods of thawing and rainfall. The precipitation for the month was 7.96 inches, the greatest on record, most of it in the form of rain. In 1898 the precipitation amounted to 7.25 inches, but all in the form of snow, so that the effect on the river was not apparent until spring.

Daily discharge, in second-feet, of Androscoggin River at Rumford Falls, Maine, for 1900.

			-									
Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
$\begin{array}{c} 1 \\ 2 \\ 2 \\ 2 \\ 3 \\ 3 \\ 4 \\ 5 \\ 5 \\ 5 \\ 7 \\ 7 \\ 7 \\ 8 \\ 9 \\ 9 \\ 9 \\ 9 \\ 10 \\ 11 \\ 12 \\ 13 \\ 14 \\ 15 \\ 15 \\ 16 \\ 14 \\ 15 \\ 15 \\ 16 \\ 12 \\ 12 \\ 12 \\ 12 \\ 12 \\ 12 \\ 12$	$\begin{array}{c} 1,231\\ 1,171\\ 1,190\\ 1,258\\ 1,228\\ 1,289\\ 1,189\\ 1,189\\ 1,189\\ 1,115\\ 1,130\\ 1,211\\ 1,135\\ 1,147\\ 1,178\\ 1,147\\ 1,178\\ 1,147\\ 1,211\\ 1,196\\ 1,221\\ 2,169\\ 1,628\\ 1,382\\ 1,628\\ 1,382\\ 1,215\\ 1,2850\\ 1,356\\ 1,285\\ 1,382\\ 1,356\\ 1,285\\ 1,382\\ 1,215\\ 1,285\\ 1,382\\ 1,215\\ 1,285\\ 1,382\\ 1,215\\ 1,285\\ 1,382\\ 1,215\\ 1,285\\ 1,382\\ 1,356\\ 1,285\\ 1,385\\ 1$	$\begin{array}{c} 1,351\\ 1,346\\ 1,369\\ 1,369\\ 1,354\\ 1,354\\ 1,354\\ 1,420\\ 1,654\\ 1,420\\ 1,654\\ 1,477\\ 1,677\\ 1,677\\ 1,777\\ 6,009\\ 2,972\\ 2,408\\ 2,146\\ 2,146\\ 2,002\\ 2,326\\ 5,150\\ 2,146\\ 2,002\\ 2,326\\ 5,162\\ 3,814\\ \end{array}$	$\begin{array}{c} 3,063\\ 2,849\\ 2,791\\ 2,190\\ 2,196\\ 2,016\\ 1,820\\ 1,794\\ 1,810\\ 1,704\\ 1,801\\ 1,708\\ 1,702\\ 1,620\\ 1,772\\ 1,620\\ 1,772\\ 2,549\\ 2,729\\ 2,425\\ 2,179\\ 2,491\\ 2,549\\ 2,729\\ 2,647\\ 2,2,255\\ 1,894\\ 1,919\\ 1,776\\ 1,788\\ $	$\begin{array}{c} 1,830\\ 1,933\\ 2,026\\ 2,561\\ 2,791\\ 3,592\\ 4,730\\ 4,603\\ 3,836\\ 3,318\\ 3,938\\ 4,093\\ 4,943\\ 4,943\\ 4,943\\ 4,943\\ 4,943\\ 4,943\\ 6,230\\ 16,130\\ 22,025\\ 21,980\\ 22,025\\ 21,980\\ 22,025\\ 21,980\\ 22,025\\ 21,980\\ 22,025\\ 21,980\\ 22,025\\ 21,930\\ 22,025\\ 22$	$\begin{array}{c} 16, 182\\ 13, 249\\ 12, 008\\ 17, 002\\ 13, 700\\ 10, 555\\ 9, 121\\ 8, 283\\ 9, 468\\ 8, 0038\\$	$\begin{array}{c} 5,582\\ 5,952\\ 6,850\\ 7,458\\ 7,458\\ 7,016\\ 6,341\\ 4,948\\ 4,850\\ 4,948\\ 4,850\\ 4,263\\ 8,311\\ 2,956\\ 3,384\\ 4,33\\ 3,115\\ 2,956\\ 3,384\\ 1,893\\ 1,855\\ 1,810\\ 1,931\\ 2,070\\ \end{array}$	$\begin{array}{c} 1,780\\ 1,781\\ 1,705\\ 1,640\\ 1,760\\ 1,760\\ 1,760\\ 1,803\\ 1,798\\ 1,719\\ 1,798\\ 1,719\\ 1,781\\ 1,949\\ 2,000\\ 1,880\\ 2,992\\ 2,561\\ 2,992\\ 2,561\\ 2,992\\ 2,561\\ 2,992\\ 2,583\\ 4,042\\ 2,855\\ 2,834\\ 2,855\\ 2,834\\ 2,855\\ 2,834\\ 2,855\\ 2,834\\ 2,855\\ 2,834\\ 2,855\\ 2,834\\ 2,855\\ 2,834\\ 2,855\\ 2,834\\ 2,855\\ 2,834\\ 2,855\\ 2,834\\ 2,855\\ 2,834\\ 2,855\\ 2,834\\ 2,855\\ 2,834\\ 2,855\\ 2,834\\ 2,855\\ 2,834\\ 2,855\\ 2,834\\ 2,855\\ 2,834\\ 2,855\\ 2,855\\ 2,834\\ 2,855\\ 2,855\\ 2,834\\ 2,855\\ 2,$	$\begin{matrix} 1, 611\\ 1, 5604\\ 1, 504\\ 1, 505\\ 1, 685\\ 1, 685\\ 1, 620\\ 1, 505\\ 1, 685\\ 1, 620\\ 1, 502\\ 1, 641\\ 1, 592\\ 1, 641\\ 1, 592\\ 1, 641\\ 1, 592\\ 1, 641\\ 1, 592\\ 1, 641\\ 1, 592\\ 1, 611\\ 1, 612\\ 1, 437\\ 1, 437\\ 1, 389\\ 1, 389\\ 1, 389\\ 1, 389\\ 1, 389\\ 1, 403\\ 1, 503\\ 1$	$\begin{matrix} 1,650\\ 1,650\\ 1,650\\ 1,682\\ 1,299\\ 1,299\\ 1,264\\ 1,275\\ 1,247\\ 1,372\\ 1,330\\ 1,352\\ 1,332\\ 1,352$	$\begin{array}{c} 1,985\\ 1,856\\ 2,0656\\ 2,0050\\ 2,0050\\ 2,0050\\ 2,0050\\ 2,0050\\ 2,0050\\ 2,0050\\ 2,0050\\ 2,0050\\ 2,705\\ 3,197\\ 2,7712\\ 3,615\\ 3,472\\ 2,7732\\ 3,615\\ 3,007\\ 3,472\\ 2,042\\ 1,930\\ 1,754\\ 1,676\\ 1,676\\ 1,630\\ 1,43$	$\begin{array}{c} 1,530\\ 1,460\\ 1,504\\ 1,504\\ 1,694\\ 10,131\\ 17,525\\ 5,230\\ 4,436\\ 3,636\\ 3,610\\ 3,330\\ 3,330\\ 3,330\\ 3,330\\ 3,330\\ 3,330\\ 4,436\\ 3,610\\ 3,500\\ 2,934\\ 4,681\\ 3,374\\ 3,374\\ 3,374\\ 3,374\\ 3,374\\ 2,834\\ $	$\begin{array}{c} 3,264\\ 3,250\\ 3,059\\ 3,069\\ 3,192\\ 2,083\\ 2,372\\ 2,373\\ 2,372\\ 2,373\\ 2,372\\ 2,$
Mean .	1,408	2,555	2,109	9, 763	12,633	4,127	2,201	1,574	1,596	2,213	3,945	2,331

C 200 1		0.000		
Drainage	area,	2,320 :	square	miles.

MERRIMAC RIVER AT LAWRENCE, MASSACHUSETTS.

Careful records of the flow of this river at Lawrence, Massachusetts, have been kept for more than fifty years, but they have never been published in full. Figures for the monthly maximum and minimum discharge from 1890 to 1897 were published in the Nineteenth Annual Report, Part IV, pages 113 to 115, and similar figures for 1898 in the Twentieth Annual Report, Part IV, page 73. In Water-Supply Paper No. 35 will be found the figures for the daily discharge for 1897, 1898, and 1899. The figures for 1900 are published herewith. Daily discharge, in second-feet, of Merrimac River at Lawrence, Massachusetts, for 1900.

			_	-								
Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1	3,230	4,631	17,350	11,129	10,674	5,332	479	2,134	1,389	2,763	2,456	8,975
2	2,696	$\frac{4,408}{2,871}$	33,802 37,732	12,507 13,412	11,597 11,485	4,356 4,397	2,653 2,370	2,192 2.338	417 284	2,490 2,289	1,468 1,608	7,374 7,641
4	1,860	2,468	33,090	15,389	12,887	6,520	311	1,505	2,340	2,137	277	6,844
5	-1,902	5,520	26,893	16,797	15,881	7,492	2,226	113	2,206	2,109	2,643	11,383
6	1,209	5,687	20,329	17,602	13,223	7,616	2,369	2,038	2,099	1,482	2,478	17,046
2	2 6.19	5,910	17,011	19,408	11,004	5 721	1,099	1,094 1.771	1,912 1 959	2 215	2,203	10,000 12,127
9	2,561	7,112	13,356	21.511	9.817	4.178	2.471	1.860	90	2.515	2.526	9,237
10	2,220	9,550	13,067	18,308	9,661	3,873	2,372	1,939	1,901	2,580	12,221	7,839
11	2,182	9,060	12,211	15, 157	10,324	5,275	2,315	1,347	1,637	2,752	12,035	6,101
2	2,327	9,930	11,403	13,660	8,880	3,899	2,339	9 509	1,540	3,300	9,477	6,020
13	1,400	12,720	10,875	14,497	7 972	3,702	1 620	2, 30.2	1,040	2 014	5 804	5 537
5	2.654	52.989	8,984	13.646	7.001	3.811	186	2,218	732	4, 103	5,063	4.338
16	2,574	41,745	10,684	14,643	8,313	2,705	2,022	2,354	37	3,316	4,473	4,023
17	2,269	28, 923	13,364	15,945	10,062	2,800	2,206	2,483	1,673	2,904	3,158	5,321
18	2,335	19,311	14,243	17,886	8,772	4,368	2,228	1,986	2,155	3,201	2,466	4,268
19	2,394	13,731	16,437	22, 312	11 510	3, 320	2,299	1,372 3,571	2,242	3,117	4,410	3,092
21	2.041	11,549	20.324	34, 926	18, 169	2,931	1,483	2,469	1,977	890	3.348	4.245
2	6,810	12, 317	19,517	30, 809	15,538	3,062	146	2,229	1,245	3,248	6,071	3,177
3	7,950	19,300	16,729	27,402	12,433	2,233	2,125	2,072	36	2,702	7,477	3,125
24	8,184	20,400	14,555	24,627	10,344	1,487	2,365	2,072	2,175	2,643	6,235	4,826
29	6 027	24,772	12,680	23, 144	9,195	3,915	2,133 2 150	1,433	2,385	2,438	$\frac{1}{7},808$	5,034 7 615
27	4.401	23, 911	11, 429	16.730	6.824	2,732	2.189	1.754	2.209	1.568	12,845	7.827
28	3,891	19, 187	11,065	14,422	7,271	2,377	1,641	2,030	2,159	961	15,338	6,859
29	6,291		11,264	11,727	6,455	2,448	242	1,958	1,498	2,887	12,689	5,119
30	5,323		11,290	11,326	5,109	1,825	2,487	1,889	309	2,484	10,844	4,139
51	4,776		11,484		0,272		2,317	1,996	•••••	2,523		5,473
Mean	3 360	16 181	16 245	18 500	10.034	3 957	1 818	1.876	1 513	9 517	5 849	6 783
mean .	0,000	10, 101	10,740	10,000	10,001	0, 301	1,010	1,010	1,010	~, 514	0,040	0,100

[Drainage area, 4,553 square miles.]

NASHUA RIVER AT CLINTON, MASSACHUSETTS.

On the south branch of this stream, near the town of Clinton, the Metropolitan Water Board is now constructing the Wachusett reservoir, for the supply of water to the city of Boston and neighboring cities and towns. Measurements of the flow of Nashua River at Clinton have been made by that board since July, 1896, but the figures have not been published. They have, however, been presented in testimony in court, and have thus been made public. Careful records of rainfall on this watershed have also been made.

SUDBURY RIVER AND LAKE COCHITUATE, MASSACHUSETTS.

Sudbury River and Lake Cochituate have been studied by the engineers of the city of Boston, the State Board of Health of Massachusetts, and the Metropolitan Water Board, and records of rainfall in the Sudbury watershed have been kept since 1875 and in the Cochituate basin since 1852, but the latter have been considered of doubtful accuracy previous to 1872. The records of run-off from 1875 to 1898, inclusive, were published in the Twentieth Annual Report, Part IV, page 75, and those for 1899 in Water-Supply Paper No. 35, page 37, where will also be found a short description of the watersheds of the river and the lake. The following table gives the record for 1900. All of the records were furnished by Mr. Desmond Fitz Gerald.

IRR 47—01——3

Month.	Sudbury River watershed.	Lake Co- chituate watershed.	Month.	Sudbury River watershed.	Lake Co- chituate watershed.
January February March April May June June July	$\begin{array}{r} 1.229 \\ 5.880 \\ 5.653 \\ 2.088 \\ 2.031 \\ .489 \\028 \end{array}$	$\begin{array}{c} 1.060\\ 4.136\\ 4.020\\ 1.454\\ 1.641\\ .455\\ .293\end{array}$	August September October November December Mean	$\begin{array}{r} -\ .\ 052 \\ .\ 101 \\ .\ 287 \\ 1.\ 026 \\ 1.\ 696 \\ \hline 1.\ 674 \end{array}$	$\begin{array}{r} .558 \\ .640 \\ .689 \\ 1.087 \\ 1.502 \\ \hline 1.445 \end{array}$

Run-off of Sudbury River and Lake Cochituate watersheds, in second-feet per square mile, for 1900.

MYSTIC LAKE, MASSACHUSETTS.

This lake has been a source of water supply for the city of Charlestown, Massachusetts, since 1864. A brief description of the watershed is given in Water-Supply Paper No. 35, page 39, and on page 40 the runoff, in inches, for the watershed from 1878 to 1897, inclusive. Records for 1898, 1899, and 1900 are not available, although observations have been continued. The lake is no longer used as a source of water supply.

CONNECTICUT RIVER AT ORFORD, NEW HAMPSHIRE.

This river has its source in Connecticut Lake, in the extreme northern portion of New Hampshire. A gaging and observation station was established August 6, 1900, by E. G. Paul, on the covered highway bridge over the river between Orford, New Hampshire, and Fairlee, Vermont, about 75 miles from the source of the stream. The gage for making observations of the variations in the height of water in the river consists of a scaleboard 20 feet long, graduated to feet and tenths, fastened horizontally to the inside timbers on the upper side of the bridge, 125 feet from the left-bank abutment, and a steel sash chain running over a side pulley with a 5-pound weight, the length of the chain from the extreme end of the weight to the copper-rivet marker being 42.95 feet.

The observer is Frank H. Gardner, of Orford, New Hampshire. One discharge measurement was made during 1900, as follows:

August 7: Gage height, 3.6 feet; discharge, 1,529 second-feet.

Daily gage height, in feet, of Connecticut River at Orford, New Hampshire, for 1900.

Day.	Aug.	Sept.	Oct.	Nov.	Dec.	Day.	Aug.	Sept.	Oct.	Nov.	Dec.
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 14 15 16 11 15 16 11 12 13 14 15 16 16 17 16 17 16 16 17 16 16 17 16 16 17 16 16 17 16 16 17 16 16 16 16 16 16 16 16 16 16	$\begin{array}{c} \hline & & \\ & &$	$\begin{array}{c} 3.\ 00\\ 3.\ 65\\ 3.\ 70\\ 2.\ 35\\ 2.\ 70\\ 2.\ 80\\ 3.\ 00\\ 2.\ 70\\ 2.\ 45\\ 2.\ 70\\ 2.\ 65\\ 2.\ 75\\ 2.\ 75\\ \end{array}$	$\begin{array}{c} 5.30\\ 6.50\\ 6.30\\ 5.20\\ 4.80\\ 4.20\\ 5.15\\ 6.20\\ 5.85\\ 6.15\\ 7.20\\ 12.43\\ 12.80\\ 10.65\\ 8.90\\ 8.15\\ \end{array}$	$\begin{array}{c} 4.60\\ 4.50\\ 4.40\\ 4.15\\ 3.85\\ 3.80\\ 4.30\\ 4.30\\ 11.25\\ 13.40\\ 10.35\\ 12.40\\ 10.35\\ 8.35\\ 8.35\\ 7.95\\ \end{array}$	$\begin{array}{c} 8.55\\ 8.40\\ 8.00\\ 7.70\\ 7.50\\ 7.50\\ 7.50\\ 7.50\\ 7.50\\ 7.50\\ 7.50\\ 7.50\\ 7.50\\ 7.60\\ 7.60\\ 7.20\\ 6.70\\ \end{array}$	17 18 19 20 21 22 23 24 25 26 27 27 28 29 29 20 21 23 24 25 26 27 27 28 29 20 30 31 21 21 23 24 25 26 27 27 27 27 27 27 27 27 27 27	$\begin{array}{c} 6,90\\ 6,45\\ 5,60\\ 5,20\\ 4,60\\ 4,15\\ 3,85\\ 3,60\\ 3,40\\ 3,45\\ 2,70\\ 3,15\\ 3,10\\ 3,05 \end{array}$	$\begin{array}{c} 3.05\\ 2.95\\ 2.85\\ 2.85\\ 2.75\\ 3.05\\ 4.35\\ 4.35\\ 5.00\\ 4.60\\ 4.15\\ 3.75\\ 3.50\\ 4.15\\ 4.85\\ \end{array}$	$\begin{array}{c} 7.95\\ 7.60\\ 7.15\\ 6.80\\ 6.50\\ 6.25\\ 5.65\\ 5.75\\ 5.65\\ 5.75\\ 5.75\\ 5.40\\ 5.00\\ 4.75\\ \end{array}$	$\begin{array}{c} 6,90\\ 6,25\\ 6,50\\ 7,95\\ 11,30\\ 13,90\\ 14,80\\ 14,30\\ 12,70\\ 11,05\\ 11,20\\ 11,40\\ 9,95\\ 8,90\\ \end{array}$	6.60 6.50 6.50 6.60 6.70 6.50 6.70 6.90 7.90 9.00 8.80 8.50 8.20

CONNECTICUT RIVER AT HOLYOKE, MASSACHUSETTS.

Measurements have been made of the flow of Connecticut River at Holyoke for many years. For records see Water-Supply Paper No. 35, pages 40 to 42. The figures are furnished by Mr. A. F. Siekman, assistant engineer of the Holyoke Water Power Company. The record for the year 1900 is not available.

CONNECTICUT RIVER NEAR HARTFORD, CONNECTICUT.

Observations of the height of Connecticut River near Hartford are made by the Connecticut River bridge and highway district, Edwin D. Graves, chief engineer, as noted in the Twentieth Annual Report, Part IV, page 77. Daily readings from February 8, 1896, to January 1, 1899, were published in Water-Supply Paper No. 35, pages 42 to 44. The record for 1900 is given in the following table:

Daily gage height, in feet, of Connecticut River near Hartford, Connecticut, for 1900.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
Day. 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 24 25 23 24 24 25 24 25 24 25	Jan. 4.0 4.0 2.5 3.0 4.0 4.0 5.1 3.1 3.2 3.0 3.0 3.0 5.5 7.9 9.9 6.9 6.9	$\begin{array}{c} \text{Feb.} \\ \hline \\ 5.7 \\ 5.6 \\ 5.6 \\ 5.6 \\ 5.6 \\ 9.8 \\ 8.7 \\ 7.3 \\ 8.6 \\ 10.7 \\ 9.45 \\ 11.8 \\ 22.0 \\ 10.3 \\ 8.4 \\ 22.0 \\ 14.0 \\ 10.3 \\ 8.4 \\ 7.6 \\ 11.7 \\ 11.3 \\ 10.5 \\ \end{array}$	Mar. 7.5 17.6 18.9 15.1 12.9 10.5 7.8 7.3 7.3 7.3 7.3 6.8 5.9 6.0 5.8 5.4 5.5 6.0 5.8 5.4 5.5 5.5 6.0 8.4 11.2 9 5.5 8.9	Apr. 7.0 8.0 8.7 8.8 9.8 10.5 14.2 13.5 12.0 10.6 10.5 11.2 10.7 12.5 14.5 17.2 22.2 22.2 22.2 22.2 22.1 3.2 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7	May. 12.1 10.7 10.9 11.2 10.2 9.5 9.0 8.4 8.4 7.9 7.3 6.7 7.2 8.4 13.3 14.7 13.9 13.0 11.0 11.2 10.2 11.2 10.	June. 5.70 5.00 4.80 7.05 5.55 4.77 4.33 4.43 4.43 4.00 3.9 3.44 3.54 2.00	July. 2.4 2.8 2.0 2.26 2.4 2.3 2.4 2.3 2.4 2.9 3.0 3.0 3.2 3.5 3.4 2.9 3.4 2.9 3.4 2.6 3.0 2.26 2.8 3.4 2.6 2.8 3.4 2.9 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0	Aug. 3.192.975 1.992.25 1.992.25 2.002.00 1.99 3.44 3.375 3.308 3.08 3.08 3.08 3.08 3.08 3.08 3.0	Sept. 2.5 2.5 2.5 2.5 2.5 2.5 2.5 2.5 2.5 2.	Oct. 2200022206699003344600666009 222222222222222222222222222222	Nov. 3330993366 330993366 4556699 44396 45560 44396 4560 7709	Dec. 7.1 7.0 6.6 6.3 8.0 9.9 9.9 8.4 6.9 8.4 4.9
26	5.7 5.4 6.0 7.2 6.7 6.4	11.1 9.7 7.8	$\begin{array}{c} 7.4 \\ 7.3 \\ 6.9 \\ 6.6 \\ 6.6 \\ 6.8 \end{array}$	$ \begin{array}{c} 20.5 \\ 20.4 \\ 17.9 \\ 13.9 \\ 13.6 \\ \end{array} $	$ \begin{array}{r} 9.5 \\ \overline{} \\ 7.4 \\ 6.9 \\ 6.5 \\ 5.9 \\ \end{array} $	3.3 3.4 3.2 3.0 3.2	3.4 3.4 3.4 3.4	2.5 3.0 2.9 2.8 2.5	$ \begin{array}{r} 1.6 \\ 1.3 \\ 1.6 \\ 2.0 \\ 1.6 \\ \hline 1.6 \\ 2.0 \\ 1.6 \\ \end{array} $	3.0 3.6 3.6 3.6 3.6 3.6 3.6	8.5 10.9 10.1 10.2 8.9	5.5 6.0 6.0 5.3 5.7

HOUSATONIC RIVER AT GAYLORDSVILLE, CONNECTICUT.

This gaging station was established October 24, 1900, by E. G. Paul. It is near Merwinsville Station, on the New York and New Haven Railroad. Gage-height observations are made by means of a weight suspended by a sash chain from the covered bridge across the river. The distance from the extreme end of the weight to the copper-rivet marker in the chain is 30.45 feet. The distance from the center of the side pulley to the datum of the gage is 29.35 feet. The gage is referred to a 16-foot scaleboard, graduated to feet and tenths, fastened horizontally to the woodwork on the inside of the covered bridge. The observer is G. H. Monroe, a farmer living within a short distance of the station. As the cross section of the river channel at the bridge was not favorable for making discharge measurements, a cable was stretched across the stream $1\frac{1}{4}$ miles below the bridge. The span of the cable is 200 feet. It is supported on the right bank by timbers 25 feet high, and is anchored to a large rock which was placed 5 feet below the surface of the ground. On the left bank the cable is fastened to a large sycamore tree, and is anchored to the base of a large oak tree by means of a turn-buckle. A tag wire with markers every 10 feet was placed above the cable. The initial point of sounding is the large sycamore tree which supports the cable on the left bank.

During 1900 the following discharge measurements were made by Mr. Paul:

August 9: Gage height, 3.30 feet; discharge, 450 second-feet. August 10: Gage height, 3.25 feet; discharge, 422 second-feet. October 20: Gage height, 3 feet; discharge, 303 second-feet. October 24: Gage height, 3.10 feet; discharge, 370 second-feet.

Daily gage height, in feet, of Housatonic River at Gaylordsville, Connecticut, for 1900.

Day.	Oct.	Nov.	Dec.	Day.	Oct.	Nov.	Dec.	Day.	Oct.	Nov.	Dec.
1 2 3 4 5 6 7 8 9 10 11		$\begin{array}{c} 3.2\\ 3.1\\ 3.1\\ 2.9\\ 3.0\\ 2.9\\ 2.8\\ 3.2\\ 3.5\\ 4.1\\ 3.9\end{array}$	$\begin{array}{r} 4.9\\ 4.6\\ 4.3\\ 4.2\\ 5.6\\ 5.8\\ 5.4\\ 5.1\\ 4.9\\ 4.5\\ 4.2\end{array}$	12. 13. 14. 15. 16. 17. 18. 19. 20. 21. 22. 13. 19. 19. 21. 22. 13. 13. 13. 14. 15. 14. 15. 16. 17. 18. 19. 18. 19. 18. 19. 19. 19. 19. 19. 19. 19. 19		$\begin{array}{r} 3.7\\ 3.6\\ 3.7\\ 3.7\\ 3.7\\ 3.6\\ 3.5\\ 3.6\\ 3.5\\ 3.6\\ 3.7\\ 4.1\\ 4.0\end{array}$	4.2 4.2 4.2 Ice. Ice. Ice. Ice. Ice. Ice. Ice. Ice.	23 24 25 26 27 27 28 28 29 30 31	2.9 3.1 3.2 3.1 3.1 3.1 3.1 3.0	$\begin{array}{c} 3.9\\ 3.9\\ 3.8\\ 4.6\\ 5.5\\ 5.4\\ 5.1\\ 4.9\end{array}$	$\begin{array}{c} 4.8\\ 5.1\\ 4.3\\ 4.2\\ 4.1\\ 4.2\\ 4.0\\ 3.9\\ 4.2\\ 4.2\end{array}$

MISCELLANEOUS MEASUREMENTS OF STREAMS NEAR GREATER NEW YORK.

Measurements of the discharge of three small streams near the city of New York were made by E. G. Paul in 1900. These streams— Tenmile Riyer, Wallkill River, and Esopus Creek—have been under consideration as possible sources for increasing the water supply of Greater New York. Following are the discharge measurements made by Mr. Paul:

Miscellaneous measurements of streams near Greater New York.

Date.	Stream.	Locality.	Dis- charge.
1900. Aug. 9 Oct. 20 Aug. 13 Aug. 14	Tenmile River do Wallkill River Esopus Creek	Webatuck, N. Y do Rockford Bridge, N. Y Brodheads Bridge, N. Y	Secft. 46 32 70 92

METHODS EMPLOYED IN THE GAGING OF NEW YORK STREAMS DURING THE YEAR 1900.¹

The location of gaging stations which have been maintained or established in New York State during the year 1900 are given in the first of the tables which follow. Most of the older stations were established either in connection with the Upper Hudson storage survey of 1895 and 1896 or by the United States Board of Engineers on Deep Waterways in 1898. All of the older stations are in connection with dams and mills. The methods employed in computing the flow of streams from such records are described in Water-Supply Paper No. 35, page 39, and records of flow for past years will be found in the same paper. In connection with all such stations an effort has been made to improve upon the methods formerly used, and to check the previous results by making current-meter measurements to determine the volume of flow through turbines, and the proper allowance to be made for leakage of dams, also to check the calculated flow over dams.

Measurements of streams in New York State have been made with the cooperation of the State engineer and surveyor, Edward A. Bond, and the deputy State engineer and surveyor, William Pierson Judson. The stations established during the year are chiefly currentmeter stations, a gage being read once or twice daily to determine the stage of the river, and the current-meter measurements made as opportunity permits, with the water at different stages. A sufficient number of current-meter measurements have not yet been made at any of the stations to permit the construction of rating curves, so that the daily flows in second-feet can not yet be given.

In addition examinations have been made of various streams, notably of those flowing from the northern slope of the Adirondack region, to determine favorable localities for establishing gaging stations, and a number of gaging records have been obtained which are not yet ready for publication.

No single method of gaging has been followed exclusively, but different methods have been pursued, with a view to checking the results obtained. In a number of instances weir and current-meter measurements have been combined at a single station, the former method being employed to calculate the flow over dams, the latter method to estimate diversion to canals or for water-power purposes.

Many of the older stations had been neglected, and at the beginning of the year the gages were out of repair. Many of the gages have been replaced by new ones having metallic figures and division marks, and other changes have been made with a view to increasing the accuracy of the results.

¹Report of Robert E. Horton, under whose direction the measurements in New York State have been made.

Location of gaging stations on New York streams.

Stream.	Location.	Kind of station.	Duration of record.	Gage reader.
Mohawk River	Ridge Mills	Dam and water-	Oct. 1, 1898, to Nov. 28 1900	Daniel Brown.
Oriskany Creek	Oriskany	Dam and feeder	Oct. 16, 1898, to Jan. 31 1901	Frank Baker.
Sauquoit Creek	New York Mills (No.3).	Dam and mill	Sept. 20, 1898, to Sept. 30, 1900.	Robert Hughes.
West Canada Creek.	Twin Rock Bridge.	Bridge	Sept. 9, 1900-Cont'd .	Utica Elec. Lt. and Power Co.
Do Mohawk River	Middleville Little Falls	Dam and mill Dam and mills	Oct. 7, 1898—Cont'd a. Sept. 23, 1898—Cont'd	E.J. Nelson. J. J. Gilbert and Wm Hoffman
East Canada	Dolgeville	Dam and power	Sept. 23, 1898—Cont'd	Henry Meyer.
Cayadutta Creek.	Below Johns-	do	Oct. 1, 1898-Cont'd	A. N. Terry.
Schoharie Creek	Fort Hunter	Dam and feeder.	Sept. 23, 1898, to July 31, 1900 b	H.J.Wittemeier.
Do	Erie Canal aque-	Bridge	May 2, 1900, to Oct. 13, 1900	James Shutts.
Do Do	Mill Point Schoharie Falls	Dam and plant	July 6, 1900-Cont'd June, 1900-Cont'd	Henry Peters. Empire State
Mohawk River	Near Schenec-	Bridge	Feb.1,1899—Cont'd c.	L. Diggins.
Do Do	Rexford Flats Dunsbach Ferry.	Dam and feeder. Dam	Dec. 8, 1898—Cont'd Mar.12,1898—Cont'dd	H. R. Betts. Kept for D. J. Howell C E
Indian River Schroon River	Indian Lake dam Below Warrens-	Storage dam Dam and mill	July 22, 1900-Cont'd. Nov. 1, 1895-Cont'd.	Frank Pelon Joseph Goodfel-
Hudson River	Fort Edward	Dam and mills.	Dec. 1, 1895-Cont'd	B. A. Carr.
Seneca River Chittenango	Baldwinsville Bridgeport	do	Nov.12, 1898—Cont'd. Sept. 16, 1898—Cont'd	Chas. Brannock. Jefferson Downs.
Oneida Creek	Kenwood	Dam and mill	Oct. 4, 1898, to Dec.	Wm. Padgham,
Fish Creek, West	McConnellsville .	Dam and mills.	Sept.13,1898-Con'd f	Frank S. Harden.
Oswego River	High dam	do	Apr. 1, 1897-Cont'd	Oswego Water.
Do Salmon River Moose River Black River	Above Minetto Above Pulaski Moose River Huntingtonville dam.	Cable Bridge Cable Waterworks dam.	Sept. 14, 1900-Cont'd Sept. 4, 1900-Cont'd June 5, 1900-Cont'd Feb. 22, 1897-Cont'd	H. L. Woodcoek. H. A. Walker, Frank W. Smith. Alonzo Dressor.

a No record February 1 to May 9, 1900, inclusive. b No record December, 1899, and February, 1900. c No record October 3, 1899, to April 7, 1900, inclusive. d No record April 1, 1899, to Angust 31, 1900, inclusive. e No record August and September, 1899, and February and May, 1900. f No record August, 1899, to April, 1900.

In the foregoing table there have been included a number of rivers which belong to the Great Lakes drainage, descriptions of which will be found in Water-Supply Paper No. 49, the same being Part III of this series, a geographic arrangement of the streams having been followed, as in former years. The streams referred to are Seneca River at Baldwinsville, Chittenango Creek at Bridgeport, Oneida Creek at Kenwood, West Branch of Fish Creek at McConnellsville, Oswego River at Minetto and at high dam, Salmon River above Pulaski, Moose River below Mc-Keever, Beaver River, and Black River at Huntingtonville.

The following table gives the results of current-meter measurements made on the principal of these streams during the year 1900. A modified form of the Price meter which has been adopted by the United States Geological Survey was used. The usual mode of procedure was to submerge the meter six-tenths of the depth of the stream, at measured intervals across the channel, and record the revolutions for a period of 100 seconds. In cases of doubt, surface and bottom

velocities were also taken, or, as a check, the flow was determined by the integrating method. Many of these measurements were made at places where permanent stations have not been maintained, and the gage-height figures given are the distances to water surface measured from some fixed point of reference, usually the coping of either a pier or an abutment. In addition to the results included in the table, 35 current-meter measurements have been made in headraces, feeders, power canals, and other channels, to determine the leakage of dams, the flow through turbines, and the amount of diversions. The results of these measurements will be found in connection with the descriptions of the various gaging stations.

Date.	Stream.	Location.	Point of measure- ment.	Hydrogra- pher.	Gage height	Dis- charge.
1. 00	M. Levels Discou	Dimenside Duiden		DETTenten	Feet.	Secft.
May 29	Monawk River.	Riverside Bridge	Rome.	R. E. Horton -	14.90	202
Aug. 31	do	Kome	feeder dam.			38
Do	do	do	feeder dam.	do		188
Apr. 22	do	Ridge Mills	At highway bridge above dam.	H.A. Pressey	1.96	1,385
Aug. 23	do	do	In channel below dam.	R.E.Horton	• • • • • • •	116
Apr. 30 Sept. 7	Oriskany Creek West Canada Creek.	Oriskany Twin Rock Bridge.	Wood road bridge	do do	12.20 .37	289 182
Sept. 10 May 1	do Mohawk River	Middleville	Suspension bridge.	do	18.70	
May 23 May 22	East Canada	do Dolgeville	Astronga Bridge	do	1.33 20.12	1,569 412
July 27	Creek.	do	do	do	20.16	452
July 29	do	do	Below High Falls	do		108
Apr. 24	Schoharie Creek	Fort Hunter	West Shore rail-	H.A.Pressey		5,573
May 2 June 21	do	do	Erie Canalaqueduct	E.D. Walker.	2.26	1,257
July 18	do	do	Below aqueduct; in-	E.D. Walker.		38
Do	do	do	Total outflow at	do		114
Aug. 22	do	do	Below aqueduct; in-	do		44
July 5	do	Mill Point		do	. 64	87
May 12	Mohawk River .	Schenectady	Freeman's bridge	do	6.50	4,135
Aug. 21	do	do	do	do	5.40	976
Oct. 19	Indian River	Sabael	Below Indian Lake	R.E.Horton.	8.20	451
July 25	Schroon River	Warrensburg	Two miles above Warrensburg.	do	16.40	383
Aug. 9	do	do	One mile above	do	••••••	286
July 26	Hudson River	Fort Edward	Highway bridge be-	do		2,704
Oct. 20	do	Mechanicsville	Highway bridge be- low Duncan & Co.'s dam.	do	21.50	1,871
June 11	Seneca River	Baldwinsville	Highway hridge he.	do	•••••	1,863
o une ro	Creek.	bridgeport	low Butternut			55
Sept. 17	Oneida Creek	Kenwood	Headrace above	do	3.25	20
June 1 May 17	Fish Creek.	Oneida Castle Point Rock		do	8.50	36 485
Sept.15	East Branch. Oswego River	Cable station	Three miles above	do	5.40	1,677
Sept. 4	Salmon River	Bridge station	Minetto. Two miles above	do	1.03	103
June 6	Black River	Glen Park Bridge	Pulaski. 'Two miles below	do		2,175
			watertown.			6

Summary of current-meter measurements of New York streams during 1900.

Field work was begun so late that in many instances current-meter measurements to check the calculated flow over dams during high water could not be made. Additional meter measurements are also needed at all of the current-meter stations to establish discharge curves. This report must therefore be considered as in some degree preliminary.

For mill streams, where the water is held back as pond storage during the dry season, and where the mills are stopped on Sundays or holidays, it is impossible to determine the natural regimen of flow. If at the time the water wheels are stopped the water stands below the level of the crest of the dam, the flow in the stream channel below will be nil, or at best will only equal the leakage of the dam, flumes, or penstocks. With regard to estimation of Sunday flow, no uniform rule has been followed. In some of the older records the Sunday fow during the dry season has been taken as the mean of the calculated flow for the preceding and following days, and in cases where this method had previously been used it has been adhered to in computing the daily discharge of the streams. In other instances the daily flow given in the table is that shown by the gaging record, and represents as nearly as may be the actual amount of water flowing in the stream channel below the dam, but it may be quite different from the amount entering the pond above the dam.

The relation existing between the canals of New York and the streams of the central portion of the State is very complicated. In many cases diversion from the headwaters of the streams for the supply of canals virtually reduces their effective drainage areas. As a result, the watersheds during the summer may be materially less in area, and in their water-yielding characteristics may differ widely from the region tributary to the streams when the canals are not in operation. It is evident that the run-off from such streams is not comparable with that from streams having an undisturbed regimen.

It often happens that a single gage reading taken at or near the culmination of a flood shows a larger flow than the mean for any single day. The results of such isolated observations, together with other data relative to extremes of flow, have been given for a number of stations.

The drainage areas of the various streams above the gaging stations and at other points are given in the following table:

Stream.	Location.	Area.
Batten Kill <i>a</i>	At mouth	Sq. miles. b 438
Do Do	Above Beaver Below Beaver	153 169
a Hudson River tributar	v. b Upper Hudson storage surveys.	

Drainage areas of New York streams.

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Drainage areas of New York streams-Continued.

Stream.	Location.	Area.
		Sq. miles.
Black Creek a	At mouth	1 020
Do	At caring station	1,950
Do	At Forestport	1,005 b268
Cavadutta Creek c	At mouth	b 62
Do	At gaging station	b 40
Chittenango Creek	At mouth	b309
Do	At Bridgeport d	b 307
East Canada Creek c	At mouth	2 8 3
Do	. At gaging station	256
Fish Creek, East Branch	At Point Rock	<i>b</i> 104
Fish Creek, West Branch	At McConnellsville d	b 187
Fulton Chain	Above Old Forge	41
Hoosic River e	At mouth	f 730
Hudson River	At Troy	18,000
Do	Above Monawk	4,021
Do	At Fort Edward	$f_{2}^{4}, 500$
Do	At Hadley a	$f_{1,000}$
Indian Lake	At gaging station	146
Lake Neatah wanta a	At mouth of outlet	23
Mohawk River	At mouth	b3,468
Do	At Rexford Flats d	b3,385
Do	At Schenectady d	3,212
Do	At Little Falls d	b1,306
Do	At Ridge Mills d.	b153
Moose River	At mouth	406
Do	At cable station	346
Ninemile Creek c	At mouth	674
Do	At gaging station	0 63
Do	At Konwood d	0149
Oneida River	At mouth	b1 409
Oriskany Creek c	do	b 146
Do	At State dam d	b144
Oswego River	At mouth	5,002
Do	At high dam	5,000
Do	At cable station	4,990
Do	At Fulton	4,916
Do	Below Three River Point	b167
Sacandaga River e	At mouth	b1,056
Salmon River	At bridge station	264
Do	One mile above falls	6 191
Do Do	At mouth	67
Schoharia Crooka	At gaging station	
Do	At Fort Hunter d	b017
Do	At Mill Point d	934
Do	At Schoharie Falls d	930
Schroon River	At gaging station	563
Seneca River	At mouth	b 3, 433
Do	At Baldwinsvilled	b 3, 103
West Canada Creek c	At mouth	569
Do	At Middlevilled	518
Do	At Trenton Falls	375
Do	At Twin Rock Bridge d	252

a Oswego River tributary. b United States Board of Engineers on Deep Waterways. c Mohawk River tributary. d Gaging station.

e Hudson River tributary. f Upper Hudson storage surveys. g Not including Schroon River.

MOHAWK RIVER GAGING STATIONS.

Gaging records have been kept on this stream at the following dams and mills: Rome waterworks pumping station at Ridge Mills, lower dam at Little Falls, New York State dam at Rexford Flats, and West Troy Company's dam at Dunsbach Ferry. A current-meter station at Freeman's bridge, below Schenectady, has also been maintained.

An important series of gagings has also been instituted on Mohawk River by the New York State canal survey, under the direction of Edward A. Bond, State engineer and surveyor. A statement regarding these gagings has been furnished by Mr. D. J. Howell, consulting engineer of the New York State canal survey. Gages have been erected at various places along the stream, from Herkimer to the confluence of the river with Hudson River at Cohoes, both above and below each dam and near the points of inflow of the more important tributaries, and the positions of the gage zeros have been determined with reference to mean tide as a datum. Gages previously maintained by the United States Geological Survey have been used wherever available. Observers are employed to take simultaneous daily readings of the gages, from which the slope of the water surface for each level or division will be determined and the velocity of flow computed. It is the intention to take cross sections of the stream channels in each level, at different stages, and to make current-meter or other discharge measurements during high water.

The regimen of Mohawk River during the navigation season is undoubtedly influenced to a large extent by the Erie Canal, which runs parallel to it from Rome to Cohoes. The water supply of the Erie Canal east of the summit level at Rome is, with a single exception, derived from Mohawk River and its tributaries. The State dams and feeders are located as follows:

Stream.	Location.
Mohawk River Do Oriskany Creek Mohawk River Do	 Delta, 6 miles above Rome. Rome. Oriskany. Little Falls. Fivemile or Rocky Rift dam.
Schoharle Creek Mohawk River	Rexford Flats.

Location of State dams and feeders.

A large diversion from the watershed at these feeders is in some measure counterbalanced by return water to the main channel, from seepage through canal and feeder banks, and from flow over wasteweirs.

The gaging records at Rexford Flats and at Little Falls indicate that during the navigation season the yield of the watershed, in

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second-feet per square mile, and frequently, also, the actual flow of the river, in second-feet, is considerably less at the former station than at the latter station. The drainage area above Rexford Flats is 3.385 square miles, or 2.6 times that at Little Falls, which is 1,306 square miles. This fact appears to be confirmed by the other gaging records kept on the stream, but the results of these have not been sufficiently worked up to permit a final discussion of the subject at this time. The diminished water-yielding capacity of the lower Mohawk Basin may be attributed in part to the low water of Schoharie Creek. The total drainage area of that creek is 947 square miles. Weir measurements at Schoharie Falls show that the flow sometimes falls below 50 second-feet. During practically the entire summer no water flows over the crest of the State dam at Fort Hunter: the major portion of the flow is diverted to the Erie Canal feeder, and the remainder leaks through the dam. During the summer of 1900, from June to October, inclusive, the direct inflow to the Mohawk from this tributary did not, with the exception of a few days, exceed 45 second-feet, or 0.05 second-foot per square mile.

MOHAWK RIVER AT RIDGE MILLS, NEW YORK.

A description of this station will be found in Water-Supply Paper No. 35, page 45. During the present season (1900) the calculated discharge of the turbines has been made to depend on current-meter measurements, instead of on the observed wheel-gate openings, as formerly.

Table showing rela	ition of speed	l of pumps to	o water flowing :	in tailrace.
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-	Date.	Speed of pumps.	Measured flow in tailrace.
May 29 August 23	1900.	Rev. per min. 15 12	Second-feet. 122 95

The discharge of the turbines is sensibly proportional to the rate at which the waterworks pumps which they drive are run, and a straightline diagram has been prepared, using the foregoing data, from which the flow through the turbines has been estimated.

On August 23, when no water was flowing over the crest, a measurement of the leakage of the dam was made in the stream channel below; it was found to be 20 second-feet, and an allowance of that amount has been made in estimating the daily flow. The results of other meter measurements at this station, and in the vicinity, will be found in the table on page 39.

The gaging record at Ridge Mills does not include any allowance for

diversion to Black River Canal at the Delta feeder, 4 miles upstream, nor for return water from seepage and wasteweirs.

Daily discharge, in second-feet, of Mohawk River at Ridge Mills, New York, for 1898.

Day.	Oet.a	Nov. a	Dec. a	Day.	Oct. a	Nov.a	Dec.a
1	154	269	123	18	215	294	169
2	149	249	144	19	199	294	144
3	133	215	133	20	249	304	159
4	121	199	133	21	215	249	342
0	140	210	109	49 99	999	009 607	009
7	100	369	1.1.4	94	704	409	630
8	173	259	169	25	519	294	419
9	159	249	169	26	609	215	344
10	149	1.134	154	27	1.251	191	319
11	143	2,134	184	28	574	199	159
12	149	697	184	29	409	134	219
13	154	515	121	30	539	104	3 24
14	259	439	136	31	314		644
15	889	371	159				
16	349	359	159	Mean	369	401	261
1	319	315	104				

[Drainage area, 153 square miles.]

a Revised figures.

Daily discharge, in second-feet, of Mohawk River at Ridge Mills, New York, for 1899.

Day.	Jan.a	Feb.a	Mar.a	Apr.a	May.a	June.	July.	Aug.	Sept.	Oct.	Nov.a	Dec.a
1	316 243	214 214	351 394	364 319	321 319	337 319	262 252	218 233		93 203	515 515	225 695
3	$\frac{296}{298}$	$\begin{array}{c} 214\\ 214\end{array}$	366 306	$254 \\ 311$	$239 \\ 204$	$279 \\ 259$	$232 \\ 249$	248 131		233 253	$ 345 \\ 295 $	395 345
$ \begin{array}{c} 5 \\ 6 \\ 7 \end{array} $	$2,373 \\ 896 \\ 409$	199 164 123	$\begin{array}{r}176\\1,074\\735\end{array}$	$ 344 \\ 391 \\ 439 $	176 151 102	214 232 232	$202 \\ 127 \\ 262$	$\begin{array}{c} 146 \\ 131 \\ 126 \end{array}$		$200 \\ 310 \\ 290$	$ 365 \\ 295 \\ 265 $	$ 295 \\ 295 \\ 275 $
8	$\frac{316}{299}$	166 126 190	$ 414 \\ 346 \\ 210 $	$1,264 \\ 1,034 \\ esc$	$94 \\ 129 \\ 129$	262 259	322 669	$ 121 \\ 125 \\ 120 $	85	260 290	295 295	235 235
$\begin{array}{c} 10 \\ 11 \\ 12 \\ \end{array}$		$129 \\ 129 \\ 129$	$254 \\ 1,174$	799 1,364	344 414	249 282	$ 379 \\ 359 $	$129 \\ 139 \\ 169$	85 95	$ 340 \\ 260 $	$ 315 \\ 295 $	315 3, 625
13 14 15	$ \begin{array}{r} 157 \\ 153 \\ 911 \end{array} $	$ \begin{array}{r} 129 \\ 173 \\ 265 \end{array} $	$1,211 \\ 701 \\ 364$	1,499 2,181 1.744	$296 \\ 361 \\ 214$	282 302 402	339 339 319	$ 265 \\ 245 \\ 275 $	89 85 99	$ \begin{array}{r} 310 \\ 260 \\ 310 \end{array} $	$ 265 \\ 265 \\ 265 $	$1,155 \\ 510 \\ 455$
16 17	725 459	$258 \\ 184 \\ 190$	321 239	1,841 1,364	$ \begin{array}{r} 161 \\ 389 \\ 261 \end{array} $	399 359	399 319	295 230	115 135	$240 \\ 220 \\ 200$	265 295	365 295
18 19 20	$ \begin{array}{r} 324 \\ 223 \\ 199 \end{array} $	$126 \\ 166 \\ 151$	$219 \\ 274 \\ 581$	$ \begin{array}{r} 1,054 \\ 2,226 \\ 2,034 \end{array} $	$ 549 \\ 614 $	$ \begin{array}{r} 339 \\ 282 \\ 279 \end{array} $	382 339	$230 \\ 245 \\ 245$		290 290 290	$\frac{295}{265}$ 245	1,075 1,495
21 22	193 208 214	$ 160 \\ 494 \\ 697 $	$ 464 \\ 364 \\ 380 $	1,404 1,264 1,130	$436 \\ 319 \\ 274$	262 259 299	302 382 200	265 295 272	79 56 56	$240 \\ 260 \\ 260$	245 265 265	1,095 315 315
24 25	261 338	389 346	436 416	959 766	239 219	259 259		289 262	56 60		265 295	345 315
26	$ \begin{array}{r} 318 \\ 244 \\ 223 \end{array} $	$\frac{296}{436}$ 451	$ \begin{array}{r} 344 \\ 274 \\ 241 \end{array} $	$ \begin{array}{r} 614 \\ 549 \\ 439 \end{array} $	$ \begin{array}{r} 204 \\ 189 \\ 386 \end{array} $	$259 \\ 249 \\ 249 \\ 249$	$ 262 \\ 289 \\ 165 $	269 309 309	69 69 53	$ \begin{array}{r} 220 \\ 310 \\ 340 \end{array} $	265 265 265	285 285 285
29 30 21	$208 \\ 170 \\ 170$		$536 \\ 436 \\ 436$	$354 \\ 319$	$1,136 \\ 546 \\ 344$	$249 \\ 229$	$ 133 \\ 178 \\ 178 $	$278 \\ 315 \\ 200$	53 79	$\frac{360}{260}$	$205 \\ 205$	285 75 75
Mean	377	244	467	997	320	281	310	226	81	278	291	

a Revised figures.

Daily dis	charge, i	in second-fe	eet, of	Mohawk	Riverat	Ridge Mills,	New York,	, for 1900.
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Day.	Jan.a	Feb.	Mar.	Apr.	May.b	June.b	July.b	Aug. b	Sept.b	Oct.b	Nov.
Day. 1	$\begin{array}{c} 3331.4\\ \hline \\ 270\\ 270\\ 290\\ 310\\ 310\\ 340\\ 1,115\\ 475\\ 530\\ 475\\ 420\\ 415\\ 305\\ 265\\ 265\\ 265\\ 345\end{array}$	200 132 100 180 100 248 128 1,628 1,628 1,628 1,628 1,628 1,928 3,162 1,928 618 578 618 578	784 815 750 630 280 254 354 359 320 280 280 219 254 219 254 219 164 149	810 1,080 1,245 2,205 1,845 1,065 1,845 1,070 740 680 930 930 930 930 930 930 1,485 1,685 3,375	$\begin{array}{c} 130\\ 130\\ 130\\ 130\\ 130\\ 130\\ 130\\ 130\\$	$\begin{array}{c} 168\\ 216\\ 285\\ 230\\ 180\\ 168\\ 215\\ 180\\ 230\\ 230\\ 230\\ 230\\ 185\\ 180\\ 180\\ 215\\ 180\\ 180\\ 185\\ 155\\ 158\\ 155\\ 158\\ 180 \end{array}$	$\begin{array}{c} 125\\125\\105\\105\\105\\105\\105\\105\\105\\105\\105\\10$	$\begin{array}{c} \text{Aug. 0}\\ 104\\ 120\\ 120\\ 92\\ 90\\ 104\\ 84\\ 107\\ 100\\ 88\\ 154\\ 305\\ 458\\ 304\\ 88\\ 84\\ 84\\ 80\end{array}$	$\begin{array}{c} & \\ & \\ & \\ & \\ & \\ & \\ & \\ & \\ & \\ & $	$\begin{array}{c} 175\\185\\165\\113\\115\\113\\115\\113\\115\\111\\113\\127\\118\\118\\118\\109\\1002\\395\\395\\395\\395\\109\end{array}$	$\begin{array}{c} 395\\ 365\\ 366\\ 340\\ 460\\ 1,970\\ 965\\ 705\\ 705\\ 705\\ 705\\ 705\\ 640\\ 620\\ 645\\ 580\\ 620\\ 640\\ 640\\ 640\\ 640\\ 640\\ 640\\ 640\\ 64$
10. 10. 20. 21. 22. 23. 24. 25. 26. 27. 28. 29. 30. 31. Mean	345 365 1,365 1,535 875 655 285 285 270 270 270 270 270 270	204 202 188 198 288 803 714 268 172 202 132 581	$\begin{array}{c} 139\\ 169\\ 544\\ 590\\ 594\\ 370\\ 164\\ 160\\ 164\\ 166\\ 164\\ 116\\ 112\\ \hline \end{array}$	a, 513 1, 805 935 930 1, 235 930 675 555 365 305 315 275 225 1, 062	$\begin{array}{c} 210\\ 147\\ 147\\ 130\\ 100\\ 105\\ 105\\ 105\\ 105\\ 105\\ 105\\ 10$	$\begin{array}{r} 180\\ 165\\ 170\\ 170\\ 165\\ 205\\ 140\\ 145\\ 123\\ 180\\ 130\\ 124\\ \hline \hline 180\\ \end{array}$	$\begin{array}{c} 140\\ 163\\ 165\\ 250\\ 185\\ 125\\ 132\\ 515\\ 270\\ 198\\ 175\\ 180\\ 107\\ 117\\ \hline 160\\ \end{array}$	$\begin{array}{r} 80\\ 84\\ 92\\ 98\\ 124\\ 97\\ 84\\ 165\\ 165\\ 120\\ 185\\ 125\\ 125\\ 124\\ 179\\ \hline 140\\ \end{array}$	118 179 625 615 415 395 205 175 185 205 185 205 198	109 90 95 95 95 895 895 415 395 410 395 345 95 95 212	040 1,550 1,760 1,480 965 9735 1,665 3,990 (c) 971

a Record doubtful; owing to ic \flat on crest of dam. b Record doubtful; flashboards changed frequently. c Dam and gage injured in flood.

ORISKANY CREEK AT ORISKANY, NEW YORK.

A description of this station, as well as of a second station which was maintained for a time at Coleman, on the same stream, will be found in Water-Supply Paper No. 35, page 47. The Oriskany station is located at the New York State dam. During the summer the entire flow, less leakage, is ordinarily diverted to the canal feeder. H. Waterbury & Company's dam, located just below the State dam, backs water above the toe of the latter dam, so that direct measurements of the leakage of the State dam can not readily be made. During the winter and spring the flow of the river is available for power from the lower dam, but during the season of navigation the inflow to the river from this tributary amounts to only a few secondfeet. The computed flow at the gaging station represents the total outflow from the pond above the State dam, and includes water diverted from Chenango River through the channel of Oriskany Creek to feed Erie Canal. A record is kept of the height of water in the pond above the dam, and also of that in the feeder channel below the head gates. The observed difference, or the head on the feeder gates, together with the area of the gate openings, have been used in the formula for discharge through submerged orifices to determine A screen rack in the forebay, just above the feeder gates, the flow. often becomes clogged with drift, causing a loss of head of several inches. In order that the correct head on the feeder gates might be obtained, at the beginning of the navigation season of 1900 a gage was placed in the forebay between the screen rack and the feeder gates.

Current-meter measurements have been made in the Oriskany feeder, as follows:

Date.	Hydrographer.	Measured dis- charge.	Computed dis- charge.
October 15, 1898 Do April 28, 1900 May 29, 1900	W. D. Lockwood do R. E. Horton do	Second-feet. 49.5 118.9 167.9 103.2	Second-feet. 48.9 119.1 170.3

Current-meter measurements in Oriskany feeder.

During the dry season the gateways leading to the feeder are wide open and the water flows through unobstructed, as in an open channel, so that the formula for discharge through orifices can not be applied.

In this connection the difficulties encountered in gaging the flow in canal feeders are worthy of comment. Broadly speaking, the amount of water required for the supply of canals is proportional to lockage and evaporation jointly, with, perhaps, a constant factor added for seepage losses. As a matter of fact, however, the rate of flow in the feeder often fluctuates, within wide limits, several times a day. Usually gates are placed in both the inlet and the outlet ends of the feeder channel. The height of the water in the feeder is influenced by the height of the water in the canal and in the supply pond above, while the velocity of flow may be varied by changes in the gate openings at either end. Isolated discharge measurements are of value in a general way, but it may be said that nothing short of a continuous record, both of the stage of the water in the feeder and of its velocity of flow, will serve to determine the actual diversion from day to day.

Daily discharge, in second-feet, of Oriskany Creek at Oriskany, New York, for 1898.

[Drainage	area,	144 s	square	miles.]
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Day.	Oct.	Nov.	Dec.	Day.	Oet.	Nov.	Dec.
$\begin{array}{c} 1 \\ 2 \\ \\ 3 \\ \\ 5 \\ \\ 6 \\ \\ 6 \\ \\ 8 \\ \\ 9 \\ \\ 10 \\ \\ 11 \\ \\ 12 \\ \\ 13 \\ \\ 14 \\ \\ 15 \\ \\ 16 \\ \\ 17 \\ \\ 17 \\ \\ 10 \\ \\ 11 \\ \\ 11 \\ \\ 11 \\ \\ 12 \\$		329 208 274 276 269 267 236 284 370 740 370 365 333 352 311 304	$\begin{array}{c} 266\\ 259\\ 428\\ 413\\ 445\\ 445\\ 445\\ 445\\ 445\\ 445\\ 445\\ 44$	18. 19. 20. 21. 22. 23. 24. 25. 26. 27. 28. 29. 30. 31. Mean	212 231 266 248 328 350 316 230 230 564 403 339 336 336 325	304 310 392 263 300 324 278 253 502 335 309 254 	160 220 195 300 3800 825 210 150 100 235 235 235 327

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Daily discharge, in second-feet, of Oriskany Creek at Oriskany, New York, for 1899.

	Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1.2		180 180	$157 \\ 167$	495 355	180 170	238 144	90 80		206 206	83 87	$ 180 \\ 138 $	$\frac{320}{175}$	90 103
3 4 5		$ \begin{array}{r} 195 \\ 220 \\ 220 \end{array} $	$ \begin{array}{r} 150 \\ 177 \\ 167 \end{array} $	$ \begin{array}{c} 425 \\ 460 \\ 910 \end{array} $	$ \begin{array}{r} 160 \\ 260 \\ 390 \end{array} $	$ \begin{array}{r} 139 \\ 139 \\ 129 \end{array} $	80 80 80		$ \begin{array}{r} 167 \\ 126 \\ 126 \end{array} $	$ \begin{array}{r} 73 \\ 10 \\ 75 \end{array} $	$ \begin{array}{r} 108 \\ 99 \\ 119 \end{array} $	$ \begin{array}{r} 115 \\ 138 \\ 144 \\ 144 \end{array} $	$ \begin{array}{r} 73 \\ 108 \\ 80 \end{array} $
6 7 8		$ \begin{array}{c} 250 \\ 285 \\ 220 \\ 2c0 \end{array} $	$217 \\ 230 \\ 243 \\ 977$		$425 \\ 525 \\ 1,270 \\ 77$	$124 \\ 122 \\ 122 \\ 122 \\ 124$	80 80 80	138 184 170 101	$ 177 \\ 177 \\ 195 \\ 105 $	108 101 133 176	$132 \\ 122 \\ 138 \\ 05$	$ \begin{array}{r} 346 \\ 374 \\ 429 \\ 261 \end{array} $	$ \begin{array}{r} 107 \\ 99 \\ 40 \\ 20 \end{array} $
$10 \\ 11 \\ 12 \\ 12$		$ \begin{array}{c} 200 \\ 220 \\ 255 \\ 255 \end{array} $	$277 \\ 343 \\ 343 \\ 343$	$ \begin{array}{r} 215 \\ 175 \\ 645 \end{array} $	$ \begin{array}{c} 600 \\ 490 \\ 1,220 \end{array} $	124 124 28 28	80 80 89 94	$104 \\ 110 \\ 117 \\ 124$	195 195 195 195 195 195 195 195 1	180 159 95			10 45 340
$ \begin{array}{c} 13 \\ 14 \\ 15 \end{array} $		$ \begin{array}{r} 410 \\ 505 \\ 550 \end{array} $	$ \begin{array}{r} 364 \\ 343 \\ 364 \end{array} $	$ \begin{array}{r} 490 \\ 340 \\ 280 \end{array} $	$1,440 \\ 1,160 \\ 910$	$25 \\ 25 \\ 30$		$124 \\ 124 \\ 124 \\ 124$	$ \begin{array}{r} 195 \\ 195 \\ 206 \end{array} $	73 87 85	$92 \\ 26 \\ 72$	$564 \\ 584 \\ 564$	330 80 65
$ \begin{array}{c} 16 \\ 17 \\ 18 \\ 10 \end{array} $		505 380 315 955	337 343 337	$255 \\ 200 \\ 230 \\ 255 $	625 370 340 200	105 122 134	$101 \\ 94 \\ 113 \\ 112$	$208 \\ 208 \\ 197 \\ 182 $	206 206 206 206	89 115 123	$ \begin{array}{r} 45 \\ 106 \\ 58 \\ 71 \end{array} $	$ 484 \\ 524 \\ 584 \\ 202 $	
$\frac{10}{20}$ $\frac{21}{22}$		$250 \\ 260 \\ 290 \\ 270$	297 390 410	$ \begin{array}{r} 370 \\ 330 \\ 285 \end{array} $	$ \begin{array}{r} 250 \\ 260 \\ 230 \\ 130 \end{array} $	$135 \\ 120 \\ 140 \\ 160$	$ \begin{array}{c} 113 \\ 113 \\ 113 \\ 113 \end{array} $	$ 183 \\ 270 \\ 270 $		$ \begin{array}{r} 113 \\ 138 \\ 161 \\ 129 \end{array} $		$53 \\ 124 \\ 154$	
23 24 25		290 290 260	404 303 287	355 280 285	$50 \\ 50 \\ 50 \\ 50$	$ \begin{array}{r} 140 \\ 115 \\ 115 \end{array} $	$ \begin{array}{r} 118 \\ 118 \\ 118 \\ 118 \end{array} $	$270 \\ 196 \\ 196$	$\frac{206}{206}$	$ \begin{array}{r} 162 \\ 102 \\ 112 \end{array} $	85 88 70	$ \begin{array}{r} 174 \\ 214 \\ 174 \end{array} $	50 70 50
$\frac{26}{27}$. 28.		$285 \\ 305 \\ 340 \\ 285$	$297 \\ 367 \\ 244$	$240 \\ 220 \\ 215 \\ 205$	416 406 120 205	$ \begin{array}{r} 159 \\ 144 \\ 139 \\ 100 \end{array} $	$ \begin{array}{c} 118 \\ 118 \\ 113 \\ 113 \end{array} $	196 196 196 196 196 100	194 184 184 184	$ 181 \\ 222 \\ 216 \\ 105 $	$ \begin{array}{r} 70 \\ 54 \\ 158 \\ $	$ \begin{array}{c c} 438 \\ 318 \\ 318 \\ 500 \end{array} $	$ 40 \\ 30 \\ 35 \\ 90 $
29 . 30 . 31 .		305 290 300		$ \begin{array}{r} 205 \\ 190 \\ 190 \end{array} $	335 325	$139 \\ 129 \\ 134$	113	$196 \\ 196 \\ 196 \\ 196$	184 98 98	185 206		582 789	30 65 70
	Mean	295	291	342	466	119	99	180	186	126	91	360	89

Daily discharge, in second-feet, of Oriskany Creek at Oriskany, New York, for 1900.

			1.			-						
Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1	64	139	254	1.318	238	95	110	100	82	70	186	250
2	133	212	786	1,391	192	95	110	100	74	70	191	205
3	81	326	876	1,046	163	95	110	100	76	70	136	185
4	96	286	776	546	163	95	110	100	84	70	117	-175
5	41	416	736	426	144	95	110	100	66	70	122	607
6	76	302	398	916	183	95	140	100	81	70	73	427
7	54	218	756	896	161	95	88	100	85	70	95	330
8	101	302	401	596	163	97	13	100	85	175	101	285
9	114	1,811	300	308	136	95	104	100	01	06	100	200
10	114	390	00%	200	100	95	101	100	10	00	105	111
19	06	±10 120	418	194	150	90	107	100	10 01	10	151	203
19	50	2 116	157	216	105	05	105	100	70	75	106	202
14	68	154	157	254	105	95	105	124	70	75	113	1.12
15	81	248	139	212	105	95	105	107	70	78	136	112
16	133	139	133	206	118	95	105	103	70	84	96	157
17	145	114	127	470	144	95	105	100	70	81	113	202
18	114	76	76	1,090	171	95	105	100	70	78	114	217
19	546	60	170	427	156	95	107	100	70	80	81	217
20	1,376	81	696	315	148	95	105	100	- 70	80	127	337
21	576	127	496	212	161	95	107	100	70	75	127	277
22	721	170	294	877	115	95	124	100	70	75	78	242
23	176	236	326	379	113	95	105	100	70	77	158	272
24	91	96	386	260	113	95	105	100	70	83	161	1,172
25	481	91	254	239	113	95	114	100	70	15	430	427
26	156	26	236	230	113	95	110	100	70	75	2,592	242
21	100	110	183	201	113	90	112	110	10	103	807	120
40	100	199	000	200	110	94	108	10%	10	100	012	170
80	114		480 888	279	110	95		100	80	100	207	102
31	156		846	614	113	95	30	100	00	191	~01	177
	100		010		110		00	100		101		111
Mean	199	378	386	488	136	95	100	103	73	85	255	272

SAUQUOIT CREEK AT NEW YORK MILLS, NEW YORK.

A description of this station will be found in Water-Supply Paper No. 35, page 48. During the summer little water flows over the dam, the entire volume being used to drive the water wheels in the adjoining cotton mills. The leakage of the dam was measured by current meter on May 31, and was found to be 5.6 second-feet.

This station was discontinued October 1, 1900.

Daily discharge, in second-feet, of Sauquoit Creek at New York Mills, New York, for 1898.

									•
Day.	Sept.	Oct.	Nov.	Dec.	Day.	Sept.	Oct.	Nov.	Dec.
1		16 * 7	$42 \\ 43$	$\begin{array}{c} 49\\ 44 \end{array}$	18 19		105 60	49 43	* 30 42
3 4		27 18	38 36	$^{34}_{*50}$	20. 21.	18 26	36 38	$^{*95}_{46}$	38 76
5 6 7		31 54 35	32 * 59 38	46 42 41	22.23.23.	18 16 99	42 * 73 71		104 288 00
8 9		23 * 23	36 38	49 42	25 26	* 37 30	48 59	$\begin{array}{c} 10\\42\\66\end{array}$	* 76 62
10 11		35 52	$132 \\ 140 \\ z_{0}$	28 * 22	27 28	$ \frac{40}{40} $	140 74 cs	* 62 36	46
13 14		40 46 46	$*69 \\ 62$	$42 \\ 42 \\ 36$	30 31	21 21	* 66 57	43 42	90 74 52
15 16		144 * 80	$52 \\ 49 \\ 40$	$37 \\ 42 \\ 24$	Mean	27	56	57	57
		105	49	54					

[Drainage area, 52 square miles.]

* Sunday.

Daily discharge, in second-feet, of Sauquoit Creek at New York Mills, New York, for 1899.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1	* 72	42	77	45	56	42	12	17	18	(*)	53	19
3	$198 \\ 58$	30 38	48 48	* 40		18	27	43	6 (*)	29 24	$\frac{42}{21}$	10
4	111	18	42	73	36	* 30	$\frac{10}{20}$	30		21	26	32
6 	74	36	109	$104 \\ 165$	$\frac{33}{28}$	56	$\frac{50}{27}$	(*)	32	16	+ 29 32	26
7	50 * 12	36	72	188	* 26	48	18	26	6	8 * 19	22	26
9	58	30	62	* 156	35	- 23	*25	22	12^{11}	18	24	12
10	38	21	60	100	26	34 * 13	31		(*)	18	$\frac{19}{20}$	* 14
12	36	* 65	* 300	160	50	28	27	14	19	18	* 29	72
13	54	35	87	585	25	20	19	(*) 25	19	16 7	29 24	64 38
15	* 185	29	82	253	47	30	13	22	5	* 13	24	32
16 17	57 68	29 33	$\frac{71}{50}$	* 228	36 52	$\frac{34}{38}$	* 30	18	15 (*)	18 15	$\frac{21}{24}$	30 * 31
18	48	37	43	118	47	*7	27	18	19	16	21	38
19	30 36	* 13 48	* 447	98	51 52	30 30	19	6 (*)	19	18	* 24 26	
21	42	58	65	90	* 12	23	11	22	14	12	26	54 95
444 23	48	100	90	*86	35	25	(*)	19	10^{11}	24	25	3
24	52	62 50	90 55	59	36	23	$\frac{27}{30}$	5	(*)	18	$\frac{21}{18}$	* 30
26	44	* 65	* 95	76	33	26	22	10	15	19	*22	3:
27	42	$173 \\ 62$	69 79	58 54	$\frac{20}{*40}$	$\frac{20}{19}$	27	(*)	13	15	$\frac{24}{24}$	16
29	* 59		76	43	42	20	14	30	18	*19	21	19
31	36 30		71 78	* 50	$42 \\ 43$	21	27	18 5	10	32 26	21 	*14
Mean	58	58	111	127	38	23	20	16	14	17	26	29

Day.	Jan	Feb	Mar	Apr.	May.	June	July.	Ang.	Sept.
Duji	000000	1000			Diregi	ounor	o arj.	and and	No p ti
1	86	87	69	* 207	81	42	* 5	23	27
2	46	77	81	337	81	$\tilde{20}$	38	23	* 5
3	46	97	35	267	81	* 29	38	34	5
4	40	* 45	* 21	135	87	42	5	10	23
5	40	69	81	135	30	42	38	*5	23
6	. 17	72	74	91	* 43	35	86	30	17
7	* 25	67	89	269	87	29	34	23	20
8	50	147	89	* 207	81	$\frac{40}{21}$	*9	23	20
9	36	495	86	103	81	24 * 17	60	20	* 0
10	42	65	38	87	74	* 17	60	17	23
10	40	* 07	* 17	112	11	43	28	$13 \\ *5$	0/
14	40	1 412	74	110	* 55	40			
10	*0	1,410	68	87	87	+1 95	99	20	10
15	50	92	68	* 135	65	32	*5	17	17
16	43	68	63	85	26	24	42	20	*5
17	50	37	42	207	35	* 5	35	20	13
18	50	* 55	* 13	297	35	29	35	37	17
19	306	74	68	170	24	41	28	*5	17
20	272	68	371	95	* 29	38	32	30	17
21	* 117	68	95	193	35	38		18	17
22	92	379	93	* 295	35	25	* 5	20	13
23	97	392	93	, 95	35	27	38	17	*9
24	115	34	55	103	35	* 5	38	17	13
25	95	* 13	* 67	91	35	32	48	18	17
20	60	80	89	81	14	38	42	* D	15
20	* 00	41	08	84	* 33	20 20	32	30	17
20	80 "	14	80	49	48 99	0% 57	* 5	01 25	13
30	00		100	01	200	32	39	00 35	10
31	63		165	91	35	00		37	. 9
***************************************	00		100		.00		00	01	
Moon	79	146	94	199	40	29	90	99	15
mean	1.4	140	04	199	49	Ðŵ	9.9	44	10

Daily discharge, in second-feet, of Sauquoit Creek at New York Mills, New York, for 1900.

* Sunday.

WEST CANADA CREEK AT TWIN ROCK BRIDGE, NEW YORK.

Twin Rock Bridge crosses West Canada Creek 2 miles above Hinckley, at practically the point of emergence of the stream from the Adirondacks. The bridge is of iron, has two spans, and is 167.5 feet long between abutments. The stream bed is of gravel and rock, and the conditions are unusually favorable for a current-meter station. A gage board was set and a record commenced on September 7, 1900. The gage is read at 7 a. m. and at 6 p. m. each day, and the average of the two daily readings is given in the appended table. A currentmeter measurement made on September 7 showed the discharge to be 182 second-feet. The gage reading was 0.37 foot.

The record at Twin Rock Bridge is kept by the Utica Electric Light and Power Company. This company is erecting a power plant at Trenton Falls, 4 miles farther downstream. A concrete dam has been constructed, which will give a head of 265 feet on the turbines, which are of special design. It is the intention, after the plant is completed, to keep a continuous record of the amount of water used by the turbines and of the flow over the spillways.

The drainage areas at the different gaging stations are as follows:

Drainage areas of West Canada Creek.

50

	Square mile
At mouth	
At Middleville	 519
At Trenton Falls	
At Twin Rock Bridge	 252

Daily gage height, in feet, of West Canada Creek at Twin Rock Bridge, New York, for 1900.

Day.	Sept.	Oct.	Nov.	Dec.	Day.	Sept.	Oct.	Nov.	Dec.
1	0.35	$\begin{array}{c} 0.85\\.75\\.65\\.70\\.60\\.55\\.65\\.85\\.75\\.75\\.00\end{array}$	$\begin{array}{c} 0.90 \\ 1.60 \\ 1.10 \\ 1.05 \\ 1.15 \\ 1.70 \\ 4.55 \\ 4.25 \\ 3.05 \\ 1.45 \end{array}$	$ \begin{array}{c} 1.60\\ 1.85\\ 2.00\\ 1.90\\ 1.75\\ 1.55\\ 1.40\\ 1.40\\ 1.50\\ 1.50 \end{array} $	17 18 19 20 21 23 24 24 24 24 24 24 24 25 26 27 28 29 20 .	$\begin{array}{c} 0.45 \\ .30 \\ .30 \\ 1.65 \\ 2.90 \\ 2.35 \\ 1.50 \\ .95 \\ 1.10 \\ .90 \end{array}$	1.05 1.00 .95 1.15 .62 .60 2.30 2.45 1.75 1.75	$\begin{array}{c} 1.50\\ 1.80\\ 5.50\\ 5.30\\ 4.45\\ 3.75\\ 2.00\\ 6.25\\ \epsilon = 90\end{array}$	$\begin{array}{c} 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.75\\ 1.70\\ 1.65\\ 1.60\\ 1.65\\ 1.60\\ 1.65\\ 1.60\\ 1.65\\ 1.60\\$
10	.32 .35 .32 .35 .35 .35 .38 .78	$ \begin{array}{r} .90\\.85\\.70\\.60\\1.25\\1.30\\1.10\end{array} $	$ \begin{array}{r} 1.45 \\ 2.05 \\ 1.90 \\ 1.55 \\ 1.60 \\ 1.50 \\ $	$ \begin{array}{r} 1.50 \\ 1.50 \\ 1.50 \\ 1.50 \\ 1.50 \\ 1.50 \\ 1$	26 27 28 29 30 31	.90 .95 1.00 .85 .90	$ \begin{array}{r} 1.70 \\ 2.55 \\ 1.95 \\ 1.15 \\ 1.20 \\ 1.50 \\ \end{array} $	$ \begin{array}{r} 6.20 \\ 4.40 \\ 3.55 \\ 1.90 \\ 1.70 \\ \end{array} $	1.60 1.55 1.50 1.50

WEST CANADA CREEK AT MIDDLEVILLE, NEW YORK.

A description of this station will be found in Water-Supply Paper No. 35, page 49. In the past the principal element of uncertainty with regard to this record was considered to be the leakage of the dam, etc., which had been taken at 50 second-feet. Current-meter measurements were made on September 10, 1900, to determine the leakage of the dam and the low-water flow of the stream at this station, with the following results:

	Second-
	feet.
Highway bridge below dam, measured flow in main stream chann	el. 113
Measured flow in hydraulic canal	132
Total flow by current-meter measurements	245
The calculated flow from the gage record is as follows:	
	Second-
Flow over dam, gage reading 0.67 foot	60
Leakage previously estimated	50
Total flow in main channel	110
Calculated diversion to water wheels	131
Total estimated flow	241

Unfortunately no current-meter measurements to check the calculated flow during high water have been made. The highest water observed was in August, 1898, when it reached a depth of 5.5 feet on the crest of the Middleville dam. The discharge at that time can not accurately be estimated, as a part of the water flowed around the end of the dam and passed overland to the stream channel below. Highwater marks at the Newport dam indicate that the spring freshet dis-

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charge has been as great as 22,000 second-feet, or 46.6 second-feet per square mile, from a drainage area of 472 square miles. The lowest water in this stream occurs on Sundays, when the flow is held back, as pond storage, by dams above Middleville. Aside from this, the most notable low-water period was September 2 to 12, inclusive, 1899, the mean flow at Middleville for eleven days being 183 second-feet per square mile.

Daily discharge, in second-feet, of West Canada Creek at Middleville, New York, for 1898.

Day.	Oct.	Nov.	Dec.	Day.	Oct.	Nov.	Dec.
1	$\begin{array}{c} & & \\$	$\begin{array}{c} 777\\ 670\\ 584\\ 595\\ 450\\ *550\\ 911\\ 626\\ 711\\ 1, 679\\ 4, 163\\ *2, 410\\ 1, 318\\ *2, 410\\ 1, 318\\ *2, 410\\ 1, 318\\ 816 \end{array}$	$\begin{array}{c} 650\\ 580\\ 580\\ *539\\ 651\\ 588\\ 405\\ 483\\ 624\\ *519\\ 552\\ 742\\ 1,123\\ 1,362\\ 1,413\end{array}$	18	$\begin{array}{c} 968\\783\\689\\737\\981*1,894\\1,758\\1,209\\1,055\\2,436\\2,554\\1,580*1,129\\979\end{array}$	752 800 997 904 801 990 983 775 602 *740 1,224 679 713 1,110	$\begin{array}{c} *1,349\\ 1,374\\ 1,469\\ 1,288\\ 1,614\\ 2,072\\ 2,083\\ *1,739\\ 1,452\\ 1,181\\ 892\\ 7111\\ 1,082\\ 1,492\\ \hline 1,024\end{array}$

[Drainage area, 519 square miles.]

* Sunday.

Daily discharge, in second-feet, of West Canada Creek at Middleville, New York, for 1899.

The second												
Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
12	*1,216 1,241	$1,135 \\ 1,205$	$1,563 \\ 1,354$	821 * 523	2,979 4,760	$1,114 \\ 763$	$198 \\ * 140$	273 292	$257 \\ 191$	* 480	$1,281 \\ 2,867$	330 580
3	$1,378 \\ 1,376$	$1,335 \\ 1,340$	$1,208 \\ 1,191$	620 622	$2,696 \\ 2,735$	593 * 550	$\frac{200}{116}$	$ 345 \\ 316 $	$^{*145}_{145}$	$470 \\ 436$	$1,744 \\ 1,199$	* 710 710
5	3,445 3,500	*1,292 1,203	*1,348 1,635	680 680	1,926 1,455	531 480	$ \begin{array}{c} 240 \\ 240 \\ 250 \end{array} $	237 * 155	$210 \\ 205 \\ 10^{-5}$	337 253	*1,040 831	518 540
8	1,858 *1,315 1 173	1,101 1,172 937	1,835 1,207 942	1,697	$^{*1,238}_{1,187}$	$ \begin{array}{r} 294 \\ 314 \\ 258 \end{array} $	236 204 *675	286 262 256	195 219 169	288 * 190 932	$ \frac{469}{542} $	1,750 1,670 840
10	782 462	1,535 1,350	812 751	$1,601 \\ 1,588$	$1,422 \\ 1,073$	182 *130	993 807	242 246	*145 188	220 234	390 420	*700
12	$786 \\ 1,119 \\ 1,129$	*1,690	*1,340	2,230 2,465	1,189 1,003	283 297	443 445	214 * 125	201 221	210 239	* 410 342	$3,150 \\ 4,710 \\ 500$
14 15 16	$^{1,132}_{*1,615}$ $^{1,615}_{1,760}$	1,227 1,666 2,640	1,632 1,181 1,071	3,228 3,582 *3,513	$^{*995}_{1,196}$	248 753 839	343 236 * 130	204 216 253	205 204 189	$*140 \\ -241$	313 372 313	2,530 740 840
17 18	$1,771 \\ 1,102$	2,500 2,111	814 944	$3,549 \\ 3,751$	$1,143 \\ 1,064$	499 * 320		239 235	$*145 \\ 197$	238 235	363 372	* 640
19 20		*2,410 1,562	*1,060 1,175	$ \begin{array}{c} 4,477 \\ 5,717 \\ 0 \end{array} $	1,183 1,633	339 331	$479 \\ 345 \\ 007$	$^{174}_{*110}$	208 213	$217 \\ 152 \\ 001$	* 220 337	1,880 3,520
22	* 535 568	1,810 1,966 2,044	1,335 1,412 1,179	5, 381 *6, 083	$^{*1,240}_{1,274}$	346 263	327 225 * 140	231 245 257	$239 \\ 238 \\ 204$	* 190 245	363 293	2,530 1,400 990
24 25	$\begin{array}{c} 616 \\ 701 \end{array}$	$1,764 \\ 1,660$	$\hat{1}, \hat{1}80 \\ 1, 203$	$5,956 \\ 5,904$	884 844	$203 \\ * 155$	$241 \\ 241 \\ 241$	$\frac{229}{254}$	$*145 \\ 209$	$225 \\ 238$	$273 \\ 273$	$*1,150 \\ 900$
26	763 640 696	*1,490 1,564	*1,313 764 705		801 728 * 810	$ 283 \\ 273 \\ 950 $	241 244 **20	$183 \\ * 110 \\ 955$	$476 \\ 433 \\ 249$	231 267	* 249 312 209	840 580
29 30	* 605 818	1, +++	762 685	3,119 4,969 *4,513	1,255 1,179	$\frac{280}{308}$ 275	239 171 * 115	$\frac{255}{247}$ 262	$248 \\ 213 \\ 386$	* 965 1,040	310 310	540 540
31	1,010		758		1, 191		234	269		629		* 860
Mean	1,150	1,594	1,176	3,365	1,456	397	324	235	221	324	577	1,259

Daily	discharge,	in	second-feet,	of	West	Canada	Creek	at	Middleville, Ne	ew [York,
					for	1900.					

Day.	Jan.	May.a	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1	824		415	* 320	362	457	470	450	1,517
2	722		358	338	450	* 320	469	320	* 1,232
3	984		* 530	381	450	459	426	285	1,025
4	1,001		490	330	315	453	401	* 270	1,175
5	1,219		524	299	* 190	464	336	270	1,325
<u>6</u>	1,221		522	289	249	494	219	340	1,325
7	* 1,240		491	358	235	534	* 193	360	1,044
8	1.244		557	* 500	206	421	369	880	1,030
9	1,100	1 008	676	523	205	* 280	467	1,010	* 818
10	1,100	1,007	* 480	448	168	401	404	1,010	677
11	972	1,043	530	454	200	393	339	* 700	573
17	937	1,228	495	238	* 303	324	321	580	483
10	900	1,429	420	442	407	218		400	400
14	1 011	1,007	414	300	1 001	270	* 280	400	480
10	1,011	1,281	000	* 3.40	1,031	\$ 190		400	* 200
17	1,001	1,009	196 *	409	1,010	* 100	120	210	* 090
10	1,000	1,144	220	517	400	441 900	466	* 110	410
10	2 410	1,200		592	* 200	200	400	- 410	410
10 	1 495	*1 269	924	497	415	404 201	200	1 420	400 509
91	*9 680	1,004	- 00±	517	217	221	* 170	2,000	561
99)	2,103	744	316	* 530	297	819	200	2 630	550
92	2,400	637	208	188	960	* 047	200	2 340	* 560
94	2 874	505	* 984	210	258	910	778	1 900	819
95	2 396	544	273	511	398	608	958	*3 120	942
96 96	2,003	437	219	636	* 320	574	797	5 920	898
97	2, 394	* 390	306	567	506	464	461	5 670	900
28	*730	466	326	445	551	364	* 460	2 900	900
29	870	423	520	* 373	674	286	464	1,980	900
30	780	380	431	481	599	* 320	454	1 665	* 1 020
31	530	413		386	534		594		955
Mean	1,366	924	406	451	463	419	448	1,536	800

a No record for February, March, and April. \ast Sunday.

MOHAWK RIVER AT LITTLE FALLS, NEW YORK.

This gaging station, which has been described in Water-Supply Paper No. 35, page 51, is located at the lower (Gilbert's) dam at Little Falls. Current-meter measurements have been made to check the calculated flows, with very satisfactory results. They are as follows:

a de la companya de l	feet.
October 20 to 21, 1898, at suspension bridge 2 miles below Little Falls,	20000
W. D. Lockwood, hydrographer:	
Total flow by current meter	1,758
Computed flow (mean of two days)	1.733
May 1, 1900, at suspension bridge 2 miles below Little Falls, R. E. Horton,	,
hydrographer:	
Total flow by current meter	4,773
Computed flow over dam 4,060	
Computed diversion to Gilbert's mill	
Computed diversion to paper mill	
Total computed flow	4.799
May 23, 1900, at Astronga Bridge, Little Falls, R. E. Horton, hydrog-	_,
rapher:	
Total flow by current meter	1.567
Computed flow over dam	-,
Computed diversion to Gilbert's mill 176	
Computed diversion to paper mill 405	
Total computed flow	1,531

Diversion to paper mill, September 19, 1900:	
Metered flow in headrace	302
Computed flow through turbines, etc	288

There are three dams at Little Falls. The two lower are used for water-power development; the upper one is a State dam, diverting water for the supply of Erie Canal. The gage record kept at the lower dam shows the amount of water flowing downstream from Little Falls, but does not include the diversion at the State dam above the gaging station, and hence does not represent the total yield or inflow from the tributary drainage area of 1,306 square miles.

Current-meter measurements were made in the feeder channel below the State dam, as follows:

Current-meter measurements in feeder channel below State dam.

Date.	Measured diversion.
1900.	Second-feet. 143
September 19	179

Adding the foregoing amounts to the mean daily flow at Gilbert's dam for the same dates, we obtain the following:

Volumes of inflow and outflow at Little Falls diversion.

	Date.	Total in- flow at Lit- tle Falls.	Outflow in main channel.
May 23	1900.	Second-feet. 1,596	Second-feet. 1,453
September 19		 693	514

Water is again diverted to the canal at Fivemile dam, below Little Falls. On November 3, 1900, the measured flow in this feeder, at Lansing's farm bridge, was 236 second-feet.

High water occurred at Little Falls as follows:

High water at Little Falls.

Date.	Depth of water on crest of dam.	Volu	me.
April 15, 1899	Feet. 7.33 8.21	Second-feet. 13,000 15,240	Secft. per sq. mile. 10.0 11.7

The most notable low-water period was August 3 to August 10, inclusive, 1899, the mean flow for eight days being only 120 second-feet, or 0.07 second-foot per square mile.

Daily discharge, in second-feet, of Mohawk River at Little Falls, New York, for 1898.

Day.	Sept.	Oct.	Nov.	Dec.	Day.	Sept.	Oet.	Nov.	Dec.
1		1,121	2,261	1,499	18		2,265	2,220	21,17
2		*916 849	1,880 1.790	1,547 1,451	19 20		1,699 1.745	2,399 *2.878	1,499 1,499
4		895	1,560	*1,173	21		1,722	2,771	1,83
6		1,627	$^{1, 545}_{*1, 501}$	1,555 1,763	23	1,125	*4,096	$2,301 \\ 2,794$	4,50
7 8		1,558 1 179	1,946 2 040	1,639 1,269	24 25	3,484 *4 093	4,339 3 240	2,694 2,538	5,279
9		*916	1,700	969	26	2,718	2,574	1,950	3,75
1		900 867	$4,420 \\ 9,433$	$^{1,462}_{*1,508}$	28	$2,449 \\ 2,220$	6,290 6,188	$^{*1,473}_{1,137}$	2,20 1,899
2		915 1.028	7,925 *6,728	1,709 1,409	29 30	1,615 1.320	5,121 *3,246	1,412 1,562	1,49 1.92
4		1,040	5,245	1,259	31		2,628		3,97
.6 .6		*5,026	2,891	1,309 1,259	Mean	2,378	2,495	2,891	2,03

[Drainage area, 1,306 square miles.]

Sunday.

Daily discharge, in second-feet, of Mohawk River at Little Falls, New York, for 1899.

					-							
Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July	Aug.	Sept.	Oct.	Nov.	Dec.
1	*2,854	941	3,258	3,041	6,360	1,957	569	506	278	*704	2,829	2,096
2	1,790	906 861	2,104 2,304	*2, 519 2 329	5 619	1,610 1 321	*493 359	006 135	*30	651	4 738	1,709
4	1,936	884	2,298	2,536	3, 925	*1,075	424	136	396	491	3,081	2,175
5	6,821	*646	*3,408	2,387	2,905	1,466	490	166	545	534	*3,262	2,097
6	7,440	1,063	5,544	4,297	2,339	1,216	663	*000	382	399	2,847	1,668
8	0,880 *1 960	983	0,044 5 154	4,037	1 801	1,010 1.062	651	100	212	240 *160	1,908 1,718	1,408 1 588
9	4.377	846	4, 534	*6. 759	1,571	962	*1.660	131	211	357	1,628	1,000 1.630
10	2, 529	803	3,054	7,079	1,470	764	2,593	130	*7	297	1,451	*1,016
11	1,467	871	2,572	6,729	1,469	*1,176	1,800	316	273	274	717	2,779
12	1,378	*789	*3,967	7,979	1,846	660	1,320	383	270	305	*1,112	6,704
13	1,298 1 002	983	6 590	9,644	2,213	660	1,222	*000	270	214	1,520 1,448	10,990
14	*4.104	1.222	6.304	12,502	2.212	960	881	352	230	*196	1,440 1,150	7,367
16	4,848	1,333	6,354	*12,649	1,746	1,860	*643	351	184	354	1,069	3,500
17	4,703	748	2,129	11,339	1,896	1,800	1,315	244	*55	339	1,120	*1,326
18	4,279	1,326	2,254	10,716	2,492	*965	1,211	251	278	344	1,037	1,692
19	1,509	*669	*3,195	10,869	2,843	568	1,086	216	267	339	*984	4,812
20	1,000 1.687	1, 440 1 523	2 704	11,000 12 150	0, 142 *2 650	1,010	1,008	158	220	331	1,070 1,120	7 216
22	*1.794	2.598	3,429	10,878	3.143	985	95	223	249	*142	1.145	5,822
23	1,885	4,506	3,494	*10,409	2,172	866	*363	235	129	350	1,066	5,147
24	1,859	4,001	3,694	10,920	1,696	745	496	203	*55	401	987	*1,753
25	2,284	3,664	3,824	9,870	1,470	*851	496	203	238	392	*909	2,186
20 97	1 813	$^{+1},430$ 2 376	2, 890	9 180	1,309	634	010 496	*136	556	387	822	1,011
28	1,175	3,201	2.345	7,880	*1.680	585	510	348	920	314	969	1.641
29	*1,574		2,514	7,139	2,323	560	460	188	642	*1,398	969	1,390
30	1,154		3,029	*6,299	3,827	535	*50	219	723	2,293	886	1,049
31	1,126		3,029		2,903		697	277		1,882		*932
Mean	2,753	1,510	3,757	8,102	2,651	1,014	803	223	298	509	1,699	3,360
					1			1	,			

* Sunday.

Daily di	scharge, in	second-feet,	of Mohawk	River at Little	Falls	, New York.	for 1900.
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						1					1	
Dov	Tan	Feb	Mar	Ann	May	Inne	Inly	A 110	Sont	Oct	Nov	Dec
Day.	oan.	1.00.	man.	Apr.	may.	J 0 0 000.	oury.	mug.	Dopt.	000	1101.	1700.
1	505	1 504	1 454	*5 785	4 672	645	*205	481	620	667	1.989	4 845
9	961	1 379	1,101	8 497	4 510	761	1.053	500	*515	8.19	1 289	*1 (197
3	1 040	1 251	1,539	10 124	4 362	*1 119	1 804	515	455	881	1 197	3 200
4	1,010	*121	*1 001	9 162	4 014	1 346	311	339	503	499	*1 264	3 109
5	608	1 457	2 228	8 114	3 774	1 174	614	*93	503	491	885	6.316
6	578	1.682	2.013	7,936	*2.443	1.014	505	284	503	493	920	5,504
7	*180	1,594	1.967	9,998	1.658	760	788	274	629	*282	982	5,727
8	1.592	1.814	2.125	*10,065	1.698	1.214	*625	195	228	449	3,350	5,620
9	1,966	4,712	2,228	8,587	2,304	1,643	1,048	374	*326	665	5,335	*4,725
10	1,921	5,053	2,250	6,660	2,591	*1,283	876	452	294	747	3,837	2,579
11	1.772	*3,449	*1,889	5,053	2,595	1,134	754	153	326	747	*2,673	2,562
12	1,726	5,305	2,013	4,532	2,330	1,134	754	*181	200	499	1,901	2,388
13	1,576	10, 192	1,818	4,304	*2,132	864	694	365	483	598	1,738	2,388
14	*1,731	11,128	1,875	4,202	1,462	864	666	2,041	515	*459	1,600	2,178
15	1,636	11,642	1,818	*4,607	1,859	896	*545	2,370	377	691	1,598	1,586
16	1,496	8,292	1,726	5,672	1,732	801	668	1,434	*461	1,231	1,368	*1,866
17	1,455	8,961	1,696	7,261	1,927	*555	724	1,084	515	1,032	1,207	1,630
18	1,455	*3,671	*1,380	11,128	1,778	702	826	874	713	983	*1,336	2,230
19	1,592	3,678	1,496	13,542	1,882	599	754	*745	501	881	1,998	1,825
20	4,302	2,334	1,967	15,242	*1,745	561	794	651	492	785	3,929	2,361
21	*7,291	1,968	3,345	15,032	1,732	650	1,170	494	599	*6:22	6,057	2,180
22	7,194	2,380	3,740	*11,275	1,037	579	*1,430	494	1,777	564	5,303	1,981
23	7,130	1,303	3,740	10,024	1,403	437	1,088	499	*1,380	043	4, 515	$^{+1},828$
24	0,100	0,014	4,100	9,401	1,400 1 1.05	171	090	410	900	1,11+	0.414 *9.004	0,009
20	4, 140	$^{\circ}1,081$ 1,509	2 405	8,491	1,100	900	9 100	0%1 *705	1,034	2,101	*3,094	$\begin{bmatrix} 0,291\\ 5,177 \end{bmatrix}$
40	4,070	1,00%	9,400	6 091	*1.014	474	1 200	- 190	910	1,004	14,000	1 1 1 1 1 1
64 00	*1 500	1,400	2,000	5 100	751	474	1,000	000	014	1,470	19,501	2 007
40	2 176	1,041	3,000	*1 550	751	674	*1 969	1 255	659	1,000	8 815	9 606
30	1 779		1 933	4 679	792	740	87.1	050	*669	1,00%	4 734	*1 900
31	1 496		5 094	2,014	793	140	696	721	008	1 1 1 92	1,101	2 159
	1, 200		0, UNT		1.00		0.00	1.41		1,104		100
Mean	2 523	3 862	2 469	8 142	2.063	801	943	694	630	899	3 854	3 240
antonn	10,000	0,000	A, 100	0,110	-, 500	001	010	501	550	500	0,001	0, 10

*Sunday.

A description of this station, together with the estimated daily discharge as originally computed, June to December, 1899, will be found in Water-Supply Paper No. 35, page 52. A new rating table for the dam has been prepared, using coefficients of discharge derived from Freeman's experiments on a model of the round-crested portion of the Croton dam, which apparently corresponds closely with the ogee section of the Dolgeville dam, as regards friction on the crest, vertical contraction of the nappe, and siphonage.¹

In computing the record here given, the new rating table has been used, beginning June 1, 1899. The flow through the turbines has also been computed from current-meter measurements made in the tailrace of the electric power plant, instead of from the observed head and the gate openings of the water wheels, as formerly. The effect of these changes has been to slightly increase the extreme high-water and low-water flows, the estimated flow for mean stages remaining substantially the same.

EAST CANADA CREEK AT DOLGEVILLE, NEW YORK.

¹See Report on New York's Water Supply, made to Bird S. Coler, comptroller (1900), by John R. Freeman, p. 137.

Current-meter measurements were made from the bridge across the tailrace below the power plant, as follows:

Current-meter measurements of flow in tailrace at Dolgeville electric-light and power dam.

Date.	Flow in tail- race.	Gate open- ing of 36- inch wheels.	Wheel.
1900. May 22	Second-feet. 84	Per cent. 0, 50	No. 2.
July 27	76	. 38	No. 2.
July 29	63	. 28	No. 1.
August 9	80	. 38	No. 1.
-			

Only one of the two 36-inch Victor turbines was running in each instance, together with the 15-inch exciter wheel. The depths of gate openings of the 36-inch wheels are shown in the foregoing table. The 15-inch exciter wheel ran at thirteen-hundredths gate in each case. The head on the wheels was 72 feet. Observations of the wheel-gate openings were taken at the beginning and end of each test, and the average is given in the table.

The results of the current-meter measurements of the total flow of the stream have been given in the general table on page 39.

The relation between the metered and calculated flows on different days is shown in the following tables, from gage readings taken at the time the measurements were made:

	Date.	Flow in tail- race.	Flow over dam.	Total flow.
May 22	1900.	Second-feet. 84	Second-feet. 328	Second-feet. 412
July 27 August 7		76 80	376 a 28	$452 \\ 108$

Current-meter measurements of East Canada Creek.

a Measured in stream channel above point of confluence with tailrace.

Calculated flow of East Canada Creek.

Date.	Crest gage reading.	Flow over dam.	Flow in tail- race.	Total flow.
1900.	Feet.	Second-feet.	Second-feet.	Second-feet.
May 22	0.69	282	84	366
July 27	.79	362	84	446
August 7	.20	29	78	107

In the first two cases the total flow was measured at the Dolgeville bridge above the dam, and the difference between the observed and calculated flows in the first instance is probably due to pond storage.

The accompanying tables of mean daily flow show the amount of water passing down the stream from the dam each day, with the exception of Sundays, for which the flow has been taken as a mean between that of the preceding and following days. Dams on this stream are not numerous, nor is there extensive pond storage, so that the tables may be taken as a fair representation of the natural regimen of flow.

The highest water observed was on April 19, 1900, when a depth of 4.5 feet on the crest of the dam was reached, corresponding to a flow of 5,750 second-feet, or 22.6 second-feet per square mile. The most notable low-water period was September 13 to 16, inclusive, 1899, when the average volume of flow was 67 second-feet, or 0.3 second-foot per square mile.

Daily discharge, in second-feet, of East Canada Creek at Dolgeville, New York, for 1898.

[Drainage area, 256 square miles.]

Day.	Sept.	Oct.	Nov.	Dec.	Day.	Sept.	Oct.	Nov.	Dec.
1 2 3 5 6 7 8 9 10 13 14 15 16 17		$\begin{array}{c} 275\\ *330\\ 275\\ 270\\ 310\\ 290\\ 290\\ 290\\ 290\\ 290\\ 290\\ 290\\ 29$	$\begin{array}{c} 503\\ 478\\ 443\\ 363\\ 343\\ 8395\\ 398\\ 378\\ 398\\ 648\\ 333\\ 1, 937\\ *1, 620\\ 1, 360\\ 1, 160\\ 850\\ 590\end{array}$	$\begin{array}{c} 3722\\ 3722\\ 3722\\ *3722\\ *3722\\ (a)\\ (a)\\ (a)\\ (a)\\ (a)\\ (a)\\ (a)\\ (a)$	18 19 20 21 23 23 24 25 26 27 28 29 30 31 Mean	485 1,180 943 680 625 465 370 355 638	$\begin{array}{r} 465\\ 4457\\ 4477\\ 4477\\ 452\\ 637\\ *1,323\\ 1,082\\ 762\\ 1,222\\ 1,082\\ 877\\ *635\\ 602\\ \hline 581\\ \end{array}$	540 540 550 550 550 465 410 *305 235 235 279 689	$ \begin{array}{c} (a) \\ (a) \\ 400 \\ 650 \\ 775 \\ 975 \\ 975 \\ *700 \\ 600 \\ 600 \\ 500 \\ 400 \\ 450 \\ 600 \\ 564 \end{array} $

*Sunday.

a Ice on crest of dam.

Daily discharge, in second-feet, of East Canada Creek at Dolgeville, New York, for 1899.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
Day. 1 Day. 1 Day. 2 Day. 2 Day. 2 Day. 2 Day. 2	$\begin{array}{c c} & Jan. \\ & & \\ $	$\begin{array}{c c} Feb. \\ \hline \\ 472 \\ 447 \\ 492 \\ 437 \\ 397 \\ 397 \\ 372 \\ 372 \\ 372 \\ 372 \\ 372 \\ 372 \\ 372 \\ 372 \\ 372 \\ 372 \\ 372 \\ 397 \\ 1410 \\ 402 \\ 402 \\ 441 \\ 477 \\ 477 \\ 402 \\ 590 \\ 2397 \\ 142 \\ 51$	$\begin{array}{c c} \text{Mar.} \\ \hline \\ 542 \\ 442 \\ 422 \\ 4372 \\ 423 \\ 833 \\ 852 \\ 767 \\ 772 \\ 447 \\ 772 \\ 772 \\ 602 \\ 602 \\ 602 \\ 602 \\ 602 \\ 602 \\ 602 \\ 7002 \\ 672 \\ 8520 \\ 602 \\ 7002 \\ 672 \\ 8520 \\ 602 \\ 7002 \\ 672 \\ 8520 \\ 602 \\ 7002 \\ 672 \\ 8520 \\ 8520 \\ 7002 \\ 8520 \\ 7002 \\ 8520 \\ 8520 \\ 7002 \\ 8520 \\ 7002 \\ 8520$	Apr. 462 * 359 4152 552 922 * 752 922 * 752 9527 1.217 1.642 2.9727 * 2.552 2.6522 4.182 2.5622 4.182 2.5622 4.182 2.5622 3.4422 2.5622 3.4422 2.5622 3.4422 2.5622 3.4422 2.5622 3.4422 2.5622 3.4422 2.5622 3.4422 2.5622 3.4422 2.5622 3.4422 2.5622 3.4422	$\begin{array}{c} \text{May.} \\ \hline \\ 1,701\\ 1,401\\ 1,301\\ 1,206\\ 7711\\ * 4721\\ 421\\ 421\\ 421\\ 431\\ * 5341\\ 601\\ 5411\\ 741\\ * 674\\ 601\\ 541\\ 441\\ 741\\ * 674\\ 421\\ 371\\ 371\\ 371\\ 371\\ 371\\ 371\\ \end{array}$	$\begin{matrix} \text{June.} \\ \hline \\ & 384 \\ 294 \\ 218 \\ *212 \\ 206 \\ 200 \\ 194 \\ 194 \\ 194 \\ 194 \\ 194 \\ 194 \\ 194 \\ 194 \\ 206 \\ 264 \\ 249 \\ 175 \\ *134 \\ 206 \\ 174 \\ 127 \\ 152 \\ 1$	$\begin{array}{c} {\rm July.}\\ \hline \\ 116\\ *82\\ 79\\ 106\\ 103\\ 126\\ 215\\ *394\\ 270\\ 194\\ 194\\ 194\\ 194\\ 194\\ 175\\ 175\\ 126\\ 126\\ 112\\ 126\\ 110\\ 100\\ *112\\ 100\\ 100\\ 100\\ 101\\ 101\\ 101\\ 101\\ $	$\begin{array}{c} {\rm Aug.} \\ {\rm I18} \\ 192 \\ 210 \\ 139 \\ 999 \\ *81 \\ 112 \\ 106 \\ 12$	Sept. 109 145 * 145 * 145 * 145 * 78 * 78 * 78 * 78 * 78 * 67 * 67 * 67 * 67 * 67 * 67 * 74 * 74 * 74 * 1922	$\begin{array}{c} \text{Oct.} \\ \hline \\ & \\ & \\ & \\ & \\ & \\ & \\ & \\ & \\ &$	Nov. 1,046 1,674 372 3404 404 372 2828 2344 2444 2452 3444 1522 * 1445 14453 144545 144545 144556 1445656 1445666	Dec. 134 2922 * 335 338 2822 234 152 153 132 * 195 258 2.000 3.029 1.530 1.094 9.14 * 733 1.325 1.917 * 676 1.422 * 874 * 757 * 648 542 330
28 29 30 31	$ \begin{array}{c} $	742	492 472 492 472 472 472 472 472	3,592 3,017 *2,141	*324 391 373 421	144 119 119	$135 \\ 115 \\ * 101 \\ 87$	74 74 74 74 74	139 126 152	89 * 266 372 246	143 134 134	282 282 254 * 259
Mean	816	439	519	1,978	633	196	166	97	92	112	377	706

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1	264	288	252	* 631	1,476	(a)	* 130	153	132	120	(<i>a</i>)	(a)
2	264	288	240	794	1,188	(a)	112	126	* 151	185	242	*(a)
3	288	288	252	914	800	(a)	112	110	129	145	218	(a)
4	288	* 288	* 227	914	610	(a)	115	111	190	144	* 194	(a)
5	300	288	240	914	474	591	118	* 93	167	110	242	1,192
6	346	266	192	1,626	* 410	394	152	82	149	116	218	844
7	* 346	264	152	2,321	346	372	184	89	157	* 100	242	614
8	410	288	192	*2,714	4/4	608	* 193	98	118	94	632	614
9	410	710	238	1, 3/4	010	821	200	108	* 118	99	122	- * 577 014
10	312	×710	340	1,094 1,009	800	* 040	182	98	150	94	382	614
11	21.2	719	* 841	1,003	546	400	107	\$111	149	80	* 43% 200	219
1.9	300	3 759	270	1,012	* 454	276	120	111 *	140	0± 94	0 00	219
19	* 958	1 320	924	1,020	269	204	194	208	126	* 21	$\left\{ a \right\}$	994
14	264	2 467	234	*1 197	349	376	* 137	974	128	928	$\begin{pmatrix} a \\ a \end{pmatrix}$	210
16	252	1.632	192	1 374	342	335	150	250	* 93	205	(a)	* 89
17	240	1.232	152	1.926	288	* 304	162	185	117	199	(a)	63
18	682	* 939	*173	4.626	288	274	202	167	104	186	* (a)	210
19	546	646	262	5.335	288	256	190	* 133	95	180	(a)	215
20	960	562	306	4,917	* 264	256	158	92	73	185	1.005	345
21	*1,704	518	340	4,842	240	250	310	110	196	* 158	1,197	215
22	1,380	540	340	*4,368	288	246	* 252	111	184	153	1,148	215
23	1,144	709	340	3,895	288	326	194	142	*130	171	1,016	* 342
24	1,012	562	340	3,095	288	* 300	374	117	154	582	713	310
25	820	* 470	* 340	2,840	276	274	686	117	99	510	*1,146	438
26	709	378	306	2,355	264	294	767	*77	<i>(a)</i>	322	3,802	345
27	604	346	282	2,243	(a)	294	422	92	(a)	350	3,164	345
28	* 508	312	282	1,586	(a)	300	276	223	(a)	* 306	1,689	317
29	410		306	*1,506	(a)	300	* 219	136	(a)	292	1,128	317
30	346		420	1,207	(a)	149	162	181	* (a)	268	929	* 252
31	346		468		(a)		110	151		(a)		263
Mean	531	879	276	2,086	486	370	221	144	133	195	957	368

Daily discharge, in second-feet, of East Canada Creek at Dolgeville, New York, for 1900.

a No record.

* Sunday.

CAYADUTTA CREEK NEAR JOHNSTOWN, NEW YORK.

A description of this station will be found in Water-Supply Paper No. 35, page 53. The record is kept at the dam of the Johnstown Electric Light and Power Company, 1 mile below Johnstown. Since the establishment of the station standard sharp-crested gaging weirs have been erected by Prof. Olin H. Landreth, C. E. One of these weirs has been placed across the main stream above the head of slack water from the dam. A second weir has been placed in the tailrace below the power house.

During the summer the water does not ordinarily flow over the dam, which is practically tight, but the entire flow passes through the turbines. A series of gagings at the tailrace weir has been made in order to determine the discharging capacity of the water wheels when running under different conditions.

Dams are located at frequent intervals along the stream, and during the dry season the amount of flow from one to another is largely controlled by the water wheels.

NEW YORK.

Daily discharge, in second-feet, of Cayadutta Creek near Johnstown, New York, for 1898.

[Drainage area, 40 square miles.]

Day.	Oct.	Nov.	Dec.	Day.	Oct.	Nov.	Dec.
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	$\begin{array}{c} 24\\ *10\\ 22\\ 25\\ 119\\ 246\\ 67\\ 55\\ *14\\ 37\\ 23\\ 38\\ 290\\ *117\\ 68\end{array}$	$\begin{array}{c} 41\\ 36\\ 38\\ 38\\ 32\\ 39\\ *12\\ 32\\ 35\\ 55\\ 57\\ 179\\ 120\\ *64\\ 65\\ 55\\ 49\\ 57\end{array}$	$\begin{array}{c} 39\\ 48\\ 46\\ *51\\ 51\\ 50\\ 39\\ 88\\ *26\\ 38\\ 38\\ 38\\ 38\\ 33\\ 33\\ 34\\ \end{array}$	18 19 20 21 23 24 25 26 27 28 29 30 31 Mean	$\begin{array}{r} 47\\ 46\\ 39\\ 47\\ 55\\ *105\\ 88\\ 36\\ 58\\ 55\\ 138\\ *13\\ 41\\ 64\end{array}$	57 97 *67 50 54 63 55 55 55 54 42 *24 42 *24 42 42 42 91	$\begin{array}{c} * 27 \\ 333 \\ 55 \\ 58 \\ 98 \\ 98 \\ 98 \\ 67 \\ * 60 \\ 60 \\ 75 \\ 42 \\ 31 \\ 34 \\ 50 \\ 44 \\ 44 \\ \end{array}$

* Sunday.

Daily discharge, in second-feet, of Cayadutta Creek near Johnstown, New York, for 1899.

	Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
$-\frac{125450789}{101121344501789}$		$\begin{array}{c} * 20\\ 39\\ 31\\ 42\\ 71\\ 69\\ 40\\ *64\\ 42\\ 29\\ 243\\ *125\\ 51\\ 43\\ 35\\ 31\\ 33\\ 28\\ *16\\ 35\\ 35\\ \end{array}$	$\begin{array}{c} 275\\ 275\\ 299\\ *19\\ 299\\ 219\\ 18\\ 18\\ 18\\ 18\\ 20\\ *14\\ 245\\ 275\\ 335\\ 91\end{array}$	$\begin{array}{c} & & & \\$	72 *70 83 192 252 263 313 503 *320 413 579 415 811 751 802 *218 190 196 225 168 135 2168 135 225 2168 135 225 2168 135 225 2168 135 225 2168 2168 2168 2175 2168 2175 2175 2175 2175 2175 2175 2175 2175	577 566 362 2877 29 265 2877 29 265 2877 29 265 2877 29 265 2877 29 265 2877 479 * 258 284 283 284 284 284 285 284 284 284 285 284 284 284 284 285 284 284 284 285 284 284 284 285 284 284 284 285 284 284 284 285 284 284 284 284 285 284 284 284 284 285 284 284 284 284 284 284 284 284 284 284	30 28 29 * 17 29 28 18 30 21 19 * 18 30 224 25 225 * 17 5 37 323 322	$\begin{array}{c} 21\\ *15\\ 24\\ 17\\ 20\\ 19\\ 34\\ *16\\ 27\\ 25\\ 18\\ 16\\ 18\\ 13\\ 23\\ 25\\ 20\\ 19\\ 23\\ *8\\ *8\end{array}$	$\begin{array}{c c} & & & \\ & & &$	$\begin{array}{c} 16\\ 16\\ 20\\ *12\\ 19\\ 28\\ 16\\ 222\\ 17\\ *7\\ 16\\ 19\\ 20\\ *11\\ 19\\ 20\\ 21\\ 20\\ 21\\ 20\\ 17\\ 19\\ 19\\ 20\\ 21\\ 20\\ 17\\ 19\\ 19\\ 19\\ 19\\ 19\\ 19\\ 19\\ 19\\ 10\\ 10\\ 10\\ 10\\ 10\\ 10\\ 10\\ 10\\ 10\\ 10$	* 12 * 12 24 25 17 15 19 * 19 * 19 * 19 * 19 * 19 * 19 * 19 * 19 * 19 * 10 24 20 24 23 13 20 * 10 * 10	331 331 288 *34 *26 226 226 228 300 221 206 *2755	$\begin{array}{c} & & \\$
24 24 26 27 26 27 28 20 31		35 40 27 32 32 24 *13 33 33	91 39 40 * 43 53 48	$ \begin{array}{r} 74 \\ 59 \\ 52 \\ * 54 \\ 48 \\ 54 \\ 48 \\ 46 \\ 48 \\ 46 \\ 48 \end{array} $	* 123 41 65 66 44 52 60 * 31	$20 \\ 31 \\ 26 \\ 25 \\ 30 \\ *15 \\ 32 \\ 13 \\ 28 \\ -$	32 32 * 18 29 26 30 30 22	$ \begin{array}{r} 88 \\ 18 \\ $	$ \begin{array}{r} 14 \\ 16 \\ 14 \\ * 11 \\ 15 \\ 16$	$ \begin{array}{c} 19\\ * 14\\ 20\\ 32\\ 36\\ 26\\ 27\\ 26\\ \hline \\ \hline $	$\begin{array}{c} & & & \\$	$ \begin{array}{c} 25 \\ 24 \\ 26 \\ * 14 \\ 30 \\ 28 \\ 28 \\ 15 \\ $	
	Mean	39	31	74	251	31	26	20	18	20	21	26	49

*Sunday.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 10 17 18 10 17	$\begin{array}{c} 27\\ 27\\ 25\\ 20\\ 18\\ 20\\ *24\\ 60\\ 39\\ 43\\ 30\\ *14\\ 35\\ 37\\ 29\\ 40\\ \end{array}$	$\begin{array}{c} 39\\ 29\\ 22\\ *20\\ 251\\ 43\\ 42\\ 148\\ 235\\ 76\\ *82\\ 116\\ 1,404\\ 89\\ 77\\ 59\\ 46\\ *23\\ \end{array}$	$\begin{array}{c} 41\\ 42\\ 44\\ *23\\ 55\\ 41\\ 50\\ 45\\ 45\\ 45\\ 45\\ 44\\ *39\\ 66\\ 48\\ 40\\ 41\\ *19\\ 9\end{array}$	$\begin{array}{c} *250\\ 292\\ 339\\ 212\\ 199\\ 200\\ 293\\ *155\\ 102\\ 78\\ 77\\ 91\\ 106\\ 78\\ *91\\ 133\\ 200\\ 314\\ \end{array}$	38 255 225 228 224 300 225 81 83 263 263 24 293 263 24 293	36 28 30 25 25 25 24 31 29 24 29 24 29 24 29 24 29 24 24 29 24 24 29 24 24 29 24 24 29 24 24 29 24 29 24 29 24 29 29 29 29 29 29 29 29 29 29 29 29 29	*6 14 20 65 15 15 15 15 87 19 18 20 23 18 *12 20 18	$\begin{array}{c} 12\\ 22\\ 20\\ 18\\ *7\\ 20\\ 20\\ 22\\ 18\\ 14\\ 42\\ 27\\ 28\\ 29\\ 4\\ 35\\ 33\\ 28\\ 29\\ 4\\ 35\\ 33\\ 33\\ 33\\ 33\\ 33\\ 33\\ 33\\ 33\\ 33$	$\begin{array}{c} 11\\ *7\\ 21\\ 17\\ 17\\ 17\\ 17\\ 21\\ *8\\ 21\\ 20\\ 6\\ 7\\ 18\\ 16\\ *9\\ 19\\ 21\\ 21\\ \end{array}$
19. 20. 21. 22. 23. 23.	$92 \\ 705 \\ *306 \\ 101 \\ 83$			164 102 76 *116 92	$26 \\ *22 \\ 25 \\ 24 \\ 19$	$24 \\ 24 \\ 22 \\ 21 \\ 17$	17 14 19 *7 15 15	*10 18 21 20 91	19 21 21 21 21 *14
24 25 26 27 28 28 29 29	$55 \\ 71 \\ 50 \\ 43 \\ *23 \\ 44$				$ \begin{array}{r} 10 \\ 22 \\ 23 \\ 26 \\ *19 \\ 22 \\ 19 \\ 10 \\ 10 \\$	*10 17 19 14 17 19	$ \begin{array}{r} 19 \\ 18 \\ 17 \\ 26 \\ 25 \\ 26 \\ *13 \end{array} $	$22 \\ 22 \\ 22 \\ *7 \\ 20 \\ 19 \\ 20$	$ \begin{array}{c} 14 \\ 32 \\ 32 \\ 21 \\ 21 \\ 23 \\ 23 \\ 23 $
30 31 Mean	36 31 71	119	165 296 62	25 	20 22 22 27	18 21	13 13 13 17	20 18 20	*10

Daily discharge, in second-feet, of Cayadutta Creek near Johnstown, New York, for 1900.

* Sunday.

NOTE. -- Records for October, November, and December are not available at present.

SCHOHARIE CREEK AT FORT HUNTER, NEW YORK.

Schoharie Creek rises on the western slope of the Catskill Mountains. In its lower stages it flows through a long, flat valley, in a stream bed covered with cobbles and gravel, over which the water finds its way in a thin sheet during the dry season.

The State dam at Fort Hunter is near the mouth of the stream, and high water from Mohawk River backs up to the toe of the dam. The condition existing at this station during the summer months has been described in connection with the Mohawk River gaging stations, page 42. A record has been kept of the elevation of the water surface in the pond above the dam, and also in the channel below the dam. The average difference, or head, is 5.25 feet, and it is nearly constant, except when water falls below the crest level above the dam.

The dam is of timber backed with gravel, and there are a number of leaks above the gravel line 2 feet below the crest. During the summer this leakage represents practically the total inflow from Schoharie Creek to the Mohawk. Current-meter measurements of the leakage were made below the Erie Canal aqueduct, at a point where the entire flow is concentrated in a narrow channel.

Current-meter measurements of leakage of Fort Hunter dam.

Date.	Hydrographer.	Leakage.
1900. June 21. July 18. August 22	R. E. Horton E. D. Walker do	Second-feet. 30 38 44

In the computation the leakage of the dam has been assumed to be 35 second-feet.

In establishing this station the intention was to maintain a record of the height of the water above and below the head gates, at the entrance to the canal feeder, from which the effective head of the gate openings could be determined and the flow computed by the formula for submerged orifices. During the dry season the water falls below the lip of the gates and flows in an open channel, making this method inapplicable. In recomputing the record the diversion to the canal feeder was estimated from the following current-meter measurements:

Current-meter measurements of flow of water in feeder.

Date.	Hydrographer.	Measured flow.
1900. June 21. July 18. August 22	R. E. Horton E. D. Walker do	Second-feet. 112 76 73

Inflow to the Erie Canal is controlled by gates at the lower end of the feeder channel, so that the flow in the feeder is not directly a function of the stage of the water. Owing to the uncertainty of the low-water measurements, this station was abandoned July 31.

The accompanying tables show the total outflow from the pond above the Fort Hunter dam. A table of the flow, as originally computed, allowing 315 second-feet for leakage, will be found in Water-Supply Paper No. 35, page 55.

The drainage areas tributary to Schoharie Creek at various gaging stations are as follows:

Drainage areas of Schoharie Creek.

	Squ	are mile	es.
At mouth	~	947	. 0
At Erie Canal aqueduct		946	. 8
At Fort Hunter dam		946	.7
At Mill Point bridge		934	. 0
At Schoharie Falls dam		930	. 0

Daily discharge, in second-feet, of Schoharie Creek at Fort Hunter, New York, for 1898.

Day.	Sept.	Oct.	Nov.	Dec.	Day.	Sept.	Oct.	Nov.	Dec.
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16		$\begin{array}{c} 161\\ 161\\ 161\\ 161\\ 1,661\\ 3,211\\ 1,361\\ 791\\ 1,761\\ 791\\ 611\\ 611\\ 581\\ 1,661\\ 2,136\\ 2,461\end{array}$	$\begin{array}{c} 1, 617\\ 1, 717\\ 917\\ 767\\ 767\\ 767\\ 767\\ 667\\ 5, 067\\ 9, 517\\ 5, 767\\ 2, 917\\ 2, 967\\ 2, 917\\ 2, 967\\ 1, 817\\ 1, 817\end{array}$	$\begin{array}{c} 1,139\\939\\1,339\\1,439\\1,639\\1,639\\1,639\\1,839\\1,839\\1,739\\1,239\\9399\\1,539\\1,639\\1,539\\1,639\\1,639\\1,639\end{array}$	18 19 20 21 22 23 24 25 26 27 28 29 30 31	129 129 129 129 129 129 129 129 129 129	$\begin{array}{c} 791\\ 861\\ 791\\ 791\\ 791\\ 1.061\\ 861\\ 861\\ 861\\ 1.361\\ 2.261\\ 1.911\\ 1.561\\ 1.661\\ \end{array}$	$\begin{array}{c} 1,517\\ 2,417\\ 3,967\\ 2,842\\ 2,067\\ 1,967\\ 1,967\\ 1,517\\ 1,517\\ 1,517\\ 1,517\\ 1,217\\ 767\\ 767\\ 767\\ \end{array}$	$\begin{array}{c} 1,539\\ 859\\ 689\\ 814\\ 1,639\\ 2,639\\ 2,089\\ 3,289\\ 814\\ 1,539\\ 1,539\\ 939\\ 1,239\\ 3,864\\ \hline\end{array}$
17		711	1,517	1,339	hittin	INC	1,110	<i>w</i> , 110	1,010

[Drainage area, 947 square miles.]

Daily discharge, in second-feet, of Schoharie Creek at Fort Hunter, New York, for 1899.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.
1	1,741	1,651	4,915	1,335	1,515	295	182	148	148	3,867	935
2	1,641	1,351	3,655	1,335	1,460	295	178	152	148	1,967	1,615
3	1,641	1,651	3,165	1,335	1,560	395	182	145	145	1,767	1,515
£	941	1,251	2,935	2,135	1,140	395	182	138	145	2,247	935
ð	5,791	1,201 051	19,035	2, 185	860	295	185	$142 \\ 145$	148	2,467	930
0	2 541	951	10,000	3,100 3,655	210	205	100	148	140	1,907	035
8	3 141	851	3 435	7 685	585	225	195	138	142	1,547	935
9	3, 541	901	2.935	5, 335	585	205	198	138	152	1.767	785
10	2,241	901	3,535	3,655	610	195	185	135	152	967	765
11	1,991	851	4,085	4,585	440	195	182	138	152	967	935
12	1,641	851	7,685	5,735	440	195	190	138	148	1,547	1,615
13	1,841	657	11,135	7,685	340	195	198	132	148	1,547	1,835
14	1,841	701	4,455	7,635	260	195	202	132	145	1,967	1,515
10	2,091	801	3,175	9,335	200	190	202	100	140	1, 047	1,515
10	2,041 2,901	901	2,000	1,080	0±0 480	199	198	100	198	3, 41 067	900
18	2 741	1 551	2 035	1 085	585	195	202	138	145	797	765
19	2.291	1.751	2.335	4, 385	510	195	195	142	145	587	765
20	2.341	1.551	2,515	3,812	585	195	195	145	148	967	765
21	1,991	3,151	2,775	3,532	585	195	190	142	148	797	635
22	1,641	2,876	2,775	2,342	510	195	185	148	148	587	635
23	1,541	3,407	2,775	3,532	440	195	185	148	148	967	453
24	1,541	3,726	2,635	3,342	340	195	165	142	148	1 000	453
20	2,741	3,720	2,510	3,193	340	195	198	145	100	1,907	515
30	2 001	4,801	2,000	9,800	260	199	185	149	6 984	2,107	495
61 98	1 841	$\frac{4}{6},005$	2 135	2 698	260	195	182	148	6,126	1 547	335
29	1.541	0,000	1, 435	2,298	340	195	190	145	5, 740	1,967	335
30	1,641		1,335	2.948	260	195	190	148	4,790	2,147	295
31	1,541		1,435		260		190	145		1,547	
Mean	2,307	1,944	3, 792	4,100	579	226	187	142	916	1,603	875

NOTE .- No record for December.

٩
Day.	Jan.	Mar.	Apr.	May.	June.	July.
Day.	$\begin{array}{c} \text{Jan.}\\ \hline\\ & 735\\ 575\\ 575\\ 575\\ 435\\ 4435\\ 4435\\ 4435\\ 4435\\ 3455\\ 4435\\ 515\\ 5755\\ 5775\\ 5755\\ 5775\\ 5755\\ 577$	Mar. 3,4465 7,335 7,515 6,785 5,585 2,485 3,335 2,740 3,335 2,740 3,335 2,740 3,335 2,740 3,335 2,255 2,255 2,255 2,255 2,255 2,255 2,1755 1,755 2,405 2,135 1,755 2,405 2,2635 2,405 2,2635 2,405 2,2635 2,405 2,2635 2,405 2,2635 2,405 2,2635 2,405 2,2635 2,405 2,2635 2,405 2,2635 2,405 2,2635 2,405 2,2635 2,405 2,2635 2,2655 2,2655 2,2405 2,405	A pr. 2,915 3,635 3,335 3,335 3,335 3,335 3,335 2,635 2,495 2,1135 2,015 2,915 2,915 2,915 3,4,735 6,615 6,615 6,6615 6,6615 2,905 2,935 2,935 2,935 2,935 2,935 2,949 3,4,735 5,635 2,949 3,535 2,945 2,915 3,535 2,955 2	$\begin{array}{c} \text{May.}\\ & 835\\ 985\\ 835\\ 985\\ 985\\ 1, 208\\ 409\\ 412\\ 409\\ 415\\ 519\\ 412\\ 330\\ 300\\ 293\\ 312\\ 330\\ 300\\ 293\\ 312\\ 330\\ 1, 550\\ 1, 520\\ 1, 550\\ 1, 500\\ 1, 550\\ 1, 500\\ 1, 550\\ 1, 500\\ 1, 550\\ 1, 500\\ 1, 550\\ 1, 500\\ 1, 500\\ 1, 550\\ 1, 500\\ $	June. 360 155 245 245 245 245 245 245 2515 276 305 305 257 2560 2600 2600 2600 2600 2601 2657 255 276 305 305 305 305 257 258 2957 295 295 295 295 295 295 295 295 295 147 143 139 139 122	$\begin{array}{c} \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\$
9 		$ \begin{array}{c} 2,113 \\ 3,035 \\ 3,035 \\ 3,035 \\ 3,035 \end{array} $	1, 885 1, 325	200 322 555 360	122 122 122	118 118 118 111
Mean	1,313	3,137	3, 530	561	219	115

Daily discharge, in second-feet, of Schoharie Creek at Fort Hunter, New York, for 1900,

NOTE.-No record for February; station abandoned July 31.

SCHOHARIE CREEK AT ERIE CANAL AQUEDUCT, NEW YORK.

The Erie Canal crosses Schoharie Creek between the Fort Hunter dam and Mohawk River. A gaging station was established at the aqueduct on May 2, 1900, by Prof. E. D. Walker. A current-meter measurement of the flow through the archways of the canal aqueduct was made by him on that day, the result being a discharge of 1,257 second-feet, with a gage height of 2.26 feet. Owing to cross currents above the aqueduct, the conditions are not favorable for meter measurements, and the station was abandoned on October 13. The record is chiefly of interest in connection with slope measurements of Mohawk River, described elsewhere (p. 42).

Daily gage height,	in feet,	of Schoharie	Creek at	Erie Canal	aqueduct, N	ew York,
		fo	r 1900.		-	í.

Day.	May.	June.	July.	Aug.	Sept.	Oct.	Day.	May.	June	July.	Aug.	Sept.
$\begin{array}{c} 1 \\ 2 \\ 3 \\ 4 \\ 5 \\ 6 \\ 7 \\ 8 \\ 9 \\ 10 \\ 11 \\ 12 \\ 13 \\ 14 \\ 15 \\ 16 \\ 16 \\ 16 \\ 16 \\ 10 \\ 10 \\ 11 \\ 11$	$\begin{array}{c} 2.24\\ 2.20\\ 2.14\\ 2.10\\ 2.00\\ 1.10\\ 2.00\\ 1.97\\ 2.00\\ 1.97\\ 1.89\\ 1.76\\ 1.70\\ 1.67\\ \end{array}$	$\begin{array}{c} 1.38\\ 1.47\\ 1.76\\ 1.62\\ .94\\ .95\\ .87\\ .90\\ 1.90\\ 1.84\\ 1.80\\ 1.40\\ 1.68\\ 1.40\\ 1.13\\ 1.20\\ \end{array}$	$\begin{array}{c} 0.60\\ .62\\ .58\\ .60\\ .60\\ .57\\ .50\\ .43\\ .52\\ .60\\ .63\\ .64\\ .60\\ .54\\ .53\end{array}$	$\begin{array}{c} 0.\ 67\\ .\ 65\\ .\ 64\\ .\ 63\\ .\ 62\\ .\ 52\\ .\ 52\\ .\ 51\\ .\ 52\\ .\ 53\\ .\ 52\\ .\ 53\\ .\ 53\end{array}$	$\begin{array}{c} 0.54\\ .53\\ .54\\ .53\\ .54\\ .54\\ .54\\ .64\\ .64\\ .65\\ .65\\ .65\\ .64\\ .65\\ .64\end{array}$	$\begin{array}{c} 0.53 \\ .54 \\ .51 \\ .53 \\ .58 \\ .61 \\ .62 \\ .58 \\ .54 \\ .52 \\ .59 \\ .56 \\ .57 \\ \hline \end{array}$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 1.58\\ 1.52\\ 1.47\\ 1.98\\ 2.84\\ 2.43\\ 2.14\\ 1.93\\ 1.87\\ 1.80\\ 1.67\\ 1.40\\ 1.47\\ 1.45\\ 1.40\\ \end{array}$	$\begin{array}{c} 0.82\\ .71\\ .82\\ .70\\ .72\\ .70\\ .60\\ .60\\ .60\\ .62\\ .61\\ .60\\ \end{array}$	$\begin{array}{c} 0.58 \\ .56 \\ .60 \\ .61 \\ .63 \\ .65 \\ .68 \\ .71 \\ .73 \\ .78 \\ .72 \\ .60 \\ .63 \\ .64 \end{array}$	$\begin{array}{c} 1.43\\ 1.32\\ 1.92\\ .97\\ .78\\ .64\\ .63\\ .54\\ .53\\ .54\\ .53\\ .54\\ .53\\ .54\end{array}$	$\begin{array}{c} 0.65\\ .65\\ .65\\ .65\\ .65\\ .65\\ .64\\ .62\\ .53\\ .53\\ .53\\ .52\\ .53\\ .52\\ .53\end{array}$

SCHOHARIE CREEK AT MILL POINT, NEW YORK.

The current-meter station was established at the Mill Point highway bridge on July 5, 1900, by Prof. E. D. Walker. The stream bed is stony and fairly permanent. The channel is of nearly constant width at all stages of the stream. The following current-meter measurements were made by Professor Walker:

July 5: Gage height, 0.64 foot; discharge, 87 second-feet. August 22: Gage height, 0.70 foot; discharge, 141 second-feet.

Daily gage height, in feet, of Schoharie Creek at Mill Point, New York, for 1900.

Day. Ji	uly. Aug	. Sept.	Oct.	Nov.	Dec.	Day.	July.	Aug.	Sept.	Oet.	Nov.	Dec.
1	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 0.35\\ .35\\ .35\\ .35\\ .22\\ .22\\ .40\\ .30\\ .25\\ .45\\ .45\\ .35\\ .35\\ .35\\ .35\end{array}$	$\begin{array}{c} 0.50\\ .50\\ .45\\ .40\\ .45\\ .35\\ .30\\ .15\\ .00\\ .00\\ .35\\ .45\\ .15\\ .30\\ .30\\ \end{array}$	$\begin{array}{c} 0.55\\ .45\\ .60\\ .60\\ .60\\ .60\\ .60\\ .60\\ .60\\ .60$	$\begin{array}{c} 2.10\\ 1.90\\ 1.80\\ 1.70\\ 2.60\\ 2.35\\ 2.25\\ 2.10\\ 1.80\\ 1.75\\ 1.75\\ 1.72\\ 1.70\\ 1.65\\ 1.60\end{array}$	17	$\begin{array}{c} 0.60\\ .65\\ .65\\ .65\\ .65\\ .90\\ .90\\ .80\\ .80\\ .80\\ .80\\ .80\\ .80\\ .70\\ .65\end{array}$	$\begin{array}{c} 0.95\\ 1.45\\ .95\\ .72\\ .70\\ .75\\ .70\\ .60\\ .55\\ .50\\ .45\\ .50\\ .50\\ .50\\ .55\\ .43\end{array}$	$\begin{array}{c} 0.35\\ .30\\ .35\\ .25\\ .00\\ .00\\ .00\\ .30\\ .30\\ .30\\ .30\\ .35\\ .45\\ .45\\ .45\\ \end{array}$	$\begin{array}{c} 6.40\\ .45\\ .45\\ .45\\ .45\\ .30\\ .60\\ .60\\ .60\\ .60\\ .70\\ .75\\ .52\\ .45\\ .52\\ .50\\ \end{array}$	$\begin{array}{c} 0.65 \\ .70 \\ .75 \\ .98 \\ 1.42 \\ 1.50 \\ 1.35 \\ 1.35 \\ 1.30 \\ 1.72 \\ 3.60 \\ 2.75 \\ 2.25 \\ 2.15 \end{array}$	$\begin{array}{c} 1.65\\ 1.70\\ 1.82\\ 1.95\\ 2.30\\ 2.10\\ 1.70\\ 1.88\\ 2.95\\ 3.70\\ 1.70\\ 1.95\\ 1.50\\ 1.60\end{array}$

SCHOHARIE CREEK AT SCHOHARIE FALLS, NEW YORK.

A dam and power plant have been erected by the Empire State Power Company, of Amsterdam, New York, at Schoharie Falls, 7 miles from Amsterdam. The dam is of masonry, backed with timber. It has a flat crest, nearly level, 380 feet long, 1 foot wide, and a slope on the upstream face of approximately $2\frac{1}{2}$ to 1. The dam was completed early in the summer of 1900, and a record of the depth of water flowing over the main spillway was kept by the engineers of the company from July 18 to December 31. Some further data are needed,

however, for the final reduction of this record, which is reserved for future publication. The dam is about 1 mile above the current-meter station on Schoharie Creek, at the Mill Point highway bridge, and it is the intention to use the results of the meter measurements made there in the preparation of a calibration curve for the spillway of the dam.

Soon after the completion of the dam a weir of standard form was placed in an opening in the water-power canal embankment, at a point where the entire flow of the stream could be concentrated so as to pass over the gaging weir. The weir has a sharp crest, 25 feet in length, with two complete contractions, and the following observations of flow were computed from the observed depths by the Francis formula:

Date.	Time of measure- ment.	Discharge.	Date.	Time of measure- ment.	Discharge.
1900, June 25 June 26 Do June 27 Do June 28 Do June 29 June 29	11 a. m. 11 a. m. 5 p. m. 11 a. m. 5 p. m. 11 a. m. 5 p. m. 11 a. m.	$\begin{array}{c} Second-feet.\\ 86.2\\ 91.6\\ 91.5\\ 92.9\\ 92.9\\ 92.9\\ 86.2\\ 91.5\\ 86.2 \end{array}$	1900. June 29 June 30 Do July 1 Do July 2 Do July 3	5 p. m. 11 a. m. 5 p. m. 11 a. m. 5 p. m. 11 a. m, 5 p. m. 9 a. m.	Second-feet. 86.2 92.9 92.9 92.9 92.9 91.5 91.6 92.9 93.4

Flow over weir at Schoharie Falls dam.

The power plant at the dam contains two double horizontal Samson turbines, each 40 inches in diameter. The turbines are designed to work under a head of 42 feet, and are rated at 1,800 horsepower per pair. A wheel similar to these has been tested at Holvoke, and with the rating curve established, which shows the proportional discharge of the wheels for various depths of gate opening, the turbines can be used as water meters to determine the flow in the power canal. The plant was set in operation about January 1, 1901, and a gaging record is being kept, which shows the depth of flow over the crest of the dam and spillway, the discharge through the flood gates, and the amount of water used by the turbines. It should be stated that this stream is subject to extreme variations of flow, and that the weir measurements given above represent unusually low water. Plans have been made for a system of storage reservoirs to conserve the entire discharge of the stream and maintain a nearly uniform regimen of flow throughout the year.

MOHAWK RIVER AT SCHENECTADY, NEW YORK.

A current-meter station at Freeman's tollbridge, near Schenectady, was established by Prof. E. D. Walker February 1, 1899, and

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remained under his supervision until October 1, 1900. A description of this station is contained in Water-Supply Paper No. 35, page 55. The following current-meter measurements were made by Professor Walker:

April 3, 1899: Gage height, 7.18 feet; discharge, 5,294 second-feet. May 26, 1899: Gage height, 6.22 feet; discharge, 2,092 second-feet. June 30, 1899: Gage height, 5,38 feet; discharge, 482 second-feet. May 12, 1900: Gage height, 6.50 feet; discharge, 4,135 second-feet. July 17, 1900: Gage height, 5.26 feet; discharge, 667 second-feet. August 21, 1900: Gage height, 5.40 feet; discharge, 976 second-feet.

A rating curve for the cross section at this station has not yet been prepared.

Daily gage height, in feet, of Mohawk River at Schenectady, New York, for 1900.

Day.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1		7.407.407.10 6.90	5.50 5.50 5.50 5.75	5.22 5.20 5.22 5.18	5.38 5.35 5.25 5.23	5.35 5.25 5.22 5.22 5.22	5.20 5.25 5.20 5.20 5.25	5.55 5.60 5.58 5.50	7.80 7.35 7.00 6.75
5 6	$\frac{11.15}{10.05}$	$\begin{array}{c} 6.80 \\ 6.65 \\ 6.45 \\ 6.20 \\ 6.45 \end{array}$	5.65 5.55 5.60 5.40 5.60	5.15 5.20 5.20 5.20 5.20 5.25	$5.25 \\ 5.20 \\ 5.15 \\ 5.18 \\ 5.10$	5.10 5.15 5.22 5.15 5.15 5.18	5.20 5.20 5.02 5.10 5.18	5.45 5.42 5.35 5.35 6.40	$ \begin{bmatrix} 8.75 \\ 8.85 \\ 8.15 \\ 8.00 \\ 7.70 $
10. 11. 12. 13. 14. 14.	8.85 8.18 7.90 8.25 8.15	$\begin{array}{c} 6.70\\ 6.70\\ 6.50\\ 6.25\\ 6.10\\ 0.05\\ \end{array}$	$\begin{array}{r} 6.45 \\ 6.00 \\ 5.75 \\ 5.60 \\ 5.55 \end{array}$	5.35 5.40 5.35 5.32 5.30	$5.08 \\ 5.10 \\ 5.10 \\ 5.10 \\ 5.10 \\ 5.15 $	5.05 5.10 5.15 5.10 5.10 5.10	5.10 5.10 5.18 5.15 5.25	$7.05 \\ 6.60 \\ 6.15 \\ 5.85 \\ 5.80 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\$	$\begin{array}{c c} 7.25 \\ 6.75 \\ 6.15 \\ 6.70 \\ 6.85 \end{array}$
10. 16. 17. 18. 19. 20.	$\begin{array}{r} 7.80 \\ 8.10 \\ 8.50 \\ 10.65 \\ 12.05 \\ \end{array}$	$\begin{array}{c} 6.05 \\ 6.00 \\ 6.05 \\ 6.00 \\ 6.95 \\ 6.95 \end{array}$	5.50 5.50 5.45 5.42 5.35 5.35	5.30 5.28 5.29 5.20 5.23	5.25 6.25 5.90 5.80 5.62	5.08 5.10 5.05 5.08 5.00	5.15 5.18 5.20 5.20 5.42 5.42	5.75 5.70 5.65 5.50 5.60	6.20 6.00 5.85 5.95 5.90
202 212 222 232 242	$ \begin{array}{c} 11.90\\ 11.68\\ 10.85\\ 11.65\\ 11.90\\ 10.05 \end{array} $	6.03 6.50 6.20 6.10 5.95 5.00	5.22 5.25 5.35 5.35 5.22	5.35 5.40 5.70 5.58 5.42	$ \begin{array}{r} 5.40 \\ 5.32 \\ 5.25 \\ 5.20 \\ 5.25 \\ 5.20 \\ 5.25 \\ 5.20 \\ 5.25 \\ 5.20 \\ 5.25 \\ 5.20 \\ 5.25 \\ 5.25 \\ 5.20 \\ 5.25 \\ 5.25 \\ 5.25 \\ 5.20 \\ 5.25 \\ 5.25 \\ 5.20 \\ 5.25 \\ 5.25 \\ 5.25 \\ 5.25 \\ 5.25 \\ 5.25 \\ 5.25 \\ 5.25 \\ 5.25 \\ 5.20 \\ 5.25 \\ $	5.05 5.08 5.10 5.10 5.70 5.52	$ \begin{array}{r} 5.35 \\ 5.20 \\ 5.18 \\ 5.20 \\ 5$	5.80 6.95 7.60 7.30 7.00 6.70	$\begin{array}{c} 6.00 \\ 6.15 \\ 6.20 \\ 6.10 \\ 6.10 \\ 6.70 \end{array}$
25	$ \begin{array}{r} 10.05 \\ 9.35 \\ 8.60 \\ 8.25 \\ 7.72 \end{array} $	$5.90 \\ 5.75 \\ 5.70 \\ 5.55 \\ 5.50 \\ 5.50 \\ 0.50 \\ $	5.20 5.20 5.18 5.20 5.20 5.22	5.43 5.38 6.15 6.05 5.72	5.25 5.28 5.22 5.20 5.20 5.25	5.53 5.45 5.22 5.28 5.28	$5.28 \\ 6.15 \\ 6.00 \\ 5.70 \\ 5.65 $	$\begin{array}{r} 6.70 \\ 8.48 \\ 11.65 \\ 11.35 \\ 10.05 \end{array}$	$ \begin{array}{r} 6.70 \\ 8.00 \\ 7.60 \\ 7.08 \\ 6.70 \\ \end{array} $
30 31	7.45	$5.45 \\ 5.50$	5.20	$5.55 \\ 5.50$	$5.20 \\ 5.45$	5.22	$5.75 \\ 5.65$	8.50	6.40 6.25

MOHAWK RIVER AT REXFORD FLATS, NEW YORK.

This station, which is located at the New York State feeder dam 4 miles below Schenectady, is described in Water-Supply Paper No. 35, page 57.

The accompanying tables of daily and monthly mean flow include the amount diverted to the Erie Canal. They therefore represent the total inflow of Mohawk River at this point, which is considerably greater than the amount which passes downstream from the dam during the season of canal navigation. Prior to 1900 the amount of diversion to the Erie Canal was assumed to be 128 second-feet. During the present year a different method of estimating diversion to the canal has been used. Current-meter measurements in the Rexford Flats feeder gave the following results:

Date.	Hydrographer.	Flow in canal feeder.
October 27, 1898 June 25, 1900	W. D. Lockwood R. E. Horton	Second-feet. 128 272

Current-meter measurements in Rexford Flats feeder.

These results were compared with the mean rate of evaporation from a water surface, as determined for several years at Rochester,¹ and it was found that an apparently constant relation existed between the two. The diversion for the remaining months of the canal season has been estimated from the observed evaporation, as follows:

Estimated monthly flow in Rexford Flats feeder.

	Secon	id-feet
May	8	200
June	%	260
July	8	290
August	%	270 -
September	8	220
October	1	148

The flow over the dam—that is, the amount of water passing downstream from Rexford Flats—compares with the total flow as follows:

Table showing relation of flow over Rexford Flats dam to total inflow of feeder.

. Month.	Total in- flow.	Flow below dam (inflow less diver- sion).
1900.	Second-feet.	Second-feet.
May	2,857	2,657
June	1,503	1,243
July	1,447	1,157
July	1,746	1,476
September.	981	761

The water did not fall below the crest of the dam during the summer of 1900, so that it was not possible to make measurements of the leakage, or a new profile of the crest, which is greatly needed. During high water for several days of the year 1900 the water on the downstream side of the dam rose above the crest level and the dam was completely submerged. Experiments on the flow over a similar submerged weir are not available, and the high-water flows have been taken from the usual discharge curve. On the morning of February

¹See annual reports of the executive board of the city of Rochester, 1892 to 1899, inclusive.

14, 1900, the water attained a depth of 9.25 feet on the crest of the dam, corresponding to a discharge of 55,700 second-feet, or 16.5 second-feet per square mile. This is the highest water observed since the record was started.

During 1900 the following discharge measurements were made by Prof. E. D. Walker, at Freeman's bridge, 3 miles above the Rexford Flats gaging station:

May 12: Gage height, 6.50 feet; discharge, 4,135 second-feet. July 17: Gage height, 5.26 feet; discharge, 667 second-feet. August 21: Gage height, 5.40 feet; discharge, 976 second-feet.

Daily discharge, in second-feet, of Mohawk River at Rexford Flats, New York, for 1898.

Day.	Dec.	Day.	Dec.	Day.	Dec.	Day.	Dec.
8 9. 10. 11. 12. 13. 14.	5,050 5,050 5,050 5,450 4,200 3,625 5,250	$\begin{array}{c} 15\\ 16\\ 17\\ 18\\ 19\\ 20\\ 21\\ \end{array}$	$\begin{array}{c} 4,959\\ 3,250\\ 2,450\\ 2,300\\ 2,675\\ 2,550\\ 2,300\\ 2,300\end{array}$	22 23 24 25 26 27 28	$\begin{array}{c} 2,850\\ 5,150\\ 11,550\\ 9,350\\ 7,350\\ 4,450\\ 4,900 \end{array}$	29 30 31 Mean	$3,3502,4001,800\overline{4,471}$

[Drainage area, 3,385 square miles.]

Daily discharge, in second-feet, of Mohawk River at Rexford Flats, New York, for 1899.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	$\begin{array}{c} 9,000\\ 4,850\\ 3,350\\ 3,650\\ 9,350\\ 12,550\\ 9,350\\ 7,925\\ 4,850\\ 3,600\\ 2,850\\ 2,850\\ 3,825\\ 4,650\\ 5,400\\ 5,400\\ 5,400\\ 5,400\\ 5,400\\ 5,400\\ 2,850\\ 9,200\\ 5,405\\ 8,750\\ 9,200\\ 5,405\\ 2,850\\ 2$	$\begin{array}{c} 2,950\\ 3,440\\ 4,350\\ 3,950\\ 3,950\\ 3,950\\ 2,700\\ 2,600\\ 2,400\\ 2,850\\ 3,350\\ 3,340\\ 2,700\\ 2,400\\ 2,400\\ 2,400\\ 2,200\\ 2,400\\ 2,250\\ 2,600\\ \end{array}$	$\begin{array}{c} 6,300\\ 5,750\\ 5,750\\ 6,920\\ 25,700\\ 15,110\\ 9,770\\ 8,350\\ 7,000\\ 9,160\\ 20,670\\ 10,950\\ 10,950\\ 10,950\\ 10,950\\ 5,750\\ 5,470\\ 8,250\\ 13,560\\ 12,660\\ 12$	5,850 6,350 5,270 7,880 10,510 14,050 14,050 18,330 21,770 21,500 24,040 29,550 23,350 20,350 20,350 20,350 20,350 21,150 21,628	$\begin{array}{c} 9,828\\ 8,828\\ 8,428\\ 8,528\\ 5,828\\ 5,828\\ 5,178\\ 2,628\\ 2,328\\ 2,178\\ 2,428\\ 2,2328\\ 2,178\\ 2,428\\ 2,2078\\ 1,578\\ 1,678\\ 1,978\\ 1,778\\ 1,678\\ 6,828\\ 2,028\\ 6,828\\ 2,178\\ 1,778\\ 1,66\\ 8,28\\ 1,978\\ 1,778\\ 1,66\\ 8,28\\ 1,978\\ 1,778\\ 1,66\\ 1,28\\ 1,978\\ 1,66\\ 1,28\\ 1,978\\ 1,778\\ 1,66\\ 1,28\\ 1,978\\ 1,778\\ 1,66\\ 1,28\\ 1,978\\ 1,778\\ 1,66\\ 1,28\\ 1,978\\ 1,778\\ 1,66\\ 1,28\\ 1,978\\ 1,778\\ 1,66\\ 1,28\\ 1,978\\ 1,778\\ 1,97$	$\begin{array}{c} 2,288\\ 2,288\\ 2,078\\ 2,078\\ 2,078\\ 1,538\\ 1,538\\ 1,538\\ 1,538\\ 1,538\\ 1,378\\ 1,28\\ 1,28\\ 1,28\\ 928\\ 1,038\\ 1,038\\ 1,038\\ 1,038\\ 1,038\\ 1,038\\ 1,28\\ 928\\ 3,528\\ 4,628\\ 3,528\\ 4,628\\ 3,298\\ 3,528\\ 4,628\\ 3,288\\ 4,628\\ 3,288\\ 3,528\\ 4,628\\ 3,288\\ 3,528\\ 4,628\\ 3,288\\ 3,528\\ 4,628\\ 3,288\\ 3,528\\ 4,628\\ 3,288\\ 3,528\\ 4,628\\ 3,288\\ 3,528\\ 4,628\\ 3,288\\ 3,288\\ 4,628\\ 3,288\\ 3,288\\ 4,628\\ 3,288\\ 3,288\\ 4,628\\ 3,288\\ 4,628\\ 3,288\\ 4,628\\ 3,288\\ 4,628\\ 3,288\\ 4,628\\ 3,288\\ 4,628\\ 3,288\\ 4,628\\ 3,288\\ 4,628\\ 3,288\\ 4,628\\ 3,288\\ 4,628\\ 3,288\\ 4,628\\ 4,628\\ 3,288\\ 4,628\\ 4,6$	928 928 679 608 608 608 438 608 528 328 328 328 328 328 328 328 328 328 3	328 328 438 528 438 528 528 278 278 278 278 278 278 278 278 278 2	201-1 2025 - 202	$\begin{array}{c} 2,728\\ 2,928\\ 2,928\\ 2,928\\ 2,928\\ 2,628\\ 2,628\\ 2,628\\ 2,328\\ 2,178\\ 1,428\\ 728\\ 728\\ 728\\ 728\\ 728\\ 728\\ 1,828\\ 1,828\\ 1,828\\ 1,828\\ 1,348\\ 1,348\\ 1,348\\ 1,348\\ 1,348\\ \end{array}$	$\begin{array}{c} 1,368\\ 1,368\\ 2,928\\ 5,028\\ 6,528\\ 6,528\\ 6,528\\ 6,528\\ 6,528\\ 6,528\\ 6,528\\ 2,928\\ 2,7928\\ 2,7928\\ 2,778\\ 2,178\\ 1,578\\ 2,778\\ 1,578\\ 1,368\\ 1,368\\ 1,368\\ 1,368\\ 1,368\\ 1,128\\ 1,228\\ 1,478\\ 1,228\\ 1,478\\ $	$\begin{array}{c} 1,328\\ 1,328\\ 1,328\\ 3,208\\ 2,908\\ 2,908\\ 3,578\\ 4,548\\ 6,078\\ 8,958\\ 10,828\\ 8,958\\ 10,828\\ 21,358\\ 24,228\\ 15,828\\ 24,228\\ 19,128\\ 13,128\\ 8$
22 23 24 25 26 27 27 28 28 29 30 31	2,850 2,750 3,050 3,450 4,300 4,475 4,950 4,750 5,575 4,850	2,000 5,450 10,150 5,750 5,550 4,650 7,000	$\begin{array}{c} 12,000\\ 11,400\\ 6,460\\ 7,050\\ 6,740\\ 5,370\\ 4,750\\ 4,650\\ 5,560\\ 5,170\\ \end{array}$	$\begin{array}{c} 19,228\\ 17,878\\ 17,878\\ 17,878\\ 17,878\\ 17,028\\ 16,428\\ 16,428\\ 16,428\\ 15,668\\ 11,148\\ \end{array}$	0, 628 6, 728 5, 428 4, 928 4, 378 3, 128 2, 228 1, 828 2, 778 2, 778 2, 778	a, 225 2, 168 2, 168 2, 078 1, 538 1, 538 1, 538 1, 428 1, 538	328 308 288 288 328 328 438 328 328 378 338	228 228 228 228 278 278 278 238 208 208 208 208	218 278 278 3,228 9,178 6,328 1,678 2,778	$1,348 \\ 1,228 \\ 1,148 \\ 1,128 \\ 1,028 \\ 828 \\ 728 \\ 1,228 \\ 1,228 \\ 1,348 \\ $	$\begin{array}{c} 1,448\\ 1,578\\ 1,578\\ 1,468\\ 1,368\\ 1,368\\ 1,128\\ 1,128\\ 1,128\\ 1,368\\ \hline\end{array}$	$\begin{array}{c} 4,926\\ 4,578\\ 4,578\\ 2,428\\ 2,928\\ 2,928\\ 2,928\\ 2,828\\ 2,828\\ 2,628\\ 2,428\\ 2,228\end{array}$
Mean .	5,739	3,935	9,004	17,057	4,084	2,014	498	294	980	1,608	2,824	7,001

_										
	Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.
1		2 030	2 850	4 650	8 750	5 500	1 470	1 500	1.970	1.920
2		1,500	1.860	4,650	9,400	4.800	1,470	940	1.830	1,670
3		1.500	2,030	4,450	11,150	4, 150	1.580	940	1.720	1.670
4		1,260	3,830	4,450	11,400	3,300	1,710	940	1.720	1,540
5		1,260	4,450	4,450	12,850	2,850	1,710	820	1,720	1,430
6.		1,500	4,950	4,800	13,550	3,000	1,470	750	1,970	1,430
7.		1,860	5,550	3,325	13,850	3,450	1,470	750	1,720	1,430
8.		2,250	7,150	3,000	14,650	3,300	1,710	820	1,970	1,020
9.		2,550	7,250	2,250	15,070	3,800	1,710	1,090	1,970	1,020
10.		2,550	7,950	2,250	15,950	4,400	1,960	1,090	1,970	1,120
11.		1,860	10,730	1,860	17,150	3,800	2,240	1,290	1,970	-1,220
12		1,610	13,050	1,610	18,300	3,650	2,910	1,500	1,970	1,020
13.		1,500	27,250	1,500	15,650	3,300	2,240	1,500	1,970	870
14.		1,500	45,050	1,500	13,850	3,300	1,580	1,290	2,250	870
15.		1,860	24,850	1,370	9,390	3,800	1,580	1,290	2,390	430
16.		2,700	14,850	1,260	9,000	3,300	1,580	1,290	2,470	430
17.		3,830	9,650	1,160	12,350	3,000	1,710	1,090	5,020	680
18.		6,500	5,750	1,160	20,750	2,850	1,710	1,090	1,830	680
19.		10,730	3,150	1,750	27,450	2,700	1,470	1,090	1,830	750
20.		21,850	2,470	3,150	25,550	2,250	1,260	1,090	1,970	870
\mathbb{Z}^{1} .	•	45,750	3,830	3,950	26,250	2,250	1,260	1,400	1,070	870
64. 00		27,850	5,100	4,800	28,370	1,750	1,260	1,610 1,740	1,070	1 080
25.		28,400	0,090	4,800	26,000	1,000	1,000	1,740	1,070	1,030
24.		21,700	8,750	5,150	21,730	1,000	1,000 1,000	1,990	1,270	1,030
20. 00		13, 300	4,800	3,930	11,000	1,000	1,000	2,270	1,170	100
20.		9,200	5,150	7,700	11,900 11,400	1,000	1,000 1,000	2,210	1,070	080
41 - 60		5,100	3,150	7,700	0,850	1,900	1,000	9 200	1 000	540
40. 90		5,150 5,150	4,000	9 430	9,000	1,000	010	2 270	1,000	600
30		4 450		8 550	7 250	1 495	910	2 270	1,070	540
31	*****	4 250		8 750	1,600	1 425	310	1,990	1 170	040
or.		T , #00		0,100		1, 1.0		1,009	1,110	
	Mean	7, 860	9,032	4,235	14,996	2,857	1,503	1,447	1,746	981

Daily discharge, in second-feet, of Mohawk River at Rexford Flats, New York, for 1900.

Note.- Records for October, November, and December are not available at present.

MOHAWK RIVER NEAR DUNSBACH FERRY, NEW YORK.

A gaging record has been kept at the dam of the West Troy Water Company near Dunsbach Ferry, 9 miles from the mouth of Mohawk River. The dam is of masonry, and has a flat granite crest 5.5 feet wide, standing 0.75 foot higher at the crest lip than at the upstream edge. An island in the center of the stream divides the dam into two sections. The crest of the right wing, at the upper end of the island, is 380 feet long, with an average elevation of 174.15 feet. The crest of the left wing, at the lower end of the island, is 280 feet in length, and stands at an elevation of from 173.46 to 173.50 feet. Openings which existed in the dam during a part of the time the record has been kept should be taken into consideration in computing the flow.

The crest of the dam at the present time stands nearly level. The elevation of the zero of the crest gage is 172 feet. Readings are taken twice daily, usually between 6 and 7 a. m. and between 5 and 6 p. m. The mean of the readings taken for each day is given in the accompanying table.

In the adjacent pumping station are two Eclipse turbines, built by Stout, Mills & Temple, of Dayton, Ohio. One is 68 and the other 72 inches in diameter. They are run with gates wide open, under a head of from 7 to 8 feet. The record at Dunsbach Ferry was established primarily for the purpose of checking a system of levels which were run for the United States Board of Engineers on Deep Waterways, by D. J. Howell, C. E., who furnished the record to the Geological Survey. No record was kept from April 1, 1899, to July 31, 1900.

The drainage area above the station at Dunsbach Ferry is 3,422 square miles.

Daily gage height, in feet, of Mohawk River near Dunsbach Ferry, New York, for 1898.

$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	Day.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
$\begin{array}{cccccccccccccccccccccccccccccccccccc$			4.00	3.20	3.00	1.40	2.50	2.80	2.40	3.60	3.20
$\begin{array}{cccccccccccccccccccccccccccccccccccc$			3.60	3.10	2.70	1.00	5.50	2.40	2.40	3.40	3.10
$\begin{array}{cccccccccccccccccccccccccccccccccccc$			3.20	3.20	2.40	. 60	2.20	2.20	2.40	3.20	-3.00
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$			2.80	$\frac{5.00}{4.20}$	2.40	. 40	2.60	2.20	2.60	3.00	3.00
$\begin{array}{cccccccccccccccccccccccccccccccccccc$			2.60	4.20	2.20	. 00	3.50	2.20	5.80	3.00	3.40
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$			2.50	4.20	2.00	10	3.00	2.40	4.20	3.00	3.30
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$			2.60	3.50	1.80	10	2.40	2.60	3.30	3.00	3.20
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	· · · · · · · · · · · · · · · · · · ·		2.60	3.10	1.70	, 10	2.00	3.00	3.20	3.10	-3.20
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$			2.40	2.60	1.70	20	1.60	2.70	3.10	3.30	-3.20
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		7 60	2.40	2.40	1.80	30	1.50	2.30	2.80	6.80	3.10
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		8.20	2.40	3.60	2.70	60	1.20	1.80	2.70	5.50	2.90
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		8.40	2,50	3.80	3,40	60	1.00	1.60	2.80	4.90	2.80
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		7.50	2.60	3.40	3.10	60	. 90	1.40	3.60	4.40	2.80
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		6.40	2.80	3.00	2.90	60	.80	1.30	4.90	4.00	-2.80
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		5.60	3.00	2.80	2.69	80	1,40	1.30	4.30	3.60	2.80
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	• • • • • • • • • • • • • • • • • • • •	5.30	2.80	2.00	2.20	70	2.40	1.20	3.40	3.60	2.80
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		6.50	2.80	2.50	2.00	1.70	2.90	1.80	3.30	4.80	-2.80
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		6.20	3.20	2.60	2.60	2.20	3.40	2.20	3.30	4.30	2.80
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		5.40	3.30	2.60	2.20	1.90	2.90	2.00	3.40	3.80	3.00
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		4.80	3.40	2.40	2.20	1.70	2.60	2.00	4.00	3.70	3.60
4.10 4.00 3.00 1.80 20 0.10 3.00 4.00 3.80 4		4.80	4.70	2.50	2.00	. 80	3.00	2.20	4.20	3.80	4.60
26 380 680 180 190 640 320 380 250 4		4.10	6.80	0.00 4 80	1.80	20	6.40	3.20	4.00	3.80	4.00
3.60 6.20 7.20 1.70 1.20 5.20 2.80 4.40 3.50 3.50		3.60	6.20	5.20	1.70	1.20	5.20	2.80	4.40	3.50	3.80
28		3.60	5.00	5.20	1.60	1.80	4.00	2.8)	5.40	3.00	3.40
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		4.00	4.30	4.00	1.40	1.60	3.20	2.60	5.00	3.00	3.00
30		4.80	3.70	3.40	1.40	1.20	2.80	2.50	4.30	3.00	2.80
31 4.70 3.29 $.60$ 2.80 3.80 3		4.70		3.20		. 60	2.80		3.80		3.20

Daily gage height, in feet, of Mohawk River near Dunsbach Ferry, New York, for 1899.

$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	Day.
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1

			_								
Day.	Aug.	Sept.	Oct.	Nov.	Dec.	Day.	Aug.	Sept.	Oct.	Nov.	Dec.
1 2 3 4 5 6 7 8 9 10	$\begin{array}{c} 2.30\\ 2.20\\ 2.10\\ 2.00\\ 2.10\\ 2.00\\ 2.00\\ 1.90\\ 1.80\\ 1.80\\ 1.80\\ \end{array}$	$\begin{array}{c} 2.20\\ 2.20\\ 2.10\\ 2.00\\ 2.00\\ 1.80\\ 1.80\\ 1.80\\ 1.90\\ 2.00\\ \end{array}$	$\begin{array}{c} 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 1.90\\ 1.80\\ 1.70\end{array}$	$\begin{array}{c} 2.40\\ 2.40\\ 2.45\\ 2.35\\ 2.30\\ 2.20\\ 2.15\\ 2.20\\ 2.85\\ 3.55\end{array}$	$\begin{array}{r} 3.75\\ 3.70\\ 3.55\\ 3.50\\ 4.80\\ 4.80\\ 4.40\\ 4.40\\ 4.20\\ 3.70\end{array}$	17	$\begin{array}{c} 2.70\\ 2.60\\ 2.40\\ 2.30\\ 2.20\\ 2.20\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.20\end{array}$	$\begin{array}{c} 1.80\\ 1.80\\ 1.60\\ 1.60\\ 1.70\\ 1.80\\ 2.00\\ 2.50\\ 2.40\\ 2.20\\ \end{array}$	$\begin{array}{c} 2.00\\ 2.20\\ 2.20\\ 2.20\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.75\end{array}$	$\begin{array}{c} 2.45\\ 2.35\\ 2.40\\ 2.50\\ 3.50\\ 4.00\\ 3.80\\ 3.45\\ 3.30\\ 4.10\end{array}$	$\begin{array}{c} 2.85\\ 2.80\\ 2.90\\ 2.90\\ 2.85\\ 2.80\\ 2.90\\ 2.90\\ 3.35\\ 4.25\end{array}$
11 12 13 14 15 16	$\begin{array}{c} 1.80 \\ 1.80 \\ 1.80 \\ 1.90 \\ 2.20 \\ 2.80 \end{array}$	$\begin{array}{c} 2.00\\ 2.20\\ 1.70\\ 1.70\\ 1.70\\ 1.70\\ 1.70\end{array}$	$\begin{array}{c} 1.70 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.90 \\ 1.90 \\ 1.90 \end{array}$	$\begin{array}{c} 3.10\\ 2.90\\ 2.75\\ 2.55\\ 2.50\\ 2.50\\ 2.50\end{array}$	$\begin{array}{c} 3.25 \\ 3.00 \\ 3.25 \\ 3.20 \\ 3.10 \\ 2.95 \end{array}$	27 28 29 30 31	$\begin{array}{c} 2.20 \\ 2.10 \\ 2.00 \\ 2.00 \\ 2.20 \end{array}$	2.20 2.20 2.00 2.00	$\begin{array}{c} 2.75 \\ 2.50 \\ 2.45 \\ 2.50 \\ 2.40 \end{array}$	6.50 6.35 5.50 4.50	$\begin{array}{c} 3.75 \\ 3.55 \\ 3.35 \\ 3.20 \\ 3.10 \end{array}$

Daily gage height, in feet, of Mohawk River near Dunsbach Ferry, New York, for 1900.

INDIAN RIVER AT INDIAN LAKE DAM, NEW YORK.

Indian River, a tributary of the upper Hudson, has a precipitous forested mountain area of 146 square miles in eastern Hamilton County. In 1898 a masonry storage dam was built at the foot of Indian Lake, replacing the lumbermen's dam which was formerly there, and raising the level of the artificial lake so formed 23 feet. The storage capacity of the present lake is 5,000,000,000 cubic feet, the area of its water surface is 5,035 acres, and the elevation of the spillway crest above mean tide is 1,650 feet. The dam was built by a federation of water-power users on Hudson River, in cooperation with the State of New York, under the direction of Mr. George W. Rafter, engineer in charge, the primary object being to store flood waters from this drainage area, to be turned into the Hudson during the low-water period of the year, thereby equalizing to some extent the flow of that Water is also used for sluicing logs during the river driving stream. season.1

Since July 22, 1900, a gaging record has been kept at the dam, with a view to determining the total outflow from this reservoir. The facts recorded are the elevation of the water surface in the reservoir, the depth of water flowing over the spillway or flashboards, the depth of opening and the head on the main and subsidiary logways, and the depth of the opening and the effective head on each of the 5-foot sluice gates. These data enable a calculation of the outflow from the reservoir to be made, and, by comparison with gaging records kept on Hudson River at Fort Edward and Mechanicsville, the effect of storage on the lowwater flow of the latter river can be determined.

A meteorological station has been established at the dam by the United States Weather Bureau, and records are kept of the rainfall, temperature, etc. The regimen of flow of Indian River below the dam is largely artificial, though in the course of a year or more the total annual run-off of the drainage area will appear in the stream, and it is hoped, in the course of time, to determine the relation between the rainfall and run-off of what constitutes a rather typical Adirondack watershed.

When the reservoir is full the excess of inflow passes over the spillway, which has a level crest 106.05 feet long in the clear. To facilitate the calculation of discharge over this spillway a series of experiments was made at Cornell University June 6, 1899, on a full-sized model of the spillway section (6.58 feet long), from which the proper coefficients of discharge have been determined.¹

The discharge through the two 5-foot sluice gates, provided for the purpose of drawing the water down as required, is calculated from the observed head and from the area of the lune-shaped gate orifices by the ordinary formula, the value of the coefficients of discharge to be applied being checked by current-meter measurements made at a convenient bridge below the dam.

A meter measurement of the flow at this point on October 19, 1900, showed the rate of draft from the reservoir to be 451 second-feet, both sluice gates being wide open and under an effective head of 11 feet. A measurement of Hudson River at Mechanicsville, made on the afternoon of the following day, October 20, showed the total flow at that point to be 1,871 second-feet.

The following table shows the stage of the Indian Lake reservoir during the year 1900, the depth being measured from the base of the invert of the 5-foot discharge tunnels, also the estimated storage capacity of the reservoir at different depths:

Water surface.	Elevation.	Area.	Storage capacity.
Original lake	${}^{Feet.}_{1,616-17}_{1,627}_{1,650}_{1,651.1}$	Acres.	Cubic feet.
Lumbermen's dam		1,000	800, 000, 000
Crest of present dam		3,007	4, 468, 000, 000
Top of flashboards of present dam		5,035	5, 000, 000, 000

Estimated storage capacity of Indian Lake reservoir.

Depth of water, in feet, in Indian Lake reservoir, New York, for 1900.

		and the second se
Day, July, Aug. Sept. Oct. Nov. Dec. Day, July, Aug. Sept. Oc	. Nov.	Dec.
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	10. 83 11. 68 11. 25 11. 58 11. 83 12. 08

¹ Proc. Am. Soc. Civ. Engs., March, 1900, p. 288.

SCHROON RIVER AT WARRENSBURG, NEW YORK.

A gaging record was established at the dam of the Schroon River Pulp Company, 2 miles below Warrensburg, by George W. Rafter, member American Society of Civil Engineers, November 1, 1895, in connection with the upper Hudson storage surveys.¹ The conditions at the Warrensburg gaging station are somewhat peculiar. During ordinary water an attempt is made to turn the entire flow of the stream, less leakage, through the water wheels, which run 24 hours a day, Sundays excepted. This is accomplished by the use of flashboards and by draft from the storage impounded by the Starbuckville dam. During extreme low water the mill is shut down altogether. As a rule, no water passes over the dam at this time, the entire flow leaking through. A balance is maintained between the inflow and the outflow by fluctuations in the pond level, thereby varying the pond storage and also the head on the leaks. As no record is kept when the mill is not running, it has been necessary to estimate the low-water flow, which was taken at 150 second-feet in 1899, this being the assumed leakage of the Starbuckville dam.² The apparently uniform regimen of the stream during considerable periods may be accounted for as the result of draft and storage from the Starbuckville dam.

A current-meter measurement of the leakage of the dam, flume, and flashboards at the Schroon River Pulp Company's mill was 'made on August 9, 1900, in the open channel about a half mile below the dam. The flow at that point was found to be 285 second-feet, which amount has been taken as the low-water flow and leakage during the present year (1900). The dam is of timber, and was considered nearly watertight when built, but there is evidence that the leakage has increased year by year.

The flow over the dam without flashboards has been taken from a diagram deduced from experiments made at Cornell University on a weir having a similar cross section. The flow over the flashboards has been calculated by means of Francis's formula, with a constant coefficient of 3.33.

¹Ann. Rept. State Engineer and Surveyor of New York, 1895, p. 118; also Water-Supply and Irrigation Paper U. S. Geol. Survey No. 35, p. 58.

²Report on a water supply from the Adirondack Mountains for the city of New York, by Geo. W. Rafter: Rept. of Merchants' Association of New York on the water supply of the city of New York, p. 337.

Daily discharge, in second-feet, of Schroon River at Warrensburg, New York, for 1899.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1	* 641	478	478	708	4,854	1,506	304	150	150	* 381	1,468	708
3	641	478	478	* 708	4,804 4,854	1,506	* 304	150	150	381	1,468 1,468	* 708
4	641	478	478	708	4,854	*1,367	301	150	150	381	1,468	708
5	641	* 478	* 478	708	4,854	1,228	304	150	150	478	* 1,468	708
6	641	478	478	708	4,854	1,228	304	* 150	150	478	1,468	708
7	608	478	478	708	* 4,487	1,228	304	150	150	478	1,468	708
9	575	478	478	*1 999	4, 121	1,228	* 304	150	150	478	1,408 1 318	708
10	575	478	478	3,291	4, 121	1,228	304	150	* 150	478	1.318	* 708
11	575	478	478	3,291	4,121	*1,228	304	150	150	478	1,171	708
12	575	* 478	* 478	3,291	4,121	1,228	304	150	150	478	*1,106	708
13	575	478	478	3,291	3,493	1,228	150	* 150	150	478	1,041	931
15	* 611	410	478	3,291	° 0, 004 	1,220 1,208	150	150	150	418	980	985
16	641	478	478	* 3. 362	3, 121	1,228	* 150	150	150	478	861	1, 101
17	641	478	478	3,443	2,931	1,228	150	150	* 150	478	841	* 1, 127
18	641	478	559	3,443	2,931	* 1,228	150	150	150	478	841	1,153
19	641	* 478	* 641	3,443	2,931	1,228	150	150	150	478	* 841	1,153
20	641	178	641	3,443 9,449	2,381	1,228	150	* 150	381	478	841	1,153 1,159
99	* 575	478	641	3,443	1 981	1,840	150	150	381	*178	.041	1,100
23	575	478	641	* 4. 273	1,981	1.228	* 150	150	381	478	841	1,153
24	575	478	718	5,103	1,981	970	150	150	* 381	478	841	*1,153
25	575	478	718	5,103	1,981	* 675	150	150	381	478	841	1,153
26	575	* 478	* 718	5,103	1,981	381	150	150	381	478	* 774	1,153
31 90	575	478	718	$ \begin{array}{c} 9,100 \\ 5,102 \end{array} $	$^{1,000}_{*1.448}$	381	150	* 100 150	281	418	708	1,101
29	* 575	710	718	5,103	1,391	381	150	150	381	* 478	708	1,041
30	575		718	* 5, 103	1,391	381	* 150	150	381	478	708	1,041
31	575		718		1,391		150	150		478		*1,041
Mean	606	478	564	2,877	3,150	1,093	210	150	234	462	1,047	948

[Drainage area, 563 square miles.]

* Sunday.

Daily discharge, in second-feet, of Schroon River at Warrensburg, New York, for 1900.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1 2 3 5 6 7 9 10 12 13 14 15 16 17 18 19	810 810 810 810 810 810 810 810	$\begin{array}{c} 810\\ 810\\ 810\\ 810\\ 810\\ 810\\ 810\\ 810\\$	$\begin{array}{c} 1, 360\\ 1, 290\\ 1, 230\\ *1, 204\\ 1, 178\\ 1, 178\\ 1, 123$	$\begin{array}{c} x pi. \\ x 1, 162 \\ 1, 215 \\ 1, 315 \\ 1, 535 \\ 1, 535 \\ 1, 535 \\ 1, 535 \\ 1, 741 \\ *1, 947 \\ 2, 155 \\ 2, 205 \\ 2, 465 \\ *2, 765 \\ 3, 065 \\ 3, 305 \\ 3, 535 \\ 3, 535 \\ 3, 535 \\ 3, 535 \\ 3, 545 \\ 3, 565 \\ 3,$	3,965 2,885 2,625 2,155 *2,045 1,748 1,715 1,715 1,715 1,715 1,585 1,585 1,585 1,555 1,555	$\begin{array}{c} & 1,085\\ 1,217\\ *1,349\\ 1,565\\ 1,990\\ 1,890\\ 1,890\\ 1,890\\ 1,890\\ 1,890\\ 1,890\\ 1,890\\ 1,890\\ 1,300\\ 1,290\\ 1,30\\ 1,300\\ $	* 885 810 810 810 810 810 810 810 810 810 810	285 285 285 285 285 285 285 285 285 285	285 285 285 285 285 285 285 285 285 285	2855 5355 5355 5355 5355 5355 5355 5355	517 517 517 *285 535 535 535 535 535 517 *285 535 535 535 535 535 535 535 535 535 5	939 *285 989 989 989 989 989 989 989 989 989 9
20 21 22 23 24 25 26 27 28 29 30 31 	830 *810 810 810 810 810 810 810 810 810 810	$1,795 \\ 1,710 \\ 1,608 \\ 1,608 \\ 1,608 \\ *1,571 \\ 1,535 \\ 1,475 \\ 1,435 \\ \hline$	$1,107 \\ 1,100 \\ 1,089 \\ 1,085 \\ 1,085 \\ 1,085 \\ 1,085 \\ 1,155 \\ 1,155 \\ 1,130 \\ 1,11$	5,365 7,010 *7,745 6,945 6,945 6,210 6,685 6,315 5,365 *5,095 4,825	$\begin{array}{c} *1,470\\ 1,415\\ 1,375\\ 1,355\\ 1,295\\ 1,295\\ 1,295\\ 1,025\\ 1,085\\ 1,085\\ 1,085\\ 1,085\\ \end{array}$	963 963 963 963 963 963 963 963 963 963	365 285 285 285 285 285 285 285 285 285 28	806 806 806 612 612 *285 285 285 285 285 285 285 285	285 285 285 285 285 285 285 285 285 285	517 *285 535 535 535 517 517 517 *285 535 535 535	535 535 535 574 285 *285 806 806 806 806 806	788 788 788 788 285 788 788 788 788 788 788 788 788 788
Mean	810	1,380	1,140	3,688	1,688	1,280	528	474	285	488	530	773

NEW YORK.

HUDSON RIVER AT FORT EDWARD, NEW YORK.

This station, located at the dam of the International Paper Company, was established in 1895, by George W. Rafter, member American Society of Civil Engineers, in connection with upper Hudson storage surveys. The dam is of timber, on slate rock foundation, and has but little leakage. The crest is straight, very nearly level, and 587.6 feet in length. The zero of the crest gage stands at the level of the lip of the dam proper. Flashboards from 15 to 18 inches in height are usually maintained on the dam. A record is kept of the heig⁻ht of the flashboards and of the times of their setting and removal.

In the adjoining mill there are 62 water wheels, nearly all of modern types, which have been tested at the Holyoke flume. A record is kept of the daily run of each wheel, in hours, as well as of the working head, which usually is 19 feet. The discharge through the turbines is estimated from diagrams expressing the flow as a function of the working head and the number of wheel-hours run.

In the winter of 1896–97 a flood spillway was cut around the south end of the dam, over which the water flows whenever it reaches the level of the crest of the flashboards. The profile of the spillway is very irregular, and causes some uncertainty in the calculated flows during high water.

When the flashboards are off the flow is computed by means of the East Indian Engineers' formula;¹ when they are on the flow is computed by Francis's well-known formula for sharp-crested weir. During the dry season little water passes over the dam, the entire flow being employed to drive the turbines. A current-meter measurement was made at the highway bridge below the dam on July 26, 1900, and the flow was found to be 2,704 second-feet.

¹ Mullin's Irrigation Manaal.

Daily discharge, in second-feet, of Hudson River at Fort Edward, New York, for 1899.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1	*2,415 2,619 2,619 2,619 2,877 2,877 4,330 3,876 2,944 3,876 3,876 2,944 3,876 3,876 3,876 3,876 3,876 3,876 3,876 3,876 5,388 5,388 5,388	$\begin{array}{c} 2,822\\ 2,822\\ 2,502\\ 2,606\\ *945\\ 1,839\\ 1,539\\ 1,539\\ 1,539\\ 1,539\\ 1,539\\ 1,539\\ 1,539\\ 1,539\\ 2,109\\ 2,109\\ 2,109\\ 2,109\\ 2,109\\ 2,109\\ 2,109\\ 2,109\\ 2,109\\ 2,109\\ 1,504\\ *1,150\\ 1,652\\ *1,150\\ 1,652\\ *1,150\\ 1,652\\ *1,150\\ 1,652\\ *1,150\\ $	$\begin{array}{c} & & \\ & & \\ 3,744 \\ 3,744 \\ 5,7$	$\begin{array}{c} A \mathrm{pr}, \\ 6, 514 \\ *1, 600 \\ 4, 378 \\ 4, 378 \\ 4, 378 \\ 4, 378 \\ 4, 378 \\ 4, 654 \\ *1, 560 \\ 4, 334 \\ 4, 654 \\ 4, 334 \\ 9, 202 \\ 9, 967 \\ 17, 428 \\ 17, 406 \\ *20, 095 \\ 21, 222 \\ 21, 800 \\ 97 \\ 050 \end{array}$	$\begin{array}{c} \text{May.}\\ \hline \\ 23,038\\ 23,033\\ 23,033\\ 28,033\\ 19,689\\ 21,949\\ 81$	3,106 3,1063,106 3,1063,106 3,106 3,106 3,106 3,106 3,1063,106 3,106 3,106 3,1063,106 3,106 3,106 3,1063,106 3,106 3,106 3,1063,106 3,106 3,106 3,1063,106 3,106 3,1063,106 3,106 3,1063,106 3,106 3,1063,106 3,106 3,1063,106 3,106	583 *945 945 945 583 289 762 *100 1,547 1,547 1,817 1,817 1,817 1,817 1,817 1,817 1,817	A fug. 363 363 363 363 363 363 363 a(a) (a)	923 923 *20 1,186 1,186 1,184 1,184 1,184 1,184 920 920 *20 975 867 631 620 577 *20 624 624 624 577	$\begin{array}{c} & & \\$	Nov. 9, 268 11, 948 12, 250 9, 402 5, 668 5, 668 6, 149 *1, 8923 3, 153 3, 133 3, 133 *2, 90	$\begin{array}{c} 1,941\\1,941\\1,941\\4,267\\4,307\\4,243$
20 21 22 23 24 25 26 26 27 28 29 30 31 30 Mean .	$\begin{array}{c} 5,388\\ 5,388\\ 5,388\\ *1,356\\ 3,491\\ 3,776\\ 3,618\\ 3,623\\ 3,623\\ 3,623\\ 3,041\\ *925\\ 2,816\\ 2,816\\ 3,527\end{array}$	1,682 1,682 1,682 2,012 2,308 1,600 *1,600 2,853 2,842	$\begin{array}{c} 6,099\\ 6,229\\ 6,229\\ 6,229\\ 5,703\\ 5,703\\ *2,415\\ 5,444\\ 5,506\\ 5,506\\ 5,506\\ 5,506\\ 5,005\\ \end{array}$	$\begin{array}{c} 27,059\\ 29,545\\ 29,618\\ *25,640\\ 32,158\\ 32,158\\ 32,159\\ 29,619\\ 29,619\\ 29,620\\ 27,032\\ *23,120\\ \hline \\ 16,811 \end{array}$	$\begin{array}{r} 8,617\\ *700\\ 4,864\\ 4,184\\ 4,282\\ 3,901\\ *1,356\\ 3,104\\ 3,104\\ \hline 9,561\\ \end{array}$	$1,454 \\988 \\752 \\590 \\8747 \\1,329 \\894 \\888 \\585 \\583 \\\hline1,617 \\$	$\begin{array}{c} 1,817\\ 1,645\\ 1,645\\ *465\\ 1,368\\ 1,300\\ 1,103\\ 1,275\\ 1,275\\ *20\\ 461\\ \hline 1,150\\ \end{array}$	$\begin{array}{r} * 20 \\ 1,176 \\ 1,176 \\ 1,176 \\ 916 \\ 916 \\ 916 \\ * 574 \\ 1,176 \\ 576 \\ 576 \\ 948 \\ \hline 714 \end{array}$	$577 \\ 954 \\ 1,024 \\ * 20 \\ 1,184 \\ 3,404 \\ 4,889 \\ 4,889 \\ 4,181 \\ 4,181 \\ 1,347 \\ 1,347 \\ 1,347 \\ 1,024 \\ 1$	$\begin{array}{r} 861\\ 1,184\\ *20\\ 1,446\\ 1,439\\ 923\\ 918\\ 919\\ 919\\ *20\\ 1,183\\ 1,183\\ 1,033\\ \end{array}$	$\begin{array}{c} 2,900\\ 2,900\\ 2,900\\ 2,580\\ 2,311\\ 2,044\\ *20\\ 2,311\\ 2,206\\ 2,206\\ 2,206\\ 2,206\\ 5,098\end{array}$	$\begin{array}{c} 8,574\\ 8,574\\ 8,574\\ 8,220\\ *2,415\\ 2,415\\ 4,809\\ 4,234\\ 4,234\\ 4,234\\ 4,234\\ *20\\ \hline 5,157\end{array}$

[Drainage area, 2,800 square miles.]

* Sunday.

a No record.

Daily discharge, in second-feet, of Hudson River at Fort Edward, New York, for 1900.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oet.	Nov.	Dec.
Day. 1 2 3 5 6 7 8 9 10 12 13 14 15 16 17 18 9	3,001 1,957 1,957 1,957 2,053 *1,401 2,217	$\begin{array}{c} \textbf{r} \text{ eb.} \\ \hline \\ 3, 481 \\ 3, 221 \\ 3, 221 \\ 3, 221 \\ 2, 961 \\ 2, 447 \\ 2, 447 \\ 2, 447 \\ 2, 447 \\ 2, 447 \\ 3, 221 \\ 3, 889 \\ * 2, 062 \\ 4, 136 \\ 7, 369 \\ * 13, 069 \\ 16, 615 \\ 17, 747 \\ 18, 499 \\ 18, 975 \\ * 13, 045 \\ 15, 531 \end{array}$	Mar. 2, 879 4, 232 *3, 019 4, 462 3, 859 3, 741 3, 471 4, 208 *3, 259 3, 743 3, 759 3, 759 3, 759 3, 759 3, 759 3, 659 3, 759 3, 759 3, 759 3, 759 3, 759 3, 759 3, 759 3, 741 3, 005 5, 759 3, 741 3, 005 3, 759 3, 759 3, 741 3, 005 3, 759 3, 759 3, 759 3, 741 3, 005 3, 759 3, 759 3, 741 3, 005 3, 759 3,	Apr. *3,237 4,932 5,261 5,701 5,701 7,376 10,566 *11,636 11,636 10,776 *9,922 10,776 12,946 17,076 23,626	$\begin{array}{c} \text{may.}\\ \hline\\ 12,486\\ 11,899\\ 10,776\\ 11,626\\ 9,646\\ *3,015\\ 7,351\\ 8,246\\ 8,3015\\ 5,836\\ 6,608\\ *4,450\\ 5,361\\ 6,378\\ 7,348\\ 5,993\\ 6,987\\ 5,961\end{array}$	$\begin{array}{c} 4,924\\ 4,924\\ *3,422\\ 4,921\\ 5,094\\ 4,674\\ 4,419\\ 4,419\\ *1,367\\ 3,859\\ 3,2924\\ 2,921\\ 2,921\\ 2,928\\ *795\\ 2,941\\ 1,677\end{array}$	$\begin{array}{c} * 175\\ * 175\\ 827\\ 30\\ 1,216\\ 931\\ 821\\ *1,215\\ 1,288\\ 827\\ 1,255\\ 827\\ 1,258\\ 827\\ 1,255\\ 827\\ 1,258\\ 827\\ 1,258\\ 827\\ 1,248\\ 1,225\\ 827\\ 1,248\\ 1,220\\ 934\\ 1,248\\ 1,220\\ 934\\ 1,248\\ 1,220\\ 934\\ 1,248\\ 1,220\\ 934\\ 1,248\\ 1,220\\ 934\\ 1,248\\ 1,220\\ 934\\ 1,248\\ 1,220\\ 1,248\\ 1,220\\ 1,248\\ 1,220\\ 1,248\\ 1,220\\ 1,248\\ 1,220\\ 1,248\\ 1,220\\ 1,248\\ 1,220\\ 1,248\\ 1,220\\ 1,248\\ 1,220\\ 1,248\\ 1,220\\ 1,248\\ 1,220\\ 1,248\\ 1,220\\ 1,248\\ 1,248\\ 1,220\\ 1,248\\ 1,248\\ 1,220\\ 1,248\\ 1,220\\ 1,248\\ 1,220\\ 1,248\\ 1,248\\ 1,220\\ 1,248\\ 1$	Aug. 1,927 1,401 1,719 1,332 *1,087 1,256 1,087 1,559 1,740 1,729 *1,740 1,729 *1,729 3,233 3,347 2,9565 3,019 2,9565 3,019 2,9565 3,347 2,986 1,420 1,42	1,044 * 956 1900 1,445 827 715 827 * 827 1,211 1,213 1,215 1,213 1,213 1,213 1,213 1,213 1,213 1	827 827 827 827 827 827 827 827 827 827	$\begin{array}{c} 1,620\\ 1,266\\ 1,406\\ *302\\ 1,462\\ *302\\ 1,266\\ 1,006\\ 1,226\\ 2,203\\ *875\\ 2,203\\ 1,883\\ 1,947\\ 1,691\\ 2,947\\ 1,691\\ 2,947\\ *1,133\\ 2,040\\ \end{array}$	$\begin{array}{c} \text{Dec.} \\ \hline \\ 5,586 \\ *5,611 \\ 7,697 \\ 4,421 \\ 4,421 \\ 4,421 \\ 4,421 \\ 4,181 \\ 2,454 \\ 2,061 \\ 2,806 \\ 2,388 \\ 2,138 \\ 2,138 \\ 2,275 \\ 1,826 \\ 1,940 \end{array}$
20 21 22 23 24	2,217 *1,401 5,858 7,312 7,577	9,340 9,141 7,611 7,013 6,259	3,419 3,479 4,830 4,942 4,942 4,942	31, 495 34, 899 *34, 470 43, 900 36, 061		1,957 2,407 1,915 1,979 *20	$ \begin{array}{r} 394 \\ 1,360 \\ 1,268 \\ * 30 \\ 1,306 \\ 1.338 \end{array} $	$ \begin{array}{r} 1,420\\ 2,242\\ 1,250\\ 1,534\\ 977\\ 940 \end{array} $	1,112 1,112 1,211 1,175 * 912 1.612	1,224 * 872 1,611 1,040 1,118		1,920 2,138 2,138 *1,795 1,590
25 26 27 28 29	$6,991 \\ 6,991 \\ 5,862 \\ *2,041 \\ 5,212$	*5,609 4,694 4,232 4,045		$\begin{array}{c} 30,945\\ 26,635\\ 23,536\\ 18,480\\ *14,250\end{array}$	3,677 4,912 *415 4,366 4,319	2,607 2,191 1,178 2,181 1,241	2,033 1,467 3,441 3,263 *175	$ \begin{array}{r} 901 \\ * 95 \\ 928 \\ 928 \\ 1,487 \end{array} $	$1,661 \\ 1,557 \\ 1,329 \\ 1,435 \\ 1,180$	$1,106 \\ 1,251 \\ 1,773 \\ * 804 \\ 2,703$	*3,260 6,268	$ \begin{array}{r} 3,170 \\ 2,637 \\ 3,136 \\ 2,887 \\ 2,887 \end{array} $
30 31 Mean .	$\frac{4,287}{3,571}$ $3,211$	7,074	$ \begin{array}{r} 4,942 \\ 4,942 \\ \overline{ 3,934} \end{array} $	$ \begin{array}{r} 14,210\\ \hline \\ 16,914\end{array} $	$ \begin{array}{r} 3,372 \\ 3,460 \\ \hline 6,358 \end{array} $	$ \begin{array}{r} 1,069 \\ \hline 2,834 \end{array} $	$ \begin{array}{r} 1,987 \\ 1,656 \\ \hline 1,248 \end{array} $	$ \begin{array}{r} 1,531 \\ 1,791 \\ \hline 1,652 \end{array} $	*865 	2,447 1,647 1,243	2,670	

NEW YORK.

HUDSON RIVER AT MECHANICSVILLE, NEW YORK.

A record of the flow of Hudson River at Mechanicsville has been kept by the Duncan Company since December, 1888. The record includes two daily readings of the depth of water on the crest of the dam and a continuous record of the water wheels in the adjoining paper mill. The accompanying tables give the daily mean flow at Mechanicsville, computed by Mr. R. P. Bloss, the engineer of the Duncan Company. A record is kept of the length and height of the flashboards at all times, with the dates of their setting and removal.

The flow over the dam has been computed by the Francis formula for the Merrimac dam, $Q=3.01 LH^{1.53}$, L being 794 feet. The same formula has been used in all cases, whether flashboards are on or off.

The flow through the water wheels has been taken from the rating tables of the manufacturers. The working head on the wheels varies from 15 to 17 feet, depending on the condition of the flashboards on the dam. A test made by Mr. Bloss of a 39-inch Hercules wheel in the mill, which has been in use about eight years, shows the actual discharge to be substantially the same as that given in the manufacturers' tables when running at the speed of greatest efficiency. When running at higher speeds the discharge may be several per cent less.

A current-meter measurement of the flow below the dam was made at the Mechanicsville tollbridge October 20, and showed a discharge of 1,871 second-feet. The result is somewhat uncertain, however, owing to slack water. No water was flowing over the dam, and the calculated turbine discharge was 1,977 second-feet.

The flow of Hudson River at Mechanicsville has been calculated by George W. Rafter, member American Society of Civil Engineers, using the East Indian Engineers' formula for flow over dam.¹ This formula gives a somewhat greater discharge than that obtained by using the Francis formula for the Merrimae dam.

¹ Rept. State Engineer and Surveyor of New York, 1895, p. 105; also Water-Supply and Irrigation Paper U. S. Geol. Survey No. 24, p. 78 Daily discharge, in second-feet, of Hudson River at Mechanicsville, New York, for 1898.

										and the second sec		
Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1	6,252	4,340	5,011	20,306	*13,474	9,490	3, 179	3,005	a 4, 345	3,222	7,954	6,300
3	5,319	$\frac{4,839}{5,034}$	4,990 4,927	* 15, 810	9,702	7,558	*3,011	6,225	a 4,001 a 4,145	$^{+2,811}_{-2,835}$	6,590	5,698
4	5,276 5,562	$\frac{4,114}{2,056}$	4,909	13,890	10,820 10,570	6,292	3,007	5,72	*a4,340	2,780	6,500	*5,185
6	5,698	(*)	(*)	10,692	10,310 11,300	5,508	2,588	5,832	4, 145	20,089	* 5,803	6,500
7	6,873 7,592	4,000 5.286	4,998 4,875	9,928	11,032 * 10,250	4,729	2,453 2 314	*5,415 5 001	4,007	9,472	5,890 5,503	6,322 5,456
9	(*)	5,139	6,418	8,158	9,700	4,335 4,249	2,220	4,335	4,217	*7,872	5,872	4,150
10	6,431 6,249	5,145 5,865	7,004 9,746	*7,924 7.915	8,695 7,875	3,978 3,425	*1,163 2,000	3,926 3,743	3,813 *3.368	6,960 6.038	-6,238 -20,256	4,675 *4.345
12	5,136	7,639	20,202	7,646	8,420	*3,857	2,182	3,387	3,304	6,109	16,262	4,290
13	11,930 11,424	9,732	(7) 39,231	8,000 9,815	11,034 10,585	4,299 4,945	2,058 2,080	* 3, 331	$ \begin{array}{r} 3,188 \\ 2,732 \end{array} $	$5,331 \\ 4,829$	$^{*}14,510$ 13,202	3,739 3,540
$\frac{15}{16}$	10,557	8,078	36,155 31,310	9,824	* 10, 161	7,662	2,184 2 150	3,362	2,597 2,487	6,888	11,385 10.266	3,850
17	10, 176	5,396	31,069	* 12, 575	10,082	5,681	*1,163	3,223	2,597	8,125	9,722	4,495
18	7,898 7.318	-6,978 -7.224	-31,794 -29.304	12,188 11,155	10,637 9.404	4,620 *4.851	2,192 2,224	3,235 3,660	$^{*2,873}_{-2.873}$	7,250 6.500	8,910 8,922	*4,590
20	8,401	(*)	(*)	11,157	9,412	5,593	2,175	4,507	3,365	6,508	* 10, 505	4,885
22	14,053 10,625	7,348	33,917 33,660	10,933 10,127	*7,954	4,003 4,399	2,192 3,188	4,495 4,718	2,975 2,899	6,310	11,167 10,366	5,035 5,035
23	(*)	6,746 6,149	30,004 26,754	9,815	8,000	4,198	3,565	3,927 5 773	2,666 3.907	* 6,894	9,610	6,908
25	9,866	5,915	24,034	20,440	9,491	4,097	3,928	a11, 167	* 5, 231	7,178	8,685	*7,747
26	9,173 8,171	5,461	(*)	-24,210 -24,338	11,953 14.758	* 4, 024	4,665 4.258	a9,953 a8,125		6,693 9.382	7,847 *6.413	6,885 5.872
28	8,101	5, 380	19,077	20,440	15,327	3,556	3,656	*08,250	4,775	11,042	5,820	4,618
39 30	(*)		19,818 22,777	18,105 14,873	14,140 12,727	-3,208 -3,238	3,352 3,175	a 4, 829	4, 343	*10.485 *10,059	6,300	4,628 4,828
31	4,822		21,805		10,490		* 3, 015	a 4, 217		9,953		5,348
Mean .	8,173	6,038	19,617	13,047	10, 525	5,069	2, 751	5,029	3,810	7,516	8,978	5,291

[Drainage area, 4,500 square miles.]

a Discharge August 25 to September 4 approximate, owing to irregular flashboards. *Sunday.

Daily discharge, in second-feet, of Hudson River at Mechanicsville, New York, for 1899.

	Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1 2		$*4,262 \\ 4,262$	$3,910 \\ 4,268$	7,847 7,040	$7,980 \\ 7,159$	$26,900 \\ 27,617$	$3,990 \\ 3,796$	2,220 *1,047	$1,520 \\ 629$	$1,713 \\ 1,561$	(*) 4,042	$4,564 \\ 8,889$	3,005 3,414
3.4-5		5,209 6,065 9,146	4,268 4,150 *4,002	6,403	6,955 7,938 9,504	25,551 22,472 19,242	3,601 *2,220 2,990	2,128	1,213 1,153 1,085	$(*) \\ 1,293 \\ 1,860$	3,453 2,850 2,745	12,020 11,899 *10,346	*3,753 5,545 6,678
6.7		8,460 8,355	4,223 4,048 4,048	16,501 12,266 0.077	9,955 11,719	15, 152 *12, 662	2,840 2,728 2,728	1,610 1,670 1,911	(*) 1,494	1,764 1,706 1,680	2,650 2,571	11,049 9,308 8,140	5,974 5,210 4,559
		8,026 6,562	4,275 3,448 3,665	8,665 7,909	*18,275 15,062 15,062	9,270 8,587	2,525 2,290	(*) 3,000	1,010 1,475 484 1,149	1,000 1,466 (*)	2,590 2,712	7,166 6,662	4,000 3,806 *3,265
$\frac{11}{12}$. 13.	· · · · · · · · · · · · · · · · · · ·	5,700 5,250 5,272	$^{3,022}_{*4,062}$ $^{4,196}_{4,196}$	$^{7,313}_{*11,739}$ $^{15,437}_{15,437}$	15,582 16,875 17,145	7, 140 7, 550 7, 155	2,399 2,505	3,296 3,243 3,243	1,140 993 (*)	1,480 1,598 1,471	2,905 2,874 2,926	$^{6,183}_{*5,490}$ $^{6,321}_{6,321}$	
14 . 15 . 16 .		5,960 *7,435 8,910	$ \begin{array}{r} 4,508 \\ 4,600 \\ 4,798 \end{array} $	12,153 10,555 10,012	21,378 27,975 *29,730	*7,060 7,772 7,346	2,230 2,135 3,078	$ \begin{array}{r} 3,002 \\ 2,800 \\ (*) \end{array} $	$1,580 \\ 1,680 \\ 1,501$	1,567 1,484 1,549	2,353 (*) 2,177	$ \begin{array}{r} 5,536 \\ 5,179 \\ 4,858 \\ \end{array} $	14,576 14,979 13,452
$\frac{17}{18}$. 19.		$ \begin{array}{r} 10,155 \\ 9,685 \\ 7,339 \end{array} $	5,598 5,691 *5,620	9,080 7,895 *9,322	$31,112 \\ 29,667 \\ 29,711$	5,738 5,729 5,928	3,060 *2,762 2,950	$2,861 \\ 3,338 \\ 2,860$	$1,815 \\ 979 \\ 1,390$	(*) 711 1,636	$2,132 \\ 1,853 \\ 1,798$	5,283 4,857 *4,359	*9,646 9,534 9,968
20 . 21 . 22 .		6,385 6,297 *5,770	$5,267 \\ 4,855 \\ 5,686$	$11,350 \\ 9,670 \\ 9,337$	$33,940 \\ 36,210 \\ 36,210$	5,917 *5,925 6,187	2,508 2,372 2,280	$2,560 \\ 2,485 \\ 2,295$	$^{(*)}_{1,610}$ 1,123	$957 \\ 941 \\ 1,448$	1,997 2,185 (*)	$4,838 \\ 4,729 \\ 4,587$	10,950 11,048 10,721
$\frac{23}{24}$. $\frac{25}{25}$.		$ \begin{array}{c c} 5,697\\ 5,522\\ 6,950 \end{array} $	$\begin{array}{c} 10,083 \\ 7,501 \\ 5,583 \end{array}$	8,645 8,657 8,095	*37,146 38,283 39,064	$5,313 \\ 4,756 \\ 4,710$	2,105 1,878 *304	$(*) \\ 2,240 \\ 2,233$	$1,743 \\ 2,460 \\ 1,383$	$1,464 (*) \\ 1,516$	2,466 2,698 2,372	4,297 3,964 3,731	9,642 *8,068 8,241
26 . 27 . 28 .		$5,775 \\ 5,438 \\ 4,545$	*5,255 6,450 10,326	$*7,492 \\ 6,895 \\ 6,615$	$\begin{array}{c} 41,475 \\ 40,664 \\ 38,300 \end{array}$	4,462 4,117 *3,985	$1,878 \\ 2,241 \\ 2,290$	$2,188 \\ 2,021 \\ 2,140$	$1,463 \ (*) \ 1,756$	$2,116 \\ 6,000 \\ 5,127$	2,304 2,128 2,216	$*3,472 \\ 4,027 \\ 3,495$	$7,821 \\ 5,832 \\ 5,435$
29 . 30 . 31 .				7,835 8,765 7,602	33, 908 *30, 292	$4,125 \\ 3,787 \\ 3,918$	2,368 2,512	1,686 (*) 2,055	$1,738 \\ 1,739 \\ 1,477$	4,413 4,870	$(*) \\ 3,198 \\ 3,815$	$3,439 \\ 3,318$	4,889 4,075 *2,585
	Mean .	6,437	5,141	9,316	24,607	9,591	2,539	2,402	1,417	2,054	2,616	6,066	7, 303

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Daug alsenarge, in second-feet, of Hudson River at Mechanicsottie, New York, Jo 1900.												
		1	-	1		y		1				
Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oet.	Nov.	Dec.
1	3,612	4,163	5,623	(*)	16,713	4,288	*2,364	2,977	2,365	2,102	2,531	9,107
2	3,276	3,349	12,924	10,088	15,493	4,932	2,368	2,809	*2,297	2,223	2,094	*8,316
3	3,294	3,737	10,299	10,413	14,676	*3,482	2,368	2,464	2,177	2,144	2,413	7,444
4	3,263	(*)	*3,800	11,188	14,593	7,644	2,191	2,386	2,519	2,071	*2,159	6,459
5	3,277	6,556	7,998	11,188	12,494	6,793	2,701	*2,167	2,289	1,752	1,977	10,694
6	3,602	8,140	5,932	12,267	*9,444	6,083	2,382	[2, 135]	2,125	1,768	1,920	9,033
7	*3,000	7,204	9,312	15,149	9,741	5,551	2,109	2,266	2,031	*3,094	1,576	7,920
8	3,810	0,777	0,900	*17,530	10, 924	5, 329	*2,200	2,001	1,720	1,895	1,000	1,024
9	9,000	19,001 11 979	0,100	18,804	9,000	3, 329	2,100	9 759	719	1,000 1.005	9 590	6 101
10	3,990	*0 666	*6 249	14 749	9,405	5 897	1 427	9 189	1 728	1, 505	*2 860	5, 010
11	3 918	7 700	6 205	14, 144	8 520	1 750	1,404	*2 550	1,700	2 063	4 331	1 662
19	3 159	24 530	5 563	14,262	*7 500	4,100	1,00%	9 541	1,801	1 947	3 820	4 988
14	(*)	41 285	5 761	13 554	7 626	3,911	2,002	2 691	1 118	*1 931	3,805	4 856
15	3 067	25 354	5 363	*11 988	7 750	4 033	*2 263	3 292	1 433	2 123	3 315	4 250
16	3, 158	22, 593	4,411	13, 588	9,390	4,054	2.292	4.299	*1.820	2.061	3, 136	*4.250
17	3,180	19.527	4.719	15,918	7.549	*3,700	2.185	5.773	2,063	2,233	2,911	4, 195
18	3,139	*16,547	*3,675	22,761	8,241	4.269	2,189	4,617	1,904	2,013	*3,036	4,265
19	4,668	14,173	4,935	33,150	7,500	3,617	1,991	*4,014	2,087	1,978	3,287	3,909
20	16,115	12,825	15,344	40,131	*9,450	2,941	1,580	3,955	2,032	1,954	3,829	4,129
21	*18,307	11,555	11,058	42,908	10,953	2,774	1,565	3,154	1,412	*1,977	5,292	3,953
22	11,307	10,060	7,999	*42,300	9,141	2,968	*2,180	2,834	1,581	2,017	9,332	4,004
23	10,176	13,310	8,324	43,546	8,029	3,141	2,299	2,510	*1,704	1,955	10, 120	*4,210
24	9,853	10,188	9,399	41,940	7,354	*1,877	-2,271	2,351	1,822	2,253	9,321	5,239
25	9,295	*9,301	*10,686	38,575	6,345	2,868	2,092	1,831	1,978	2,195	*8,796	3,763
26	8,449	1,042	8,220	33, 983	3,758	3,210	2,690	*1,708	1,953	2,167	9,483	6,536
20	6,913	5,390	1,541	28,578	*4,651	3,713	4,082	1,702	2,002	2,203	11,027	4,700
28	(*)	0,25%	7,626	25,618	0,451	2,181	3,898	1,814	2, 4:44	*2,320	11,694	4,679

* Sunday.

2,5083,2103,7132,7872,361

2,530

4,093

2,1952,1672,203*2,3202,583

3,287

3.124

2,128

 $11,694 \\ 11,347$

9,670

5,077

4,459*4,593

4,535

5,331

2.145

*2,135

1,886

2,1922,1422,278

2,703

*2,836

3,951

3,248

2,352

12,484

6, 145

5,808

4,453

5,841

29

30

31

Mean

7,626

8 014

9,075

7,740

19,510

22,614

*25,741

 $6,454 \\ 5,333$

 $4,042 \\ 3,857$

8,992

CROTON RIVER AT OLD CROTON DAM, NEW YORK.

Records of the yield of the Croton watershed have been prepared by the engineers of the aqueduct commission. Tables of the monthly discharge of the river, in second-feet, for the years 1870 to 1898, inclusive, were printed in the Twentieth Annual Report, Part IV, page 83, and in the Twenty-first Annual Report, Part IV, page 75, is a table of the rainfall and run-off of the watershed for the years 1868 to 1899, The following table, furnished by Mr. W. R. Hill, chief inclusive. engineer of the aqueduct commission, is the record for 1900. The figures of rainfall are those obtained at Boyds Corners, in Croton Basin.

Estimated monthly discharge of Croton River at old Croton dam, New York, for 1900.

			Run	-off.	
Month.	Discharge.	Total.	Per square mile.	Depth.	Rainfall.
January February March April May June June	Second-feet. 537 2, 179 1, 724 553 716 357 78	$\begin{array}{c} \textit{Acre-feet.} \\ 33,020 \\ 121,032 \\ 106,013 \\ 32,915 \\ 43,991 \\ 21,254 \\ 4.774 \end{array}$	$\begin{array}{c} \textit{Second-feet.} \\ 1.59 \\ 6.45 \\ 5.10 \\ 1.64 \\ 2.12 \\ 1.06 \\ .23 \end{array}$	Inches. 1.83 6.71 5.88 1.83 2.45 1.18 .27	Inches. 4.18 7.97 5.06 2.16 6.40 2.17 4.28
August September October November December The year	$ \begin{array}{r} 77\\ 107\\ 174\\ 346\\ 639\\ \hline 624 \end{array} $	$\begin{array}{r} 4,716\\ 6,357\\ 10,674\\ 20,573\\ 39,258\\ \hline 444,577\end{array}$	$ \begin{array}{r} $	$ \begin{array}{r} 2.27 \\ .36 \\ .59 \\ 1.14 \\ 2.18 \\ 24.69 \\ $	$ \begin{array}{r} 1.75\\ 3.27\\ 4.73\\ 4.91\\ 2.58\\ \hline 49.46 \end{array} $

[Drainage area, 338 square miles.]

DELAWARE RIVER AT LAMBERTVILLE, NEW JERSEY.

This station, which was established July 23, 1897, by E. G. Paul, is described in Water-Supply Paper No. 35, page 62. The results of measurements for 1899 will be found in the Twenty-first Annual Report, Part IV, page 77. During 1900 the following measurements of discharge were made by Mr. Paul:

May 22: Gage height, 5.10 feet; discharge, 17,750 second-feet. September 27: Gage height, 2.95 feet; discharge, 1,824 second-feet.

Daily gage height, in feet, of Delaware River at Lambertville, New Jersey, for 1900.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1 2	$\stackrel{(a)}{_{(a)}}$	(a) (a)	$5.40 \\ 12.00$	$4.25 \\ 4.20$	$4.45 \\ 4.35$	$\frac{3.30}{3.40}$	$2.65 \\ 2.50$	$3.40 \\ 3.15$	$2.95 \\ 3.05$	$2.90 \\ 2.50$	$2.80 \\ 2.75$	$4.15 \\ 4.05$
3 4 5	(a) (a) (a)	$(a) \\ 7.00 \\ 6.85$	$10.70 \\ 7.95 \\ 6.80$	$\begin{array}{r} 4.30 \\ 4.40 \\ 4.50 \end{array}$	$4.25 \\ 4.20 \\ 4.05$	$ \begin{array}{c} 3.45 \\ 3.65 \\ 3.80 \end{array} $	$2.60 \\ 2.90 \\ 3.10$	3.00 3.05 3.05	$2.75 \\ 2.90 \\ 2.70$	$2.55 \\ 2.65 \\ 2.80$	2, 85 3, 20 3, 25	$3.95 \\ 3.95 \\ 4.40$
6 7 8	$(a) \\ (a) \\ (a)$	$5.75 \\ 5.30 \\ 5.45 \\ $	$6.20 \\ 6.05 \\ 5.80 \\ 0.05 \\ $	$ \begin{array}{r} 4.40 \\ 4.30 \\ 4.40 \\ 4.90 \end{array} $	$ \frac{4.00}{3.95} 3.90 $	3.70 3.55 3.35	$3.40 \\ 3.80 \\ 3.65 \\ 5$	2.70 3.25 2.70	2.70 2.60 2.65	2.55 2.75 2.70	$3.20 \\ 3.20 \\ 3.15 \\ 0.00$	$\begin{array}{r} 4.90 \\ 5.40 \\ 4.95 \\ 4.95 \end{array}$
9 10 11 12	(a)	5.60 6.95 6.55	$\begin{array}{c} 6.00\\ 5.60\\ 5.45\\ 5.90\end{array}$	$4.60 \\ 4.55 \\ 4.45 \\ 4.20$	3.80 3.80 3.90	3.30 3.55 3.85	3.65 3.55 3.50	2.60 2.65 2.80	2.90 2.85 3.00 2.95	2.75 2.75 2.75	3.20 3.10 2.90 2.75	4.00 4.45 4.20 2.05
14 15		$ \begin{array}{r} 3.00 \\ 7.46 \\ 11.40 \\ 9.70 \end{array} $	$ \begin{array}{r} 3.20 \\ 4.90 \\ 4.60 \\ 4.55 \end{array} $	4.30 4.35 4.40 4.50	3,80 3,80 3,80 3,70	3.50 3.45 3.95	ə. əə 3. 35 3. 20 3. 30	2.55 2.55 3.05 3.05	$ \begin{array}{r} 3.23 \\ 3.10 \\ 3.00 \\ 2.85 \end{array} $	2.00 2.50 3.15 2.95	2.75 2.55 2.70 2.60	3.90 3.90 4.40
16 17 18		8.10 6.65 5.95	4.50 4.20 4.20	$ \begin{array}{r} 4.30 \\ 4.30 \\ 4.75 \end{array} $	$ 3.60 \\ 3.60 \\ 4.00 $		$ \begin{array}{r} 3.50 \\ 3.35 \\ 3.25 \end{array} $	2.80 2.85 2.85 2.80	3.45 3.25 3.00		$ \begin{array}{r} 2.85 \\ 2.85 \\ 2.10 \end{array} $	(a) (a) (a)
19 20 21	$\begin{array}{r} 3.70 \\ 4.45 \\ 7.70 \end{array}$	$5.25 \\ 5.05 \\ 4.90$	$\begin{array}{c} 4.10 \\ 5.15 \\ 5.90 \end{array}$	$ \begin{array}{r} 6.60 \\ 7.15 \\ 6.50 \end{array} $	$ \begin{array}{r} 4.80 \\ 5.35 \\ 5.40 \end{array} $	$3.45 \\ 3.45 \\ 3.25$	3.30 3.35 3.30	2.95 3.15 3.10	$ \begin{array}{r} 3.00 \\ 2.70 \\ 2.55 \end{array} $	2.40 2.35 2.60	$2.85 \\ 2.80 \\ 2.75$	(a) (a) (a)
22 23 24	$7.75 \\ 6.20 \\ 5.75$	$ \begin{array}{r} 6.05 \\ 9.65 \\ 8.70 \\ \end{array} $	$\begin{array}{c} 6.30 \\ 5.65 \\ 5.30 \end{array}$	$\begin{array}{c} 6.00 \\ 5.85 \\ 5.95 \end{array}$	$5.05 \\ 4.60 \\ 4.25$	$3.20 \\ 3.05 \\ 3.15$	$3.50 \\ 3.35 \\ 3.45$	$2.95 \\ 2.90 \\ 2.80$	$2.65 \\ 2.85 \\ 2.85 \\ 2.85$	$2.65 \\ 2.25 \\ 2.40$	$2.85 \\ 3.10 \\ 3.40$	(a) (a) 3.40
25 26 27	$5.25 \\ 5.00 \\ 5.20$	$\begin{array}{c} 7.10 \\ 6.10 \\ 5.25 \end{array}$	$5.15 \\ 5.00 \\ 4.85 \\ 5.00$	5.95 5.70 5.25	$4.15 \\ 4.05 \\ 3.95 \\ 0.95 \\ $	$3.20 \\ 3.15 \\ 3.00$	$ \begin{array}{r} 3.35 \\ 4.35 \\ 4.10 \\ 4.05 \end{array} $	2.65 3.10 3.05	2.80 2.90 2.95	2.40 2.50 2.50	$3.15 \\ 3.75 \\ 3.50 \\ 100$	3.60 3.50 3.80
28 29 30 21	$\begin{pmatrix} (a) \\ (a) \\ (a) \\ (a) \end{pmatrix}$	4.90	4.95 4.60 4.50 4.35	$4.95 \\ 4.80 \\ 4.65$	3.75 3.60 3.60 3.45	2.90 2.70 2.70	3.85 3.65 3.60 3.50	2.95 2.80 2.85 3.10	2.90 2.65 2.95	2.85 2.80 2.85 2.95	4.10 4.75 4.40	$4.05 \\ 4.05 \\ (a) \\ 4.00$
	(a)		T. 00		0.40		0.00	0.10		A. 30		Ŧ, 00

a Frozen.

TOHICKON CREEK AT POINT PLEASANT, PENNSYLVANIA.

The stream is described in the Twentieth Annual Report, Part IV, page 98, which also contains (pages 98–103) the figures for monthly flow for the years 1890 to 1898. Figures for daily flow for 1899 were published in Water-Supply Paper No. 35, page 64. In the Twenty-first Annual Report, Part IV, pages 83 to 85, will be found the monthly flow for 1899 and diagrams of the discharge from 1883 to 1899, inclusive. The following tables give the figures for daily flow since 1883, when the station was established, from which the diagrams were constructed. Daily records of gage heights were not kept during 1900. The average monthly discharge, which will appear in the Twenty-second Annual Report, Part IV, has been computed by Mr. John E. Codman, hydrographer of the water department of the city of Philadelphia, from the rainfall and the monthly flow of Neshaminy and Perkiomen creeks.

Daily discharge, in second-feet, of Tohickon Creek at Point Pleasant, Pennsylvania, for 1883.

_										
	Day.	Sept.	Oct.	Nov.	Dec.	Day.	Sept.	Oct.	Nov.	Dec.
1234567891011213141516			$\begin{array}{c} 3\\ 6\\ 10\\ 228\\ 24\\ 11\\ 11\\ 13\\ 7\\ 12\\ 7\\ 9\\ 5\\ 7\\ 8\\ 18\\ 18\\ 10\\ 10\\ 10\\ 10\\ 10\\ 10\\ 10\\ 10\\ 10\\ 10$	$\begin{array}{c} 90\\ 55\\ 39\\ 26\\ 26\\ 30\\ 30\\ 36\\ 35\\ 151\\ 118\\ 118\\ 79\\ 54\\ 429\\ 29\end{array}$	49 46 43 31 43 37 41 61 81 81 81 41 41 41 41	18 19 20 21 22 23 24 25 26 27 28 29 30 31	11 5 4 3 4 2 2 5 5 8 6 5 5 5 5 5 5	$\begin{array}{c} & 7\\ 9\\ 18\\ 12\\ 12\\ 13\\ 456\\ 189\\ 99\\ 95\\ 69\\ 356\\ 687\\ 179\\ \hline 77\\ 77\end{array}$	20 15 23 17 21 18 8 21 24 220 165 85 49	$\begin{array}{c} & 41\\ & 41\\ & 41\\ & 110\\ & 1000\\ & 1000\\ & 1000\\ & 1000\\ & 1000\\ & 1000\\ & 2600\\ & 2600\\ & 2500\\ & 2400\\ & 2300\\ & 230\\ & 866\end{array}$
17	·	2	15	20	41					

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Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1	331	406	384	359	29	10	589	35	29	7	150	159
8	470	390		000 400	20	10	012	41	18	6	120	159
4	445	306	006	270	20	6	247		18	9 5	10%	139
5	354	396	419	217	20	5	2 309	100	11	5	313	40
6	354	396	392	155	20	7	1.507	103	15	4	253	256
7	467	1,989	365	92	19	8	863	76	7	2	81	1.560
8	2,593	2,412	362	80	18	9	612	42	7	2	64	309
9	3,492	1,270	359	408	17	10	256	32	7	2	21	164
10	2,749	1,270	356	373	129	35	131	22	7	2	21	77
11	1,579	889	1,113	338	150	35	39	20	9	1	22	50
12	590	399	1,871	305	103	34	25	20	6	I	23	662
18	590	1,743	1,148	223	10	33	31	19	2	1	19	651
14	200	4,100	4.50	141	049		01 91	10	20	1	12	1 110
16	200	424	205	200	02 02	22	21	10	9	1	16	1,114
17	390	621	380	258	54	33	26	5	3	1	12	159
18	377	1.218	365	216	36	34	22	5	3	ě	12	108
19	361	1,000	1.114	173	34	34	22	4	4	ŏ	10	73
20	361	1,862	1,390	109	49	- 33	15	4	4	ŏ	13	251
21	382	1,314	414	46	67	31	15	4	2	0	25	315
22	409	1,204	400	42	59	22	15	7	3	0	25	323
23	409	2,008	380	- 38	43	9	10	12	3	2	46	363
24	409	900	1,000	44	29	4	9	11	4	4	859	211
20	409	800	425	30	24	4 970	9	9	Ð	Ð	211	159
40	409	109	800	28	15	4,319	1	4 9	4	4	100	123
94 9Q	400	507	336	15	10	$1, \pm 00$ 1 949	0 77	0		0	00 59	100
29	415	392	321	15	10	1 024	11	17		- 20	201	107
30	415	000	306	41	10	807	20	26	ñ	20	159	240
31	415		385		9		22	28		250		2,372
	more		For								100	
Mean	703	990	580	175	57	314	242	25	7	12	108	353

Daily discharge, in second-feet, of Tohickon Creek at Point Pleasant, Pennsylvania, for 1884.

Daily discharge, in second-feet, of Tohickon Creek at Point Pleasant, Pennsylvania, for 1885.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
Day. 1 2 3 5 6 7 8 9 10 12 13 14 15 16 17 18 20 21 22 23	$\begin{array}{c} 2,614\\ 480\\ 138\\ 138\\ 138\\ 140\\ 1,599\\ 949\\ 232\\ 176\\ 167\\ 822\\ 1,404\\ 423\\ 103\\ 784\\ 1,267\\ 216\\ 101\\ 98\\ 87\\ 991\\ 98\end{array}$	$\begin{array}{c} \hline \\ \hline $	$\begin{array}{c} 59\\ 61\\ 102\\ 119\\ 119\\ 183\\ 218\\ 231\\ 196\\ 174\\ 115\\ 83\\ 69\\ 9\\ 64\\ 149\\ 162\\ 2002\\ 180\\ 178\\ 178\\ 178\\ 178\\ 178\\ 176\\ 69\\ 64\end{array}$	$\begin{array}{c} 1,291\\1,004\\518\\1,013\\3,664\\2,411\\2,411\\868\\203\\169\\146\\118\\118\\112\\766\\766\\766\\766\\766\\766\\76\\59\\422\\42\\42\\42\\42\\9\\29\\29\end{array}$	$\begin{array}{c c} \text{may.}\\ \hline \\ \hline \\ \hline \\ \\ \hline \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} & & \\$	$\begin{matrix} 1 \\ 35 \\ 696 \\ 1, 489 \\ 188 \\ 500 \\ 588 \\ 210 \\ 180 \\ 180 \\ 120 \\ 120 \\ 120 \\ 333 \\ 61 \\ 499 \\ 299 \\ 235 \\ 19 \\ 177 \\ 7 \\ 111 \\ 18 \\ 17 \end{matrix}$	$\begin{array}{c} 87777725554664666744133522111511 \end{array}$	$\begin{array}{c} 1\\ 1\\ 5\\ 3\\ 3\\ 5\\ 5\\ 3\\ 6\\ 6\\ 7\\ 6\\ 5\\ 10\\ 3\\ 18\\ 12\\ 11\\ 10\\ 6\\ 8\\ 44\\ 112\\ 10\\ 6\\ 8\\ 44\\ 112\\ 6\\ 66\end{array}$	$\begin{array}{c} 84\\ 84\\ 635\\ 345\\ 131\\ 73\\ 61\\ 55\\ 953\\ 1,137\\ 286\\ 151\\ 94\\ 46\\ 39\\ 55\\ 266\\ 39\\ 29\\ 233\\ 244 \end{array}$	$\begin{array}{c} 123\\123\\14\\155\\128\\132\\132\\132\\132\\132\\132\\132\\132\\132\\132$
24 25 26 27 28 29 30 31	$ \begin{array}{r} 301 \\ 101 \\ 104 \\ 97 \\ 82 \\ 90 \\ 96 \\ 99 \\ 89 \\ 89 \\ \end{array} $	100 116 107 90 86	$51 \\ 190 \\ 592 \\ 931 \\ 1,027 \\ 783 \\ 783 \\ 850$	29 29 36 39 43 49 49	19 19 20 25 18 20 16 15 12 12			$ \begin{array}{c} 17 \\ 14 \\ 10 \\ 8 \\ 13 \\ 12 \\ 5 \\ 8 \end{array} $	4 2 2 1 1 1 1 1	$ \begin{array}{r} 34 \\ 17 \\ 24 \\ 27 \\ 24 \\ 12 \\ 244 \\ 202 \\ \end{array} $	720 449 363 322 235 194 147	57 50 57 66 80 38 30 65
Mean	401	340	265	415	44	7	20	112	3	31	236	158

Daily discharge, in	second-feet, of	[*] Tohickon Creek a	t Point	Pleasant, 1	Pennsylvania,
0 0 1		for 1886.			

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	Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oet.	Nov.	Dec.
$-\frac{1}{2} \frac{2}{3} \frac{4}{4} \frac{5}{6} \frac{6}{7} \frac{8}{2} \frac{9}{10} \frac{11}{112} \frac{11}{12} \frac{14}{15} \frac{16}{17} \frac{16}{12} \frac{12}{22} \frac{22}{22} \frac{22}$	Day.	Jan. 278 112 83 833 3,352 720 148 105 182 207 258 236 176 110 149 150 150 150 150 171 227 372 110 163 163	$\begin{tabular}{ c c c c c c c c c c c c c c c c c c c$	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$\begin{array}{c} {\rm Apr.} \\ \hline \\ 2,523 \\ 647 \\ 198 \\ 149 \\ 222 \\ 3,692 \\ 2,320 \\ 1,085 \\ 428 \\ 239 \\ 150 \\ 155 \\ 283 \\ 130 \\ 85 \\ 722 \\ 552 \\ 283 \\ 130 \\ 85 \\ 722 \\ 550 \\ 433 \\ 332 \\ 231 \\ 31 \\ 31 \\ \end{array}$	May. 32 21 21 26 26 26 26 24 2,121 1,746 348 159 1,319 313 673 283 136 117 613 283 136 117 117 117 117 117 117 117 11	June. 299 257 366 366 367 37 24 28 199 18 225 1766 482 181 95 772 72 72 72 72 176 482 199 188 225 176 422 255 176 267 277 366 366 367 377 376 366 327 327 327 326 327 327 327 327 327 327 327 327	$\begin{array}{c} \textbf{July.}\\ \hline \\ \textbf{34}\\ \textbf{19}\\ \textbf{20}\\ \textbf{10}\\ \textbf{17}\\ \textbf{15}\\ \textbf{12}\\ \textbf{10}\\ \textbf{10}\\ \textbf{17}\\ \textbf{15}\\ \textbf{12}\\ \textbf{10}\\ \textbf{9}\\ \textbf{14}\\ \textbf{14}\\ \textbf{19}\\ \textbf{21}\\ \textbf{19}\\ \textbf{21}\\ \textbf{19}\\ \textbf{21}\\ \textbf{19}\\ \textbf{21}\\ \textbf{16}\\ \textbf{16}\\ \textbf{16}\\ \textbf{378}\\ \textbf{132}\\ \textbf{275}\\ \textbf{83}\\ \textbf{51}\\ \textbf{10}\\ \textbf{26}\\ \textbf{10}\\ \textbf{26} \end{array}$	$\begin{tabular}{ c c c c c c c c c c c c c c c c c c c$	Sept. 3152212211322155222255532	Oct. 24 4 3 1 1 2 2 1 1 2 2 1 1 2 2 1 1 2 2 1 1 2 2 1 1 2 2 1 1 2 2 1 1 2 2 1 1 2 2 1 1 2 2 1 1 2 2 2 1 1 2 2 2 1 1 2 2 2 1 1 2 2 2 1 1 2 2 2 1 1 2 2 2 1 1 2 2 2 1 1 2 2 2 1 1 2 2 2 2 1 1 2 2 2 2 1 1 2 2 2 2 1 1 2 2 2 2 1 1 2 2 2 2 1 1 2 2 2 2 1 1 2 2 2 2 1 2 2 2 2 1 1 2 2 2 2 2 1 2 2 2 2 2 1 2 2 2 2 2 2 1 2 2 2 2 2 2 1 2 2 2 2 1 2 2 2 2 1 2 2 2 2 2 1 2 2 2 2 1 2 2 2 2 2 2 1 2 2 2 2 2 1 2 2 2 2 1 2 2 2 2 1 2 2 2 2 2 1 2 2 2 2 1 2 2 2 2 2 2 1 2 2 2 2 2 2 2 2 2 2 2 2 2	$\begin{array}{c c} \text{Nov.} \\ \hline \\ 15 \\ 12 \\ 12 \\ 12 \\ 12 \\ 13 \\ 9 \\ 9 \\ 9 \\ 7 \\ 7 \\ 9 \\ 9 \\ 9 \\ 7 \\ 7$	Dec. 62 46 59 59 110 104 63 88 63 86 86 55 23 34 285 2283 31 56 283 31 56 272 285 372 1,016 7100 230 148
252027220000000000000000000000000000000		$ \begin{array}{r} 311 \\ 197 \\ 117 \\ 679 \\ 984 \\ 908 \\ 200 \\ \end{array} $	1, 123 2, 108 324 231	$125 \\ 101 \\ 100 \\ 783 \\ 948 \\ 2, 150 \\ 2, 598$	37 35 35 34 32 24	$ \begin{array}{c} 115 \\ 94 \\ 77 \\ 81 \\ 67 \\ 43 \\ 41 \\ \end{array} $	210 128 81 54 38 28	20 366 100 36 28 25 25	3 6 8 7 3 2	$1 \\ 1 \\ 2 \\ 1 \\ 3 \\ 1$	$ \begin{array}{r} 2 \\ 4 \\ 8 \\ 15 \\ 17 \\ 12 \\ 15 \\ $	$756 \\ 2,064 \\ 257 \\ 107 \\ 73 \\ 61$	$985 \\ 336 \\ 189 \\ 103 \\ 142 \\ 144 \\ 175$
	Mean	388	910	382	438	304	129	69	9	2	4	180	212

Daily discharge, in second-feet, of Tohickon Creek at Point Pleasant, Pennsylvania, for 1887.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1 2 3 4 5	$\begin{array}{c} 330\\ 400\\ 300\\ 220\\ 150\\ 180\\ 190\\ 100\\ 100\\ 100\\ 100\\ 100\\ 100\\ 10$	$\begin{array}{c} 205\\ 109\\ 107\\ 127\\ 155\\ 136\\ 438\\ 838\\ 531\\ 770\\ 623\\ 275\\ 168\\ 425\\ 2357\\ 168\\ 425\\ 2357\\ 644\\ 456\\ 644\\ 456\\ 641\\ 466\end{array}$	$\begin{array}{r} 246\\ 155\\ 152\\ 121\\ 121\\ 96\\ 80\\ 816\\ 736\\ 612\\ 210\\ 159\\ 149\\ 612\\ 210\\ 159\\ 149\\ 536\\ 66\\ 51\\ 50\\ 48\\ 59\\ 125\\ 275\\ 284\\ 945\end{array}$	$\begin{array}{c} 106\\ 101\\ 132\\ 153\\ 142\\ 101\\ 101\\ 101\\ 101\\ 101\\ 101\\ 101\\ 10$	$\begin{array}{c} 57\\ 57\\ 49\\ 30\\ 38\\ 36\\ 29\\ 244\\ 669\\ 508\\ 195\\ 118\\ 73\\ 43\\ 31\\ 7\\ 34\\ 43\\ 31\\ 37\\ 34\\ 20\\ 200\\ 18\\ 58\\ 43\\ 31\\ 37\\ 34\\ 45\\ 20\\ 200\\ 18\\ 58\\ 31\\ 37\\ 34\\ 45\\ 20\\ 31\\ 58\\ 31\\ 37\\ 34\\ 31\\ 35\\ 45\\ 31\\ 31\\ 35\\ 31\\ 31\\ 31\\ 31\\ 31\\ 31\\ 31\\ 31\\ 31\\ 31$	$188 \\ 161 \\ 148 \\ 90 \\ 50 \\ 40 \\ 35 \\ 44 \\ 48 \\ 38 \\ 34 \\ 25 \\ 27 \\ 20 \\ 14 \\ 11 \\ 14 \\ 13 \\ 9 \\ 25 \\ 27 \\ 27 \\ 27 \\ 27 \\ 27 \\ 27 \\ 27$	$\begin{array}{c} & & \\ & 18 \\ 12 \\ 10 \\ 11 \\ 434 \\ 449 \\ 149 \\ 82 \\ 79 \\ 68 \\ 43 \\ 355 \\ 233 \\ 15 \\ 14 \\ 70 \\ 63 \\ 40 \\ 29 \\ 222 \\ 78 \\ 335 \\ 284 \\ \end{array}$	$\begin{array}{c} & \\ 1,148\\ 196\\ 279\\ 86\\ 52\\ 85\\ 116\\ 68\\ 46\\ 68\\ 46\\ 24\\ 22\\ 39\\ 22\\ 4\\ 18\\ 22\\ 39\\ 22\\ 4\\ 18\\ 21\\ 19\\ 16\\ 6\\ 22\\ 23\\ 166\\ 1,883\\ 549 \end{array}$	$\begin{array}{c} 20\\ 20\\ 18\\ 16\\ 14\\ 15\\ 13\\ 10\\ 11\\ 11\\ 10\\ 180\\ 349\\ 111\\ 11\\ 10\\ 180\\ 349\\ 111\\ 11\\ 10\\ 180\\ 349\\ 111\\ 11\\ 10\\ 159\\ 159\\ 15\\ 15\\ 15\\ 15\\ 15\\ 16\\ 10\\ 10\\ 10\\ 10\\ 10\\ 10\\ 10\\ 10\\ 10\\ 10$	$\begin{array}{c} 18\\ 30\\ 25\\ 26\\ 32\\ 25\\ 22\\ 14\\ 16\\ 11\\ 14\\ 14\\ 13\\ 14\\ 13\\ 14\\ 13\\ 14\\ 13\\ 14\\ 13\\ 11\\ 10\\ 9\\ 7\\ 51\\ 11\\ 10\\ 10\\ 90\\ 75\\ 54\\ 35\\ 25\\ 25\\ 25\\ 25\\ 25\\ 25\\ 25\\ 25\\ 25\\ 2$	$\begin{array}{c} 24\\ 18\\ 16\\ 18\\ 14\\ 15\\ 9\\ 15\\ 13\\ 20\\ 20\\ 16\\ 220\\ 20\\ 20\\ 20\\ 20\\ 20\\ 20\\ 20\\ 20\\ 2$	$\begin{array}{c} & 25\\ 33\\ 24\\ 24\\ 20\\ 24\\ 35\\ 35\\ 30\\ 70\\ 1,201\\ 639\\ 470\\ 4128\\ 708\\ 2055\\ 75\\ 131\\ 137\\ 184\\ 221\\ 320\\ 137\\ 184\\ 291\\ 320\\ 320\\ 474\\ 177\\ 184\\ 291\\ 320\\ 320\\ 137\\ 184\\ 291\\ 320\\ 320\\ 320\\ 320\\ 320\\ 320\\ 320\\ 320$
26 27 28 29 30	$ \begin{array}{c} 1,112\\ 602\\ 214\\ 202\\ 1,473\\ 1,542 \end{array} $	166 613 466		$ \begin{array}{r} 30 \\ 134 \\ 147 \\ 88 \\ 100 \\ 92 \end{array} $	$ \begin{array}{r} 32 \\ 24 \\ 17 \\ 31 \\ 19 \end{array} $			$ \begin{array}{r} 343 \\ 151 \\ 89 \\ 47 \\ 36 \\ 27 \end{array} $	$10 \\ 12 \\ 14 \\ 19 \\ 25 \\ 20$	$ \begin{array}{r} 22 \\ 19 \\ 17 \\ 22 \\ 14 \end{array} $		$ \begin{array}{r} 111 \\ 187 \\ 158 \\ 701 \\ 1, 139 \\ 652 \end{array} $
31 Mean	415 449	517	144 342	93	87	110	36 145	23 173		21 23	24	306 283

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1	3,190	150	122	318	37	43	11	8	21	38	94	144
2	3,492	150	120	235	32	- 33	7	8	18	40	80	294
3	683	116	130	189	31	22	9	7	20	37	76	275
4	294	109	164	131	28	27	4	11	17	35	71	81
5	217	201	154	692	28	27	11	16	21	32	65	81
6	154	446	125	2,019	28	22	3	22	19	72	60	83
7	198	712	106	1,790	29	25	- 3	14	9	265	51	87
8	669	671	85	911	31	17	7	47	10	199	49	83
9	514	608	83	135	- 33	12	4	48	25	99	67	172
10	237	521	79	780	34	14	8	11	111	47	336	262
11	143	401	100	1,797	39	13	8	11	199	36	494	159
12	151	253	908	435	89	20	6	26	604	- 38	173	115
13	188	208	123	237	92	22	11	34	337	41	- 98	84
14	280	190	750	382	78	27	7	29	165	42	81	71
15	234	122	473	344	70	17	- 3	23	87	42	1,130	71
16	334	104	380	254	63	6	3	15	103	43	982	63
17	606	118	570	291	51	6	8	18	1,351	43	333	2,374
18	714	127	620	150	45	4	4	15	5,546	39	237	2,689
19	647	352	494	113	45	8	8	11	1,991	39	935	434
20	590	1,377	950	103	52	8	2	4	270	53	864	148
21	590	2,768	2,659	86	47	9	2	392	2,710	62	311	133
22	369	1,751	1,886	63	36	12	8	3,489	472	56	175	176
23	350	890	594	61	- 34	9	7	333	191	48	131	205
24	310	828	253	52	35	6	8	92	117	82	132	117
25	185	2,188	151	44	- 39	8	5	52	84	110	132	72
26	226	1,650	173	41	38	8	5	30	75	82	214	72
27	242	661	1,633	38	35	3	6	25	73	491	423	345
28	405	526	938	- 33	37	7.	11	24	60	993	401	337
29	120	277	1,330	32	63	10	10	19	41	694	212	198
30	86		630	36	78	13	9	15	36	239	169	111
31	289		460		57		9	17		131		91
Mean	571	637	556	393	46	15	7	157	499	138	286	310

Daily discharge, in second-feet, of Tohickon Creek at Point Pleasant, Pennsylvania, for 1888.

Daily discharge, in second-feet, of Tohickon Creek at Point Pleasant, Pennsylvania, for 1889.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1	$\begin{array}{r} 86\\ 87\\ 772\\ 124\\ 968\\ 637\\ 263\\ 691\\ 1,080\\ 288\\ 149\\ 90\\ 288\\ 104\\ 104\\ 104\\ 99\\ 81\\ 1,530\\ 742\\ 230\\ 112\\ 230\\ 112\\ \end{array}$	$\begin{array}{c} 124\\ 99\\ 92\\ 86\\ 8\\ 82\\ 71\\ 125\\ 148\\ 88\\ 8\\ 8\\ 8\\ 8\\ 8\\ 8\\ 61\\ 60\\ 60\\ 61\\ 45\\ 514\\ 819\\ 683\\ 228\\ 148\\ 812\\ 812\\ 828\\ 148\\ 812\\ 812\\ 812\\ 812\\ 812\\ 812\\ 812\\ 81$	$\begin{array}{r} 36\\ 52\\ 386\\ 2,567\\ 2,141\\ 320\\ 195\\ 134\\ 108\\ 100\\ 84\\ 79\\ 92\\ 997\\ 84\\ 75\\ 88\\ 105\\ 113\\ 214\\ \end{array}$	$\begin{array}{c} 295\\ 958\\ 330\\ 183\\ 103\\ 83\\ 78\\ 75\\ 66\\ 55\\ 55\\ 53\\ 64\\ 67\\ 64\\ 61\\ 56\\ 54\\ 49\\ 49\\ 44\end{array}$	$\begin{array}{c} 135\\ 101\\ 79\\ 63\\ 54\\ 48\\ 43\\ 42\\ 36\\ 43\\ 40\\ 40\\ 44\\ 44\\ 44\\ 44\\ 44\\ 44\\ 44\\ 44$	$\begin{array}{c} 340\\ 441\\ 156\\ 82\\ 64\\ 552\\ 45\\ 39\\ 321\\ 31\\ 242\\ 308\\ 63\\ 110\\ 565\\ 263\\ 383\\ 310\\ 110\\ 565\\ 263\\ 383\\ 383\\ 383\\ 382\\ 550\\ 161\\ 822\\ 500\\ 565\\ 565\\ 565\\ 565\\ 565\\ 565\\ 565$	$\begin{array}{c} 210\\ 939\\ 1,482\\ 1,053\\ 697\\ 574\\ 123\\ 80\\ 54\\ 88\\ 70\\ 111\\ 11\\ 12,156\\ 787\\ 188\\ 82\\ 262\\ 1,975\\ 422 \end{array}$	$\begin{array}{c} 2,602\\ 815\\ 367\\ 195\\ 211\\ 194\\ 119\\ 84\\ 662\\ 555\\ 2,177\\ 83\\ 2,115\\ 2,177\\ 406\\ 164\\ 98\\ 69\\ 59\\ 49\\ 59\\ 49\end{array}$	$\begin{array}{c} 17\\ 16\\ 17\\ 20\\ 11\\ 9\\ 11\\ 11\\ 11\\ 11\\ 14\\ 16\\ 166\\ 155\\ 532\\ 2,019\\ 3,028\\ 320\\ 367\\ 201\\ \end{array}$	$\begin{array}{c} 63\\ 68\\ 62\\ 49\\ 46\\ 425\\ 333\\ 31\\ 39\\ 32\\ 55\\ 96\\ 314\\ 248\\ 51\\ 111\\ 68\\ 51\\ 111\\ 44\\ 43\\ 97\end{array}$	$\begin{array}{c} 139\\ 131\\ 1,041\\ 813\\ 263\\ 166\\ 166\\ 131\\ 116\\ 2,308\\ 406\\ 233\\ 963\\ 2333\\ 1,339\\ 331\\ 166\\ 119\\ 102\\ 1,623\\ 1,041\\ 508\end{array}$	$\begin{array}{c} 151\\ 120\\ 111\\ 103\\ 85\\ 75\\ 75\\ 136\\ 351\\ 214\\ 165\\ 148\\ 111\\ 108\\ 248\\ 171\\ 560\\ 606\\ 606\\ 337\\ 241\\ 158\end{array}$
22 23 24 25 26 27 28 29 29 30 31	$\begin{array}{c} 1397\\ 263\\ 211\\ 258\\ 313\\ 778\\ 1,096\\ 440\\ 187\\ 191\\ \end{array}$	94 66 51 74 73 45 37	$\begin{array}{c} 951\\ 623\\ 266\\ 158\\ 114\\ 97\\ 112\\ 124\\ 104\\ 87\\ \end{array}$	$\begin{array}{r} 42\\ 71\\ 54\\ 29\\ 424\\ 2,126\\ 1,439\\ 582\\ 241\\ \end{array}$	$\begin{array}{c} 450\\ 186\\ 95\\ 68\\ 357\\ 744\\ 244\\ 118\\ 80\\ \end{array}$	$39 \\ 33 \\ 28 \\ 29 \\ 807 \\ 610 \\ 214 \\ 368 \\ 215 $	$\begin{array}{c} 139\\ 88\\ 69\\ 48\\ 41\\ 58\\ 65\\ 91\\ 844\\ 4,714\\$	$ \begin{array}{c} 41\\ 47\\ 37\\ 39\\ 33\\ 35\\ 37\\ 33\\ 22\\ 19\\ 20\\ \end{array} $	$\begin{array}{c} 163\\ 115\\ 85\\ 459\\ 524\\ 260\\ 140\\ 93\\ 70\\ \end{array}$	$129 \\ 104 \\ 97 \\ 72 \\ 57 \\ 2,958 \\ 1,648 \\ 392 \\ 194 \\ 147 \\ 147 \\ 147 \\ 104$	816 302 163 457 557 724 2,768 645 234	$\begin{array}{c} 119 \\ 106 \\ 92 \\ 74 \\ 150 \\ 225 \\ 100 \\ 75 \\ 69 \\ 55 \\ \end{array}$
Mean	389	149	341	264	151	189	570	334	317	207	733	172

Daily discharge, in second-feet, of Toi	ickon Creek at Point Pleasant, Pennsylvania,
	for 1890.

	Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
$-\frac{1}{22} + \frac{1}{2} + $		$51 \\ 53 \\ 57 \\ 51 \\ 62 \\ 98 \\ 102 \\ 87 \\ 76 \\ 65 \\ 57 \\ 48 \\ 45 \\ 45 \\ 45 \\ 1,110 \\ 1,586 \\ 422 \\ 160 \\ 100 \\ 10$	$\begin{array}{c} 114\\ 84\\ 95\\ 155\\ 239\\ 131\\ 75\\ 2,512\\ 2,000\\ 298\\ 176\\ 141\\ 117\\ 420\\ 806\\ 192\\ 124\\ 107\\ \end{array}$	$\begin{array}{c} 766\\ 349\\ 124\\ 92\\ 87\\ 83\\ 71\\ 71\\ 71\\ 71\\ 71\\ 71\\ 71\\ 1,18\\ 978\\ 978\\ 978\\ 440\\ 1,993\\ 1,993\\ 168\\ 228\\ 166\end{array}$	$\begin{array}{c} 176\\ 197\\ 126\\ 378\\ 721\\ 191\\ 143\\ 778\\ 758\\ 241\\ 128\\ 244\\ 128\\ 99\\ 84\\ 68\\ 61\\ 54\\ 48\end{array}$	$\begin{array}{c} & \\ & 41 \\ & 34 \\ & 34 \\ & 24 \\ & 2497 \\ & 153 \\ & 115 \\ & 788 \\ & 60 \\ & 53 \\ & 417 \\ & 1,037 \\ & 480 \\ & 146 \\ & 88 \end{array}$	$51 \\ 50 \\ 33 \\ 337 \\ 388 \\ 107 \\ 66 \\ 41 \\ 322 \\ 91 \\ 4852 \\ 352 \\ 118 \\ 65 \\ 466 \\ 38 \\ 38$	$\begin{array}{c} 14\\ 125\\ 436\\ 687\\ 147\\ 71\\ 36\\ 45\\ 233\\ 18\\ 12\\ 12\\ 12\\ 16\\ 18\\ 9\\ 19\\ 20\\ \end{array}$	$\begin{array}{c} 22\\ 22\\ 17\\ 12\\ 53\\ 32\\ 25\\ 25\\ 216\\ 22\\ 19\\ 14\\ 13\\ 11\\ 10\\ 14\\ \end{array}$	$\begin{array}{c} 34\\ 30\\ 27\\ 21\\ 17\\ 18\\ 12\\ 17\\ 18\\ 12\\ 17\\ 10\\ 15\\ 97\\ 438\\ 612\\ 797\\ 438\\ 612\\ 797\\ 438\\ 612\\ 797\\ 438\\ 612\\ 797\\ 438\\ 612\\ 797\\ 438\\ 612\\ 797\\ 797\\ 438\\ 612\\ 797\\ 797\\ 797\\ 797\\ 797\\ 797\\ 797\\ 79$	$\begin{array}{c} 23\\ 18\\ 810\\ 783\\ 194\\ 281\\ 163\\ 91\\ 67\\ 49\\ 255\\ 54\\ 75\\ 73\\ 935\\ 405 \end{array}$	$\begin{array}{c} 75\\ 64\\ 52\\ 48\\ 42\\ 38\\ 35\\ 35\\ 35\\ 35\\ 37\\ 45\\ 107\\ 89\\ 63\\ 48\\ 43\\ 112\\ 249 \end{array}$	$\begin{array}{c c} & & & & \\ & & & & \\ & & & & \\ & & & & $
$\frac{19}{20} \frac{21}{22} \frac{22}{2} \frac{24}{2} \frac{25}{2} \frac{27}{2} \frac{29}{2} \frac{31}{31}$	Mon	$\begin{array}{c} 108\\ 109\\ 265\\ 109\\ 120\\ 109\\ 78\\ 50\\ 62\\ 71\\ 64\\ 97\\ 160\\ \hline \end{array}$	94 693 414 146 107 115 186 219 154 482	$\begin{array}{c} 132\\ 151\\ 1,290\\ 2,942\\ 1,908\\ 422\\ 214\\ 436\\ 264\\ 1,695\\ 919\\ 206\\ 161\\ \end{array}$	48 42 36 42 44 39 36 42 51 56 50 43	$\begin{array}{c} 65\\ 214\\ 292\\ 117\\ 70\\ 53\\ 422\\ 1,278\\ 1,967\\ 416\\ 154\\ 92\\ 67\\ \hline 270\end{array}$	36 31 31 34 35 44 42 27 20 17 15 25	$ \begin{array}{c} 17 \\ 12 \\ 12 \\ 11 \\ 4 \\ 9 \\ 11 \\ 317 \\ 122 \\ 68 \\ 43 \\ 34 \\ 29 \\ \hline 79 \\ \hline 79 \\ \hline 70 \\ \hline $	$\begin{array}{c} 27\\ 478\\ 290\\ 130\\ 159\\ 57\\ 38\\ 36\\ 405\\ 261\\ 95\\ 119\\ 45\\ \end{array}$	81 4323 3323 232 232 232 232 232 232 232 2	$\begin{array}{c} 143\\118\\104\\79\\469\\2,624\\358\\183\\122\\103\\128\\115\\\hline\end{array}$	$ \begin{array}{c} 100\\ 89\\ 64\\ 54\\ 85\\ 82\\ 41\\ 31\\ 26\\ 21\\ 33\\ 27\\ 63\\ \end{array} $	239 154 121 90 88 68 80 80 173 193 191 106 73 68
	Mean	181	371	602	165	270	68	79	81	112	320	63	135

Daily discharge, in second-feet of Tohickon Creek at Point Pleasant, Pennsylvania, for 1891.

		1	1		1	1		1	1	l'	1		1
	Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
$-\frac{1}{223} \\ \frac{4}{45} \\ \frac{6}{6} \\ \frac{7}{89} \\ \frac{9}{10} \\ \frac{11}{123} \\ \frac{14}{156} \\ \frac{19}{202} \\ \frac{222}{24} \\ \frac{2}{22} \\ \frac{2}{2} \\ 2$		$\begin{array}{c} 61\\ 1,397\\ 1,4213\\ 150\\ 116\\ 148\\ 104\\ 85\\ 57\\ 767\\ 2,331\\ 354\\ 179\\ 127\\ 94\\ 185\\ 748\\ 267\\ 188\\ 141\\ 1,146\\ 364\\ 250\\ 234\\ 204\\ 466\\ 1,269\\ 1091\\ 1,091\\ \end{array}$	1,726 1,726 1,105 779 614 213 180 210 637 516 972 320 975 516 972 320 130 97 975 782 820 663 241 150 130 97 975 782 820 663 241 1,005 130 97 241 130 130 97 272 130 130 97 204 130 130 97 204 130 130 97 204 130 130 97 204 130 130 97 204 130 130 97 204 130 130 97 204 130 130 97 204 130 97 204 130 97 204 130 97 204 130 97 204 130 97 204 130 130 97 204 130 204 130 204 130 204 130 204 130 204 130 204 130 204 130 204 130 204 130 204 130 204 130 204 130 204 130 204 130 204 130 204 130 204 130 204 105 100 204 130 204 100 204 100 204 100 204 100 204 100 204 100 204 100 100 100 100 100 100 100 1	$\begin{array}{c} 202\\ 148\\ 110\\ 85\\ 93\\ 93\\ 82\\ 116\\ 601\\ 713\\ 1,500\\ 601\\ 718\\ 1,500\\ 601\\ 718\\ 1,500\\ 601\\ 718\\ 1,82\\ 228\\ 158\\ 208\\ 208\\ 208\\ 188\\ 158\\ 208\\ 208\\ 208\\ 208\\ 208\\ 208\\ 208\\ 20$	$\begin{array}{c} 125\\ 125\\ 178\\ 814\\ 814\\ 814\\ 814\\ 814\\ 814\\ 814\\ 81$	$\begin{array}{c c} & & & \\ & & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & &$	$\begin{array}{c} 19\\ 19\\ 18\\ 13\\ 11\\ 12\\ 13\\ 12\\ 14\\ 26\\ 26\\ 15\\ 13\\ 12\\ 26\\ 16\\ 323\\ 20\\ 28\\ 23\\ 22\\ 23\\ 22\\ 23\\ 214\\ 21\\ 17\\ 6\\ 9\end{array}$	$\begin{array}{c} 8 \\ 8 \\ 7 \\ 8 \\ 7 \\ 7 \\ 6 \\ 6 \\ 5 \\ 13 \\ 9 \\ 12 \\ 5 \\ 4 \\ 4 \\ 7 \\ 3 \\ 34 \\ 299 \\ 120 \\ 31 \\ 229 \\ 321 \\ 229 \\ 321 \\ 2571 \\ 611 \\ 515 \end{array}$	$\begin{array}{c c} 1172\\ 91\\ 60\\ 38\\ 31\\ 31\\ 31\\ 31\\ 31\\ 31\\ 31\\ 31\\ 31\\ 31$	$\begin{array}{c} 276\\ 276\\ 123\\ 92\\ 78\\ 326\\ 532\\ 249\\ 116\\ 68\\ 53\\ 249\\ 49\\ 49\\ 49\\ 49\\ 49\\ 49\\ 49\\ 49\\ 49\\ $	$\begin{array}{c} 10\\ 10\\ 11\\ 10\\ 8\\ 15\\ 15\\ 15\\ 15\\ 15\\ 11\\ 20\\ 10\\ 10\\ 10\\ 10\\ 10\\ 10\\ 10\\ 10\\ 10\\ 1$	$\begin{array}{c} 27\\ 27\\ 300\\ 200\\ 17\\ 17\\ 18\\ 21\\ 16\\ 6\\ 129\\ 299\\ 27\\ 299\\ 24\\ 21\\ 58\\ 136\\ 61\\ 426\\ 428\\ 128\\ 386\\ 618\\ 442\\ 128\\ 386\\ 108\\ 45\\ 55\\ 55\\ 55\\ 55\\ 55\\ 59\\ 59\\ \end{array}$	$\begin{array}{c} 566\\ 388\\ 333\\ 333\\ 333\\ 333\\ 333\\ 333\\ 3$
	Mean	545	540	446	144	25	17	81	349	85	39	58	379

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
Day.	Jan. 148 1,090 1,177 262 158 108 120 150 120 150 120 150 120 150 2,863 3,158 2,580 260 261 1,618	$\begin{tabular}{ c c c c c c c c c c c c c c c c c c c$	Mar. 1, 645 831 433 348 283 218 237 1, 421 1, 421 1, 421 1, 421 1, 421 1, 421 1, 421 1, 421 1, 625 390 207 84 86 86 87 88 86 87 87 87 87 87 87 87 87 87 87	Apr. 113 100 100 105 95 86 67 47 49 35 33 133 177 90 057 42	May. 40 47 1599 108 70 60 60 555 557 43 39 39 39 39 39 143 857 555 555 555 555 555 555 555	June. 76 60 43 45 64 45 58 43 90 555 287 108 61 46 41 32 31 92 17 17	$\begin{array}{c c} \textbf{July.} \\ \hline \\ \\ \hline \\$	Aug. 21 37 31 33 21 24 24 9 15 15 15 15 15 15 15 16 7 7 101 38 28 23 13 14 11	Sept. 20 16 12 10 15 19 13 13 16 12 5 9 10 13 13 13 16 12 13 13 16 12 10 13 13 16 12 10 13 16 12 10 13 16 12 10 13 16 12 10 13 16 12 10 13 16 12 10 13 16 12 10 13 16 12 10 13 16 12 10 13 16 12 10 13 13 16 12 10 13 16 12 10 13 16 16 12 10 13 16 16 17 16 16 17 16 16 17 16 16 17 16 16 17 16 16 16 17 16 16 17 16 16 17 16 16 17 16 16 17 16 17 16 17 16 17 17 17 17 17 17 17 17 17 17	Oct. 15 8 11 14 17 14 17 14 17 14 17 14 17 14 11 16 8 7 9 11 11 16 8 6 8 6 6 6 6 6 6 6 6 6 6 6 6 6	Nov. 8 9 8 6 9 9 9 6 57 3013 113 64 483 2,962 522 669 896 896 896 896 896 896 896	Dec. 160 98 71 59 57 380 118 105 78 54 283 300 158 118 105 78 9 9 9 9 9 9 9 9 9 9 9 9 9
20 21 22 23		$ \begin{array}{r} 35 \\ 73 \\ 109 \\ 112 \\ 12 \end{array} $	65 65 65	$35 \\ 44 \\ 95 \\ 191$	$ \begin{array}{r} 340 \\ 401 \\ 529 \\ 458 \\ 458 \end{array} $	$22 \\ 23 \\ 15 \\ 15 \\ 15 \\ 15 \\ 15 \\ 15 \\ 15 \\ 1$	7 6 5 8	$9 \\ 11 \\ 10 \\ 10 \\ 10$	17 27 11 18 1		$509 \\ 370 \\ 88 \\ 64 \\ 64$	80 85 74 85
24 25 26 27 28 28 29	$ \begin{array}{r} 131 \\ 121 \\ 119 \\ 129 \\ 193 \\ 277 \end{array} $	$ \begin{array}{r} 105 \\ 92 \\ 156 \\ 190 \\ 121 \\ 87 \end{array} $	$271 \\ 727 \\ 574 \\ 1,036 \\ 1,115 \\ 413$	$ \begin{array}{r} 131 \\ 71 \\ 57 \\ 46 \\ 46 \\ 50 \end{array} $	$250 \\ 177 \\ 132 \\ 1,333 \\ 522 \\ 184$	$ \begin{array}{r} 17 \\ 16 \\ 20 \\ 26 \\ 21 \\ 14 \end{array} $	9 8 8 5 5 8		$25 \\ 13 \\ 227 \\ 59 \\ 33 \\ 22$	$\begin{array}{r} 4\\ 4\\ 6\\ 11\\ 10\\ 6\end{array}$	$51 \\ 48 \\ 40 \\ 35 \\ 180 \\ 676$	$ \begin{array}{r} 125 \\ 184 \\ 246 \\ 154 \\ 201 \\ 168 \end{array} $
30 31 Mean	226 166 580	116	194 135 433	50 77	112 86 188	14 65	9 12 45	30 30 29	19 	5 5 8	195 	103 68 148

Daily discharge, in second-feet, of Tohickon Creek at Point Pleasant, Pennsylvania, for 1892.

Daily discharge, in second-feet, of Tohickon Creek at Point Pleasant, Pennsylvania, for 1893.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28	$\begin{array}{c} \cdot\\ & 474\\ 1,406\\ 301\\ 158\\ 104\\ 100\\ 131\\ 140\\ 140\\ 140\\ 160\\ 204\\ 203\\ 138\\ 140\\ 203\\ 138\\ 165\\ 170\\ 118\\ 95\\ 63\\ 105\\ 95\\ 61\\ 59\\ 65\\ 53\\ \end{array}$	$\begin{array}{r} 489\\8003\\1,366\\1,118\\1,168\\1,113\\2,597\\1,742\\320\\2,597\\1,732\\462\\846\\905\\1,113\\672\\248\\846\\905\\1,113\\201\\162\\136\\114\\922\\87\\87\\87\\87\\87\\87\\87\\87\\87\\87\\87\\87\\87\\$	$\begin{array}{r} 78\\97\\108\\108\\108\\87\\2,200\\850\\2,406\\857\\2,200\\2,406\\856\\162\\295\\246\\295\\246\\295\\246\\295\\318\\254\\114\\114\\114\\114\\114\\114\\114\\114\\114\\1$	$\begin{array}{c} 78\\68\\51\\58\\54\\49\\140\\145\\132\\249\\150\\106\\358\\1,68\\151\\515\\1,903\\448\\185\\135\\1903\\48\\185\\135\\289\\289\end{array}$	$\begin{array}{c} 279\\ 348\\ 832\\ 2,994\\ 1,102\\ 872\\ 413\\ 207\\ 124\\ 872\\ 811\\ 712\\ 124\\ 89\\ 811\\ 712\\ 830\\ 811\\ 712\\ 585\\ 655\\ 3309\\ 919\\ 801\\ 877\\ 711\\ 574\\ 496\\ 422\\ 496\\ 422\\ 496\\ 433\\ 833\\ 833\\ 833\\ 833\\ 833\\ 833\\ 833$	$\begin{array}{c} 35\\ 331\\ 209\\ 195\\ 395\\ 39\\ 35\\ 21\\ 14\\ 17\\ 16\\ 139\\ 99\\ 170\\ 217\\ 585\\ 428\\ 25\\ \end{array}$	$\begin{array}{c} 16\\ 155\\ 125\\ 252\\ 123\\ 12\\ 29\\ 9\\ 11\\ 9\\ 6\\ 62\\ 122\\ 13\\ 9\\ 7\\ 5\\ 6\\ 6\\ 4\\ 3\\ 3\\ 4\\ 7\\ 6\\ 6\\ 12\\ 22\\ 12\\ 12\\ 19\\ 9\\ 7\\ 5\\ 6\\ 6\\ 4\\ 3\\ 3\\ 4\\ 7\\ 6\\ 6\\ 12\\ 22\\ 12\\ 12\\ 12\\ 12\\ 12\\ 12\\ 12\\ 12$	$\begin{array}{c} 8\\ 8\\ 129\\ 9\\ 4\\ 3\\ 9\\ 5\\ 4\\ 10\\ 5\\ 5\\ 4\\ 10\\ 5\\ 5\\ 6\\ 3\\ 3\\ 3\\ 3\\ 4\\ 4\\ 545\\ 5\\ 6\\ 3\\ 3\\ 3\\ 3\\ 4\\ 4\\ 545\\ 5\\ 119\\ 5\\ 5\\ 4\\ 4\\ 5\\ 119\\ 5\\ 5\\ 4\\ 4\\ 5\\ 4\\ 5\\ 4\\ 5\\ 5\\ 5\\ 6\\ 5\\ 5\\ 6\\ 5\\ 5\\ 6\\ 5\\ 5\\ 6\\ 5\\ 6\\ 5\\ 5\\ 6\\ 5\\ 6\\ 5\\ 5\\ 6\\ 5\\ 6\\ 5\\ 6\\ 5\\ 6\\ 5\\ 5\\ 6\\ 6\\ 5\\ 6\\ 6\\ 5\\ 6\\ 5\\ 6\\ 5\\ 6\\ 6\\ 5\\ 6\\ 6\\ 5\\ 6\\ 6\\ 6\\ 6\\ 6\\ 5\\ 6\\ 6\\ 6\\ 6\\ 6\\ 6\\ 6\\ 6\\ 6\\ 6\\ 6\\ 6\\ 6\\$	$\begin{array}{c} & & & \\ & & & & \\ & & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & &$	$\begin{array}{c} 11\\ 11\\ 12\\ 10\\ 12\\ 17\\ 10\\ 12\\ 10\\ 12\\ 10\\ 12\\ 10\\ 11\\ 11\\ 12\\ 30\\ 49\\ 39\\ 31\\ 22\\ 20\\ 23\\ 15\\ 9\\ 68\\ 9\\ 506\\ 506\end{array}$	$\begin{array}{c} 51\\ 48\\ 48\\ 1,094\\ 1,288\\ 184\\ 123\\ 101\\ 79\\ 711\\ 62\\ 54\\ 60\\ 103\\ 130\\ 90\\ 60\\ 53\\ 48\\ 46\\ 496\\ 312\\ 120\\ 81\\ 62\\ 55\\ 1,244\\ \end{array}$	$\begin{array}{c} 1222\\ 1022\\ 102\\ 1021\\ $
29 30 31	83 312 511		97 92 83	160 118	31 33 33 	21	9 7 4	499 198 92	20 17	279 116 66	479 188	81 83 75
Mean	197	699	403	293	333	40	10	139	16	55	244	215

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1	73	125	216	64	47	267	20	7	4	13	522	37
2	10	113	148	63	41	189	10	0	4	10	1 109	243
ð	61	89	291	0% 54		14%	13	95	0	11	1,195 707	450
5	74	88	1 065	254	34	01	10	20	9	13	719	103
6	114	119	1,174	141	34	75	29	24	$\tilde{2}$	11	966	73
7	131	156	1,102	92	58	64	47	35	3	7	282	58
8	109	115	488	79	53	61	31	18	4	9	545	126
9	87	651	258	71	50	49	22	8	5	12	439	606
10	70	1,113	220	73	42	40	17	5	20	1,674	224	284
11	52	911	188	73	28	34	16	5	31	885	168	635
12	46	383	153	1 128	29	27	11	5	33	127	115	3,342
13	46	140	131	1,168	16	23	10	5	25	125	83	1,811
14	49	140	109	1,203	17	23	10	0	23	180	11	3//
10	49	119	109	999	17	20	5	0	20	110	01	190
10	64	112	102	144	17	19	6	0	41 92	47	70	140
19	51	098	71	103	16	15	10	11	3 510	20	101	97
10	51	1 606	67	79	17	14	8	11	3 556	34	104	83
20	46	1.257	64	71	616	10	ß	8	1.306	32	73	75
21	41	723	61	71	8,650	12	11	8	245	27	73	66
22	43	379	71	303	4,310	7	68	9	83	23	97	61
23	45	208	534	321	904	7	49	9	50	21	93	58
24	51	118	351	132	1,827	6	25	9	41	29	75	57
25	89	151	143	101	1,577	13	21	10	29	725	63	46
26	98	151	122	81	450	36	14	6	23	477	61	42
27	10	151	100	68	1 228	:29	10	6	19	168	49	44
28	68	231	70	10	1,080	26	8	11	20	99	44	83
20	107		70	47	506	19) A	4		59	40	109
21	137		79	41	267	19	4	4	40	610	- 59	140
01	101		10		1.01		0	4		940		110
Mean	71	373	275	209	760	49	17	10	306	186	245	316

Daily discharge, in second-feet, of Tohickon Creek at Point Pleasant, Pennsylvania, for 1894.

Daily discharge, in second-feet, of Tohickon Creek at Point Pleasant, Pennsylvania, for 1895.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1 2 3 4 5 6 7 8 9 10 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29	$\begin{array}{c} 622\\ 622\\ 800\\ 899\\ 127\\ 50\\ 381\\ 848\\ 418\\ 448\\ 4982\\ 204\\ 146\\ 169\\ 112\\ 204\\ 146\\ 169\\ 112\\ 800\\ 112\\ 515\\ 15\\ 16\\ 169\\ 112\\ 12\\ 10\\ 169\\ 112\\ 10\\ 10\\ 10\\ 10\\ 10\\ 10\\ 10\\ 10\\ 10\\ 10$	$\begin{array}{c} 138\\ 156\\ 180\\ 163\\ 1193\\ 104\\ 711\\ 54\\ 92\\ 168\\ 108\\ 108\\ 108\\ 108\\ 108\\ 108\\ 108\\ 245\\ 58\\ 148\\ 245\\ 255\\ 245\\ 255\\ 245\\ 245\\ 245\\ 266\\ 902\\ \end{array}$	$\begin{array}{c} 1,296\\ 1,064\\ 706\\ 495\\ 352\\ 248\\ 197\\ 1,116\\ 943\\ 491\\ 451\\ 317\\ 383\\ 31,519\\ 437\\ 200\\ 166\\ 192\\ 343\\ 450\\ 162\\ 328\\ 328\\ 328\\ 328\\ 328\\ 328\\ 328\\ 32$	$\begin{array}{c} 1222\\117\\2100\\239\\131\\99\\889\\1,404\\3,857\\1,760\\616\\146\\1,131\\1,191\\5271\\117\\88\\271\\117\\88\\55\\51\\49\\47\\43\\41\\41\\42\\599\\76\\69\\69\\69\\69\\69\\69\\69\\69\\69\\69\\69\\69\\69$	$\begin{array}{c} 107\\ 866\\ 157\\ 47\\ 42\\ 39\\ 400\\ 35\\ 35\\ 35\\ 35\\ 35\\ 35\\ 89\\ 155\\ 93\\ 63\\ 44\\ 44\\ 31\\ 333\\ 35\\ 333\\ 33\\ 33\\ 33\\ 33\\ 33\\ 33\\ $	$\begin{array}{c} 36\\ 33\\ 33\\ 39\\ 26\\ 57\\ 58\\ 47\\ 23\\ 20\\ 223\\ 20\\ 223\\ 20\\ 223\\ 20\\ 223\\ 20\\ 20\\ 223\\ 20\\ 10\\ 10\\ 10\\ 11\\ 11\\ 11\\ 11\\ 9\\ 10\\ 8\\ 8\\ 7\\ 9\\ 9\\ 14\\ 16\\ 14\\ 14\\ 14\\ 55\\ 16\\ 16\\ 16\\ 16\\ 16\\ 16\\ 16\\ 16\\ 16\\ 16$	$\begin{array}{c} 61\\ 96\\ 61\\ 57\\ 579\\ 648\\ 240\\ 1000\\ 554\\ 327\\ 21\\ 18\\ 12\\ 158\\ 12\\ 10\\ 88\\ 250\\ 200\\ 14\\ 12\\ 11\\ 11\\ 11\\ 11\\ 11\\ 9\\ 71\\ \end{array}$	$\begin{array}{c} 7 \\ 6 \\ 8 \\ 310 \\ 145 \\ 299 \\ 16 \\ 9 \\ 9 \\ 229 \\ 12 \\ 10 \\ 9 \\ 229 \\ 12 \\ 17 \\ 17 \\ 8 \\ 6 \\ 10 \\ 9 \\ 5 \\ 7 \\ 6 \\ 5 \\ 5 \\ 4 \\ 4 \\ 4 \\ 5 \\ 1 \\ 5 \\ 1 \\ 5 \\ 5 \\ 5 \\ 5 \\ 5 \\ 5$	4 3 5 6 2 4 5 6 4 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	33332333433555222594144115778766665555	$\begin{array}{c} 15\\233\\29\\16\\22\\21\\1\\12\\10\\9\\15\\3\\12\\13\\22\\15\\15\\11\\1\\9\\9\\66\\38\\5\\38\\5\end{array}$	$\begin{array}{c} 222\\546\\866\\51\\886\\825\\200\\88\\825\\200\\88\\820\\88\\820\\88\\82\\91\\11\\8\\8\\420\\22\\24\\24\\291\\54\\46\\60\\88\\57\\7\\11\\14\\420\\22\\24\\25\\46\\60\\88\\57\\7\\11\\14\\420\\22\\25\\25\\16\\16\\16\\16\\16\\16\\16\\16\\16\\16\\16\\16\\16\\$
31 Mean	102 351	167	114 476	426	50 62	25	7 71	4 32	3	8	20	109 59

16

225

94

102

16

214

71

	Day Jan Feb Mar Anr May June July Aug Sent Oct Nov Dec														
Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.			
1 2 3 4 5 6 7 8 9 10 12 13 14 15 16 17 18 19 20 21 22 23 24 25 25	$\begin{array}{r} 327\\ 93\\ 59\\ 399\\ 399\\ 399\\ 28\\ 17\\ 16\\ 13\\ 16\\ 13\\ 13\\ 16\\ 6\\ 6\\ 5\\ 5\\ 5\\ 5\\ 5\\ 5\\ 5\\ 5\\ 5\\ 151\\ 2399\\ 136\\ 239\\ 136\\ 239\\ 136\\ 239\\ 136\\ 239\\ 238\\ 238\\ 238\\ 238\\ 238\\ 238\\ 238\\ 238$	$\begin{array}{c} 55\\ 90\\ 83\\ 58\\ 138\\ 6,515\\ 1,720\\ 487\\ 201\\ 174\\ 225\\ 156\\ 156\\ 107\\ 327\\ 206\\ 107\\ 75\\ 75\\ 75\\ 75\\ 75\\ 75\\ 75\\ 75\\ 75\\ 7$	$\begin{array}{c} 498\\ 192\\ 50\\ 48\\ 59\\ 59\\ 59\\ 57\\ 444\\ 42\\ 44\\ 42\\ 444\\ 42\\ 551\\ 51\\ 51\\ 51\\ 51\\ 51\\ 2,028\\ 3,343\\ 1,205\\ 7429\\ 449\\ 193\\ 98\\ 371\\ 198\\ 98\\ 371\\ 198\\ 98\\ 371\\ 108\\ 108\\ 108\\ 108\\ 108\\ 108\\ 108\\ 10$	$\begin{array}{c} 297\\ 236\\ 193\\ 101\\ 71\\ 72\\ 81\\ 85\\ 727\\ 53\\ 51\\ 111\\ 51\\ 11\\ 51\\ 11\\ 51\\ 40\\ 33\\ 33\\ 33\\ 25\\ 25\\ 21\\ 11\\ 11\\ 51\\ 11\\ 51\\ 25\\ 25\\ 25\\ 25\\ 25\\ 25\\ 25\\ 25\\ 25\\ 25$	$\begin{array}{c} 20\\ 23\\ 18\\ 21\\ 26\\ 25\\ 25\\ 25\\ 25\\ 25\\ 25\\ 19\\ 11\\ 12\\ 11\\ 12\\ 11\\ 12\\ 11\\ 12\\ 10\\ 14\\ 4\\ 11\\ 11\\ 12\\ 10\\ 14\\ 10\\ 16\\ 61\\ 61\\ 72\\ 38\\ 23\\ 23\\ 23\\ 23\\ 23\\ 23\\ 23\\ 23\\ 23\\ 23$	$\begin{array}{c} 35\\ 35\\ 31\\ 28\\ 10\\ 11\\ 11\\ 9\\ 12\\ 11\\ 11\\ 9\\ 28\\ 28\\ 28\\ 28\\ 28\\ 28\\ 28\\ 28\\ 28\\ 11\\ 7\\ 8\\ 14\\ 16\\ 11\\ 12\\ 21\\ 21\\ 21\\ 21\\ 21\\ 21\\ 21\\ 21$	$\begin{array}{c} 11\\ 10\\ 10\\ 10\\ 7\\ 5\\ 13\\ 16\\ 38\\ 104\\ 76\\ 33\\ 104\\ 76\\ 33\\ 104\\ 222\\ 15\\ 10\\ 10\\ 9\\ 9\\ 6\\ 6\\ 9\\ 2, 417\\ 704\\ 304\\ 85\\ 46\\ 46\\ 5\\ 46\\ 5\\ 85\\ 85\\ 85\\ 85\\ 85\\ 85\\ 85\\ 85\\ 85\\$	$\begin{array}{c} 113\\56\\35\\27\\12\\22\\12\\12\\10\\9\\12\\9\\10\\47\\6\\8\\8\\8\\9\\7\\5\\3\\6\\6\\7\\6\\6\\6\end{array}$	$\begin{array}{c} 3\\ 3\\ 4\\ 5\\ 10\\ 1,665\\ 319\\ 95\\ 44\\ 29\\ 23\\ 14\\ 14\\ 10\\ 10\\ 10\\ 10\\ 10\\ 10\\ 10\\ 10\\ 10\\ 10$	$\begin{array}{c} 167\\ 59\\ 27\\ 29\\ 24\\ 200\\ 17\\ 10\\ 16\\ 16\\ 29\\ 215\\ 103\\ 48\\ 38\\ 28\\ 38\\ 28\\ 38\\ 28\\ 38\\ 28\\ 38\\ 28\\ 55\\ 76\\ 6\\ 54\\ 55\\ 4\\ 54\\ 54\\ 54\\ 54\\ 54\\ 54\\ 54\\$	$\begin{array}{c} 23\\19\\20\\20\\21\\1,851\\1,249\\273\\180\\279\\131\\180\\103\\136\\103\\136\\103\\136\\36\\36\\36\\35\\37\\37\\37\\47\\42\\46\\46\\46\\46\\36\\36\\36\\36\\36\\36\\36\\36\\36\\36\\36\\36\\36$	$\begin{array}{c} 177\\ 104\\ 78\\ 65\\ 59\\ 59\\ 51\\ 61\\ 72\\ 289\\ 242\\ 98\\ 98\\ 98\\ 71\\ 556\\ 53\\ 44\\ 45\\ 52\\ 57\\ 44\\ 49\\ 51\\ 44\\ 44\\ 44\\ 43\\ 59\\ 399\\ 39\end{array}$			
24 28 29 30 31	$ \begin{array}{r} 70 \\ 59 \\ 46 \\ 28 \\ 31 \end{array} $	229 851	590 311 2,444 1,238 527	35 26 20		10 13 15 10 13 15 15 10	$ \begin{array}{c c} & 44 \\ & 163 \\ & 184 \\ & 2,182 \\ & 410 \end{array} $	0 10 10 00 00 00 00		38 31 31 30 27	$ \begin{array}{r} 35 \\ 45 \\ 856 \\ 439 \end{array} $	39 39 35 31 27			

67

486

Daily discharge, in second-feet, of Tohickon Creek at Point Pleasant, Pennsylvania,

Daily discharge, in second-feet, of Tohickon Creek at Point Pleasant, Pennsylvania, for 1897.

27

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 20 21 22 23 24 25 26 27 28 29 30 31	$\begin{array}{c} 31\\ 49\\ 157\\ 3300\\ 404\\ 256\\ 89\\ 71\\ 553\\ 49\\ 49\\ 49\\ 49\\ 49\\ 49\\ 49\\ 49\\ 49\\ 49$	$\begin{array}{c} 73\\ 97\\ 79\\ 65\\ 49\\ 430\\ 2, 312\\ 882\\ 311\\ 175\\ 109\\ 68\\ 89\\ 9\\ 65\\ 733\\ 246\\ 404\\ 320\\ 0\\ 122\\ 203\\ 329\\ 659\\ 337\\ 151\\ 111\\ 87\\ 65\\ \end{array}$	$\begin{array}{c} 58\\ 65\\ 54\\ 75\\ 142\\ 523\\ 296\\ 119\\ 102\\ 135\\ 152\\ 191\\ 210\\ 150\\ 147\\ 135\\ 89\\ 79\\ .220\\ 150\\ 125\\ 89\\ 227\\ 380\\ 150\\ 125\\ 514\\ 513\\ 146\\ 97\\ 76\\ 61\\ 54\\ 47\\ \end{array}$	$\begin{array}{c} 46\\ 40\\ 31\\ 15\\ 55\\ 42\\ 70\\ 70\\ 71\\ 957\\ 227\\ 119\\ 93\\ 75\\ 101\\ 160\\ 137\\ 109\\ 74\\ 44\\ 44\\ 44\\ 439\\ 39\\ 37\\ 31\\ 33\\ 39\\ 26\\ 24\\ 19\\ \hline \end{array}$	$\begin{array}{c} 20\\ 2,587\\ 3766\\ 207\\ 114\\ 800\\ 60\\ 47\\ 58\\ 60\\ 57\\ 3,683\\ 1,987\\ 973\\ 35683\\ 1,987\\ 973\\ 354\\ 124\\ 90\\ 74\\ 54\\ 61\\ 73\\ 56\\ 62\\ 128\\ 124\\ 57\\ 46\\ 61\\ 25\\ 128\\ 124\\ 57\\ 46\\ 113\\ 356\\ 62\\ 128\\ 124\\ 141\\ 141\\ 141\\ 141\\ 141\\ 141\\ 141$	$\begin{array}{c} 70\\ 40\\ 40\\ 44\\ 66\\ 76\\ 76\\ 72\\ 3906\\ 240\\ 906\\ 240\\ 906\\ 240\\ 906\\ 240\\ 300\\ 23\\ 8\\ 111\\ 75\\ 55\\ 50\\ 48\\ 46\\ 49\\ 44\\ 48\\ 45\\ 75\\ 330\\ 23\\ 8\\ 15\\ 12\\ 12\\ 14\\ 14\\ 14\\ 9\\ 9\end{array}$	$\begin{array}{c} 10\\ 9\\ 7\\ 6\\ 6\\ 5\\ 5\\ 4\\ 4\\ 5\\ 6\\ 6\\ 6\\ 5\\ 5\\ 35\\ 22\\ 23\\ 14\\ 8790\\ 2300\\ 177\\ 201\\ 1932\\ 83\\ 64\\ 413\\ 1, 292\\ 193\\ 83\\ 64\\ 413\\ 1, 292\\ 3216\\ 11\\ 292\\ 3216\\ 11\\ 292\\ 3216\\ 12\\ 292\\ 3216\\ 12\\ 326\\ 12\\ 326\\ 12\\ 326\\ 12\\ 326\\ 12\\ 326\\ 12\\ 326\\ 12\\ 326\\ 12\\ 326\\ 12\\ 32\\ 12\\ 12\\ 12\\ 12\\ 12\\ 12\\ 12\\ 12\\ 12\\ 1$	$\begin{array}{c} 64\\ 49\\ 43\\ 38\\ 103\\ 75\\ 110\\ 84\\ 33\\ 28\\ 29\\ 20\\ 15\\ 8\\ 50\\ 36\\ 34\\ 32\\ 22\\ 20\\ 17\\ 745\\ 745\\ 21\\ 20\\ 21\\ 20\\ 225\\ 22\\ 22\\ 5\\ 21\\ 20\\ 5\\ 20\\ 20\\ 20\\ 20\\ 20\\ 20\\ 20\\ 20\\ 20\\ 20$	$\begin{array}{c} 17\\ 14\\ 31\\ 221\\ 17\\ 14\\ 11\\ 11\\ 11\\ 10\\ 56\\ 67\\ 77\\ 64\\ 4\\ 66\\ 6\\ 4\\ 4\\ 8\\ 12\\ 10\\ 9\\ 5\\ 4\\ 12\\ 11\\ 11\\ 11\\ 11\\ 11\\ 11\\ 11\\ 11\\ 11$	$\begin{array}{c} 333344556733333389536333498115122293\\1151221913\\1221913\\1221221221\\1221221\\221221\\221221\\22$	$\begin{array}{c} 6\\ 1,400\\ 616\\ 131\\ 63\\ 44\\ 434\\ 299\\ 63\\ 61\\ 60\\ 60\\ 60\\ 60\\ 60\\ 422\\ 377\\ 292\\ 59\\ 64\\ 433\\ 333\\ 333\\ 333\\ 333\\ 333\\ 333\\$	866 577 499 600 1,765 6700 216 1311 977 979 79 79 79 79 73 88 84 84 84 84 84 84 84 84 84 84 84 84
Mean	160	287	194	142	411	157	238	65	11	7	163	362

Mean

48

435

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1	133	110	82	251	151	65	4	7	7	5	113	364
2	131	99	67	131	103	. 53	5	13.	7	3	60	271
3	90	98	70	98	79	44	4	8	7	5	46	201
4	49	95	79	82	71	35	3	10	8	5	37	1,230
ā	49	90	79	80	73	31	5	28	5	5	31	2,932
6] 36	89	68	83	109	31	6	96	5	1 7	31	683
7	55	87	64	111	404	27	3	44	5	5	27	466
8	87	80	61	103	2,940	14	3	- 39	14	3	31	139
9	87	73	53	13	1,711	10	3	39	14	4	1 509	87
10	81	10	49	60	398	10		320	9	0	1,303 1,003	19
11	01	450	40	08	229	10	2	3/4	9	0	1,097	1 1 AL
10	1111	400	40	10	557	10	4	10/	-	0	140	00
10	409	207	41	60	946	10	0 9	41	7	9	107	
15	452	253	30	338	1 201	16	3	25	8	E E	80	40
16	400	108	20	980	847	16	5	20	6	l s	60	
17	251	138	30	154	789	11	5	25	7	8	60	35
18	107	132	39	89	299	9	6	17	6	17	378	23
19		154	39	71	145	9	5	134	5	23	3,451	27
20	375	4.160	39	68	125	9	7	88	4	23	896	472
21	748	1.737	57	64	117	10	17	64	- 4	24	279	531
22		860	376	61	91	9	20	39	6	79	136	237
23	2,890	427	469	53	69	5	13	27	8	70	811	2.134
24	680	231	304	569	297	5	7	23	13	52	518	536
25	226	159	283	544	573	5	11	21	15	66	283	251
26		115	175	323	767	5	11	22	5	224	210	131
27	320	97	131	238	495	7	11	14	7	495	185	107
28	439	97	242	525	266	7	11	6	10	171	194	89
29	370		393	810	158	4	5	11	9	68	248	79
30	- 133		1,078	322	119	4	8	11	7	94	341	73
31	259		433		89		8	5		169		114
Mean	328	397	162	195	447	17	7	66	8	54	412	375
		1										

Daily discharge, in second-feet, of Tohickon Creek at Point Pleasant, Pennsylvania, for 1898.

Daily discharge, in second-feet, of Tohickon Creekat Point Pleasant, Pennsylvania, for 1899.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26	$\begin{array}{r} 144\\ 136\\ 154\\ 204\\ 1,172\\ 1,360\\ 503\\ 503\\ 413\\ 124\\ 158\\ 169\\ 186\\ 311\\ 432\\ 569\\ 186\\ 311\\ 432\\ 569\\ 186\\ 311\\ 432\\ 528\\ 258\\ 116\\ 84\\ 79\\ 9\\ 526\\ 2,032\\ 392\\ 392\\ 392\\ 392\\ 392\\ 392\\ 392\\ 3$	$\begin{array}{c} 158\\ 125\\ 125\\ 125\\ 151\\ 184\\ 210\\ 189\\ 142\\ 180\\ 189\\ 142\\ 180\\ 189\\ 142\\ 180\\ 189\\ 162\\ 180\\ 102\\ 655\\ 914\\ 1,582\\ 767\\ 695\\ 914\\ 1,582\\ 1,000\\ 541\\ 1,582\\ 1,000\\ 541\\ 2,999\\ 102\\ 1,582\\ 1,000\\ 541\\ 1,582\\ 1,000\\ 541\\ 1,582\\ 1,000\\ 541\\ 1,582\\ 1,000\\ 541\\ 1,582\\ 1,000\\ 541\\ 1,582\\ 1,000\\ 541\\ 1,582\\ 1,000\\ 541\\ 1,582\\ 1,000\\ 541\\ 1,582\\ 1,000\\ 541\\ 1,582\\ 1,000\\ 541\\ 1,582\\ 1,000\\ 541\\ 1,582\\ 1,000\\ 541\\ 1,582\\ 1,000\\ 541\\ 1,582\\ 1,000\\ 541\\ 1,582\\ 1,000\\ 541\\ 1,582\\ 1,000\\ 1,00$	$\begin{array}{c} 793\\ 600\\ 601\\ 708\\ 2,819\\ 1,109\\ 277\\ 217\\ 2017\\ 217\\ 2017$	$\begin{array}{c} 178\\ 131\\ 131\\ 131\\ 779\\ 68\\ 61\\ 1,328\\ 389\\ 160\\ 92\\ 87\\ 79\\ 799\\ 799\\ 700\\ 153\\ 396\\ 144\\ 84\\ 68\\ 61\\ 58\\ 61\\ 58\\ 61\\ 58\\ 499\\ 45\\ 1 \end{array}$	35 31 31 31 31 31 31 31 31 31 31 31 32 228 327 31 320 228 35 7 31 31 31 31 31 31 31 31 31 31 31 31 31	1599910987775866775355543222722277	$\begin{array}{c} 14\\ 14\\ 11\\ 19\\ 10\\ 10\\ 10\\ 10\\ 8\\ 8\\ 7\\ 6\\ 7\\ 6\\ 7\\ 7\\ 7\\ 7\\ 8\\ 8\\ 8\\ 3\\ 5\\ 3\\ 3\\ 8\\ 3\\ 4\\ 4\end{array}$	$\begin{array}{c} 4\\ 399\\ 267\\ 113\\ 52\\ 222\\ 222\\ 15\\ 254\\ 417\\ 182\\ 666\\ 666\\ 666\\ 838\\ 28\\ 19\\ 14\\ 112\\ 88\\ 667\\ 7\\ 7\\ 8\\ 22\\ 22\\ 25\\ 15\\ 15\\ 25\\ 15\\ 15\\ 25\\ 15\\ 15\\ 25\\ 15\\ 15\\ 25\\ 15\\ 15\\ 15\\ 15\\ 15\\ 15\\ 15\\ 15\\ 15\\ 1$	$\begin{array}{c} 18\\18\\19\\99\\28\\19\\28\\19\\203\\499\\163\\287\\2103\\499\\163\\58\\466\\18\\18\\23\\58\\545\\404\\239\\61\\422\\239\\61\\242\\239\\242\\239\\242\\239\\242\\239\\242\\239\\242\\239\\242\\239\\242\\239\\242\\239\\242\\239\\242\\239\\242\\239\\242\\239\\242\\239\\242\\239\\242\\239\\242\\242\\242\\242\\242\\242\\242\\242\\242\\24$	$\begin{array}{c} 466\\ 400\\ 275\\ 233\\ 18\\ 200\\ 233\\ 200\\ 177\\ 16\\ 11\\ 109\\ 99\\ 99\\ 99\\ 99\\ 99\\ 99\\ 99\\ 99\\ 99\\ $	$\begin{array}{c} 522\\ 522\\ 181\\ 121\\ 921\\ 3066\\ 121\\ 733\\ 58\\ 405\\ 325\\ 405\\ 353\\ 405\\ 353\\ 405\\ 353\\ 405\\ 553\\ 445\\ 447\\ 447\\ 447\\ 538\\ 333\\ 333\\ 499\\ 557\\ 446\\ 455\\ 557\\ 445\\ 358\\ 358\\ 495\\ 557\\ 445\\ 358\\ 358\\ 358\\ 358\\ 358\\ 358\\ 358\\ 35$	$\begin{array}{c} 344\\ 34\\ 449\\ 499\\ 399\\ 399\\ 311\\ 233\\ 27\\ 444\\ 955\\ 101\\ 600\\ 499\\ 399\\ 855\\ 101\\ 653\\ 879\\ 9913\\ 2082\\ 20$
28 29 30 31	$ \begin{array}{r} 145 \\ 166 \\ 169 \\ 184 \end{array} $	1,058	$\begin{array}{r} & 035 \\ & 779 \\ 1,307 \\ & 520 \\ & 239 \end{array}$	39 39 39 39	12 9 12 14 15	12 5 17 27	4 6 7 4	317 62 34 27	$ \begin{array}{r} 504 \\ 158 \\ 78 \\ 51 \\ \end{array} $	$ \begin{array}{c} 11 \\ 11 \\ 10 \\ 12 \\ 17 \end{array} $	$ \begin{array}{r} 30 \\ 31 \\ 36 \\ 39 \\ \end{array} $	97 79 65 53 49
Mean	419	546	797	144	22	7	7	90	271	17	94	113

NESHAMINY CREEK, PENNSYLVANIA, BELOW THE FORKS.

This station, which was established in 1884, is described in the Twentieth Annual Report, Part IV, pages 103 and 104. The same report contains also (pages 104 to 108) the figures for monthly flow for the years 1890 to 1898, inclusive, as well as diagrams of discharge for the same period. Water-Supply Paper No. 35 contains, on page 65, a table of daily discharge for 1899. The results by months and a diagram of the daily discharge for that year are given on page 86 of the Twenty-first Annual Report, Part IV. The following tables give the daily discharge of this stream from 1884 to 1900, inclusive.

Daily discharge, in second-feet, of Neshaminy Creek. Pennsylvania, below the forks, for 1884.

Day.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Day.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1 2 3 4 5 6.		24 19 27 25 235 905	$ \begin{array}{r} 116 \\ 101 \\ 56 \\ 57 \\ 436 \\ 462 \end{array} $	$ \begin{array}{c} 15 \\ 11 \\ 10 \\ 10 \\ 12 \\ 8 \end{array} $	55668 8	$ \begin{array}{r} 13 \\ 14 \\ 12 \\ 8 \\ 16 \\ 18 \end{array} $	$55 \\ 44 \\ 26 \\ 20 \\ 23 \\ 235 $	18 19 20 21 22 23	$ \begin{array}{r} 13 \\ 9 \\ 10 \\ 8 \\ 7 \\ 5 \end{array} $	$ \begin{array}{r} 14 \\ 18 \\ 16 \\ 13 \\ 15 \\ 16 \end{array} $	$\begin{array}{c} 20 \\ 21 \\ 16 \\ 18 \\ 18 \\ 17 \end{array}$	554455		5 5 9 10 5 3	157 175 200 363 959 940
7 8 9		$ 146 \\ 76 \\ 48 $			6 5 5		1,907 192 98	24 25 26	$5\\6\\2,271$	$ \begin{array}{c} 14 \\ 15 \\ 17 \end{array} $	17 17 17	5 5 4	5 4 4	$ \begin{array}{r} 441 \\ 110 \\ 47 \end{array} $	937 811 710
10 11 12 13	$ \begin{array}{r} 12 \\ 12 \\ 14 \\ 17 \end{array} $	$ \begin{array}{r} 36 \\ 27 \\ 27 \\ 29 \\ 99 \\ \end{array} $	$ 38 \\ 34 \\ 31 \\ 28 $		5 5 5 4	11 7 7 6	$74 \\ 56 \\ 841 \\ 414$	27 28 29 30	331 80 56 31	$ \begin{array}{c} 17 \\ 14 \\ 22 \\ 20 \\ 20 \end{array} $	$ \begin{array}{c} 13 \\ 10 \\ 13 \\ 20 \end{array} $			$29 \\ 24 \\ 180 \\ 121$	
14 15 16 17			$ \begin{array}{r} 25 \\ 22 \\ 22 \\ 17 \\ \end{array} $	$\begin{array}{c} 4\\ 3\\ 4\\ 4\\ 4\end{array}$	4 3 3 3	7 8 6 5	$ \begin{array}{r} 166 \\ 2,354 \\ 336 \\ 173 \end{array} $	31 Mean	139		18 61	6	12 5	39	1,161

[Drainage area, 139.3 square miles.]

Daily discharge, in second-feet, of Neshaminy Creek, Pennsylvania, below the forks, for 1885.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
Day. . 1 . 2 . 3 . 4 . 5 . 6 . 9 . 10 . 12 . 13 . 14 . 15 . 16 . 17 . 18 . 20 . 23 . 24 . 25 . 26 . 27 . 28 . 290 .	5 an. 6666 215 5 120 130 130 1, 886 823 3422 204 151 151 151 152 204 153 150 220 204 153 150 220 204 153 150 220 204 157 255 204 157 255 204 157 255 204 157 255 204 157 255 204 157 255 204 157 255 204 157 255 204 157 255 265 265 265 265 265 265 265	$\begin{array}{c} 139\\ 128\\ 142\\ 156\\ 156\\ 156\\ 156\\ 156\\ 156\\ 156\\ 156$	$\begin{array}{c} 74\\ 284\\ 343\\ 492\\ 492\\ 1,053\\ 948\\ 456\\ 208\\ 84\\ 456\\ 208\\ 84\\ 456\\ 208\\ 84\\ 785\\ 114\\ 136\\ 169\\ \mathbf$	$\begin{array}{c} \text{Apr:} \\ 334\\ 222\\ 334\\ 222\\ 10\\ 206\\ 206\\ 206\\ 206\\ 206\\ 206\\ 206\\ 20$	$\begin{array}{c} 46\\ 52\\ 55\\ 55\\ 47\\ 44\\ 88\\ 63\\ 474\\ 44\\ 222\\ 1411\\ 114\\ 78\\ 66\\ 57\\ 57\\ 444\\ 44\\ 44\\ 437\\ 334\\ 28\\ 8\\ 31\\ 31\\ 326\\ 296\\ 296\\ 290\\ 200\\ 200\\ 200\\ 200\\ 200\\ 200\\ 200$	$\begin{array}{c} 19\\ 19\\ 222\\ 14\\ 15\\ 15\\ 15\\ 15\\ 15\\ 10\\ 13\\ 13\\ 11\\ 11\\ 10\\ 8\\ 6\\ 6\\ 9\\ 10\\ 7\\ 5\\ 9\\ 8\\ 6\\ 4\\ 4\\ 4\\ 6\\ 7\\ 5\\ 5\\ 9\\ 8\\ 6\\ 4\\ 4\\ 4\\ 5\\ 5\\ 5\\ 9\\ 8\\ 6\\ 6\\ 4\\ 4\\ 4\\ 5\\ 5\\ 5\\ 9\\ 8\\ 6\\ 6\\ 6\\ 6\\ 8\\ 8\\ 6\\ 6\\ 8\\ 8\\ 6\\ 8\\ 8\\ 6\\ 8\\ 8\\ 6\\ 8\\ 8\\ 8\\ 8\\ 8\\ 8\\ 8\\ 8\\ 8\\ 8\\ 8\\ 8\\ 8\\$	$\begin{array}{c} 7 \\ 7 \\ 4 \\ 4 \\ 4 \\ 3 \\ 4 \\ 4 \\ 1 \\ 2 \\ 1 \\ 7 \\ 7 \\ 4 \\ 3 \\ 4 \\ 4 \\ 1 \\ 2 \\ 1 \\ 7 \\ 7 \\ 4 \\ 3 \\ 4 \\ 4 \\ 3 \\ 5 \\ 3 \\ 3 \\ 4 \\ 4 \\ 5 \\ 3 \\ 3 \\ 2 \\ 2 \\ 2 \\ 2 \\ 2 \\ 2 \\ 2 \\ 2$	Aug. 3 4 723 2,377 399 994 17 16 16 15 111 111 111 111 11 111 111 11 11 11 11 11 11 12 6 6 6 6 6 6 7 7 7 7 7 7 7 7 7 7	99943557433455245554443343343243282149 20 20	$\begin{array}{c} & \\ & \\ & \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\$	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\begin{array}{c} \begin{array}{c} & & \\ $
30 31 Mean	220 192 382	589	161 298 203	54 171	21 22 65	9 9 9	2 2 6	5 8 112	1 4.	$\frac{44}{54}$	134 	63 114 200

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1	209	452	165	1,637	59	64	38	36	8	4	14	46
2	109	410	104	270	48	49 53			8	3 3	10	48
4	141	425	132	252	48	53	29	24	7	4	9	89
5	2,478	350	121	423	49	45	26	20	4	3	10	64
6	413	300	109	4,734	41	39	28	18	5	2	9	46
<i>4</i>	195	200	97	1,198	9 246	30 90	22	20	6	29	1	97 97
9	599	175	92	371	749	35	19	46	6	2	10	68
10	601	150	88	303	227	45	182	31	4	2	11	74
11	574	5,767	78	231	168	49	149	24	4	4	11	85
12	417	5,132	77	207	140	37	48	18	4	2	10	64
13	346	4,195	89	293	218	29	32	19	3	20	80	100
14	307	508	81	207	232	291	44	10	5	2	27	345
16	300	528	75	168	615	100	294	12	10	2	27	393
17	285	217	70	157	242	95	297	16	7	2	16	279
18	272	173	66	139	159	108	100	11	ĩ	2	26	649
19	285	204	79	133	164	07	136	10	4	3	37	2,228
91	272	199	902	108	155	34	58	9	6	3	17	278
22	660	146	477	99	131	31	75	Ğ	5	2	16	190
23	580	127	216	93	173	732	62	6	4	3	111	133
24	375	122	141	90	134	315	48	6	4	3	203	203
25	330	694	132	85	113	149	31	4	3	3	160	662
20	390	1,100 189	128	95 86	108	111	598	ß	03	11	194	175
28	1.744	177	439	81	96	73	114	6	4	28	64	145
29	3,735		456	76	85	63	73	4	2	38	52	228
30	1,269		1,389	65	67	45	42	9	2	25	50	178
31	615		1,870		59		41	9		15		229
Mean	609	843	266	431	244	110	92	17	5	6	67	272

Daily discharge, in second-feet, of Neshaminy Creek, Pennsylvania, below the forks, for 1886.

Daily discharge, in second-feet, of Neshaminy Creek, Pennsylrania, below the forks, for 1887.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oet.	Nov.	Dec.
1 2 3 5 6 7 8 9 10 12 13 14 15 16 17 18 19 20 21	$\begin{array}{c} 323\\ 550\\ 434\\ 254\\ 221\\ 193\\ 181\\ 138\\ 181\\ 181\\ 159\\ 153\\ 740\\ 940\\ 420\\ 2300\\ 210\\ 160\\ 160\\ 160\\ \end{array}$	$\begin{array}{c} 239\\ 239\\ 156\\ 220\\ 203\\ 204\\ 165\\ 612\\ 742\\ 625\\ 337\\ 767\\ 552\\ 189\\ 223\\ 337\\ 767\\ 552\\ 189\\ 223\\ 337\\ 767\\ 554\\ 370\\ 1,344\\ 1,708\\ 430\\ 321 \end{array}$	$\begin{array}{c} 2966\\ 262\\ 335\\ 195\\ 195\\ 162\\ 186\\ 324\\ 779\\ 545\\ 828\\ 405\\ 2213\\ 196\\ 160\\ 154\\ 139\\ 120\\ 154\\ 139\\ 120\\ 110\\ 100\end{array}$	$\begin{array}{c} 204\\ 202\\ 228\\ 228\\ 2228\\ 2228\\ 2228\\ 1777\\ 147\\ 121\\ 107\\ 107\\ 107\\ 107\\ 92\\ 81\\ 777\\ 788\\ 80\\ 69\\ 210\\ 359\\ 118\\ 134\\ 134\\ \end{array}$	$\begin{array}{c} 115\\ 105\\ 96\\ 87\\ 83\\ 76\\ 160\\ 310\\ 244\\ 148\\ 91\\ 448\\ 118\\ 91\\ 77\\ 69\\ 566\\ 555\\ 488\\ 47\\ 38\\ 34\end{array}$	$\begin{array}{c} 208\\ 137\\ 104\\ 101\\ 53\\ 39\\ 107\\ 158\\ 84\\ 44\\ 44\\ 35\\ 31\\ 26\\ 23\\ 28\\ 24\\ 25\\ 50\\ 34\\ 29\end{array}$	$\begin{array}{c} & 42 \\ 41 \\ 34 \\ 30 \\ 132 \\ 1,570 \\ 132 \\ 223 \\ 155 \\ 155 \\ 942 \\ 146 \\ 89 \\ 66 \\ 66 \\ 66 \\ 553 \\ 477 \\ 40 \\ 558 \\ 39 \\ 40 \\ 558 \\ 39 \\ 40 \\ 35 \\ \end{array}$	$\begin{array}{c c} 11113\\ \hline \\ 1144\\ 149\\ 218\\ 139\\ 218\\ 139\\ 88\\ 73\\ 373\\ 65\\ 50\\ 44\\ 108\\ 236\\ 65\\ 50\\ 44\\ 108\\ 236\\ 67\\ 44\\ 41\\ 36\\ 992\\ 236\\ 71\\ 40\\ 30\\ \end{array}$	21 21 24 224 227 17 23 19 20 18 218 218 218 218 218 218 218 219 20 20 20 20 20 20 20 20 20 20 20 20 20	$\begin{array}{c} 477\\ 473\\ 333\\ 331\\ 223\\ 188\\ 188\\ 188\\ 20\\ 211\\ 221\\ 19\\ 17\\ 14\\ 138\\ 18\\ 18\\ 13\\ 398\\ 398\\ \end{array}$	37 37 28 28 27 27 27 27 27 27 27 27 27 27 27 27 27	$\begin{array}{c} 40\\ 39\\ 26\\ 29\\ 23\\ 55\\ 48\\ 40\\ 29\\ 176\\ 61, 648\\ 400\\ 199\\ 153\\ 610\\ 607\\ 210\\ 0277\\ 303\\ 249\\ 411\end{array}$
22 23 24 25 26 27 28 29 29 30 31 20 21 29 29 29 29 20 20 20 20 20 20 20 20 20 20 20 20 20	$\begin{array}{r} 220\\ 590\\ 2,891\\ 628\\ 490\\ 532\\ 400\\ 1,661\\ 900\\ 408\\ \end{array}$	406 376 630 314 294 1,210 454	$\begin{array}{c} 413\\ 551\\ 437\\ 691\\ 432\\ 255\\ 2,185\\ 521\\ 246\\ 235\\ \end{array}$	108 294 663 203 275 205 153 191 154	33 32 41 53 86 44 39 25 33 32	$\begin{array}{c} 411\\ 3, 159\\ 412\\ 179\\ 119\\ 102\\ 81\\ 62\\ 51\\ \end{array}$	$\begin{array}{c} 38\\ 462\\ 1,047\\ 484\\ 177\\ 282\\ 134\\ 147\\ 121\\ 141\\ \end{array}$	37 64 379 288 84 45 42 39 32 31	24 22 20 21 20 20 20 26 41 74	139 63 63 36 34 34 29 31 27 32	44 37 31 29 27 26 29 61 38	$\begin{array}{r} 111\\ 447\\ 289\\ 248\\ 169\\ 175\\ 145\\ 1,597\\ 913\\ 364\\ 435\\$
Mean	490	507	380	176	82	199	226	93	51	42	32	334

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1	4,890	233	160	376	77	65	19	10	12	68	131	178
2	2.786	235	145	306	72	12	13	11	13	75	124	152
3	505	230 •	139	262	72	- 39	15	11	15	65	114	140
4	388	285	114	211	72		13	9	15	50	106	135
5	323	1,553	95	295	63	- 31	13	7	12	47	97	131
6	267	2,111	162	2.227	51	31	15	7	9	191	93	139
7	310	798	77	428	51	29	13	7	9	212	87	136
8	636	389	101	254	54	22	10	17	224	130	84	120
9	404	308	95	206	48	25	14	21	376	74	91	118
10	261	310	88	631	48	24	22	14	134	57	171	132
11	251	313	602	1,394	78	21	21	11	129	52	347	135
12	432	283	1,571	341	129	23	14	78	474	53	137	118
13	682	230	338	271	103	17	11	206	280	68	105	80
14	493	220	375	242	75	15	10	154	174	69	100	178
15	356	220	432	197	61	17	9	22	88	63	1,821	· 248
16	287	235	564	781	58	19	11	20	84	53	588	131
17	342	287	743	557	57	14	12	15	1,052	69	301	3,759
18	455	362	565	200	48	10	11	9	3,099	63	209	1,821
19	480	587	367	171	52	16	10	7	401	63	877	431
20	477	2,112	1,001	160	61	20	11	6	227	68	560	311
21	288	2,675	3,126	154	56	20	11	29	1,710	69	258	230
22	199	579	1,455	125	40	14	8	1,500	319	54	193	253
23	206	411	350	119	36	65	10	153	185	60	166	- 365
24	251	265	264	119	40	57	11	55	151	101	153	354
25	172	3,619	248	97	40	14	9		132	132	150	302
26	151	938	449	88	45	15	9	15	135	82	245	209
27	186	368	1,387	80	43	11	65	19	125	406	671	351
28	175	228	783	80	42	8	125	20	92	688	345	553
29	195	191	1,485	72	95	15	24	15	72	459	218	329
30	226		578	68	130	24	19	14	64	209	196	127
31	232		489		91		19	13		151		135
Mean	558	709	592	350	64	25	18	80	327	129	291	380

Daily discharge, in second-feet, of Neshaminy Creek, Pennsylvania, below the forks, for 1888.

Daily discharge, in second-feet, of Neshaminy Creek, Pennsylvania, below the forks, for 1889.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1	139	183	101	87	214	312	94	1,760	53	185	244	324
2	140	140	114	558	182	293	346	1,083	58	179	216	275
3	131	154	484	250	154	158	649	1,047	51	155	616	263
4	116	159	3,197	198	138	120	905	761	53	133	526	238
5	197	144	1,364	156	122	122	598	705	44	126	254	203
6	940	120	503	139	108	116	247	480	38	117	212	197
7	490	214	296	120	105	95	168	595	41	123	186	188
8	260	328	215	111	89	88	135	296	50	106	180	207
9	552	188	169	111	80	96	113	228	41	94	2,879	- 333
10	776	116	142	96	80	97	94	321	44	94	1,044	109
11	275	102	133	92	12	93	124	239	- 07	91	461	176
12	200	110	131	88	11	143	158	174	108	87	364	182
13	166	124	131	92	100	120	490	152	777	267	1,422	223
14	157	133	137	84	108	141	33%	746	381	208	1,179	270
10	145	118	138	12	134	89	3,386	2,046	830	401	246	338
16	144	390	130	00	80	172	420	188	403	213	2396	228
10	800	1 110	110	01		118	201	100	2,000	119	200	288
18	449	1,110	110	00 20	30	301	1/0	$\frac{180}{109}$	2,947	115	200	440
19	110	1004	110	51	41	100 #1	2 050	100	490	98	4,900	000
20	140	195	110	50	7.91	57	3,900	126	4/49	9.5	5.17	499
41	407	120	400 097	60	201	01 54	401 98:9	100	910	110	941	200
(viv	404	00	175	60	1901	49	200	120	916	190	400	194
91	955	07	953	61	197	40	160	140	108	179	324	168
95	387	110	204	48	100	40	148	130	990	137	668	156
26	394	00	169	689	215	562	132	110	564	102	458	142
97	1 130	89	146	9.958	738	400	201	105	381	3 749	1 171	999
28	872	87	143	1 121	538	148	231	89	242	967	3 528	211
20	361	0,	141	501	403	92	174	72	201	388	415	128
30	213		122	284	330	80	528	65	184	274	407	121
31	214		89		141		5, 531	49		232		116
Mean	356	208	348	257	214	145	658	410	443	304	783	228

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1	107	135	722	346	115	95	30	38	46	28	145	52
2	110	114	347	351	87	80	33	41	31	32	135	72
0 4	100	163	197	200 610	64	53	566	20	25	188	123	137
5	108	192	178	626	114	48	107	31	26	88	102	144
6	130	147	282	272	138	65	56	21	26	67	90	102
7	128		229	228	191	65	44	27	20	135	90	116
8	115	2,818	141 132	270	152	1 1 5 35	42	19	18	129	89	193
10	90	293	149	639	96	35	27	17	18	78	79	103
11	92	250	581	280	75	112	19	16	19	83	116	81
12	80	228	560	219	76	1,150	17	16	26	75	140	85
13	84	212	282	180	78	667	15	13	29	64	114	165
14	1 501	020 601	1,200	1.19	142	212	30	10	29 55	74	90 85	100
16	800	237	544	139	223	225	22	14	180	64	75	83
17	281	192	323	119	87	75	19	27	147	564	118	276
18	187	189	290	105	62	70	60	27	61	188	231	848
19	150	339	261	96	49	60	33	27	50	130	120	193
20	298	331	1 939	86	264	65	19	222	31	136	85	182
22	144	197	2,990	85	94	76	21	670	29	146	81	106
23	170	266	1,512	71	63	56	20	118	20	585	73	115
24	159	213	500	74	52	41	17	50	20	2,400	68	$ 105 \\ 100$
20	155	260	11/4	101	47	48	415	-38	19	241	12	120
27	119	210	320	96	1.986	39	180	163	40	240	66	201
23	119	357	1,419	104	309	29	59	48	33	198	52	189
29	101		635	87	168	27	113	56	23	203	70	173
30	162		367	61	126	27	54	54	29	204	52	157
31	182		313		102		34	58		167		130
Mean	201	397	620	222	181	133	73	63	39	262	98	165

Daily discharge, in second-feet, of Neshaminy Creek, Pennsylvania, below the forks, for 1890.

Daily discharge, in second-feet, of Neshaminy Creek, Pennsylvania, below the forks, for 1891.

$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccc} 41 & 91 \\ 37 & 74 \\ 39 & 50 \\ 29 & 347 \\ 35 & 994 \\ 43 & 199 \\ 37 & 920 \\ 39 & 442 \\ 39 & 442 \\ \end{array}$	$ \begin{array}{c} 41 \\ 37 \\ 39 \\ 29 \\ 35 \end{array} $	91 74 50 347 994
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 43\\ 37\\ 39\\ 39\\ 35\\ 54\\ 75\\ 75\\ 75\\ 75\\ 75\\ 75\\ 75\\ 75\\ 75\\ 75$	$\begin{array}{c} 199\\ 9920\\ 4433\\ 2055\\ 167\\ 1422\\ 167\\ 999\\ 999\\ 1000\\ 1005\\ 977\\ 944\\ 933\\ 611\\ 577\\ 661\\ 4935\\ 651\\ 650\\ 261\\ 261\\ 261\\ 261\\ 261\\ 261\\ 2070\\ 1070\\ $
31 935 182 31 122 248 52 52 Mean 703 600 525 182 39 31 40 235 157 65	674 73 366	73	674 366

Daily discharge,	in	second-feet, o	f	Neshaminy Creek,	Pennsylvania,	below the	forks,
				for 1892.			-

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1 2 3 4 5	$\begin{array}{r} 9999\\ 1,870\\ 743\\ 293\\ 242\\ 193\\ 293\\ 242\\ 193\\ 193\\ 193\\ 193\\ 193\\ 193\\ 193\\ 114\\ 146\\ 3584\\ 2,364\\ 414\\ 2,364\\ 2,364\\ 444\\ 2,172\\ 731\\ 382\\ 280\\ 250\\ 250\\ 250\\ 250\\ 280\\ 332\\ 332\\ 332\\ 332\\ 332\\ 332\\ 332\\ 33$	$\begin{array}{c} 191\\ 1799\\ 174\\ 159\\ 149\\ 155\\ 125\\ 125\\ 120\\ 115\\ 125\\ 121\\ 93\\ 81\\ 81\\ 81\\ 81\\ 81\\ 81\\ 108\\ 81\\ 108\\ 103\\ 159\\ 124\\ 108\\ 103\\ 159\\ 185\\ 117\\ \end{array}$	$\begin{array}{c} 2,582\\ 554\\ 329\\ 259\\ 209\\ 221\\ 207\\ 1,359\\ 207\\ 1,359\\ 207\\ 1,359\\ 149\\ 130\\ 125\\ 135\\ 149\\ 130\\ 125\\ 135\\ 149\\ 141\\ 135\\ 144\\ 135\\ 114\\ 117\\ 386\\ 502\\ 409\\ 9006\\ 1,026\\ 410\\ 251\end{array}$	$\begin{array}{c} 179\\ 167\\ 179\\ 167\\ 174\\ 154\\ 154\\ 144\\ 133\\ 121\\ 119\\ 110\\ 996\\ 992\\ 102\\ 193\\ 108\\ 193\\ 108\\ 193\\ 108\\ 193\\ 155\\ 161\\ 109\\ 99\\ 93\\ 88\\ 88\\ 88\\ 88\\ 88\\ 88\\ 88\\ 88\\ 88\\ 8$	$\begin{array}{c} & 79 \\ 107 \\ 193 \\ 114 \\ 86 \\ 73 \\ 55 \\ 55 \\ 55 \\ 55 \\ 55 \\ 55 \\ 55$	$\begin{array}{c} 118\\ 102\\ 103\\ 99\\ 92\\ 111\\ 107\\ 79\\ 93\\ 140\\ 130\\ 80\\ 533\\ 48\\ 36\\ 36\\ 36\\ 332\\ 32\\ 229\\ 26\\ 722\\ 4\\ 75\\ 109\\ 69\\ 37\end{array}$	$\begin{array}{c} 39\\ 82\\ 297\\ 519\\ 144\\ 73\\ 53\\ 42\\ 34\\ 31\\ 31\\ 31\\ 31\\ 31\\ 31\\ 31\\ 31\\ 31\\ 31$	$\begin{array}{c} & & \\$	$\begin{array}{c} 15\\ 15\\ 14\\ 12\\ 11\\ 10\\ 13\\ 13\\ 8\\ 6\\ 6\\ 6\\ 7\\ 7\\ 8\\ 96\\ 17\\ 15\\ 15\\ 15\\ 15\\ 15\\ 11\\ 10\\ 10\\ 10\\ 10\\ 10\\ 10\\ 10\\ 10\\ 10$	565444456545566558855445556755554	$\begin{array}{c} 6\\ 6\\ 6\\ 6\\ 6\\ 7\\ 7\\ 5\\ 5\\ 6\\ 8\\ 32\\ 99\\ 99\\ 99\\ 19\\ 734\\ 605\\ 643\\ 104\\ 114\\ 2346\\ 605\\ 643\\ 184\\ 114\\ 114\\ 86\\ 89\\ 56\\ 54\\ 241\\ 611\\ 9413\\ 241\\ 611\\ 9413\\ 241\\ 611\\ 9413\\ 241\\ 611\\ 9413\\ 241\\ 611\\ 9413\\ 241\\ 611\\ 9413\\ 241\\ 611\\ 9413\\ 9414$ 9413\\ 9414 9414\\ 9414 9413\\ 9414 9413\\ 9414 94	$\begin{array}{c} 149\\ 106\\ 002\\ 80\\ 77\\ 68\\ 80\\ 59\\ 96\\ 88\\ 101\\ 93\\ 36\\ 88\\ 101\\ 93\\ 68\\ 85\\ 162\\ 226\\ 97\\ 162\\ 226\\ 97\\ 122\\ 221\\ 224\\ 11\\ 106\\ 101\\ 106\\ 115\\ 15\\ 115\\ 115\\ 115\\ 115\\ 115\\ 115$
31	233		209		142		101	13		5		120
Mean	627	125	431	126	194	71	66	24	13	5	220	127

Daily discharge, in second-feet, of Neshaminy Creek, Pennsylvania, below the forks, for 1893.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1	$\begin{array}{c} 1,357\\ 1,678\\ 227\\ 125\\ 125\\ 125\\ 125\\ 125\\ 125\\ 125\\ 125$	$\begin{array}{c} 385\\ 568\\ 741\\ 692\\ 540\\ 484\\ 1,590\\ 714\\ 307\\ 2,727\\ 809\\ 808\\ 801\\ 1,299\\ 1,136\\ 858\\ 8495\\ 625\\ 371\\ 305\\ 484\\ 404\\ 385\\ 309\\ 258\\ 179\\ 194\\ 242\\ \hline \end{array}$	$\begin{array}{c} 463\\ 599\\ 481\\ 281\\ 710\\ 169\\ 337\\ 2,387\\ 2,$	$\begin{array}{c} 133\\ 116\\ 102\\ 109\\ 98\\ 85\\ 98\\ 153\\ 140\\ 177\\ 290\\ 198\\ 1544\\ 2,448\\ 2900\\ 2290\\ 2290\\ 2900\\ 2900\\ 290\\ 293\\ 293\\ 293\\ 293\\ 293\\ 293\\ 293\\ 293$	$\begin{array}{c} 362\\ 318\\ 6164\\ 3,154\\ 420\\ 512\\ 404\\ 420\\ 512\\ 404\\ 189\\ 149\\ 144\\ 273\\ 617\\ 223\\ 161\\ 135\\ 161\\ 135\\ 161\\ 135\\ 105\\ 105\\ 105\\ 105\\ 105\\ 399\\ 722\\ 777\\ 77\\ 77\\ 63\\ 358\\ \end{array}$	$57 \\ 557 \\ 557 \\ 46 \\ 544 \\ 733 \\ 154 \\ 751 \\ 396 \\ $	$\begin{array}{c} 23\\ 23\\ 25\\ 21\\ 18\\ 18\\ 17\\ 20\\ 221\\ 20\\ 223\\ 222\\ 222\\ 19\\ 17\\ 15\\ 15\\ 15\\ 15\\ 15\\ 15\\ 15\\ 15\\ 15\\ 15$	$\begin{array}{c} 14\\ 11\\ 10\\ 7\\ 7\\ 9\\ 19\\ 7\\ 7\\ 6\\ 6\\ 6\\ 5\\ 6\\ 8\\ 9\\ 12\\ 254\\ 254\\ 254\\ 254\\ 254\\ 254\\ 254\\ 25$	59 54 839 355 259 341 357 351 351 353 749 2588 107 75 548 416 332 259 333 329 339 339 339 339 339 339 339 33	$\begin{array}{c} 26\\ 21\\ 23\\ 24\\ 21\\ 20\\ 22\\ 21\\ 20\\ 27\\ 24\\ 24\\ 23\\ 20\\ 21\\ 20\\ 21\\ 18\\ 199\\ 199\\ 263\\ 119\\ 963\\ 119\\ 461\\ 401\\ 481\\ 206\\ 104\\ 481\\ 206\\ 104\\ 88\\ \hline 70\\ \end{array}$	$\begin{array}{c} 61\\ 59\\ 59\\ 1, 281\\ 1, 759\\ 352\\ 221\\ 188\\ 241\\ 179\\ 139\\ 124\\ 115\\ 115\\ 303\\ 234\\ 131\\ 123\\ 109\\ 94\\ 101\\ 330\\ 213\\ 135\\ 99\\ 991\\ 112\\ 112\\ 112\\ 109\\ 996\\ 210\\ \end{array}$	$\begin{array}{c} 175\\ 154\\ 217\\ 154\\ 217\\ 198\\ 306\\ 274\\ 4211\\ 2533\\ 258\\ 258\\ 255\\ 255\\ 255\\ 255\\ 205\\ 258\\ 205\\ 258\\ 205\\ 258\\ 205\\ 205\\ 205\\ 205\\ 205\\ 205\\ 205\\ 205$
	10110	001	505	000	000	00	10	TON		.0	Citata	010

					<i>j</i> 07 10	004.						
Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
$\begin{array}{c} 1 \\ 2 \\ 2 \\ 3 \\ 4 \\ 5 \\ 5 \\ 6 \\ 7 \\ 8 \\ 9 \\ 9 \\ 10 \\ 11 \\ 12 \\ 13 \\ 14 \\ 15 \\ 15 \\ 15 \\ 15 \\ 15 \\ 15 \\ 10 \\ 10$	$\begin{array}{c} & 107\\ - & 109\\ - & 109\\ - & 89\\ - & 98\\ - & 130\\ - & 136\\ - & 116\\ - & 105\\ - & 97\\ - & 88\\ - & 88\\ - & 88\\ - & 88\\ - & 88\\ - & 76\\ - & 73\\ - $	$\begin{array}{c} 115\\ 110\\ 90\\ 58\\ 60\\ 58\\ 57\\ 60\\ 1,063\\ 757\\ 517\\ 267\\ 164\\ 164\\ 130\\ \end{array}$	$\begin{array}{c} 198\\ 227\\ 882\\ 986\\ 776\\ 777\\ 698\\ 416\\ 313\\ 291\\ 277\\ 243\\ 380\\ 355\\ 171\end{array}$	$\begin{array}{c} 128\\ 110\\ 97\\ 111\\ 189\\ 142\\ 112\\ 115\\ 114\\ 13\\ 146\\ 363\\ 1,521\\ 833\\ 490\\ \end{array}$	$\begin{array}{c} 97\\ 86\\ 98\\ 98\\ 80\\ 68\\ 76\\ 80\\ 68\\ 57\\ 43\\ 39\\ 39\\ 42\\ 45\\ 45\\ \end{array}$	$\begin{array}{c} 368\\ 285\\ 247\\ 233\\ 231\\ 280\\ 315\\ 235\\ 194\\ 161\\ 144\\ 130\\ 127\\ 127\\ 116\end{array}$	$\begin{array}{c} 68\\ 43\\ 37\\ 34\\ 36\\ 165\\ 177\\ 75\\ 51\\ 40\\ 34\\ 36\\ 34\\ 29\\ 26\\ \end{array}$	$\begin{array}{c} 32\\ 19\\ 400\\ 1455\\ 6\\ 61\\ 28\\ 14\\ 16\\ 15\\ 67\\ 82\\ 24\\ 24\\ \end{array}$	$\begin{array}{c} 7\\ 8\\ 8\\ 6\\ 6\\ 6\\ 5\\ 857\\ 1,247\\ 102\\ 108\\ 73\\ 36\\ 28\\ 28\\ 28\\ 28\end{array}$	$\begin{array}{r} 40\\ 47\\ 41\\ 45\\ 71\\ 655\\ 43\\ 34\\ 41\\ 1,715\\ 380\\ 173\\ 164\\ 250\\ 172\end{array}$	$\begin{array}{r} 428\\ 196\\ 1,371\\ 640\\ 860\\ 866\\ 245\\ 342\\ 464\\ 313\\ 258\\ 198\\ 179\\ 175\\ 165\end{array}$	$\begin{array}{c} 115\\ 268\\ 315\\ 161\\ 133\\ 124\\ 229\\ 616\\ 257\\ 629\\ 1,824\\ 853\\ 241\\ 300\end{array}$
10 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 250\\ 114\\ 1,630\\ 1,990\\ 1,185\\ 603\\ 3999\\ 366\\ 287\\ 204\\ 105\\ 147\\ 200\\ \hline \end{array}$	$\begin{array}{c} 178\\ 171\\ 144\\ 144\\ 144\\ 136\\ 179\\ 571\\ 279\\ 194\\ 182\\ 159\\ 131\\ 149\\ 152\\ \end{array}$	$\begin{array}{c} 306\\ 239\\ 198\\ 174\\ 166\\ 188\\ 418\\ 291\\ 186\\ 159\\ 141\\ 122\\ 114\\ 109\\ 105\\ \end{array}$	$39 \\ 36 \\ 36 \\ 685 \\ 9, 012 \\ 4, 036 \\ 823 \\ 3, 779 \\ 1, 523 \\ 277 \\ 2, 893 \\ 2, 036 \\ 553 \\ 443 \\ 443 \\ 1, 523 \\ 2, 036 \\ 553 \\ 443 \\ 1, 553 \\ 443 \\ 1, 553 \\ 1, 5$	$97 \\ 92 \\ 94 \\ 87 \\ 77 \\ 72 \\ 69 \\ 60 \\ 51 \\ 51 \\ 82 \\ 89 \\ 60 \\ 45 \\ 65 \\$	$ \begin{array}{c} 101\\ 212\\ 60\\ 31\\ 31\\ 31\\ 22\\ 23\\ 22\\ 22\\ 22\\ 22\\ 22\\ 22\\ 22\\ 22$	$233 \\ 200 \\ 111 \\ 160 \\ 222 \\ 221 \\ 111 \\ 150 \\ 133 \\ 144 \\ 100 \\ 877 \\ 7$	$\begin{array}{c} 23\\ 19\\ 1,001\\ 3,197\\ 797\\ 245\\ 141\\ 111\\ 91\\ 81\\ 81\\ 81\\ 62\\ 46\\ 48\\ 40\\ \end{array}$	$\begin{array}{c} 110\\ 106\\ 90\\ 78\\ 72\\ 63\\ 59\\ 60\\ 200\\ 233\\ 125\\ 82\\ 79\\ 790\\ \end{array}$	$\begin{array}{c} 149\\ 170\\ 227\\ 176\\ 145\\ 150\\ 170\\ 154\\ 152\\ 143\\ 125\\ 120\\ 112\\ 103\\ 96\\ \end{array}$	237 228 194 172 159 147 149 145 1355 1355 1355 135 1350 130 130 131
Mean	95	37	323	250	895	143	52	41	284	180	296	279

Daily discharge, in second-feet, of Neshaminy Creek, Pennsylvania, below the forks, for 1894.

Daily discharge, in second-feet, of Neshaminy Creek, Pennsylvania, below the forks, for 1895.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 20 21 22 23 24 25 26 27 28 29	$\begin{array}{c} 155\\ 98\\ 117\\ 98\\ 98\\ 156\\ 891\\ 818\\ 879\\ 2,289\\ 850\\ 550\\ 295\\ 295\\ 295\\ 295\\ 295\\ 150\\ 150\\ 150\\ 164\\ 181\\ 166\\ 120\\ 2,05\\ 164\\ 181\\ 166\\ 120\\ 2,05\\ 120\\ 120\\ 120\\ 2,05\\ 150\\ 120\\ 120\\ 120\\ 120\\ 120\\ 120\\ 120\\ 12$	$\begin{array}{c} 156\\ 98\\ 106\\ 147\\ 201\\ 189\\ 176\\ 176\\ 178\\ 188\\ 188\\ 176\\ 178\\ 178\\ 178\\ 177\\ 182\\ 201\\ 201\\ 201\\ 201\\ 201\\ 201\\ 201\\ 20$	$\begin{array}{c} 1,217\\ 1,019\\ 584\\ 533\\ 475\\ 265\\ 321\\ 1,531\\ 694\\ 594\\ 605\\ 273\\ 723\\ 1,632\\ 273\\ 723\\ 1,632\\ 292\\ 240\\ 376\\ 625\\ 526\\ 287\\ 336\\ 292\\ 240\\ 247\\ 213\\ 190\\ \end{array}$	$\begin{array}{c} 160\\ 249\\ 367\\ 231\\ 163\\ 142\\ 2,542\\ 3,234\\ 359\\ 250\\ 661\\ 755\\ 338\\ 253\\ 253\\ 253\\ 253\\ 136\\ 182\\ 168\\ 152\\ 136\\ 130\\ 130\\ 118\\ 107\\ 101\\ 127\\ 261\\ 159\end{array}$	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\begin{array}{c} 46\\ 42\\ 82\\ 95\\ 95\\ 157\\ 126\\ 41\\ 41\\ 43\\ 156\\ 41\\ 41\\ 162\\ 44\\ 436\\ 34\\ 31\\ 28\\ 256\\ 31\\ 9\\ 25\\ 9\\ 89\\ 202\\ 6\\ 10\\ 202\\ 6\\ 10\\ 202\\ 6\\ 10\\ 202\\ 6\\ 10\\ 202\\ 6\\ 10\\ 202\\ 6\\ 10\\ 10\\ 10\\ 10\\ 10\\ 10\\ 10\\ 10\\ 10\\ 10$	$\begin{array}{c} 528\\148\\759\\664\\616\\2002\\77\\79\\49\\44\\48\\40\\33\\8\\48\\8\\99\\26\\19\\23\\39\\39\\36\\8\\28\\48\\19\\26\\39\\39\\36\\8\\28\\18\\18\\18\\18\\18\\18\\18\\18\\18\\18\\18\\18\\18$	$\begin{array}{c} 27\\ 20\\ 18\\ 1,225\\ 94\\ 43\\ 44\\ 29\\ 20\\ 70\\ 70\\ 40\\ 29\\ 22\\ 22\\ 22\\ 22\\ 17\\ 70\\ 40\\ 29\\ 20\\ 17\\ 10\\ 19\\ 20\\ 10\\ 11\\ 10\\ 10\\ 9\\ 9\\ 9\\ 13\\ 11\\ 11\\ 11\\ 11\\ 11\\ 11\\ 11\\ 11\\ 11$	8891011877766666665567877776555555546	66455555677786994272295876555555	$\begin{array}{c} 27\\ 31\\ 310\\ 155\\ 17\\ 16\\ 17\\ 12\\ 11\\ 19\\ 8\\ 7\\ 9\\ 8\\ 8\\ 9\\ 7\\ 7\\ 13\\ 9\\ 10\\ 9\\ 7\\ 8\\ 8\\ 8\\ 8\\ 9\\ 7\\ 7\\ 13\\ 18\\ 28\\ 8\end{array}$	$\begin{array}{c} 155\\ 277\\ 766\\ 500\\ 455\\ 511\\ 400\\ 255\\ 550\\ 550\\ 550\\ 577\\ 166\\ 88\\ 66\\ 66\\ 66\\ 66\\ 66\\ 66\\ 66\\ 88\\ 88$
31	178		$\begin{array}{r}160\\149\end{array}$	187	63 48	 	25 31	10 10	6	6 9	15	24 573
Mean	412	237	515	417	84	68	106	81	7	10	14	49

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1	186 83	$39 \\ 45$	$\frac{960}{463}$	$\frac{286}{286}$	$\begin{array}{c} 81 \\ 65 \end{array}$	$\frac{24}{22}$	27 22	$71 \\ 48$	$\frac{11}{8}$	$ \begin{array}{c} 155 \\ 60 \end{array} $	28 30	299 193
3 4 5	69 72 55	$51 \\ 51 \\ 63$	$99 \\ 57 \\ 57$	$260 \\ 217 \\ 172$	$51 \\ 63 \\ 59$	22 22 17	24 24 19	37 35 30		$\frac{38}{31}$	33 36 1.305	115 115 100
6 7 8	$32 \\ 48 \\ 36$		$101 \\ 127 \\ 111$	$154 \\ 164 \\ 154$	39 44 41	$ \begin{array}{r} 17 \\ 20 \\ 17 \end{array} $	$17 \\ 22 \\ 87$	$ \begin{array}{c} 24 \\ 25 \\ 30 \end{array} $		33 29 24	579 220 106	90 90 120
9 10 11	23 19 19	635 624 383	88 85 82	$135 \\ 129 \\ 129 \\ 129$	30 23 25	18 66 46	57 86 71	$ \begin{array}{r} 30 \\ 31 \\ 22 \\ 17 \end{array} $	32 22 20	26 24 19	$ \begin{array}{r} 100 \\ 289 \\ 119 \\ 115 \end{array} $	$ \begin{array}{r} 120 \\ 307 \\ 252 \\ 154 \end{array} $
12 13	15 14 14 14	228 187 282	102 91 79	$125 \\ 125 \\ 125 \\ 120$	38 42 34	31 24 196	29 22 20	25 23 28		$ \begin{array}{r} 44 \\ 1,480 \\ 345 \end{array} $	$110 \\ 154 \\ 169 \\ 135$	$130 \\ 125 \\ 100$
15 16 17	15 15 15	379 274 191	92 81 77	110 93	31 31 31	$ \begin{array}{r} 130 \\ 236 \\ 73 \\ 59 \end{array} $			$14 \\ 13 \\ 593$	206 129	102 88	95 90
18 19	19 19 19 29 2	$119 \\ 110 \\ 100$	$118 \\ 5,408 \\ 1,904$	93 92 91	31 31 31	$138 \\ 72 \\ 25$	$16 \\ 13 \\ 12$	17 17 17	765 290	100 74 62 51	85 80	95 95 80
20 21 22 22	31 27	105 88 90	715 414 200	$135 \\ 147 \\ 07$	31 31 31	29 26	$13 \\ 1,373 \\ 400$	14 11 10		53 51	66 69 79	75 60
23 24 25 	565 377	75 84	$ \begin{array}{r} 509 \\ 250 \\ 211 \\ 240 \\ \end{array} $	88 97	31 31 31	31 36		$10 \\ 14 \\ 14 \\ 14 \\ 10 \\ 10 \\ 10 \\ 10 \\ $	26 26	$61 \\ 63 \\ 50$	72 72 72	54 52
20 27 28				88 85	$ \begin{array}{r} 31 \\ 110 \\ 125 \end{array} $	50 32	97 97	$10 \\ 10 \\ 14 \\ 15$	19 17	53 37		50 50 50
30 31	59 43 36	1,042	$2,061 \\ 760 \\ 389$	- 81 	135 61 86	43 43	561 155	$15 \\ 12 \\ 13$	21 308	33 38 40	869 385	45 40 30
Mean	71	611	528	133	46	50	126	25	120	112	190	106

Daily discharge, in second-feet, of Neshaminy Creek, Pennsylvania, below the forks, for 1896.

Daily discharge, in second-feet, of Neshaminy Creek, Pennsylvania, below the forks, for 1897.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1 2 3 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	$\begin{array}{c} 88\\ 88\\ 121\\ 209\\ 351\\ 125\\ 125\\ 107\\ 87\\ 72\\ 772\\ 772\\ 772\\ 772\\ 772\\ 772\\$	$\begin{array}{c} 41\\ 41\\ 41\\ 41\\ 41\\ 2,973\\ 840\\ 334\\ 166\\ 135\\ 115\\ 110\\ 94\\ 72\\ 63\\ 54\\ 41\\ 48\\ 48\\ 131\\ 101\\ 101\\ 101\\ 101\\ 101\\ 101\\ 101$	$\begin{array}{c} 88\\ 88\\ 115\\ 169\\ 290\\ 190\\ 360\\ 208\\ 144\\ 144\\ 160\\ 220\\ 171\\ 215\\ 149\\ 129\\ 135\\ 179\\ 700\\ 328\end{array}$	$\begin{array}{c} 93\\77\\71\\65\\131\\166\\125\\99\\1,750\\2705\\166\\2725\\205\\166\\144\\208\\218\\164\\145\\125\\107\\88\end{array}$	$\begin{array}{c} 76\\ 1,610\\ 439\\ 2399\\ 179\\ 135\\ 1111\\ 92\\ 80\\ 75\\ 97\\ 997\\ 926\\ 2,215\\ 755\\ 800\\ 235\\ 190\\ 150\\ 140\\ 126\\ 164 \end{array}$	$\begin{array}{c} 445\\ 115\\ 84\\ 123\\ 130\\ 84\\ 103\\ 84\\ 103\\ 84\\ 103\\ 84\\ 103\\ 84\\ 223\\ 202\\ 159\\ 144\\ 137\\ 131\\ 124\\ 117\\ 112\end{array}$	$\begin{array}{c} 45\\ 42\\ 42\\ 42\\ 42\\ 37\\ 329\\ 299\\ 311\\ 311\\ 375\\ 275\\ 376\\ 61\\ 366\\ 311\\ 311\\ 40\\ 3566\\ 367\end{array}$	$\begin{array}{c} 221\\ 184\\ 115\\ 105\\ 105\\ 105\\ 85\\ 77\\ 80\\ 83\\ 86\\ 83\\ 83\\ 64\\ 64\\ 289\\ 160\\ 67\\ 54\\ 63\\ 66\end{array}$	$\begin{array}{c} & 43 \\ 41 \\ 41 \\ 41 \\ 31 \\ 31 \\ 31 \\ 31 \\$	$\begin{array}{c} 17\\13\\13\\13\\17\\17\\15\\15\\15\\15\\15\\15\\15\\15\\15\\15\\15\\15\\15\\$	$\begin{array}{c} 80\\ 80\\ 1,354\\ 287\\ 108\\ 81\\ 71\\ 287\\ 108\\ 81\\ 74\\ 42\\ 366\\ 611\\ 74\\ 40\\ 555\\ 99\\ 399\\ 370\\ 400\\ 411\\ 411\\ 411\\ 40\\ 40\end{array}$	$\begin{array}{c} 105\\ 94\\ 91\\ 118\\ 1,305\\ 204\\ 155\\ 144\\ 136\\ 126\\ 336\\ 126\\ 336\\ 2,436\\ 2,696\\ 492\\ 318\\ 2455\\ 197\\ 175\\ 175\\ 175\end{array}$
22	369	529	209	88	165	97	3,083	64	22	14	40	173
23 24 25 26 27 27 28 29 30 31	$ \begin{array}{r} 139 \\ 97 \\ 73 \\ 48 \\ 48 \\ 36 \\ 31 \\ 36 \\ 31 \\ 36 \\ \hline 1 36 \\ $	$ \begin{array}{c} 1,826 \\ 301 \\ 105 \\ 89 \\ 63 \\ 63 \\ \hline \\ \hline \\ \\ \hline \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\$	$170 \\ 469 \\ 327 \\ 189 \\ 154 \\ 139 \\ 129 \\ 125 \\ 115 \\ 115 \\ 125 \\ 115 $	88 88 80 84 84 72 66 66	$ \begin{array}{c} 117\\ 127\\ 711\\ 185\\ 110\\ 84\\ 74\\ 77\\ 628\\ \hline 021 \end{array} $	$76 \\ 73 \\ 85 \\ 74 \\ 53 \\ 59 \\ 56 \\ 48 \\$	$1,256 \\ 630 \\ 391 \\ 181 \\ 491 \\ 2,119 \\ 900 \\ 298 \\ 214 \\$	$53 \\ 1,075 \\ 209 \\ 119 \\ 93 \\ 73 \\ 60 \\ 50 \\ 49 \\$	24 27 27 23 21 21 21 21	$ \begin{array}{r} 14\\ 14\\ 59\\ 85\\ 48\\ 27\\ 22\\ 19\\ 16\\ \hline 16$	39 39 36 36 1,033 238 142 124	$ \begin{array}{r} 162\\ 154\\ 154\\ 154\\ 154\\ 171\\ 166\\ 154\\ 539\\ \hline 0 \end{array} $
Mean	156	339	210	191	331	307	358	130	27	20	147	395

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1	377	164	164	249	193	115	29	32	24	12	65	436
2	340	164	160	150	162	105	29	251	17	8	39	300
3	340	164	160	176	147	105	21	65	14	6 ~	31	1 288
4	233	164	164	159	138	97	10	105	14	<u><u></u></u>	24	1,777
ð	130	104	104	10±	1.29	110	10	100	10	÷	19	5,009
0	120	104	144	164	249	60	~0 95	26	1.1	6		304
6	105	164	130	104	3 153	62		90	16	8	27	218
0	92	189	131	131	846	62	22	20	20	7	24	147
10	88	213	127	122	378	55	26	32	17	7	933	144
11	97	294	122	120	303	45	15	397	12	9	852	135
12	188	566	115	133	349	43	16	- 99	13	10	239	125
13	257	530	109	123	483	48	17	57	11	14	165	115
14	215	258	106	115	254	51	17	36	9	13	125	105
15	633	228	97	195	1,473	45	16	32	8	10	125	105
16	553	313	88	136	1,060	40	10	24	10	1	1.01	105
17	264	100	88	120	983	48	19		11	Ö	101	105
18	100	130	90	105	220	21	14	1 615	11	14	3 590	90
19	109	5 0*6	21	105	210	31	11	278	é	13	559	1 006
20	490	1 205	108	93	439	48	58	113	ě	24	268	293
20	398	691	196	81	258	31	66	65	7	49	202	480
23	2,985	445	349	77	213	28	36	45	9	49	828	1,670
24	476	- 330	273	294	258	34	22	36	11	27	484	408
25	313	273	164	400	280	34	18	31	13	24	355	203
26	554	221	166	254	250	36	20	31	12	59	269	149
27	462	200	175	189	242	31	22	31	14	176	242	129
28	267	182	246	645	209	34	22	27	14	81	445	115
29	215		391	182	170	34	19	20	11	40	4.3.4	110
91	146	• • • • • • •	1,202	914	134	29	11	20	13	81	404	90
91	104		±~0		108		14			el		101
Mean	374	469	199	211	459	55	23	128	12	27	376	418

Daily discharge, in second-feet. of Neshaminy Creek, Pennsylvania, below the forks, for 1898.

Daily discharge, in second-feet, of Neshaminy Creek, Pennsylvania, below the forks, for 1899.

$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		T		D
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	lar. Apr. May.	June. July. Aug.	Sept. Oct. Nov.	Dec.
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c}$
$ \begin{array}{c} 30 \\ 31 \\ 31 \\ 31 \\ 31 \\ 31 \\ 31 \\ 31 \\ 31$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	63 48
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\frac{443}{895} \frac{\dots}{208} \frac{27}{49}$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	48

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Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1 2 3 4 5 6 7 8 9 10 12 13 14 15 16 17 20 21 22 23 24 26 27 30 31	$\begin{array}{c} 60\\ 63\\ 48\\ 57\\ 80\\ 88\\ 88\\ 88\\ 88\\ 88\\ 88\\ 88\\ 88\\ 88$	$\begin{array}{c} 173\\ 194\\ 182\\ 188\\ 2,302\\ 553\\ 521\\ 1,330\\ 1,244\\ 3322\\ 379\\ 2,235\\ 566\\ 358\\ 340\\ 191\\ 142\\ 142\\ 142\\ 142\\ 142\\ 142\\ 142\\ 14$	$\begin{array}{c} 2,675\\ 1,434\\ 1,725\\ 209\\ 2005\\ 2224\\ 228\\ 2213\\ 201\\ 176\\ 154\\ 135\\ 105\\ 147\\ 1,972\\ 214\\ 175\\ 115\\ 105\\ 147\\ 1,972\\ 214\\ 175\\ 101\\ 189\\ 173\\ 101\\ 189\\ 173\\ 101\\ 189\\ 173\\ 378\\ \end{array}$	$\begin{array}{c} 105\\ 105\\ 105\\ 100\\ 100\\ 105\\ 102\\ 97\\ 96\\ 84\\ 78\\ 84\\ 78\\ 84\\ 78\\ 82\\ 100\\ 102\\ 800\\ 84\\ 78\\ 82\\ 100\\ 102\\ 800\\ 800\\ 1470\\ 800\\ 800\\ 116\\ 115\\ 85\\ 88\\ 64\\ 64\\ 153\\ 85\\ 85\\ 85\\ 85\\ 85\\ 85\\ 85\\ 85\\ 85\\ 85$	$\begin{array}{c} 64\\ 52\\ 40\\ 44\\ 40\\ 33\\ 36\\ 40\\ 41\\ 44\\ 45\\ 53\\ 31\\ 30\\ 26\\ 2,49\\ 27\\ 134\\ 139\\ 226\\ 137\\ 1390\\ 2,490\\ 279\\ 216\\ 137\\ 136\\ 115\\ 82\\ 279\end{array}$	$\begin{array}{c} 47\\ 411\\ 411\\ 411\\ 37\\ 37\\ 381\\ 36\\ 38\\ 38\\ 38\\ 38\\ 38\\ 38\\ 38\\ 38\\ 38\\ 38$	$\begin{array}{c} 31\\ 222\\ 222\\ 529\\ 542\\ 559\\ 542\\ 559\\ 542\\ 559\\ 542\\ 559\\ 542\\ 559\\ 542\\ 559\\ 542\\ 559\\ 542\\ 559\\ 542\\ 559\\ 542\\ 559\\ 542\\ 542\\ 542\\ 542\\ 542\\ 542\\ 542\\ 542$	$\begin{array}{c} 36\\ 31\\ 27\\ 222\\ 19\\ 15\\ 15\\ 15\\ 15\\ 15\\ 15\\ 15\\ 15\\ 15\\ 15$	$\begin{array}{c} 177 \\ 111 \\ 100 \\ 100 \\ 98 \\ 88 \\ 88 \\ 88 \\ 88 \\ 88 \\ 88 \\ $	$\begin{array}{c} 15\\11\\8\\14\\10\\0\\9\\8\\1\\1\\15\\13\\10\\10\\118\\27\\15\\15\\15\\15\\15\\15\\15\\15\\15\\15\\15\\15\\15\\$	$\begin{array}{c} 11\\ 11\\ 13\\ 15\\ 15\\ 15\\ 15\\ 15\\ 15\\ 13\\ 13\\ 13\\ 13\\ 13\\ 13\\ 13\\ 13\\ 13\\ 13$	$\begin{array}{c} 39\\ 314\\ 31\\ 31\\ 31\\ 31\\ 32\\ 32\\ 32\\ 32\\ 32\\ 32\\ 32\\ 32\\ 32\\ 32$
		500	5.00	100		104				4.0		

Daily discharge, in second-feet, of Neshaminy Creek, Pennsylvania, below the forks, for 1900.

PERKIOMEN CREEK AT FREDERICK, PENNSYLVANIA.

Measurements of this creek were begun on August 20, 1884. The station is described in the Twentieth Annual Report, Part IV, pages 89 and 90, followed by tables of monthly flow for the years 1890 to 1899, inclusive. Water-Supply Paper No. 35 contains tables of the daily discharge for the entire period from 1884 to 1899, inclusive. Diagrams of daily discharge, constructed from these tables, were published in the Twenty-first Annual Report, Part IV, pages 79 and 80, and figures for the monthly flow for 1899 on page 78 of that report. The following records of daily discharge for 1900 are furnished by Mr. John E. Codman, hydrographer of the water department of Philadelphia.
PENNSYLVANIA.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 20 21 22 23 24 25 20 21 22 23 24 25 20 21 22 23 24 25 20 21 22 23 24 25 31 31	$\begin{array}{r} 52\\ 53\\ 43\\ 35\\ 32\\ 30\\ 38\\ 36\\ 41\\ 460\\ 123\\ 106\\ 135\\ 106\\ 135\\ 106\\ 135\\ 106\\ 135\\ 138\\ 106\\ 135\\ 138\\ 106\\ 135\\ 138\\ 106\\ 135\\ 138\\ 101\\ 126\\ 135\\ 138\\ 106\\ 135\\ 158\\ 158\\ 158\\ 158\\ 158\\ 158\\ 158\\ 15$	$\begin{array}{c} 168\\ 178\\ 178\\ 178\\ 178\\ 188\\ 198\\ 198\\ 198\\ 198\\ 3,112\\ 284\\ 208\\ 198\\ 3,112\\ 284\\ 208\\ 198\\ 188\\ 158\\ 158\\ 158\\ 158\\ 158\\ 158\\ 15$	$\begin{array}{c} 360\\ 360\\ 1, 648\\ 1, 212\\ 368\\ 219\\ 208\\ 208\\ 208\\ 208\\ 208\\ 208\\ 208\\ 208$	$\begin{array}{c} 148\\ 158\\ 158\\ 158\\ 123\\ 123\\ 123\\ 123\\ 125\\ 198\\ 98\\ 993\\ 88\\ 135\\ 163\\ 183\\ 101\\ 98\\ 145\\ 362\\ 1,212\\ 315\\ 178\\ 178\\ 178\\ 178\\ 178\\ 178\\ 178\\ 178$	$\begin{array}{c} 84\\ 80\\ 102\\ 110\\ 84\\ 60\\ 566\\ 63\\ 67\\ 755\\ 63\\ 58\\ 585\\ 585\\ 585\\ 585\\ 585\\ 585\\ 129\\ 988\\ 802\\ 102\\ 102\\ 102\\ 67\\ 711\\ 67\\ 58\end{array}$	$\begin{array}{c} 52\\ 555\\ 555\\ 566\\ 466\\ 499\\ 449\\ 423\\ 433\\ 633\\ 544\\ 555\\ 554\\ 551\\ 466\\ 466\\ 469\\ 499\\ 499\\ 466\\ 467\\ 334\\ 384\\ 411\\ 366\\ \hline \end{array}$	$\begin{array}{c} 29\\ 24\\ 34\\ 62\\ 71\\ 75\\ 38\\ 36\\ 36\\ 36\\ 36\\ 36\\ 36\\ 36\\ 36\\ 242\\ 22\\ 24\\ 41\\ 41\\ 41\\ 18\\ 18\\ 255\\ 6900\\ 1,502\\ 116\\ 71\\ 52\\ 135\\ 52\\ 135\\ 52\\ 135\\ 52\\ 135\\ 135\\ 135\\ 135\\ 135\\ 135\\ 135\\ 135$	$\begin{array}{c} 84\\ 64\\ 64\\ 54\\ 55\\ 36\\ 36\\ 36\\ 34\\ 24\\ 36\\ 34\\ 26\\ 26\\ 36\\ 34\\ 24\\ 31\\ 122\\ 26\\ 93\\ 63\\ 54\\ 41\\ 31\\ 31\\ 31\\ 31\\ 31\\ 31\\ 31\\ 31\\ 31\\ 3$	41 41 31 29 36 31 29 26 31 29 26 31 21 41 23 36 36 36 36 36 36 36 36 36 3	$\begin{array}{c} 36\\ 36\\ 36\\ 36\\ 36\\ 31\\ 20\\ 58\\ 47\\ 37\\ 36\\ 39\\ 63\\ 34\\ 37\\ 326\\ 63\\ 652\\ 46\\ 46\\ 46\\ 46\\ 46\\ 41\\ 36\\ 386\\ 36\\ 26\\ 26\\ 26\\ 26\\ 26\\ 31\\ 41\\ 41\\ 41\\ 41\\ 41\\ 41\\ 41\\ 41\\ 41\\ 4$	$\begin{array}{c} 41\\ 36\\ 36\\ 31\\ 31\\ 31\\ 36\\ 36\\ 41\\ 41\\ 43\\ 32\\ 46\\ 67\\ 42\\ 23\\ 31\\ 31\\ 31\\ 31\\ 31\\ 31\\ 31\\ 31\\ 31\\ 3$	$\begin{array}{c} 588\\ 555\\ 544\\ 2700\\ 565\\ 565\\ 565\\ 565\\ 588\\ 582\\ 338\\ 433\\ 433\\ 433\\ 433\\ 838\\ 366\\ 366\\ 366\\ 366\\ 366\\ 366\\ 3$
mean	299	741	321	178	117	44	127	94	33	38	50	84

Daily discharge, in second-feet, of Perkiomen Creek at Frederick, Pennsylvania, for 1900.

[Continued in Water-Supply and Irrigation Paper No. 48.]

0

ixteenth Annual Report of the United States Geological Survey, 1894-95, Part II, Papers of an economic character, 1895; octavo, 598 pp.

Contains a paper on the public lands and their water supply, by F. H. Newell, illustrated by a large map showing the relative extent and location of the vacant public lands; also a report on the water resources of a portion of the Great Plains, by Robert Hay.

geological reconnoissance of northwestern Wyoming, by George H. Eldridge, 1894; octavo, 72 pp. Bulletin No. 119 of the United States Geological Survey; price, 10 cents.

Contains a description of the geologic structure of portions of the Bighorn Range and Bighorn Basin, especially with reference to the coal fields, and remarks upon the water supply and agricultural possibilities.

teport of progress of the division of hydrography for the calendar years 1893 and 1894, by F. H. Newell, 1895; octavo, 176 pp. Bulletin No. 131 of the United States Geological Survey; price, 15 cents.

Contains results of stream measurements at various points, mainly within the arid region, and records of wells in western Nebraska, western Kansas, and eastern Colorado.

1896.

eventeenth Annual Report of the United States Geological Survey, 1895-96, Part II, Economic geology and hydrography, 1896; octavo, 864 pp.

Contains papers on "The underground water of the Arkansas Valley in eastern Colorado," by G K Gilbert; "The water resources of Illinois," by Frank Leverett; and "Pre-liminary report on the artesian waters of a portion of the Dakotas," by N. H. Darton.

rtesian-well prospects in the Atlantic Coastal Plain region, by N. H. Darton, 1896; octavo, 230 pp., 19 plates. Bulletin No. 138 of the United States Geological Survey; price, 20 cents.

Gives a description of the geologic conditions of the coastal region from Long Island, N. Y., to Georgia, and contains data relating to many of the deep wells.

teport of progress of the division of hydrography for the calendar year 1895, by F. H. Newell, hydrographer in charge, 1836; octavo, 356 pp. Bulletin No. 140 of the United States Geological Survey; price, 25 cents.

Contains a description of the instruments and methods employed in measuring streams and the results of hydrographic investigations in various parts of the United States.

1897.

ighteenth Annual Report of the United States Geological Survey, 1896–97, Part IV, Hydrography, 1897; octavo, 756 pp.

Contains a "Report of progress of stream measurements for the calendar year 1896," by Arthur P. Davis; "The water resources of Indiana and Ohio," by Frank Leverett; "New developments in well boring and irrigation in Sonth Dakota," by N. H. Darton; and "Reservoirs for irrigation," by J. D. Schwyler.

1899.

lineteenth Annual Report of the United States Geological Survey, 1897–98, Part IV, Hydrography, 1899; octavo, 814 pp.

Contains a "Report of progress of stream measurements for the calendar year 1898," by F. H. Newell and others; "The rock waters of Ohio," by Edward Orton; and "A pre-liminary report on the geology and water resources of Nebraska west of the one hundred and third meridian," by N. H Darton. Part II of the Nineteenth Annual contains a paper on "Principles and conditions of the movements of ground water," by F. H. King, and one on "Theoretical investigation of the motion of ground waters," by C. S. Slichter.

wentieth Annual Report of the United States Geological Survey, 1898-99, Part IV, Hydrography, 1900; octavo, 660 pp.

Contains a "Report of progress of stream measurements for the calendar year 1898," by F. H. Newell, and "Hydrography of Nicaragua," by A. P. Davis.

1901.

wenty-first Annual Report of the United States Geological Survey, 1899-1900, Part IV, Hydrography, 1900; octavo, 768 pp.

Contains a "Report of progress of stream measurements for the calendar year 1899," by F H. Newell; "Preliminary description of the geology and water resources of the southern half of the Black Hills and adjoining regions in Sonth Dakota and Wyoming," by N. H. Darton; and "The High Plains and their utilization," by W. D. Johnson.

Bulletins can be obtained only by prepayment of cost, as noted above. Money hould be transmitted by postal money order or express order, payable to the Direcor of the United States Geological Survey. Postage stamps, checks, and drafts an not be accepted. Correspondence should be addressed to The Director, U.S. eol. Survey, Washington, D. C.

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WATER-SUPPLY AND IRRIGATION PAPERS.

1. Pumping water for irrigation, by Herbert M. Wilson, 1896.

- 2. Irrigation near Phœnix, Arizona, by Arthur P. Davis, 1897.
- 3. Sewage irrigation, by George W. Rafter, 1897.
- 4. A reconnoissance in southeastern Washington, by Israel C. Russell, 1897.
- 5. Irrigation practice on the Great Plains, by E. B. Cowgill, 1897.
- 6. Underground waters of southwestern Kansas. by Erasmus Haworth, 1897.
- 7. Seepage waters of northern Utah, by Samuel Fortier, 1897.
- 8. Windmills for irrigation, by E. C. Murphy, 1897.
- 9. Irrigation near Greeley, Colorado, by David Boyd, 1897.
- 10. Irrigation in Mesilla Valley, New Mexico, by F. C. Barker, 1898.
- 11. River heights for 1896, by Arthur P. Davis, 1897.
- 12. Underground waters of southeastern Nebraska, by N. H. Darton, 1898.
- 13. Irrigation systems in Texas, by W. F. Hutson, 1898.
- 14. New tests of pumps and water lifts used in irrigation, by O. P. Hood, 1898.
- 15, 16. Operations at river stations, 1897, Parts I, II, 1898.
- 17. Irrigation near Bakersfield, California, by C. E. Grunsky, 1898.
- 18. Irrigation near Fresno, California, by C. E. Grunsky, 1898.
- 19. Irrigation near Merced, California, by C. E. Grunsky, 1899.
- 20. Experiments with windmills, by Thomas O. Perry, 1899.
- 21. Wells of northern Indiana, by Frank Leverett, 1899.
- 22. Sewage irrigation, Part II, by George W. Rafter, 1899.
- 23. Water-right problems of Bighorn Mountains, by Elwood Mead, 1899.
- 24, 25. Water resources of the State of New York, Parts I, II, by G. W. Rafter, 1899.
- 26. Wells of southern Indiana (continuation of No. 21), by Frank Leverett, 1899.
- 27, 28. Operations at river stations, 1898, Parts I, II, 1899.
- 29. Wells and windmills in Nebraska, by Erwin Hinckley Barbour, 1899.
- 30. Water resources of the lower peninsula of Michigan, by Alfred C. Lane, 1899.
- 31. Lower Michigan mineral waters, by Alfred C. Lane, 1899.
- 32. Water resources of Porto Rico, by H. M. Wilson, 1900.
- 33. Storage of Water on Gila River, Arizona, by J. B. Lippincott, 1900.
- 34. Geology and water resources of southeastern S. Dak., by J. E. Todd, 1900.
- 35-39. Operations at river stations, 1899, Parts I-V, 1900.
- 40. The Austin dam, by Thomas U. Taylor, 1900.
- 41, 42. The windmill: its efficiency and use, Parts I, II, by E. C. Murphy, 1901.
- 43. Conveyance of water in irrigation canals, etc., by Samuel Fortier, 1901.
- 44. Profiles of rivers, by Henry Gannett, 1901.
- 45. Water storage on Cache Creek, California, by Albert E. Chandler, 1901.
- 46. Reconn. of Kern and Yuba rivers, Cal., by F. H. Olmsted and M. Manson, 1901.
- 47-52. Operations at river stations, 1900, Parts I-VI, 1901.

Other papers are in various stages of preparation. Provision has been made for printing these by the following clause in the sundry civil act making appropriations for the year 1896–97:

Provided, That hereafter the reports of the Geological Survey in relation to the gaging of streams and to the methods of utilizing the water resources may be printed in octavo form, not to exceed 100 pages in length and 5,000 copies in number; 1,000 copies of which shall be for the official use of the Geological Survey, 1,500 copies shall be delivered to the Senate, and 2,500 copies shall be delivered to the House of Representatives, for distribution. [Stat. L., vol. 29, p. 453.]

The endeavor is made to send these pamphlets to persons who have rendered assistance in their preparation through replies to schedules or who have furnished data. Requests made for a certain paper and stating a reason for asking for it are granted whenever practicable, but it is impossible to comply with general demands, such as to have all of the series sent.

Application for these papers should be made either to members of Congress or to THE DIRECTOR, UNITED STATES GEOLOGICAL SURVEY, WASHINGTON, D. C.

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DEPARTMENT OF THE INTERIOR

WATER-SUPPLY

AND

IRRIGATION PAPERS

OF THE

UNITED STATES GEOLOGICAL SURVEY

No.

OPERATIONS AT RIVER STATIONS, 1900,-PART II

WASHINGTON GOVERNMENT PRINTING OFFICE 1901

IRRIGATION REPORTS.

The following list contains titles and brief descriptions of the principal reports relating to water supply and irrigation prepared by the United States Geological Survey since 1890:

1890.

First Annual Report of the United States Irrigation Survey, 1890; octavo, 123 pp.

Printed as Part II, Irrigation, of the Tenth Annual Report of the United States Geological Survey, 188-89. Contains a statement of the origin of the Irrigation Survey, a preliminary report on the organization and prosecution of the survey of the arid lands for purposes of irrigation, and report of work done during 1890.

1801.

Second Annual Report of the United States Irrigation Survey, 1891; octavo, 395 pp.

Published as Part II, Irrigation, of the Eleventh Annual Report of the United States Geological Survey, 1889-90. Contains a description of the hydrography of the arid region and of the engineering operations carried on by the Irrigation Survey during 1890; also the statement of the Director of the Survey to the House Committee on Irrigation, and other papers, including a bibliography of irrigation literature. Illustrated by 29 plates and 4 figures.

Third Annual Report of the United States Irrigation Survey, 1891: octavo, 576 pp.

Printed as Part II of the Twelfth Annual Report of the United States Geological Survey, 1890-91. Contains "Report upon the location and survey of reservoir sites during the fiscal year ended June 30, 1891," by A. H. Thompson; "Hydrography of the arid regions," by F. H. Newell; "Irrigation in India," by Herbert M. Wilson. Illustrated by 93 plates and 190 figures.

Bulletins of the Eleventh Census of the United States upon irrigation, prepared by

F. H. Newell; quarto. No. 35, Irrigation in Arizona; No. 60, Irrigation in New Mexico; No. 85, Irrigation in Utah; No. 107, Irrigation in Wyoming; No. 153, Irrigation in Montana; No. 157, Irrigation in Idaho; No. 163, Irrigation in Nevada; No. 178, Irrigation in Oregon; No. 193, Artesian wells for irrigation; No. 198, Irrigation in Washington.

1892.

Irrigation of western United States. by F. H. Newell; extra census bulletin No. 23, September 9, 1892; quarto, 22 pp.

Contains tabulations showing the total number, average size, etc., of irrigated holdings, the total area and average size of irrigated farms in the subhumid regions, the percentage of number of farms irrigated, character of crops, value of irrigated lands, the average cost of irrigation, the investment and profits, together with a résumé of the water supply and a description of irrigation by artesian wells. Illustrated by colored maps, showing the location and relative extent of the irrigated areas.

1893.

Thirteenth Annual Report of the United States Geological Survey, 1891–92, Part III, Irrigation, 1893; octavo, 486 pp.

Consists of three papers: "Water supply for irrigation," by F. H. Newell; "American irrigation engineering" and "Engineering results of the Irrigation Survey," by Herbert M. Wilson: "Construction of topographic maps and selection and survey of reservoir sites," by A. H. Thompson. Illustrated by 77 plates and 119 figures.

A geological reconnoissance in central Washington, by Israel Cook Russell, 1893; octavo, 108 pp., 15 plates. Bulletin No. 108 of the United States Geological Survey; price, 15 cents.

Contains a description of the examination of the geologic structure in and adjacent to the drainage basin of Yakima River and the great plains of the Columbia to the east of this area, with special reference to the occurrence of artesian waters.

1894.

Report on agriculture by irrigation in the western part of the United States at the Eleventh Census, 1890, by F. H. Newell, 1894; quarto, 283 pp.

Consists of a general description of the condition of irrigation in the United States, the area irrigated, cost of works, then value and profits; also describes the water supply, the value of water, of artesian wells, reservoirs, and other details; then takes up each State and Territory in order, giving a general description of the condition of agriculture by irrigation, and discusses the physical conditions and local peculiarities in each county.

Fourteenth Annual Report of the United States Geological Survey, 1892-93, in two parts; Part II, Accompanying papers, 1894; octavo, 597 pp.

Contains papers on "Potable waters of the eastern United States," by W J McGee; "Natural mineral waters of the United States," by A. C. Peale; "Results of stream measure-ments," by F. H. Newell. Illustrated by maps and diagrams.

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(Continued on third page of cover.)

DEPARTMENT OF THE INTERIOR

WATER-SUPPLY

AND

IRRIGATION PAPERS

OF THE

UNITED STATES GEOLOGICAL SURVEY

No. 48



WASHINGTON GOVERNMENT PRINTING OFFICE 1901 r

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UNITED STATES GEÒLOGICAL SURVEY

CHARLES D. WALCOTT, DIRECTOR

OPERATIONS AT RIVER STATIONS, 1900

A REPORT OF THE

DIVISION OF HYDROGRAPHY

 $\mathbf{OF}\cdot\mathbf{THE}$

UNITED STATES GEOLOGICAL SURVEY

PART II



WASHINGTON GOVERNMENT PRINTING OFFICE 1901

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	Shouandeah Diver at Millyille, West Virginia	1.
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	Deep River at Cumnock, North Carolina	18
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	Yadkin River at Siloam, North Carolina	18
	Yadkin River at Salisbury, North Carolina	18
	Yadkin River at Norwood, North Carolina	1-
	Catawba River near Morganton, North Carolina	1-
	Linville River near Bridgewater, North Carolina	1-
	John River near Morganton, North Carolina	14
	Catawba River at Catawba, North Carolina	1-
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	100	

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OPERATIONS AT RIVER STATIONS, 1900. PART II.

MEASUREMENTS AT RIVER STATIONS.¹

WISSAHICKON CREEK NEAR PHILADELPHIA, PENNSYLVANIA.

This station is described in the Twentieth Annual Report, Part IV, page 94, followed by tables of monthly flow for 1897 and 1898. In Water-Supply Paper No. 35, page 74, will be found the figures for the daily discharge for 1899, ending with June 5, when the observations were discontinued temporarily, and were not again resumed until July 1, 1900. The figures for monthly flow for 1899 and diagrams of daily discharge for the entire period of observation (1897 to 1899, inclusive) will be found in the Twenty-first Annual Report, Part IV, pages 81 and 82. The following tables contain the figures for the daily discharge from which the diagrams were constructed, as well as those for 1900, diagram for which is not yet plotted.

Daily discharge, in second-feet, of Wissahickon Creek near Philadelphia, Pennsylvania, for 1897.

Day.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1	$\begin{array}{c} 91\\ 83\\ 75\\ 71\\ 77\\ 77\\ 845\\ 182\\ 182\\ 140\\ 117\\ 98\\ 86\\ 84\\ 79\\ 99\\ 99\\ 99\\ 99\\ 99\\ 99\\ 91\\ 85\\ 204\\ 85\\ 85\\ 204\\ 85\\ 85\\ 204\\ 85\\ 85\\ 204\\ 85\\ 85\\ 85\\ 85\\ 85\\ 85\\ 85\\ 85\\ 85\\ 85$	$\begin{array}{c} 84\\ 87\\ 74\\ 137\\ 168\\ 1175\\ 132\\ 132\\ 132\\ 132\\ 132\\ 132\\ 132\\ 132$	$\begin{array}{c} 62\\ 72\\ 63\\ 66\\ 56\\ 56\\ 56\\ 56\\ 56\\ 56\\ 56\\ 56\\ 56$	$\begin{array}{c} 162\\ 148\\ 148\\ 139\\ 131\\ 129\\ 108\\ 120\\ 108\\ 117\\ 160\\ 110\\ 101\\ 100\\ 110\\ 100\\ 550\\ 497\\ 158\\ 897\\ 97\\ 933\\ 888\\ 142\\ 79\\ 91\\ 888\\ 142\\ 79\\ 91\\ 888\\ 142\\ 79\\ 91\\ 888\\ 142\\ 79\\ 91\\ 888\\ 142\\ 79\\ 91\\ 888\\ 142\\ 79\\ 91\\ 888\\ 142\\ 79\\ 91\\ 888\\ 142\\ 79\\ 91\\ 888\\ 142\\ 79\\ 91\\ 888\\ 142\\ 79\\ 91\\ 888\\ 142\\ 79\\ 91\\ 888\\ 142\\ 79\\ 91\\ 888\\ 142\\ 79\\ 91\\ 888\\ 142\\ 79\\ 91\\ 142\\ 888\\ 142\\ 79\\ 91\\ 142\\ 888\\ 142\\ 79\\ 91\\ 142\\ 888\\ 142\\ 79\\ 91\\ 142\\ 142\\ 142\\ 142\\ 142\\ 142\\ 142\\ 14$	76 102 74 559 67 532 532 532 532 535 535 535 535	4154498898982755883399884444558513987489393875	$\begin{array}{c} 68\\ 432\\ 132\\ 775\\ 465\\ 445\\ 48\\ 48\\ 48\\ 48\\ 48\\ 48\\ 48\\ 48\\ 48\\ 48$	$\begin{array}{c} 65\\ 655\\ 65\\ 74\\ 2766\\ 866\\ 866\\ 866\\ 866\\ 866\\ 866\\ 868\\ 868\\ 868\\ 833\\ 1632\\ 1632\\ 1632\\ 105\\ 833\\ 105\\ 894\\ 800\\ 733\\ 755\\ 775\\ 872\\ 872\\ 872\\ 872\\ 872\\ 872\\ 872\\ 872$
Mean	95	148	204	147	•47	32	71	127

[Drainage area, 64.6 square miles.]

¹Continued from Water-Supply and Irrigation Paper No. 47.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1	118 91 92	113 110 110	118 115 110	143 110 101	98 89	94 93		29 30	$ 24 \\ 24 \\ 24 $	19 19	46 29	$129 \\ 107 \\ 107$
3 4 5		$113 \\ 118 \\ 116$	119 115 110	$ 101 \\ 93 \\ 101 $	$ \begin{array}{c} 73 \\ 77 \\ $	80 84 80	35 35 34	$ \begin{array}{r} 68 \\ 79 \\ 164 \end{array} $	$ \begin{array}{r} 24 \\ 24 \\ 23 \end{array} $	18 18 19	$ \begin{array}{c} 24 \\ 26 \\ 24 \end{array} $	103 354 923
6 7 8	$71 \\ 75 \\ 71$	108 98 93	$110 \\ 110 \\ 103$	$ \begin{array}{r} 101 \\ 101 \\ 100 \end{array} $	$79 \\ 111 \\ 744$	79 79 77	34 34 33	$ \begin{array}{r} 108 \\ 64 \\ 64 \end{array} $	23 23 22	18 16 17	23 27 33	183 142 125
9 10	64 68 67	93 93 101	94 93 06	91 87	$256 \\ 136 \\ 125$	79 78	32 32 21	66 84	20 22	$17 \\ 16 \\ 15$		$110 \\ 101 \\ 02$
11 12 13	97 136	$104 \\ 146 \\ 143 \\ 109$	96 91	87 87	125 125 235	70 68	30 30 30	$135 \\ 125 \\ 118 \\ 02$	20 20 21	13 17 19	82 63	93 93
$\begin{array}{c} 1+\\ 15\\ 16\\ \end{array}$	$ \begin{array}{r} 105 \\ 215 \\ 177 \\ 177 \\ \end{array} $	$108 \\ 108 \\ 96 \\ 96$	87 84	93 93 87	281 242	60 64	29 29 30		21 20 21	$21 \\ 24 \\ 25 \\ 10$	50 75 70	95 86 80
17 18 19	105 78 75 75 75 75 75	$93 \\ 93 \\ 120$	86 84 82	79 75 75	$ \begin{array}{r} 323 \\ 139 \\ 131 \end{array} $		28 26 28	$ \begin{array}{r} 108 \\ 416 \\ 859 \end{array} $	$ \begin{array}{c} 21 \\ 20 \\ 19 \end{array} $	18 20 29	$ \begin{array}{r} 79 \\ 125 \\ 918 \end{array} $	79 75 84
20 21 22	$ \begin{array}{r} 132 \\ 223 \\ 134 \end{array} $	$1,512 \\ 338 \\ 210$	$ \begin{array}{r} 79 \\ 89 \\ 101 \end{array} $	79 79 75	$ \begin{array}{r} 155 \\ 230 \\ 125 \end{array} $		$ \begin{array}{r} 30 \\ 32 \\ 64 \end{array} $	$ \begin{array}{c} 123 \\ 65 \\ 55 \end{array} $	$ \begin{array}{c} 19 \\ 19 \\ 19 \\ 19 \end{array} $	$ 28 \\ 37 \\ 61 $	176 104 89	294 143 129
23 24 25	$751 \\ 193 \\ 140$	158 140 133	$ \begin{array}{r} 105 \\ 113 \\ 113 \end{array} $	$ \begin{array}{r} 75 \\ 108 \\ 122 \end{array} $	$ \begin{array}{r} 110 \\ 128 \\ 128 \end{array} $	$55 \\ 55 \\ 54$		44 40 55	28 33 25	35 26 22	$ \begin{array}{r} 140 \\ 141 \\ 118 \end{array} $	$531 \\ 166 \\ 122$
26 27 28	$205 \\ 201 \\ 128$	130 128 124	93 84 104	$ \begin{array}{r} 107 \\ 98 \\ 225 \end{array} $	$ \begin{array}{r} 146 \\ 116 \\ 113 \end{array} $	$54 \\ 46 \\ 125$		42 42 26	25 26 21	47 70 60	118 100 100	115 98 80 80
29 30 31	125 118 113			235 107	107 107 107 100	79 60	$50 \\ 34 \\ 31$	27 70 67	20 19	44 31 48	168 129	84 101 143
Mean	139	176	110	103	162	71	43	111	22	28	118	163

Daily discharge, in second-feet, of Wissahickon Creek near Philadelphia, Pennsylvania, for 1898.

Daily discharge, in second-feet, of Wissahickon Creek near Philadelphia, Pennsylvania, for 1899.

Day.	Jan. Feb.	Mar.	Apr.	May.	June.	Day.	Jan.	Feb.	Mar.	Apr.	May.	June.
1 2 3 4 5 6 7 9 10 11 12 13 14 15 16 17	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 285\\ 245\\ 243\\ 236\\ 1,059\\ 365\\ 241\\ 204\\ 198\\ 198\\ 198\\ 198\\ 198\\ 198\\ 198\\ 346\\ 346\\ 359\\ 186\end{array}$	$\begin{array}{c} 191\\ 175\\ 175\\ 175\\ 173\\ 159\\ 151\\ 166\\ 451\\ 205\\ 152\\ 152\\ 140\\ 140\\ 140\\ 140\\ 140\\ 142\\ 142\\ 142\end{array}$	$\begin{array}{r} 89\\ 96\\ 103\\ 93\\ 80\\ 80\\ 87\\ 75\\ 75\\ 105\\ 108\\ 90\\ 87\\ 87\\ 87\\ 87\\ 87\\ 87\\ 87\\ 87\\ 87\\ 87$	45 42 33 21	18	$\begin{array}{c} 147\\ 118\\ 116\\ 115\\ 106\\ 259\\ 925\\ 184\\ 142\\ 133\\ 136\\ 136\\ 136\\ 207\\ \end{array}$	227 350 466 436 779 630 359 250 245 1,285 1,285 423 271	$\begin{array}{c} 273\\ 603\\ 340\\ 202\\ 521\\ 328\\ 232\\ 202\\ 216\\ 198\\ 434\\ 813\\ 260\\ 218\\ 326\\ \end{array}$	$\begin{array}{c} 129\\ 129\\ 123\\ 115\\ 106\\ 106\\ 106\\ 106\\ 106\\ 106\\ 101\\ 98\\ 95\\ \hline \end{array}$	96 90 73 68 75 96 96 75 64 64 54 54 59 54 81	

PENNSYLVANIA.

Day.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Day.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1	$\begin{array}{c} 15\\ 17\\ 20\\ 17\\ 17\\ 17\\ 17\\ 17\\ 17\\ 16\\ 40\\ 54\\ 32\\ \end{array}$	$\begin{array}{c} 47\\ 24\\ 20\\ 16\\ 16\\ 17\\ 20\\ 17\\ 17\\ 15\\ 12\\ 98\\ 31\\ 31\\ \end{array}$	$ \begin{array}{r} 16 \\ 15 \\ 15 \\ 13 \\ 10 \\ 9 \\ 8 \\ 13 \\ 13 \\ 9 \\ 8 \\ 13 \\ 9 \\ 9 \\ 8 \\ 13 \\ 9 \\ 13 \\ 13 \\ 13 \\ 13 \\ 13 \\ 13 \\ 9 \\ 9 \\ 9 \\ 9 \\ 9 \\ 9 \\ 9 \\ 9 \\ 13 \\ 13 \\ 13 \\ 13 \\ 13 \\ 13 \\ 13 \\ 13 \\ 13 \\ 13 \\ 9 \\ 9 \\ 9 \\ 9 \\ 9 \\ 9 \\ 9 \\ 10 \\ $	$\begin{array}{c} 64\\ 40\\ 17\\ 15\\ 14\\ 12\\ 27\\ 54\\ 47\\ 23\\ 15\\ 16\\ 274 \end{array}$	$ 18 \\ 17 \\ 15 \\ 15 \\ 17 \\ 18 \\ 14 \\ 16 \\ 15 \\ 10 \\ 15 \\ 18 \\ 14 \\ 14 \\ 15 \\ 10 \\ 15 \\ 18 \\ 14 \\ 14 \\ 15 \\ 15 \\ 18 \\ 14 \\ 14 \\ 15 \\ 15 \\ 18 \\ 14 \\ 14 \\ 15 \\ 15 \\ 18 \\ 14 \\ 14 \\ 15 \\ 15 \\ 18 \\ 14 \\ 14 \\ 15 \\ 15 \\ 18 \\ 14 \\ 14 \\ 15 \\ 15 \\ 18 \\ 14 \\ 14 \\ 15 \\ 15 \\ 18 \\ 14 \\ 14 \\ 15 \\ 15 \\ 18 \\ 14 \\ 14 \\ 15 \\ 15 \\ 18 \\ 14 \\ 14 \\ 15 \\ 18 \\ 14 \\ 14 \\ 15 \\ 15 \\ 18 \\ 14 \\ 14 \\ 15 \\ 15 \\ 18 \\ 14 \\ 14 \\ 16 \\ 15 \\ 18 \\ 14 \\ 14 \\ 16 \\ 15 \\ 18 \\ 14 \\ 14 \\ 16 \\ 15 \\ 18 \\ 14 \\ 14 \\ 16 \\ 15 \\ 18 \\ 14 \\ 14 \\ 16 \\ 15 \\ 18 \\ 14 \\ 14 \\ 16 \\ 15 \\ 18 \\ 14 \\ 14 \\ 16 \\ 15 \\ 18 \\ 14 \\ 16 \\ 15 \\ 18 \\ 14 \\ 16 \\ 15 \\ 18 \\ 14 \\ 16 \\ 15 \\ 18 \\ 14 \\ 16 \\ 15 \\ 18 \\ 14 \\ 16 \\ 15 \\ 16 \\ 16 \\ 16 \\ 16 \\ 15 \\ 16 \\ 16 \\ 16 \\ 16 \\ 16 \\ 16 \\ 16 \\ 15 \\ 18 \\ 14 \\ 16 \\ $	$\begin{array}{c} 2244479\\22447943388822241\\3388852241\\24\\24124\\3388852241\\24\\24\\24\\24\\24\\24\\24\\24\\24\\24\\24\\24\\24\\$	18 19 20 21 23 24 25 26 27 28 29 30 31	$13 \\ 9 \\ 10 \\ 18 \\ 21 \\ 114 \\ 114 \\ 19 \\ 116 \\ 826 \\ 17 \\ 176 \\ 219 \\ 17 \\ 176 \\ 219 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10 \\ $	$59 \\ 152 \\ 80 \\ 43 \\ 27 \\ 26 \\ 31 \\ 20 \\ 47 \\ 40 \\ 32 \\ 27 \\ 27 \\ 152 $	$39 \\ 17 \\ 17 \\ 14 \\ 14 \\ 12 \\ 13 \\ 10 \\ 10 \\ 10 \\ 13 \\ 13 \\ 37 \\ 37 \\ 10 \\ 10 \\ 13 \\ 37 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10 \\ 1$	25 19 21 21 21 20 17 14 12 15 15	$\begin{array}{c} 11\\ 12\\ 14\\ 13\\ 12\\ 11\\ 10\\ 11\\ 367\\ 86\\ 26\\ 20\\ 25\\ \end{array}$	24 22 21 21 21 21 21 21 20 20 20 20 20 20 20
15 16 17	$ \begin{array}{c} 15 \\ 18 \\ 15 \end{array} $	$ \begin{array}{c} 24 \\ 18 \\ 18 \end{array} $	$ \begin{array}{r} 12 \\ 278 \\ 85 \end{array} $	92 54 35	13 11 11	31 30 26	Mean	42	35	26	34	29	42

Daily discharge, in second-feet, of Wissahickon Creek near Philadelphia. Pennsylvania. for 1900.

SCHUYLKILL RIVER ABOVE PHILADELPHIA, PENNSYLVANIA.

This river is described in Water-Supply Paper No. 35, page 74. Records of the height of the river at Fairmount dam have been kept for many years, but measurements for computing the daily discharge were not made until 1898. The first of the following tables does not represent the total flow of the stream, but the amount wasted over the flashboards at the dam, to which must be added the pumpage from the river, the leakage, and the quantity used for power at Fairmount. The second table is an estimate of the total monthly yield, in cubic feet, including the foregoing items. The figures were furnished by Mr. John E. Codman, hydrographer for the water department of the city of Philadelphia.

Daily discharge, in second-feet, of Schuylkill River above Philadelphia. Pennsylvania, for 1900, being amount wasted over flashboards at Fairmount dam.

$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	Day.	Jan.	Feb.	Mar.	Apr.	May.	July.	Dec.
	1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 1 1 1 1	$\begin{array}{c} & & \\ & & \\ & & \\ & & \\ \hline \\ \hline$	$\begin{matrix} 15,673\\8,103\\3,077\\3,890\\5,618\\3,441\\1,712\\1,348\\9,531\\5,905\\3,559\\2,489\\2,076\\1,005\\1,349\\2,478\\2,076\\8,225\\2,4,642\\2,076\end{matrix}$	$\begin{array}{c} 5,526\\ 19,061\\ 3,197\\ 7,318\\ 3,814\\ 3,8146\\ 2,2076\\ 2,076\\ 1,027\\ 1,027\\ 1,027\\ 359\\ 3477\\ 4,243\\ 9,3,641\\ 2,439\\ 9,3,641\\ 2,439\\ 9,3,641\\ 2,439\\ 9,3,641\\ 2,439\\ 9,3,641\\ 1,348\\ 2,439\\ 1,524\\ 1,348\\ 1,188\\ 1,188\\ \end{array}$	1, 027 8803 613 207 148 260 2600 378 378 238 238 238 238 238 238 238 23	4,103 6,243 923 211 211	80 54 119 2, 861 2, 525 923	425 2,041 2,041 1,302 644 68

NOTE.—The amount wasted over the flashboards on June 28 was 1,088 second-feet, on August 13 it was 79 second-feet, and on November 27 and 28 it was 43 and 18 second-feet, respectively.

Total monthly yield of Schuykill River above Philadelphia, Pennsylvania, for 1900.

Month.	Yield.	Month.	Yield.
January February March April May June	$\begin{array}{c} Cubic feet.\\ 6, 610, 500, 000\\ 33, 771, 128, 000\\ 14, 666, 146, 000\\ 5, 730, 472, 000\\ 5, 073, 978, 000\\ 2, 743, 671, 000 \end{array}$	July	$\begin{array}{c} Cubic feet.\\ 2,856,566,000\\ 2,040,927,000\\ 1,229,059,000\\ 1,372,271,000\\ 1,579,652,000\\ 3,429,617,000 \end{array}$

NORTH BRANCH OF SUSQUEHANNA RIVER AT WILKESBARRE, PENN-SYLVANIA.

This station, which was established by E. G. Paul March 30, 1899, is described in Water-Supply Paper No. 35, page 76. The results of measurements for 1899 will be found in the Twenty-first Annual Report, Part IV, page 88. A bench mark was established September 26, 1900, being the extreme west end of the stone doorsill of the north entrance to the Coal Exchange Building, at 32.99 feet above datum of the gage. During 1900 two measurements of discharge were made by Mr. Paul, as follows:

May 20: Gage height, 5.60 feet: discharge, 6,772 second-feet.

September 26: Gage height, 2.20 feet; .discharge, 961 second-feet.

The measurement of September 26 was made at Retreat, Pennsylvania, 10 miles below Wilkesbarre.

Jan. Feb. May. June. July. Day. Mar. Apr. Aug. Sept. Oct. Nov. Dec $\begin{array}{c} 10.\ 40 \\ 17.\ 75 \\ 14.\ 55 \end{array}$ $\begin{array}{c} 3.\,00\ 2.\,80\ 2.\,70\ 2.\,90 \end{array}$ 2.30 6.80 6.20 7.40 $6.90 \\ 7.50$ 6.10 ${3.80 \atop {3.70} \atop {4.20}}$ $\frac{3.20}{3.20}$ 3.10 $2.70 \\ 2.60$ 10.50 2.30 6.80 3.00 $5.80 \\ 5.50$ 9.20 $\frac{2.60}{2.50}$ 9.80 $\frac{3.00}{2.90}$ 2.30 $8.10 \\ 7.40$ 6.40 6.30 3.106 50 11.20 2.303.90 6.80 11.80 5.30 3.00 $\tilde{2}.90$ 2.902.902.802.702.702.3011.10 3.70 2.70 $\frac{7.00}{7.00}$ 8.40 9.90 5.20 9.202.902.202.808.50 8.40 9.40 5.00 3.80 3.40 11.902.102.107.90 9.60 3.70 2.903.00 11.30 8.20 4.80 3.90 6.90 8.10 $11.70 \\ 12.20$ 4.70 3.60 2.902.90 9.90 7.80 6.803.602.902.60 $\overline{2}$. $\overline{20}$ 2.90 8.90 6.50 14.45 $7.70 \\ 8.40$ 4.603.60 3.402.609.20 10.90 3.80 2.802.20 2.90 $\frac{8.20}{7.50}$ 6.10 4.50 3.202.802.802.702.705.80 9.80 9.00 9.20 4.503,90 3.10 2.20 3.00 5.90 9.20 7. $\tilde{90}$ 4.30 2.90 $\overline{2}$ 20 6.60 7.803.104.802.102.702.502.402.509.20 30 4.30 3.00 $\tilde{2}$ 20 3.30 6.20 5.606.80 4.90 $7.30 \\ 7.70$ 5.90 12.10 6.30 4.80 2.60 $\mathbf{2}$. 20 3.50 6.10 4.803.002.60 2.60 2.60 2.50 2.50 5.60 13.65 $5.70 \\ 5.70$ 8.10 $\frac{1}{4}, \frac{70}{70}$ 4.30 3.00 2 20 3.50 a10.30 2.305.50 11.80 7. 80 4.003.00 3.40 9.80 $\frac{2.40}{2.30}$ 9.20 9.00 7.60 4.90 3.80 2.90 2.40 3.30 9.20 5.50 5.20 7.70 8.10 10.035.00 3,60 2.90 2.40 3.20 8.70 2.402.502.502.502.202.202.202.80 5.10 8.90 8.30 12.45 5.103.50 2.50 3.20 9. 20 12.40 5.80 10.70 8.50 3.40 3.102. 70 3.10 9.60 5.602.102.20 $\frac{2.60}{2.60}$ 14.65 9.80 10.85 11.10 5.20 3,30 3.203.10 9 40 3.20 2.5016.85 11.409.70 10.00 5.00 3.10 $\bar{3}.20$ 9.10 $\frac{2.20}{2.20}$ 13.50 16.109.20 9.50 4.80 3.50 3.00 2.803.002. 70 3.60 10.30 2.9014.75 8.40 3.30 11.304.602.904.00 $\frac{2}{2}, \frac{20}{20}$ 2.802.808.50 11.00 9.90 10.70 3.30 2,90 2.904.304.507.80 4.30 8.80 8.70 9.50 3.20 4.00 2.60 4.70 70 70 70 70 8.10 2.2. 16.7520.757.008.40 3.203.70 2.702.307.904.106.208.50 $\begin{array}{c} 7.10 \\ 7.00 \end{array}$ 7.50 3.10 3.40 2.802.20 4.002.80 $\tilde{2}$. 9.20 6.90 3.20 2.20 14.65 3,90 3.1011.40 9.00 6,80 6.50 3.30 3.10 2.302 11.80 30 3.80 3.108.70 6.50 3.70 3.30 3.10 2.60 11.40.

Daily gage height, in feet, of North Branch of Susquehanna River at Wilkesbarre, Pennsylvania, for 1900.

a Ice backed water at gage.

PENNSYLVANIA.

NORTH BRANCH OF SUSQUEHANNA RIVER AT DANVILLE, PENNSYLVANIA.

This station, which was established March 25, 1899, by E. G. Paul, is described in Water-Supply Paper No. 35, page 77. The results of measurements for 1899 will be found in the Twenty-first Annual Report, Part IV, page 89. A bench mark was established, being the extreme south end of the stone doorsill at the east entrance of the city filtering plant, at 31.7 feet above datum of the gage. During 1900 two measurements were made by Mr. Paul, as follows:

May 20: Gage height, 4.60 feet; discharge, 10,515 second-feet. September 25: Gage height, 1.60 foot; discharge, 822 second-feet.

Daily gage height, in feet, of North Branch of Susquehanna River at Danville, Pennsylvania, for 1900.

-													
	Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
-12345678900112344567890011234456789001123222222222222222222222222222222222	Day.	Jan. (a) (a) (a) (a) (a) (a) (a) (a)	(a) (a) (a) (a) (a) (a) (a) (a) (a) (a)	Mar. 7,555 15,25 13,10 10,65 9,25 7,10 7,30 6,85 6,75 7,50 6,40 5,65 5,20 4,90 4,90 4,90 4,90 5,05 5,10 7,95 5,10 7,95 5,10 7,95 5,20 4,90 7,90 7,95 5,20 1,0,65 5,20 1,0,65 5,20 1,0,65 5,20 1,0,65 5,20 1,0,65 5,20 1,0,65 5,20 1,0,65 5,20 1,0,65 5,20 1,0,65 5,20 1,0,65 5,20 1,0,65 5,20 1,0,05 5,20 1,00 5,50 5,20 1,00 5,50 5,20 1,00 5,50 5,20 1,00 5,50 5,20 1,00 7,20 1,00 5,55 5,20 1,00 7,20 1,00 7,20 1,00 5,55 5,20 1,00 7,20 1,00 1,00 1,00 1,00 1,00 1,00 1,00 1	$\begin{array}{c} {\rm Apr.} \\ \hline \\ 5.60 \\ 5.80 \\ 6.75 \\ 8.40 \\ 9.30 \\ 8.45 \\ 7.40 \\ 8.75 \\ 9.45 \\ 8.25 \\ 7.10 \\ 6.30 \\ 6.30 \\ 6.30 \\ 6.65 \\ 7.00 \\ 6.30 \\ 6.35 \\ 7.05 \\ 8.95 \\ 8.95 \\ 8.95 \\ 8.10 \\ 8.95 \\ 8.40 \\ 8.40 \end{array}$	$\begin{array}{c} {\rm May.} \\ \hline \\ 5.35 \\ 5.05 \\ 4.80 \\ 4.55 \\ 4.40 \\ 4.25 \\ 4.05 \\ 4.00 \\ 4.00 \\ 4.00 \\ 4.00 \\ 4.00 \\ 4.00 \\ 4.00 \\ 4.00 \\ 4.40 \\ 4.40 \\ 4.40 \\ 3.90 \\ 3.90 \\ 3.60 \\ 3$	June. 3.00 2.90 3.50 3.50 3.30 3.10 3.00 2.90 2.90 3.10 3.30 3.90 3.90 3.90 3.90 3.90 3.90 3.90 2.90 2.90 2.90 2.90 3.10 3.00 2.90 2.00 2.90 2.90 2.90 2.00 2.90 2.00 2.90 2.00 2.90 2.00 2.90 2.00 2.90 2.00 2.90 2.00 2.90 2.00 2.90 2.00 2.90 2.00 2.90 2.00 2.90 2.00 2.90 2.00 2.90 2.00 2.90 2.000 2.00	July. 2.30 2.30 2.30 2.20 2.30 2.90 2.90 2.90 2.50 2.50 2.50 2.30	Aug. 2.40 2.30 2.20 2.20 2.20 2.20 2.20 2.20 2.2	Sept. 2.20 2.20 2.20 2.20 2.20 2.10 2.00 1.80 1.80 1.80 1.80 1.80 1.80 1.80 1	Oct. 1.70 1.80 1.80 1.80 1.80 1.80 1.80 1.80 1.80 1.80 1.90 1.90 1.80 1.80 1.80 1.90 1.90 1.80 1.80 1.80 1.90 1.90 1.80 1.90 1.80 1.90 1.90 1.80 1.90 1.90 1.80 1.90	Nov. 2.00 2.50	Dec. 8. 75 7. 5. 90 5. 500 7. 10 8. 85 8. 85 5. 7. 55 5. 6. 85 5. 6. 80 6. 80 (a) (a) (a) (a) (a) (a) (a) (c) (5. 10 (c) (c) (c) (c) (c) (c) (c) (c) (c) (c)
26 27 28 29 30 31		$\begin{array}{c} 6.80 \\ 6.45 \\ 6.30 \\ 5.80 \\ 5.80 \\ (\alpha) \end{array}$	8.95 6.85 5.45	$\begin{array}{c} 7.65 \\ 6.95 \\ 6.50 \\ 5.85 \\ 5.90 \\ 5.65 \end{array}$	$\begin{array}{c} 8.40 \\ 7.40 \\ 6.65 \\ 6.10 \\ 5.65 \end{array}$	$\begin{array}{c} 3.60 \\ 3.40 \\ 3.20 \\ 3.20 \\ 3.10 \\ 3.00 \end{array}$	$\begin{array}{c} 2.60 \\ 2.50 \\ 2.50 \\ 2.40 \\ 2.40 \\ 2.40 \end{array}$	$\begin{array}{c} 2.30 \\ 3.00 \\ 2.80 \\ 2.60 \\ 2.40 \\ 2.40 \end{array}$	$\begin{array}{c} 2.10 \\ 2.20 \\ 2.10 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \end{array}$	$\begin{array}{c} 1.70 \\ 1.70 \\ 1.70 \\ 1.70 \\ 1.70 \\ 1.70 \\ 1.70 \\ \end{array}$	$\begin{array}{c} 2.20 \\ 2.10 \\ 2.10 \\ 2.10 \\ 2.00 \\ 2.00 \end{array}$	3.90 8.45 16.60 12.65 10.20	7.05 8.60 7.55 6.95 6.55 6.30
-													

a River frozen.

WEST BRANCH OF SUSQUEHANNA RIVER AT ALLENWOOD, PENN-SYLVANIA.

This station, which was established by E. G. Paul March 23, 1899, is described in Water-Supply Paper No. 35, page 78. The results of measurements for 1899 will be found in the Twenty-first Annual Report, Part IV, page 90. A bench mark was established on September 24, 1900. It consists of a copper bolt set in the capstone of the wing wall on the lower side of the west end of the bridge, and is 33.19 feet above datum of the gage. During 1900 two measurements of discharge were made by Mr. Paul, as follows:

May 19: Gage height, 3.2 feet: discharge, 4,812 second-feet. September 24: Gage height, 1.8 feet: discharge, 511 second-feet.

				1			(_		
Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
									-			
1	4.50	3.20	7.55	5.00	4.30	3.90	2.10	1.90	2.00	1.30	2.10	5.75
2	5.50	3.20	9.60	5.30	4.20	3,90	2.30	1.80	1.90	1.30	2.10	5.40
3	5.70	3.40	7.70	5.40	4.20	3.90	2.60	1.80	1.90	1.20	2.10	-5.00
4	5.80	3.40	7.00	5.80	4.00	4.00	2.50	1.80	1.80	1.20	2.10	5.80
5	5.90	3.50	6.00	5.90	3.80	4.10	2.30	1.70	1.80	1.20	2.10	5.90
6	5.90	3.60	5.40	6.20	3.50	3.90	2.30	1.70	1.70	1.20	2.00	6.40
T	5.90	3.80	5.80	6.40	3.30	3.60	2.20	1.70	1.70	1.20	1.90	6.70
8	4.70	4.50	5.90	6.20	3.39	3.50	2.20	1.60	1.70	1.20	1.90	6.00
9	3.70	5.00	6.10	7.30	3.20	3.40	2.20	1.60	1.60	1.80	1.90	5.50
10	3.90	5.30	6.40	6.00	3.20	3.30	2.30	1.50	1.60	2.20	1.90	4.90
10	4.20	5.60	6,90	5.70	3.20	3.20	2.50	1.40	1.60	2.20	1.90	4.60
12	4.50	5.30	6.20	5.30	3.20	3.00	2.70	1.50	1.50	2.10	1.90	4.20
10	4.40	0.00	5.40	4.90	3, 30	3.00	2.90	1.00	1.50	2.10	1.90	4.00
14	4.20	7.40	0.00	4.80	3.40 9.40	3.00	2.80	1.40	1.40	2.10	1.90	3.80
10	4.00	4.50	4.00	4.00	0, 40 9 90	9,00	9.00	1.40	1.40	2.10 9.10	1.90	0,00
17	4.00	6.20	3.00	4.00	3.00	9.00	2.00	1.40	1.40	2.10	1.00	9.90
19	4.90	5 40	3.80	6 00	2 20	2.80	2.00	1.40	1.00	9.90	1.00	2.90
19	4 50	5.60	3.70	7 00	3.50	2.70	2 20	1.40	1.30	2 10	1 70	3 10
90	5.30	5.00	6.20	6 90	3.50	2 70	2 00	1.40	1.00	2 00	1 70	3 10
21	13 20	6.00	7 10	6.30	3.30	2.60	2.00	1.40	1.30	1 90	1 70	3 10
99	12.20	8.20	6.90	6 20	3 20	2 50	1 90	2 30	1.30	1.00	1 90	3 00
23	8.50	10.15	6.60	6.00	3.00	2 40	1.90	2.30	1.30	2 10	2.40	3.00
24	6.50	7.85	6.10	6.30	3.00	2.40	1.90	2.30	1.30	2.20	3.00	3.00
25	6.30	6.50	5.90	6.00	3.00	2.30	1.90	2.30	1.30	2.40	5.00	3.00
26	6.10	5.00	5.50	5.60	3.00	2.30	1.90	2.30	1.30	2.50	7.70	3.00
27	5.30	5.00	5.20	5.30	3.40	2.30	2.20	2.20	1.30	2.60	15.75	3.00
28	4.60	4.80	5.10	4.80	3.20	2.20	2.20	2.20	1.30	2.40	10.05	3.00
29	4.60		5.00	4.60	3.00	2.20	2.20	2.10	1.30	2.40	8.25	3.00
30	4.50		4.90	4.40	3.00	2.10	2.20	2.10	1.30	2.30	6.60	3.00
31	-3.20		4.80		3.20		2.00	2.00		2.20		

Daily gage height, in feet, of West Branch of Susquehanna River at Allenwood, Pennsylvania, for 1900.

JUNIATA RIVER AT NEWPORT, PENNSYLVANIA.

This station, which was established March 21, 1899, by E. G. Paul, is described in Water-Supply Paper No. 35, page 79. The results of measurements for 1899 will be found in the Twenty-first Annual Report, Part IV, page 91. The bench mark is the extreme east end of the stone doorsill of the south entrance of Butz's store, on the right bank, and is 28.83 feet above datum of the gage. During 1900 two measurements of discharge we're made by Mr. Paul, as follows:

May 17: Gage height, 3.40 feet; discharge, 1,778 second-feet. September 23: Gage height, 2.80 feet; discharge, 418 second-feet. Daily gage height, in feet, of Juniata River at Newport, Pennsylvania, for 1900.

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Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1	i 10	3 70	5.90	4.50	4 10	3 30	3 30	3.00	3 30	2.80	3.00	1 40
2	4 10	3.40	12.90	4.50	4,10	3.30	3.20	3.00	3.20	2.90	3.00	4.10
3	4.60	3.40	8.00	4.50	4.00	3.40	3.10	3,00	3.20	3,00	3.00	3.90
4	5.00	3.50	6.00	4.40	3.90	3.70	3.10	3.00	3.10	3.00	3.00	3.90
5	5.00	3.80	5.50	4.50	3.80	3.60	3.10	3.00	2.90	2.90	2.90	5.50
6	4.70	4.40	5.40	4.60	3.70	3.40	3.10	3.00	-2.90	2.90	2.90	-7.00
7	. 5.20	4.10	6.00	4.50	3.70	3.40	-3.10	2.90	2.90	2.90	3.00	6.30
8	4.00	4.20	6.40	4.40	3.70	3:30	3.10	2.90	2.80	2.90	3.00	5.20
9	. 4.20	5.10	5.60	4.40	3.60	3.40	3.10	2.90	2.80	2.90	3.00	4.60
10	4.10	5.60	5.40	4.40	3.60	3.50	3.10	2.80	2.80	2.90	3.00	4.50
11	4.10	4.80	5.10	4.40	3.50	3.40	3.10	2.80	2.80	2.90	2.90	4.30
	4.80	4.60	5.10	4.30	3.50	3.30	3.10	2.80	2.80	3.00	2.90	1.20
13	4.60	5.40	4.90	4.30	3. 00	3.30	3.10	2.80	2.80	3.00	2.90	4.00
14	4.20	9.40	4.80	4.00	0.00 2.50	$\frac{0.00}{2.20}$	0.00	2.80	2.80	3.00	2.90	3.80
10	. 5.90	5 00	4.40	4.00	0.00	2 20	3.00	2.00	2 80	2.00	2.00	0.10
10	4 10	5 20	4.10	4.10	3.40	3 20	3.00	2 80	2.80	3.00	3.00	3.60
18	3.80	4 90	4.10	4.00	3 40	3.30	3.00	2.80	2.80	3.00	3.00	3.30
19	4 20	4 10	4 10	4 40	3 50	3 30	2.90	2.80	2.80	3.00	3.00	3.50
20	4.90	4.20	4.40	4.70	3.70	3.30	2.90	2.80	2.80	3.00	3.00	3.70
21	10.60	4.40	6.50	4.50	4.00	3.30	2.90	2.80	2.80	3.00	3.00	3.80
).)	10.20	11.70	6.50	4.50	3.70	3.30	2.90	2.80	2.80	3.00	3.00	3.80
23	7.20	11.10	5.70	4.50	3.70	3.30	2.90	2.80	2.80	2.90	3.10	3.60
24	6,00	8.20	5.70	4.70	3.60	3.30	3.20	2.80	2.80	3.70	3.10	3.40
25	5.20	5.90	5.60	4.70	3.50	3.20	3.10	3.30	2.80	-3.40	-4.00	3.80
26	5.00	4.50	5.40	4.70	3.50	3.20	3.10	3,30	2.80	3.30	6.30	3.50
27	4.80	4.40	5.10	4.40	3.20	3.60	3.10	3.70	2.80	3.30	11.60	3.30
28	4.40	4.60	5.00	4.30	3.30	3.40	3.10	3.40	2.80	3.20	8.00	3.20
39	4.40		4.80	4.20	3.30	3.30	3.00	3.30	2.80	3.20	5.70	3.20
30	. 4.20		4.60	4.20	3.30	3.30	3.00	3.70	2.80	3.10	4.80	3.20
51	4.10		4.50		3.30		3,00	3,60		3.00		3.20
	1				1							

SUSQUEHANNA RIVER AT HARRISBURG, PENNSYLVANIA.

Gage-height observations were established at this station by E. Mather, president of the Harrisburg water board, in 1890. Discharge measurements were first made by E. G. Paul on March 31, 1897, from the Walnut street bridge. The station is described in Water-Supply Paper No. 35, page 80. The datum of this gage is the low-water mark of 1803, which is recorded on a large rock above the bridge. During 1900 three measurements were made by Mr. Paul, as follows:

May 16: Gage height, 2.42 feet; discharge, 17,621 second-feet. September 21: Gage height, 0.08 foot; discharge, 2,655 second-feet. September 28: Gage height, -0.04 foot; discharge, 2,357 second-feet. Daily gage height, in feet, of Susquehanna River at Harrisburg, Pennsylvania, for 1900.

-												
Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1	$\begin{array}{c} 1.83\\ 1.66\\ 4.50\\ 4.91\\ 4.83\\ 5.25\\ 5.50\\ 5.33\\ 4.91\\ 4.58\\ 4.50\\ 5.591\\ 4.51\\ 4.52\\ 5.25\end{array}$	$\begin{array}{c} 2.91\\ 1.83\\ 3.91\\ 4.00\\ 4.66\\ 4.33\\ 5.50\\ 5.00\\ 4.00\\ 4.83\\ 5.75\\ 5.56\\ 5.66\\ 5.66\\ 5.66\\ 5.66\end{array}$	$\begin{array}{c} 4.00\\ 13.12\\ 12.33\\ 9.50\\ 7.91\\ 6.91\\ 6.06\\ 6.50\\ 5.83\\ 5.66\\ 6.25\\ 5.75\\ 5.75\\ 4.66\end{array}$	$\begin{array}{c} 4.16\\ 4.00\\ 4.16\\ 4.41\\ 5.33\\ 6.00\\ 5.41\\ 5.08\\ 6.16\\ 6.75\\ 6.50\\ 5.58\\ 5.00\\ 4.50\end{array}$	$\begin{array}{c} 4.00\\ 3.75\\ 3.550\\ 3.33\\ 3.08\\ 2.83\\ 2.83\\ 2.550\\ 2.550\\ 2.550\\ 2.42\\ 2.33\\ 2.42\\ 2.42\\ 2.42\\ 2.42\\ \end{array}$	$\begin{array}{c} 2.58\\ 2.50\\ 2.33\\ 2.17\\ 2.50\\ 2.67\\ 2.50\\ 2.17\\ 2.17\\ 2.08\\ 2.00\\ 2.00\\ 1.92\\ 1.92\end{array}$	$\begin{array}{c} 1.17\\ 1.08\\ 1.00\\ 1.08\\ 1.33\\ 1.17\\ 1.33\\ 1.17\\ 1.42\\ 1.42\\ 1.33\\ 1.17\\ 1.42\\ 1.08\\ 1.08\end{array}$	$\begin{array}{c} 1.25\\ 1.00\\ 1.00\\ .92\\ .75\\ .67\\ .67\\ .50\\ .58\\ .50\\ .33\\ .33\\ .25\\ \end{array}$	$\begin{array}{c} 1.00\\ 1.00\\ .83\\ 1.17\\ .92\\ .58\\ .58\\ .58\\ .58\\ .58\\ .58\\ .58\\ .50\\ .42\\ .33\\ .17\\ .25\end{array}$	$\begin{array}{c} 0.04\\ .04\\ .04\\ .04\\ .04\\ .04\\ .04\\ .04$	$\begin{array}{c} 0.83\\ .835\\ .755\\ .666\\ .666\\ .666\\ .558\\ .58\\ .58\\ .75\end{array}$	$\begin{array}{c} 7.00\\ 5.83\\ 5.25\\ 4.500\\ 7.25\\ 7.41\\ 7.08\\ 6.00\\ 5.25\\ 4.08\\ 3.60\end{array}$
14 15 16 17 17 18 20 21 22 23 24 25 25 26 27	$\begin{array}{c} 5.25\\ 5.25\\ 5.25\\ 4.66\\ 5.00\\ 4.83\\ 4.00\\ 4.25\\ 10.66\\ 12.00\\ 9.16\\ 7.25\\ 6.08\\ 5.00\end{array}$	$\begin{array}{c} 7.66\\ 8.00\\ 8.25\\ 7.41\\ 6.00\\ 4.75\\ 3.91\\ 2.16\\ 3.58\\ 9.50\\ 11.16\\ 9.75\\ 6.83\\ 5.50\end{array}$	$\begin{array}{c} 4.66\\ 4.50\\ 4.00\\ 3.66\\ 3.16\\ 3.00\\ 3.00\\ 3.91\\ 6.87\\ 6.83\\ 6.00\\ 5.75\\ 5.83\\ 5.00\\ 5.75\\ 5.83\\ 5.00\\ 5.75\\ 5.83\\ 5.00\\ 5.83\\ 5.83\\ 5.00\\ 5.83\\ 5.00\\ 5.83\\ 5.00\\ 5.83\\ 5.00\\ 5.83\\ 5.00\\ 5.83\\ 5.00\\ 5.83\\ 5.00\\ 5.83\\ 5.00\\ 5.83\\ 5.00\\ 5.83\\ 5.00\\ 5.83\\ 5.00\\ 5.83\\ 5.00\\ 5.83\\ 5.00\\ 5.83\\ 5.00\\ 5.83\\ 5.00\\ 5.83\\ 5.00\\ 5.83\\ 5.00\\ 5.83\\ 5.00\\ 5.00\\ 5.83\\ 5.00\\$	$\begin{array}{c} 4.50 \\ 4.33 \\ 4.50 \\ 4.41 \\ 4.33 \\ 5.08 \\ 7.08 \\ 7.08 \\ 7.33 \\ 6.83 \\ 6.08 \\ 5.83 \\ 6.00 \\ 6.25 \end{array}$	$\begin{array}{c} 2.42\\ 2.50\\ 2.40\\ 2.33\\ 2.55\\ 2.92\\ 2.59\\ 2.17\\ 2.83\\ 2.58\\ 2.42\\ 2.55\\$	$\begin{array}{c} 1.92\\ 2.00\\ 2.17\\ 2.17\\ 2.00\\ 1.83\\ 1.83\\ 1.83\\ 1.75\\ 1.75\\ 1.58\\ 1.42\\ 1.33\\ 1.32\end{array}$	$\begin{array}{c} 1.08\\ 1.00\\ 1.00\\ 1.00\\ 1.08\\ .92\\ .92\\ .92\\ .83\\ .75\\ .75\\ .75\\ .75\\ .75\\ .83\\ .83\\ .85\\ .83\\ .85\\ .83\\ .85\\ .83\\ .85\\ .83\\ .85\\ .83\\ .85\\ .83\\ .85\\ .85\\ .85\\ .85\\ .85\\ .85\\ .85\\ .85$	$\begin{array}{r} .25\\ .17\\ .17\\ .25\\ .17\\ .17\\ .17\\ .17\\ .33\\ .30\\ .50\\ 1.25\\ 1.00\\ 1.17\end{array}$	25 25 25 25 25 25 25 25 25 25 25 25 25 2	$\begin{array}{c} .83\\ .83\\ .75\\ .58\\ .66\\ .66\\ .58\\ .50\\ .50\\ .50\\ .50\\ 1.00\\ 1.08\end{array}$	$\begin{array}{c} .75\\ .66\\ .83\\ .91\\ .75\\ .91\\ .91\\ .91\\ .83\\ 1.00\\ 1.08\\ 1.66\\ .61\end{array}$	$\begin{array}{c} 3.60\\ 2.91\\ 2.85\\ 2.25\\ 2.08\\ 2.08\\ 2.08\\ 2.08\\ 2.08\\ 2.16\\ 2.16\\ 2.33\\ 2.41\\ 2.33\\ 2.41\\ 2.41\\ 2.33\\ 2.41\\ 3.33\\ 2.41\\ 3.33\\ 3.41\\ 3.33\\ 3.41\\ 3.33\\ 3.41\\ 3.33\\ 3.41\\ 3.33\\ 3.41\\ 3.33\\ 3.41\\ 3.33\\ 3.41\\$
24 28 29 30 31	$\begin{array}{c} 5.00 \\ 4.50 \\ 4.08 \\ 3.33 \\ 2.50 \end{array}$	5.50 4.50	$5.20 \\ 5.25 \\ 4.83 \\ 4.50 \\ 4.41 $	$ \begin{array}{r} 5.75 \\ 5.08 \\ 4.58 \\ 4.17 \\ \end{array} $	$\begin{array}{c} 2.14 \\ 2.00 \\ 2.00 \\ 2.00 \\ 1.92 \end{array}$	1.33 1.33 1.33 1.17	$ \begin{array}{r} 1.50 \\ 1.25 \\ 1.25 \\ 1.42 \\ 1.25 \\ 1.42 \end{array} $	$ \begin{array}{r} 1.1, \\ 1.50 \\ 1.33 \\ 1.00 \\ 1.08 \end{array} $	-0.04 -0.04 +0.04	$1.00 \\ 1.25 \\ 1.16 \\ 1.00 \\ .91$	$5.91 \\ 13.04 \\ 12.33 \\ 8.91$	2.00 2.66 2.91 2.58 2.50

MISCELLANEOUS DISCHARGE MEASUREMENTS IN PENNSYLVANIA.

During the year 1900 the following measurements of the Pennsylvania Canal and of Lehigh River were made by E. G. Paul:

Miscellaneous discharge measurements in Pennsylvania during 1900.

Date.	Stream.	Locality.	Discharge.
1900. May 16 September 21 May 18 September 23 May 18 September 23	Pennsylvania Canal do do do do do do	Harrisburg do Steelton Highspire do	Secfeet. 376 369 360 193 161 152 150
September 26 September 27	do Lehigh River	Nanticoke Easton, Glendon Bridge.	328 303

PATAPSCO RIVER AT WOODSTOCK, MARYLAND.

This station, which was established August 6, 1896, by E. G. Paul, is located at the county bridge on the road from Woodstock to Granite, Maryland, $1\frac{1}{2}$ miles below the junction of the North Branch. It is described in Water-Supply Paper No. 35, page 83, where will also be found the gage heights for 1899. The discharge measurements for 1899 were published in the Twenty-first Annual Report, Part IV, page 94. During 1900 the following measurements were made by Mr. Paul:

June 29: Gage height, 3.6 feet; discharge, 165 second-feet. September 29: Gage height, 3.6 feet; discharge, 152 second-feet.

Daily gage height, in feet, of Patapsco River at Woodstock, Maryland, for 1900.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.a
1	3.90	3. 85	6.50	4.00	3.90	3.60	3.60	3.25	5.30	3.55	3.45
2	3.90	3.75	4.90	4.15	3.90	3.55	3,65	3.30	5.30	3.55	3.45
ð	0.90	9.40	4.00	4.10	2.05	0.00	0.00 9.45	2.15	$ 5.40 \\ 5.20 $	0.00	0.00
¥	3.90	4 40	4 25	$\frac{1}{4}$ 10	4 00	3 75	3 55	3 15	4 85	3 35	3.50
6	3.85	3 90	4 40	4 15	4 00	3 65	4.00	3 10	5 20	· 3 35	3 50
7	0.00	3.85	4.40	4.15	4.05	3.65	3.85	3.00	5.20	3.30	3.45
8	4.05	4.10	4.40	4.10	3, 90	3.75	3, 55	3.00	5.25	3.35	3.50
9	3.85	4.25	4.25	4.15	4.10	3.85	3.55	3.00	5.25	3.55	3.45
10	3.85	4.05	4.30	4.15	3.95	3.30	3.55	3.05	5.25	3.55	3.45
11	3.85	4.05	4.20	4.35	4.00	3.65	3.45	3.05	5.25	3.55	3.45
12	5.25	4.10	4.25	4.35	3.90	3.55	3.35	3.00	5.35	3.55	3.85
13	3.95	7.65	4.20	4.35	4.00	3.60	3.35	3.05	5.35	3.35	3.55
14	3.85	5.15	4.25	4.20	3.80	3.60	3.25	3.00	5.40	3.30	3.40
15	3.80	4.30	4.25	4.10	3.90	4.00	3.15	3.00	5. 55	3.15	3.45
16	0.80 9.07	4.15	4.30	4.10	4.00	(D)	3.05	3.00	5.30	3.00	5.40
10	0.90	9.05	4 10	4.20	2.00	(0)	0.00 9.05	9.10 9.00	0,40 5 10	0,00	0.40
10	3.00	2.05	4.10	4.10	5.90 4 30	$\begin{pmatrix} 0 \\ b \end{pmatrix}$	2.05	2 10	5.10	2 95	9.40
20	4 50	3 95	4 20	4 15	4 20	(h)	3.05	5 20	5.05	3 40	3 45
21	5.60	4.00	6 60	4.25	4.10	(b)	3.00	6 10	5.05	5.30	3.45
22	4.15	8.70	4.90	4.10	3.75	(\tilde{b})	3.50	5.95	5.05	3.45	3.50
23	4.05	4.95	4.35	4.15	3.75	(b)	3.20	5.75	5.05	3.45	3.40
24	4.05	4.55	4.35	4.20	3.70	(<i>b</i>)	3.55	5.65	5.15	3.45	3.50
25	4.00	3.90	4.30	4.05	3.75	(b)	7.15	5.55	5.00	3.50	3.30
26	3.90	4.30	4.10	-4.00	3.80	(b)	6.35	5.40	5.10	3.45	3.40
27	3.85	4.15	4.30	3.90	3.90	(b)	5.75	5.40	5.05	3.50	3.40
28	3.85	4.35	4.20	3,90	3.80	(b)	4.50	5.70	4.95	3.45	3.35
29	3.85		4.20	3.80	3.80	(b)	4.50	5.40	4.20	3 45	3.45
30	3.85		4.40	4.00	0.00 9.95	(0)	4.45	5.45	3.50	3.45	3.40
31	5.85		4.20		5.55		5.05	0.40		3.40	

 α No record for December.

b June 16 to 30, no readings; gage broken.

NORTH BRANCH OF POTOMAC RIVER AT PIEDMONT, WEST VIRGINIA.

This station, which was established January 27, 1899, by E. G. Paul, is located at the highway bridge connecting Luke, Maryland, with Piedmont, West Virginia. It is described in Water-Supply Paper No. 35, page 84, where will be found gage heights and discharge measurements for 1899. During 1900 the following measurements were made by Mr. Paul:

February 22: Gage height, 3.75 feet; discharge, 735 second-feet. June 20: Gage height, 4.40 feet; discharge, 1,249 second-feet. September 12: Gage height, 1.8 feet; discharge, 34 second-feet.

Daily gage .	height,	in feet,	of	North	Branch	of	Potomac	River	at	Piedmont,	West
				Vir	ginia, fo	r 1	900.				

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1	2.70	3.00	3.55	4.60	3.15	3.30	3.00	2.95	2.10	2.85	2.10	3. 55
3	$\frac{2.70}{2.70}$	3.05 3.10	4.50	$\frac{4.80}{4.65}$	3.10 3.10	$\frac{3.25}{3.25}$	2.85 2.70	$\frac{2.75}{2.65}$	2.00 2.00	2.45 2.20	$2.10 \\ 2.25$	3.45 3.25
4	2.70	3.10	4.00	4.50	3.10	3.05	2.70	2.60	2.00	2.10	2.65	5.80
6	2.80	ə.əə 3.60	4.25	4.25	2.95	2.85	2.70 2.60	2.40 2.30	1.95	$2.20 \\ 2.20$	$\frac{2.10}{2.50}$	0.00 4.70
7	2.90 3.00	$\frac{3.70}{5.30}$	5.80 5.00	4.15	2.90	2.85 3.15	2.70	2.30	1.90	2.20 2.10	2.40	4.2
9	3.30	5.40	4.55	4.20	2.95	3.15	2.85	2.20	1.90	2.05	2.40	3.80
0	3.50 3.50	$\frac{4.65}{4.40}$	4.40	$\frac{3.95}{3.75}$	3.20 3.05	2.95	2.70 2.60	2.10 2.05	1.90 1.80	2.00 2.00	2.50 2.50	3.60
2	4.70	4.05	4.15	3.70	3.00	2.70	2.45	2.00	1.80	2.00	2.60	3.40
3	$\frac{4.25}{3.90}$	5,90 5,50	$\frac{4.10}{4.10}$	$\frac{3.65}{3.55}$	2.90 2.80	2.70 3.15	2.60 2.65	2.10 2.00	$1.80 \\ 1.80$	2.00 3.05	2.60 2.50	3.40
5	3,90	4.80	4.00	3.40	2.80	3.20	2.55	2.00	1.80	3.20	2.50	3.30
7	4.4 0	4.35	a. 80 3. 70	3,40 3,40	2.80	5.95 7.55	2.30	2.10	1.80 1.90	2.05	2.40	3.0
8	4.10 4.15	$\frac{4.05}{2.70}$	3.70	3.55	2.70	5.85	2.25	2.25	1.90	2.40	2.40	3.1
20	5.80	3.65	5.95	3.65	3.95	4.45	2.90	2.45	1.90	2.20	2.50	3.2
21	5.70	3.60 3.75	5.35 4.75	3.50 3.50	3.55 3.35	3.95	2.75	2.20 2.20	1.80 1.80	2.10 2.10	2.60 3.20	3.2
3	4.35	4.00	4.60	3.65	3.20	3.50	2.45	2.65	1.80	2.15	3.00	3.00
25	4.10	3.70 3.60	$\frac{4.60}{4.50}$	3.85 3.65	$\frac{3.15}{3.05}$	3.35 3.25	$\frac{2.40}{3.20}$	$2.45 \\ 2.40$	$1.80 \\ 1.80$	$2.35 \\ 2.80$	$\frac{2.90}{3.35}$	3.0
6	3.80	3.40	4.25	3.50	3.00	3.25	4.05	2.45	1.80	2.50	7.95	3.0
8	a. 55 3. 40	5.40 3.40	$\frac{4.35}{4.15}$	3.40 3.40	2.99	5.05 2.90	4.40 3.20	2.30	1.80	2.30	5.20 4.45	2.90
29	3.30		$\frac{4.00}{4.75}$	3,30	3.30 3.25	$\frac{3.55}{3.15}$	3,00	2.20 2.15	1.95 2.70	2.20 2.20	4.05	3.4
31	3.10		4.60		3.10		3.25	2.10		2.20		3.30

SOUTH BRANCH OF POTOMAC RIVER NEAR SPRINGFIELD, WEST VIRGINIA.

The station on the South Branch at Springfield was originally (April, 1894) established at the railroad bridge 2 miles south of that town, by C. C. Babb, but was discontinued in 1896. The present station, which was established by E. G. Paul, January 26, 1899, is located on the iron highway bridge one-fourth of a mile from Grace Station and 1 mile from Springfield. It is described in Water-Supply Paper No. 35, page 85, where will also be found the gage heights and discharge measurement for 1899. During 1900 the following measurements were made by Mr. Paul:

February 23: Gage height, 7.7 feet; discharge, 3,808 second-feet. June 20: Gage height, 7 feet; discharge, 3,435 second-feet. September 11: Gage height, 4 feet; discharge, 144 second-feet.

WEST VIRGINIA AND MARYLAND.

Daily gage height, in feet, of South Branch of Potomac River near Springfield, West Virginia, for 1900.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1 2 3 4 5 6 7 8 10 11 12 13 14 15 16 17 18 20 21 22 23 24 25 26 27 28 29 30 31	$ \begin{array}{c} (a) \\ (a) $	$ \begin{array}{c} (a) \\ (a) $	$\begin{array}{c} 9.848842084048274086084827796644827796654408577668482776684827766848277668482776684827666677766666777666666777666666777666666$	$\begin{array}{c} \textbf{7.7.6555220086220085442246085206220174}\\ \textbf{4.4.443333445668200744}\\ \textbf{4.4.43333445668200744}\\ \textbf{4.4.433334456685555444}\\ \textbf{4.4.43333445668665555444}\\ \textbf{4.4.433334456666665555444}\\ \textbf{4.4.4333344566666665555444}\\ \textbf{4.4.4333344566666665555444}\\ \textbf{4.4.4333344566666665555444}\\ 4.4.433334456666666666666666666666666666$	$\begin{array}{c} 4.4322411\\ 4.4322411\\ 4.40009888766655075544211\\ 4.4000988333334556\\ 6.5075544211\\ 4.4560\\ 3.33333333\\ 4.5560\\ 4.5075544221\\ 4.533333333\\ 4.5560\\ 4.5050\\ 4.500$	$\begin{array}{c} 4.08\\ 4.4\\ 4.42\\ 4.42\\ 4.42\\ 4.42\\ 4.40\\ 0.9\\ 3.99\\ 9.55\\ 5.6\\ 4.9\\ 9.55\\ 5.6\\ 4.99\\ 4.5\\ 5.5\\ 5.6\\ 4.99\\ 5.5\\ 5.6\\ 4.99\\ 5.5\\ 5.6\\ 4.99\\ 5.5\\ 5.6\\ 5.5\\ 5.6\\ 4.99\\ 5.5\\ 5.6\\ 5.5\\ 5.6\\ 5.5\\ 5.5\\ 5.5\\ 5.5$	$\begin{array}{c} 5.0\\ 5.022\\ 5.522\\ 0.555\\ 5.55\\ 5.5\\ 5.5\\ 5.5\\ 5.5\\ 5.5\\ $	$\begin{array}{c} 3.64 \\ 3.44 \\ 3.34 \\ 4.33222 \\ 1.3333 \\ 3.320 \\ 0.00 \\ 3.300 \\ 0.99 \\ 9.99 \\ 9.822 \\ 4.4 \\ 4.20 \\ 0.833 \\ 3.4 \\ 4.40 \\ 8.6 \\ 5.5 \\ \end{array}$	$\begin{array}{c} 3.5 \\ 4.3 \\ 4.4 \\ 3.3 \\ 3.3 \\ 3.3 \\ 3.1 \\ 8.4 \\ 4.0 \\ 6.3 \\ 3.0 \\ 9.9 \\ 9.2 \\ 9.8 \\ 8.0 \\ 0.0 \\ 3.0 \\ 0 \\ 3.0 \\ 0 \\ 3.0 \\ 0 \\ 3.0 \\ 0 \\ 3.0 \\ 0 \\ 3.0 \\ 0 \\ 3.0 \\ 0 \\ 3.0 \\ 0 \\ 3.0 \\ 0 \\ 3.0 \\ 0 \\ 3.0 \\ 0 \\ 3.0 \\ 0 \\ 0 \\ 3.0 \\ 0 \\ 0 \\ 3.0 \\ 0 \\ 0 \\ 3.0 \\ 0 \\ 0 \\ 0 \\ 3.0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\$	0 8 7 5 4 4 6 6 5 5 5 3 2 2 8 7 6 6 6 5 5 5 5 5 5 4 2 2 2 4 5 4 3 3 3 3 8 8 3 8 3 3 3 3 8 8 8 3 3 3 3	$\begin{array}{c} 3.66\\ 3.66\\ 4.0\\ 3.38\\ 3.66\\ 4.0\\ 3.38\\ 3.66\\ 3.52\\ 3.1\\ 1.3\\ 1.1\\ 3.4\\ 4.3\\ 3.8\\ 3.8\\ 3.8\\ 3.8\\ 3.8\\ 3.8\\ 3.8\\ 3$	$\begin{array}{c} 5.2\\ 5.0\\ 5.0\\ 5.0\\ 5.0\\ 12.0\\ 12.0\\ 12.0\\ 12.0\\ 14.5$

a Ice.

ANTIETAM CREEK NEAR SHARPSBURG, MARYLAND.

This station was established at Myers's mill, 1 mile east of Sharpsburg, Maryland, on the road to Keedysville, Maryland, on June 24, 1897, by Arthur P. Davis. It is described in Water-Supply Paper No. 35, page 86, where will be found the gage heights for 1899. Records of discharge measurements for the year 1899 will be found in the Twenty-first Annual Report, Part IV, page 95. During 1900 the following measurements were made by E. G. Paul:

June 28: Gage height, 1.80 feet; discharge, 139 second-feet. September 16: Gage height, 1.75 feet; discharge, 131 second-feet.

IRR 48-01-2

Daily gage height, in feet. of Antietam Creek near Sharpsburg, Maryland, for 1900.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
Day.	Jan. 1.50 1.50 1.50 1.60 1.70 1.70 1.70 1.80 1.80 1.80 1.80 1.70 1.80 1.70 1.80 1.80 1.70 1.80 1.70 1.80 1.70 1.80 1.70 1.80 1.80 1.70 1.80 1.80 1.70 1.80 1.70 1.80 1.70 1.80 1.70 1.80 2.100 1.90	Feb. 1.60 1.50 1.50 1.50 1.50 2.00 2.00 2.00 2.00 2.00 2.70 2.40 2.20 2.20 2.20 2.20 2.40 2.20 2.20 2.40 2.20 2.20 2.30 2.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 5.50	Mar. 3.80 3.60 2.70 2.75 2.50 2.50 2.50 2.50 2.50 2.40 2.40 2.40 2.40 2.40 2.40 2.40 2.40 2.40 2.40 2.40 2.40 2.40 2.40 2.40 2.40 2.40 2.50 2.40 2.40 2.40 2.40 2.40 2.50 2.50 2.50 2.50 2.50 2.50 2.50 2.40 2.50 2.70	Apr. 2 50 2 50 2 50 2 30 2 30	May. 2 10 2 10 2 00 2 10 2 00 1 90 1 90 1 90 1 80 1 90 1 80 2 00 2 10 2 10 2 00 2 10 2 10 2 10 2 00 2 10 2 10	$\begin{array}{c} June.\\ \hline \\ 2.00\\ 1.90\\ 1.90\\ 2.00\\ 1.90\\ 1.90\\ 1.90\\ 1.90\\ 1.90\\ 1.90\\ 1.90\\ 1.90\\ 1.90\\ 1.80\\ 2.00\\ 2.55\\ 2.10\\ 2.55\\ 2.10\\ 2.55\\ 2.10\\ 1.80\\ 2.20\\ 1.80\\ 1.70\\ 1.80\\ $	$\begin{matrix} July.\\ \hline \\ 1,70\\ 1,60\\ 1,50\\ 1,50\\ 1,60\\ 1,60\\ 1,60\\ 1,60\\ 1,60\\ 1,50\\ 1,55\\ 1,50\\ 1,55\\ 1,60\\ 1,50\\ 1,50\\ 1,50\\ 1,50\\ 1,50\\ 1,60\\ 1,50\\ 1,60\\ 1,50\\ 1,60\\ 1,50\\ 1,60\\ 1,50\\ 1,60\\ 1,50\\ 1,60\\ 1,50\\ 1,60\\ 1,50\\ 1,60\\ 1,50\\ 1,60\\ 1,50\\ 1,60\\ 1,50\\ 1,60\\ 1,50\\ 1,60\\ 1,50\\ 1,60\\ 1,50\\ 1,60\\ 1,50\\ 1,60\\ 1,50\\ 1,60\\ 1,50\\ 1,60\\ 1,50\\ 1,6$	Aug. 1.40 1.50 1.50 1.50 1.40 1.40 1.40 1.40 1.50 1.40 1.40 1.50 1.50 1.60 1.60 1.60 1.60 1.60 1.60 1.60 1.60 1.60 1.60 1.60 1.60 1.60 1.60 1.50 1.60 1.60 1.60 1.60 1.60 1.60 1.60 1.60 1.60 1.60 1.80 1.80 1.80 1.80 1.80 1.80 1.80 1.80 1.80 1.80 1.80 1.80 1.80 1.80 1.80 1.70 1.80 1.80 1.70 1.80 1.70 1.80 1.80 1.70 1.80	Sept. 1.60 1.60 1.60 1.70 1.60 1.50 1.50 1.40 1.40 1.40 1.40 1.60 1.60 1.60 1.50 1.50 1.50 1.60 1.50 1.40 1.50 1.40 1.40 1.40 1.40 1.40 1.50 1.40 1.50 1.40 1.50 1.40 1.50 1.50 1.40 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.40 1.50 1.40 1.50 1.50 1.40 1.50 1.30 1.40 1.30 1.30 1.40 1.40 1.30 1.40 1.40 1.30 1.40 1.40 1.30 1.40	Oct. 1.40 1.50 1.40 1.50 1.40 1.50 1.40 1.50 1.60 1.50 1.60 1.50 1.60 1.50 1.60 1.50 1.60 1.50 1.60 1.60 1.60 1.60 1.50 1.60 1.60 1.50 1.60 1.50 1.60 1.60 1.50 1.60 1.50 1.60 1.50 1.60 1.50 1.50 1.50 1.50 1.60 1.50	$\begin{tabular}{ c c c c c c c c c c c c c c c c c c c$	$\begin{array}{c} \text{Dec.}\\\hline\\1.55\\1.55\\1.55\\1.55\\1.56\\1.56\\2.30\\2.40\\2.000\\1.60\\1.50\\1.60\\1.50\\1.50\\1.50\\1.50\\1.50\\1.50\\1.50\\1.5$
26 27 28 29 30 31	$\begin{array}{c} 1.10\\ 2.30\\ 2.20\\ 2.00\\ 1.80\\ 1.60\\ 1.60\end{array}$	3.30 3.00 3.00	$\begin{array}{c} 2.50 \\ 2.60 \\ 2.50 \\ 2.50 \\ 2.60 \\ 2.60 \\ 2.60 \end{array}$	2.20 2.10 2.10 2.10 2.00	$\begin{array}{c} 2.00 \\ 1.90 \\ 1.90 \\ 2.00 \\ 1.90 \\ 2.10 \end{array}$	1.80 1.90 1.80 1.80 1.70	$\begin{array}{c} 1.00\\ 2.00\\ 1.90\\ 1.80\\ 1.55\\ 1.40\\ 1.40\\ \end{array}$	$\begin{array}{c} 1.70 \\ 1.70 \\ 2.00 \\ 1.90 \\ 1.80 \\ 1.70 \end{array}$	$1.40 \\ 1.40 \\ 1.40 \\ 1.50 \\ 1.60$	$1.50 \\ 1.50 \\ 1.40 \\ 1.30 \\ 1.40 \\ 1.60$	$\begin{array}{c} 1.50 \\ 2.50 \\ 2.10 \\ 1.80 \\ 1.70 \\ 1.60 \end{array}$	$\begin{array}{c} 1.60\\ 1.60\\ 1.50\\ 1.50\\ 1.50\\ 1.40\\ 1.50\\ 1.50\\ \end{array}$

NORTH AND SOUTH RIVERS AT PORT REPUBLIC, VIRGINIA.

These stations were established in August, 1895. They are described in Water-Supply Paper No. 35, page 86, where records of past measurements will be found. Both stations were discontinued on April 1, 1899.

NORTH BRANCH OF SHENANDOAH RIVER NEAR RIVERTON, VIRGINIA.

This station, which was established June 26, 1899, by Arthur P. Davis, is about 2 miles northwest of Riverton. It is described in Water-Supply Paper No. 35, page 88, where will be found records of discharge measurements made during 1899. During 1900 the following measurements were made by E. G. Paul:

February 13: Gage height, 3.25 feet; discharge, 645 second-feet. June 18: Gage height, 5.30 feet; discharge, 2,923 second-feet. September 10: Gage height, 2.60 feet; discharge, 146 second-feet.

VIRGINIA.

	Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1		3.00 3.00	$\frac{4.00}{4.00}$	$4.05 \\ 6.85$	$3.70 \\ 3.58$	$3.25 \\ 3.18$	$2.80 \\ 2.80$	$2.90 \\ 2.90$	2.73 2.65	$\frac{2.60}{2.60}$	3.80 3.80	3.70 3.73	$4.15 \\ 3.93$
0044		3.00 3.00 2.00	4.00 4.00 2.00	5.55 4.40 4.10	3.53 3.48 3.40	3.15 3.10 2.05	2.80 2.90	2.85 2.78 2.78	2.60 2.55 2.52	2.63 2.63 2.58	3.75 3.70 3.70	3.70 3.75 2.70	4.03
000		3.00 3.00 3.00	3, 50 3, 50 3, 38	4.10 3.88 3.83	3.33 3.28	3.05 3.05 3.00	2.83	2.73 2.70	2.50 2.50 2.50	2.60 2.60 2.60	$ \begin{array}{r} 3.10 \\ 3.70 \\ 3.78 \end{array} $	$\begin{array}{c} 3.10 \\ 3.70 \\ 3.70 \end{array}$	5.70 5.15
800 10		$3.00 \\ 3.00 \\ 3.00$	$ \begin{array}{r} 3.10 \\ 3.00 \\ 2.95 \end{array} $	3.75 3.68 3.60	$3.25 \\ 3.20 \\ 3.15$	2.98 2.95 2.93	2.80 2.80 2.80	2.70 2.68 2.68	2.55 2.58 2.60	$2.58 \\ 2.60 \\ 3.10$	3.80 3.70 3.70	3.70 3.65 3.63	4.70 4.45 4.45
11		3.00	3.00 2.98 9.12	3.50 3.40	3.15 3.15 3.15	2.90	2.75	2.63	2.60 2.58	$ \begin{array}{r} 3.60 \\ 3.60 \\ 2.50 \\ 50 \end{array} $	3.68 3.65 2.50	3.70 3.60	4.35
18 14 13	· · · · · · · · · · · · · · · · · · ·	3.00 2.98 2.93		5. 55 3. 35 3. 35	5.15 3.15 3.10	2.90 2.90 2.90 2.90	2.70 2.73 2.75	2.65 2.65 2.63	$2.50 \\ 2.50 \\ 2.50$	a. 58 3. 60 3. 60	$3.70 \\ 3.70 \\ 3.70$	3.60 3.68 3.65	$ \begin{array}{c} 3.95 \\ 3.95 \\ 4.00 \end{array} $
16 17 15		2.90 2.80 2.80	3.88 3.63 3.43	3.35 3.30 3.25	$\begin{array}{c} 3.10 \\ 3.10 \\ 3.10 \end{array}$	$2.83 \\ 2.80 \\ 2.80$	2.78 3.45 4.75	2.60 2.68 2.63	2.50 2.60 2.60	$ \begin{array}{r} 3.70 \\ 3.68 \\ 3.65 \end{array} $	$3.70 \\ 3.78 \\ 3.80$	3.60 3.60 3.63	$ \begin{array}{r} 3.95 \\ 4.05 \\ 3.90 \end{array} $
19 20		2,93	3.35 3.35	5.50 5.95	3.20 3.55	2.80 2.80	4.75 3.98	$ \begin{array}{c} 2.60 \\ 2.60 \\ 2.60 \\ 2.00 \\ $	2.55 2.55	3.68 3.60	3.75 3.70	3.63 3.65	3.90
222		$ \begin{array}{r} 6.50 \\ 4.65 \\ 3.90 \end{array} $	$ \begin{array}{r} 3.25 \\ 3.75 \\ 5.98 \\ \end{array} $	$ \begin{array}{r} 7.20 \\ 5.70 \\ 4.90 \end{array} $	$ \begin{array}{r} 3.60 \\ 3.60 \\ 4.23 \end{array} $	$2.80 \\ 2.80 \\ 2.80$	3.30 3.20	2.63 2.70 2.83	2.50 2.55 2.60	5.60 3.58 3.58	$3.70 \\ 3.70 \\ 3.70$	3.70 3.63 3.60	3, 70 3, 60 3, 80
24 25 96		$\begin{array}{c} 3.55\\ 3.25\\ 3.03\end{array}$	5.30 4.63 4.15	$4.43 \\ 4.17 \\ 4.00$	4.40 4.10 3.75	2.80 2.80 2.80	3.15 3.08 3.00	4.28 3.33 3.23	2.60 2.60 2.60	3.60 3.55 3.60	3.78 3.78 3.85	3.68 3.70 4.65	$ \begin{array}{c} 3.75 \\ 3.70 \\ 3.75 \end{array} $
21 28		3.00 3.00 3.00	3.90 3.80	4.00	3.63 3.50	2.80 2.80 2.80	2.93	3.00 2.93	2.55 2.60	3.60	3.90 3.80	7.00 5.25	3.80 3.78
22 3(3])	$ \begin{array}{r} 3.50 \\ 4.00 \\ 4.00 \end{array} $		3, 90 3, 85 3, 80	3.43 3.33	2.80 2.80 2.75	2.90	2.83 3.08 2.80	2.63 2.60 2.63	5.43 3.95	5.15 3.73 3.70	5.35 4.45	3, 18 3, 73 3, 73

Daily gage height, in feet, of North Branch of Shenandoah River near Riverton, Virginia, for 1900.

SOUTH BRANCH OF SHENANDOAH RIVER AT FRONT ROYAL, VIRGINIA.

This station was established by Arthur P. Davis on June 26, 1899. It is described in Water-Supply Paper No. 35, page 89, where will also be found record of discharge measurement made in 1899. During 1900 the following measurements were made by E. G. Paul:

February 14: Gage height, 5.75 feet; discharge, 1,955 second-feet. June 19: Gage height, 7.90 feet; discharge, 5,703 second-feet.

120OPERATIONS AT RIVER STATIONS, 1900. - PART II. [NO. 48.

				Virg	inia, j	for 19	00.					
Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
$\begin{array}{c} 1 \\ 2 \\ 3 \\ 4 \\ 5 \\ 6 \\ 7 \\ 8 \\ 9 \\ 10 \\ 11 \\ 12 \\ 13 \\ 14 \\ 15 \\ 16 \\ 17 \\ 18 \\ 19 \\ 19 \\ 19 \\ 19 \\ 19 \\ 10 \\ 10 \\ 10$	$\begin{array}{c} 5.55\\ 5.55\\ 5.65\\ 5.55\\ 5.50\\ 5.35\\ 5.05\\ 5.05\\ 4.95\\ 5.00\\ 4.95\\ 5.00\\ 5.665\\ 5.00\\ 4.80\\ 4.80\\ 4.80\\ 4.80\\ 4.80\\ 00\\ \end{array}$	$\begin{array}{c} 4.95\\ 4.80\\ 5.00\\ 5.60\\ 5.20\\ 5.65\\ 5.40\\ 5.00\\ 5.00\\ 5.00\\ 5.00\\ 6.35\\ 5.10\\ 6.35\\ 5.10\\ 6.50\\ 6.20\\ 5.95\\ 5.70\end{array}$	$\begin{array}{c} 6.40\\ 10.65\\ 8.80\\ 7.55\\ 6.90\\ 6.60\\ 6.35\\ 6.20\\ 6.10\\ 6.00\\ 5.90\\ 5.70\\ 5.60\\ 5.50\\ 5.50\\ 5.50\\ 5.50\\ 5.50\\ 5.65\end{array}$	$\begin{array}{c} 5.90\\ 5.75\\ 5.70\\ 5.60\\ 5.50\\ 5.40\\ 5.30\\ 5.20\\ 5.20\\ 5.20\\ 5.20\\ 5.20\\ 5.10\\ 5.10\\ 5.10\\ 5.10\\ 5.10\\ 5.00\\ 5.00\\ 5.00\\ \end{array}$	$\begin{array}{c} 5.30\\ 5.25\\ 5.15\\ 5.10\\ 5.00\\ 5.00\\ 5.00\\ 4.90\\ 4.80\\ 4.80\\ 4.80\\ 4.80\\ 4.70\\ 4.70\\ 4.70\\ 4.70\\ 4.70\\ 4.70\\ 4.70\\ 4.70\\ 4.70\\ 4.70\\ 4.70\\ 4.70\\ 4.70\\ 4.70\\ 4.70\\ 1.50\\$	$\begin{array}{c} 4.95\\ 4.85\\ 4.80\\ 4.80\\ 4.80\\ 4.80\\ 4.70\\ 4.70\\ 4.70\\ 4.60\\ 4.50\\ 4.50\\ 4.50\\ 4.50\\ 5.70\\ 6.25\\ 7.25\\ 7.25\\ 7.65\\ \end{array}$	$\begin{array}{c} 4.80\\ 4.70\\ 4.60\\ 4.60\\ 4.50\\ 4.50\\ 4.50\\ 4.50\\ 4.40\\ 4.40\\ 4.40\\ 4.30\\ 4.30\\ 4.30\\ 4.30\\ 4.30\\ 4.30\\ 4.30\\ 4.30\\ 4.30\\ 4.30\\ 4.20\\ \end{array}$	$\begin{array}{c} 4.60\\ 4.55\\ 4.45\\ 4.40\\ 4.30\\ 4.30\\ 4.30\\ 4.20\\ 4.20\\ 4.20\\ 4.20\\ 4.20\\ 4.20\\ 4.20\\ 4.20\\ 4.20\\ 4.20\\ 4.20\\ 4.20\\ 4.20\\ 4.20\\ 4.00\\ 4.00\\ \end{array}$	$\begin{array}{c} 4.10\\ 4.10\\ 4.10\\ 4.10\\ 4.00\\ 4.00\\ 4.00\\ 4.00\\ 4.00\\ 4.00\\ 3.90\\ 3.90\\ 3.90\\ 3.90\\ 4.65\\ 4.65\\ 4.65\\ 4.65\\ 4.15\\ \end{array}$	$\begin{array}{c} 4.30\\ 4.25\\ 4.25\\ 4.25\\ 4.40\\ 4.30\\ 4.40\\ 4.30\\ 4.40\\ 4.30\\ 4.40\\ 4.30\\ 4.40\\ 4.30\\ 4.40\\ 4.25\\ 4.30\\ 4.30\\ 4.30\\ 4.40\\ 4.40\\ \end{array}$	$\begin{array}{c} 4.50\\ 4.50\\ 4.40\\ 4.45\\ 4.55\\ 4.60\\ 4.50\\ 4.50\\ 4.50\\ 4.50\\ 4.40\\ 4.40\\ 4.40\\ 4.40\\ 4.40\\ 4.30\\ 4.30\\ 4.30\\ 4.30\\ 4.30\end{array}$	$\begin{array}{c} 5.30\\ 5.35\\ 5.15\\ 5.580\\ 7.60\\ 5.860\\ 7.60\\ 5.850\\ 5.645\\ 5.100\\ 5.90\\ 5.510\\ 9.850\\ 4.850\\ 4.850\\ 4.850\\ 4.850\\ 4.850\\ 4.850\\ 5.650\\ 5.650\\ 5.650\\ 5.50\\ 5$
20 21 22 93	7.20 10.70 8.35 7.15	5.55 5.45 6.25 8.90	$ \begin{array}{r} 6.55 \\ 9.55 \\ 8.35 \\ 7.50 \end{array} $	5.40 5.75 5.90 6.55	5.30 5.75 5.55 5.35	6.85 6.20 5.80 5.30	4.20 4.55 4.90 4.85	4.00 4.10 4.20 4.25	$\begin{array}{r} 4.15 \\ 4.15 \\ 4.15 \\ 4.15 \\ 4.10 \end{array}$	$4.30 \\ 4.25 \\ 5.05 \\ 6.25$	4.30 4.30 4.40 4.85	$ \begin{array}{r} 4.70 \\ 4.60 \\ 4.60 \\ 4.60 \\ 4.60 \end{array} $
24 25 26 27 20	$\begin{array}{c} 1.19 \\ 6.50 \\ 6.15 \\ 5.80 \\ 5.60 \\ 5.60 \end{array}$		$\begin{array}{c} 6.60 \\ 6.55 \\ 6.45 \\ 6.30 \\ 6.97 \end{array}$	$6.35 \\ 6.25 \\ 6.30 \\ 5.75 \\ $	5.25 5.20 5.35 5.05	5.35 5.20 5.10 5.10 5.10 5.20	$\begin{array}{c} 4.65 \\ 4.85 \\ 4.95 \\ 5.00 \\ 4.90 \end{array}$	$\begin{array}{c} 4.30 \\ 4.30 \\ 4.30 \\ 4.25 \\ 4.25 \end{array}$	$\begin{array}{c c} 4.10 \\ 4.20 \\ 4.30 \\ 4.35 \\ 4.15 \\ 4.05 \end{array}$		$\begin{array}{c} 4.05 \\ 4.95 \\ 5.65 \\ 6.65 \\ 8.45 \\ 7.20 \end{array}$	$\begin{array}{c} 4.60 \\ 4.60 \\ 4.60 \\ 4.60 \\ 4.50 \\ 4.50 \end{array}$
29	0.00 5.55	6.20	6.15	$ \begin{array}{r} 5.35 \\ 5.40 \end{array} $	4.90	5.05	4.90	$\frac{4.20}{4.20}$	4.05	$ \begin{array}{r} 5.05 \\ 4.65 \end{array} $	6,35	4.50

Daily gage height, in feet, of South Branch of Shenandoah River at Front Royal,

SHENANDOAH RIVER AT MILLVILLE, WEST VIRGINIA.

4.80

5.45

 $\frac{4.80}{4.70}$

4.90

4.10 4.10

5.40

6.00

5.95

5.85

4.65 $\frac{4.05}{4.55}$ $\frac{4.50}{4.50}$

4.20

4.50

9

30

31

 $\begin{array}{c} 5.55\\ 5.50 \end{array}$

5.20

This station, which was established April 15, 1895, is 4 miles above the mouth of Shenandoah River. It is described in Water-Supply Paper No. 35, pages 90 and 91. Records of measurements for 1899 will be found in the Twenty-first Annual Report, Part IV, page 96. During 1900 the following measurements were made by E. G. Paul:

February 24: Gage height, 5.9 feet; discharge, 12,985 second-feet. June 19: Gage height, 4.5 feet: discharge, 9,132 second-feet. September 15: Gage height, 0.4 foot: discharge, 500 second-feet.

Daily gage height, in feet, of Shenandoah River at Millville, West Virginia, for 1900.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
				•				Ŭ				
1	1.25	2.10	3.00	2.55	1.80	1.50	1.30	1.15	0.60	0.60	0.80	-2.00
2	1.30	1.20	4.80	2.50	1.75	1.50	1.25	1.00	. 60	.70	, 80	1.70
3	1.20	1.60	6.50	2.40	1.70	1.30	1.25	1.05	. 60	. 70	, 80	1.50
4	1.15	1.55	4.80	2.25	1.60	1.30	1.20	1.00	. 60	.70	. 90	1,60
5	1.20	2.00	3.90	2.20	1.60	1.30	1.20	. 90	. 55	. 60	. 90	2.25
6	1.30	2.00	3.40	2.10	1.50	1.25	1.30	.85	. 50	. 55	. 90	4.80
7	1.30	1.50	2.90	2.00	1.50	1.15	1.10	. 80	. 50	. 50	. 85	3,60
8	1.30	1.40	2.80	1.90	1.40	1.10	1.00	. 75	. 45	. 50	. 90	2.80
9	1.20	1.40	2.70	1.85	1.40	1.95	. 90	.70	. 45	. 75	. 85	3.40
10	1.15	1.40	2,60	1.80	1.40	1.00	. 85	. 70	. 45	. 60	. 80	-2.20
11	1.20	1.40	2.50	1.70	1.30	. 95	. 80	. 70	. 45	. 55	. 80	1.90
12	1.10	1.40	2.40	1.70	1.30	. 90	. 80	. 65	. 40	. 50	. 80	1.75
13	1.30	1.50	2.30	1.70	1.30	1.00	.80	. 70	. 40	. 50	. 80	1.60
14	1.40	1.90	2.20	1.70	1.20	. 90	. 75	. 60	. 40	. 70	. 75	1.50
15	1.50	3.80	2.10	1.70	1.20	1.10	. 75	. 60	. 40	. 90	. 75	1.40
16	1.30	3.30	2.10	1.60	1.15	1.30	. 70	. 55	. 50	1.10	. 75	1.35
17	1.20	2.80	2.10	1.60	1.10	2.30	. 70	. 60	. 60	. 90	. 70	1.30
18	1.15	2.50	2.00	1.55	1.10	2.70	. 60	. 60	. 55	. 80	. 70	-1.20
19	1.20	2.30	2.00	1.60	1.20	4.50	. 60	. 60	1.10	. 80	. 65	1.15
20	1.80	2.20	3.30	1.65	1.10	3.70	1.20	. 60	. 80	.70	. 65	1.15
21	6.00	2.50	5.95	2.10	1.90	3.00	, 80	. 65	. 70	. 60	. 60	1.10
22	5.90	2.45	6.20	2.40	1.90	2.60	1.00	. 60	. 60	. 55	. 65	1.00
23	4.20	4.35	4.70	2.55	1.70	2.10	1.10	. 55	. 55	. 50	.70	1.00
24	3.30	5.90	3.90	3.00	1.60	1.90	1.40	. 60	. 55	. 65	. 70	1.00
25	2.80	4.50	3.45	3.00	1.40	1.70	2.50	. 60	. 50	. 80	. 70	1.00
26	2.50	3.80	3.15	2.70	1.25	1.55	2.80	. 55	. 50	2.10	1.10	1.00
27	2.25	3.40	3.00	2.50	1.50	1.45	1.70	. 65	. 45	. 60	2.10	. 95
28	2.00	2.80	2.95	2.30	1.50	1.40	1.50	. 70	. 50	1.25	4.50	. 90
29	1.90		2.80	2.15	1.50	1.35	1.30	. 60	. 55	1.10	3.15	. 90
30	1.80		2.70	2.00	1.40	1.30	1.30	. 60	. 50	. 95	2.45	. 90
31	1.85		2.60		1.30		1.20	. 60		. 90		. 90

POTOMAC RIVER AT POINT OF ROCKS, MARYLAND.

This station was established February 17, 1895, at the tollbridge over the Potomac River at Point of Rocks. It has been described and results of measurements have been given in the various Annual Reports and in the Water-Supply and Irrigation Papers containing reports of the operations at river stations. More or less difficulty has been experienced with the wire gage, due to its stretching, and no record of this lengthening has been noted. A thorough study of the changes of the gage have been made in this office, based on measurements and on a study of the average depth of soundings, with the result that it has been found necessary to modify the gage heights in order to refer them to a common datum. This has also necessitated a revision of the rating table. In some cases it has been impossible to reduce the measurements to the known datum, and it has therefore been thought best to discard them and to publish here only such gage heights and discharge measurements as could be reduced to a common datum and on which reliance can be placed as giving a correct estimate of the discharge.

As originally placed the gage was located in the third span of the bridge from the north shore. The next year (1896) the wire became rusted and broke frequently, and a new wire gage was placed in the east side of the first span of the bridge, but it was referred to a different datum. During 1897 there was a further change in the length

of the gage, which was not recorded, and therefore it has been necessary to discard the records during those two years—that is, 1896 and 1897.

On January 25, 1898, the gage wire was compared with the bench mark, and the observations since that date have been referred to this datum. The bench mark to which the gage has been referred is a copper bolt in a large capstone on the lower wing wall of the north abutment, about 10 feet from the north end of the first iron truss and 41.30 feet above the datum of the gage. The length of the cable of the wire gage is 44.22 feet. The measurements of 1895 are considered correct within themselves, but there was a difference between the datum of that gage and that of the present standard of 0.4 foot, making it necessary to deduct that amount from the gage readings of 1895 in order to reduce them to the present datum. Tables of the corrected gage heights and of the discharge measurements computed from them are published herewith.

The flood discharge of February 23, 1897, is also considered correct, and is given in the table of discharge measurements. There is no change in the published discharge measurements or the gage heights for 1898, 1899, and 1900, but they are reproduced here in order to bring together all of the records that could be reduced to one standard.

Date.	Gage height.	Discharge.	Date.	Gage height.	Discharge.
1895. April 5. April 5. April 23. May 1. May 7. May 17. May 28. June 3. June 3. June 17. July 10. November 6. 1897. February 23.	$\begin{array}{c} Feet. \\ 3.05 \\ 3.42 \\ 4.27 \\ 2.10 \\ 4.35 \\ 3.10 \\ 2.35 \\ 2.45 \\ 1.53 \\ 1.53 \\ 1.50 \\ .40 \\ 21.70 \end{array}$	$\begin{array}{c} Secft.\\ 10,524\\ 14,062\\ 17,516\\ 7,371\\ 21,073\\ 12,484\\ 8,918\\ 9,189\\ 4,536\\ 4,233\\ 4,695\\ 1,202\\ \end{array}$	1898. January 25. August 19. October 3. 1899. January 28. May 20. September 5. October 29. 1900. June 28. October 2.	Feet, 6.50 3.30 .65 3.80 8.15 .80 .50 1.50 .30	$\begin{array}{c} Secft.\\ 33,344\\ 14,309\\ 1,939\\ 17,330\\ 45,986\\ 2,360\\ 1,628\\ 5,212\\ 1,259\end{array}$

Discharge measurements of Potomac River at Point of Rocks, Maryland.

MARYLAND.

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Day.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1		6.10	3.10	3. 30	1.80	2.00	1.00	0.60	0.30	0.40	0.40
2		9.70	3.00	5.90	1.70	2.70	. 90	. 70	. 30	. 40	. 50
3		10.60	2.90	5.80	1.50	2.30	. 80	. 90	. 30	. 30	. 50
4		9.60	3.60	5.40	1.40	2.10	. 80	. 70	.30	. 30	. 50
5		7.10	3.50	4.40	1.40	1.90	. 90	. 60	. 30	. 30	. 50
6		5.60	3.00	3.70	1.40	1.70	. 80	. 60	. 30	. 40	. 60
7		4.80	2.70	3.10	1.20	1.50	.80	. 60	. 30	. 30	. 80
8		4.30	2.60	2.70	. 80	1.50	.80	. 50	. 30	. 30	. 80
9		4.10	3.00	2.70	1.30	1.70	1.10	. 50	. 30	. 30	. 60
10		4.10	10.80	2.80	1.20	1.60	1.00	. 60	. 30	. 40	. 50
11		4.00	- 7.90	2.80	1.10	1.50	. 90	. 50	. 30	. 40	. 50
12		3.60	5.80	2.70	1.10	1.50	. 80	. 50	. 40	. 50	. 50
13		3.60	4.50	2.70	1.20	1.30	. 80	. 50	. 20	. 40	1.60
14		3.60	3.80	2.80	1.20	1.20	. 70	. 50	. 20	. 40	1,60
15		4.70	3. 50	3.00	1.50	1.10	. 70	. 50	. 30	. 40	. 60
16		5.90	3.40	2.60	1.30	1.00	. 60	. 50	. 30	. 40	. 50
17	1.60	8.10	3.30	2.40	1.20	1.00	. 60	. 40	. 30	. 40	. 40
18	1.60	6.90	3.00	2.20	1.10	1.00	. 60	. 40	. 30	. 40	. 40
19	1.60	5.40	2.40	2.20	1.10	1.10	.60	. 50	. 30	. 40	. 30
20	1.60	4.90	2.60	2.40	1.00	1.00	. 60	. 30	. 30	. 40	. 30
21	1.70	4.10	2.40	2.30	.90	1.00	. 00	. 40	. 20	. 40	. 30
~~~~~~	1.80	3.80	2.20	2.40	1.00	1.00	. 50	. 40	. 20	. +0	. 00
23	2.00	- 3.40	2.10	2.80	1.00	1.10	. 30	.40	. 30	. 40	. 00
21	2.00	3.20	2.00	3.80	. 90	. 90	. 50	. 50	. 30	. 40	1.00
20	2.00	3,00	2.00	ð. 30 9. co	. 80	. 90	. 40	. 50	. 30	. +0	1.00
26	2.10	2.90	1.90	2.00	1.80	1.00	. 40	. 40	. 00	. 40	1.20
Al	2.90	0.00	1.80	2. 00 9. 40	1.30	1.20	. 40	. 40	. 00	. 40	1.00
20	5.60	0.80 2.20	1.80	2, 40	1 80	1.00	. ±0	. ±0	. 00	. 30	1.40
29		5.20	1.80	A. 40 9.90	1.50	1.20	. 40	. 30	. 30	. 30	. 90
00		4.00	2.20	2.20	1.90	1.10	. 50	. 50	. 30	. ±0	1 20
91		5. 90		A. 00		1.10	. 50		. 30		1.00

Daily gage height, in feet, of Potomac River at Point of Rocks, Maryland, for 1898.

-	Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
	1	2.90	2.80	1.90	6.10	2.60	2.20	0.90	1.50	1.20	0.70	2.70	2.10
1		2.90	1.70	1.80	5.20	2.40	2.00	. 80	1.70	1.10	. 70	2.50	2.10
	1	3.20	1.90	1.70	4.00	2 00	$1.00 \\ 1.70$	.00	1.40 1.20	1.10	.00	2 20	2.50
ł	5	3.20	1.90	1.60	3. 80	1.90	1.60	.70	2.20	1.00	. 80	2.00	5.00
	6	3.30	$\hat{2}.00$	1.60	3,60	1.80	1.40	.70	7.20	1.00	. 80	1.80	9.20
1	7	3.20	2.00	1.60	3.20	2.20	1.30	. 70	6.10	1.00	1.00	1.80	6.10
1	8	2.90	1.90	1.50	2.90	5.40	1.30	. 80	3.70	1.00	1.10	1.70	4.50
	9	3.00	1.90	1.50	2.40	11.05	1.20	. 70	3.90	1.00	1.00	1.60	3,60
1		3.20	1.80	1.40	2.50	9.60	1.20	. 70	5.60	. 90	1.00	1.60	3.00
1		3.90	1.80	1.40	2.50	6.50	1.10 1.10	. 70	14.00	. 90	. 90	$\frac{2.00}{1.80}$	2.60
	÷	5.70	1.90	1.50	2.40	0.20	$1.10 \\ 1.10$	. 00	10.00	. 90	1.40	1.80	2.40
ť	4	5.30	1 90	1.50	2.50	3 70	1.10	. 50	9.00	. 60	1.40	2.00	2.20
1	5	5.50	1.90	1.60	2.50	3 10	1.30 1.30	. 50	7 20	.80	1.00	2.00	2 00
1	6	6.70	2.00	1.70	4.00	3.00	1.30	.50	6.10	. 80	. 80	1.80	1.80
1	7	8,00	2.00	1.70	9.00	3.20	1.30	. 50	5.20	. 80	. 80	1.80	1.80
1	8	6.70	1.80	2.00	6.70	4.60	1.20	. 50	4.30	. 80	. 80	1.80	-2.00
1	9	5.60	1.70	5.80	5.10	4.40	1.50	. 70	3.30	. 80	1.40	2.20	2.10
2	9	4.90	1.70	4.60	4.20	3.50	1.40	. 70	3.10	. 70	9.00	3.00	-2.20
2		4.70	2.80	3.50	3.50	2.30	1.30	. 90	3.00	. 70	5.40	3.60	2.60
20	2	4.00	3.80	3.50	3.20	2.90	1.30 1.20	.90	3.80	.10	<b>a</b> . 30	3.30	3.30
3	1	0.40	2.40	6.20	2.60	0.10 2.00	1.00	1.10	2.00	. 10	10.10	3.40	6.90
2	5	8 40	2.90	6 10	2.60	5.10	1.10	. 30	2.00	. 70	5 90	3.00	6.90
$\tilde{2}$	6	5.10	2.60	10.50	2.60	5.60	1.10	.90	1.80	70	4.50	2.70	5.30
2	7	5.00	2.30	7.20	2.50	4.10	1.00	1.20	1.50	. 90	3.80	2.60	4.30
2	8	5.10	2.10	5.30	3.30	3,40	1.00	1.00	1.50	. 80	3.60	2.40	3.70
2	9	5.10		4.40	3.00	3.00	. 90	1.20	1.40	. 70	3.40	2.20	3.20
3	0	3.60		4.30	2.80	2.80	. 90	1.40	1.30	. 70	3.00	2.10	3.00
3	I	3.40		6.20		2.40		1.70	1.30		2.80		2.70

Daily gage height, in feet, of Potomac River at Point of Rocks, Maryland, for 1899.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oet.	Nov.	Dec.
1	3.00	2.40	11.90	5.30	1.60	2.00	1.00	0.70	0,90	0.70	0.80	0.80
3 	2.90 2.70	2.00 2.10 2.10	8.20 7.60	4.00	$\frac{1.00}{2.10}$	3.40 3.80 2.60	1.10	. 70	. 80	. 60	2.50 2.00	. 80
5	2.30 4.10	2.00 2.00	$8.50 \\ 16.55$	3.30 3.00	$1.70 \\ 2.10$	$2.10 \\ 1.80$	.90	$1.00 \\ 1.10$	$.80 \\ .70$	. 60 . 60	$1.80 \\ 1.40$	.80
7 8	$6.90 \\ 8.10$	$2.00 \\ 2.30$	$12.90 \\ 10.00$	$\frac{2.80}{3.00}$	$2.00 \\ 1.90$	$     \begin{array}{r}       1.60 \\       1.50     \end{array} $	$\frac{1}{2.00}$	1.10 1.10	$.70 \\ .60$	$.70 \\ .70$	$1.40 \\ 1.30$	$.70 \\ .70$
9 10	$6.80 \\ 5.40 $	<b>2.30</b> <b>3.60</b>	$8.10 \\ 6.00 \\ 6.00$	$3.50 \\ 3.40 \\ 4.20$	$1.00 \\ 2.40 \\ 4.60$	$1.40 \\ 1.70 \\ 1.00$	1.00 .90	$1.00 \\ 1.00 \\ 0.00$	. 60 . 60	.70 .60	$1.20 \\ 1.00$	.70 .70
$11 \\ 12 \\ 19$	4.60 3.90 3.60	$4.20 \\ 4.20 \\ 4.00$	5.80 5.60 5.00	4.20 4.50 2.40	4.50 3.80 3.40	1.80 1.70 1.70	. 90 . 80 . 80	. 90 . 80 60	. 60 . 80 1. 20	. 60	.90	.70
14	3.40 3.40	3,90 3,80	$4.80 \\ 4.50$	3.20 3.00	3.20 2.80	1.60 1.50	. 80	. 60	$1.10 \\ 1.00$	.50	.80	1.20 3.00
$\begin{array}{c} 16 \\ 17 \end{array}$	$     4.00 \\     5.70   $	$4.00 \\ 4.50$	$\begin{array}{r} \textbf{4.60} \\ \textbf{4.70} \end{array}$	$2.80 \\ 2.70$	$2.50 \\ 2.30$	$\begin{array}{c} 1.50\\ 1.40\end{array}$	$\begin{array}{c}1.10\\.90\end{array}$	$.70 \\ .70$	. 90 . 80	. 50 . 50	. 80 . 80	$2.10 \\ 1.70$
18 19	5.20 4.70	5.00 5.20	$4.40 \\ 5.20 \\ 5.40$	2.60 2.50	2.40 8.55	1.40 1.30 1.20	.70 .70 .70	. 60	.70	. 50	$.70 \\ .70 \\ .70 \\ .70$	1.50 1.60
20 21 22	$4.40 \\ 4.00 \\ 3.50$	5.40 6.00 8.50	5.40 5.30 4.70	2.40 2.20 2.10	5.00 3.60	1.30 1.20 1.20	.70 .70 .70	. 60	. 90 . 70 . 80	. 50	. 70	1.30 1.30 1.10
23 24	$3.30 \\ 3.20$	$14.80 \\ 13.70$	4.20	2.00 2.00	$3.00 \\ 2.70$	$1.10 \\ 1.10$	. 70	. 50 . 50	. 90 . 99	$.50 \\ .50$	. 80 . 80	$1.00 \\ 1.20$
25 26 	3.30 4.80	9.00	$3.90 \\ 3.70 \\ 2.70$	2.00 1.90	2.40 2.10	1.00 1.00 1.00	. 60 . 60	.50	.90 1.00	.50 .50	. 90	1.80 2.10
27 28 29	4.70 3.90 3.20	$9.25 \\ 13.90$	3.50 3.40 3.60	1.90 1.80 1.70	$     \begin{array}{r}             2.00 \\             1.80 \\             1.70         \end{array}     $	1.00 1.20 1.10	. 60	1.20 1.10 1.10	$.80 \\ .70 \\ .70$	. 50	. 80 . 80 . 80	$1.60 \\ 1.50 \\ 1.60$
30 31	2.80 2.60		8.60 7.00	1.70	$1.70 \\ 1.80$	1.00	.80	$1.00 \\ 1.00$	. 80	.50	. 80	1.60 1.60 1.60

Daily gage height, in feet, of Potomac River at Point of Rocks, Maryland, for 1900.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oet.	Nov.	Dec.
1	1.50	1.00	3.50	4 80	1.90	1.30	1.20	1.20	0.70	0.30	0.50	2 40
9	1.50	1 60	4 50	3.80	1 70	1 30	1.10	1 10	70	30	50	1 90
3	1.40	2.00	6.60	3.40	1.60	1.30	1.00	1.00	. 60	. 30	. 50	1.60
4	1.50	2.10	5.90	3.10	1.50	1.40	1.00	. 90	. 60	. 30	. 50	1.60
5	1.50	2.20	4.40	2.80	1.50	1.60	. 90	. 90	. 50	. 30	. 50	2.00
6	1.40	1.90	4.00	2.70	1.40	1.60	1.30	. 80	. 60	. 30	.40	4.10
7	1.40	1.80	3.60	2.60	1.40	1.50	1.00	. 80	. 50	. 30	. 40	5.90
8	1.30	1.50	3.90	2.50	1.30	1.40	. 90	. 70	.40	, 30	. 40	3.70
9	1.30	1.80	4.50	2.40	1.30	1.40	. 80	. 60	. 40	. 30	. 50	3.00
10	1.20	2.30	4.00	2.30	1.30	1.30	. 70	. 60	. 30	. 30	. 60	2.50
11	1.30	3,00	3.60	2.10	1.20	1.20	. 60	. 50	. 40	. 30	. 50	2.10
1%	1.40	2.50	3.20	2.10	1.20	1.10	. 60	. 50	. 30	. 30	. 40	1.80
13	1.40	3.00	2.90	2.00	1.10	1.00	. 50	. 40	. 30	. 30	. 40	1.60
14	1.50	4.00	2.80	1.90	1.10	. 90	, 50	, 40	. 40	, 30	. 40	1.50
10	1.80	0.30	2.70	1.90	1.10	1.30	. 50	. 40	. 40	. 90	. 40	1.40
10	2.10	4.00	2.00	1.80	1.10	1.00	. 40	. 40	. 40	. 30	. 40	1.40
10	1.90	0.80	2.40	1.80	1.00	1.80	. 40	. 40	. 30	. 40	. 40	1.00
10	1.70	0.10	2.00	1.70	1.00	2.00	.40	. 40	, 50	. 40	, 50	1.20
19	2 20	2 20	2 60	1.70	1.20	6,00	1 40	. 40	. 30	, 50	. 20	1,10
91	3.60	1 90	5.80	1.00	1.80	4 60	1.40	40	. 50	. 50	- 20	1.10
99	6.80	3.00	8.70	2 20	1 00	3 60	1.00	40	. 30	50	.00	1,00
93	5.50	6.90	6 60	2 50	2.00	2 70	- 80	40	. 30	40	40	
24	4.00	7.10	5 40	2.80	1 70	2 30	1.80	40	. 30	.40	40	80
25	3.30	5.60	5.00	3.00	1.50	2.10	1.60	. 50	. 30	.40	.40	.80
26	2.80	3.90	4.50	2.80	1.40	2.00	2.00	60	. 30	. 40	1.20	. 80
27	2.50	3.30	4.10	2.50	1.40	1.80	1.40	. 70	. 30	. 50	3.30	. 80
28	2.10	3.00	3.70	2.30	1.40	1.50	1.20	. 90	. 20	. 50	8.20	. 89
29	1.80		3.50	2.10	1.30	1.40	1.00	. 90	. 30	. 50	5.40	. 80
30	1.30		3.30	2.00	1.20	1.30	1.30	. 80	. 30	. 50	3.20	. 80
31	1.20		3.20		1.30		1.30	. 80		. 50		. 80

#### MONOCACY RIVER NEAR FREDERICK, MARYLAND.

This station was established August 4, 1896, by E. G. Paul, at the county bridge on the turnpike 4 miles northeast of Frederick, on the road leading from Frederick to Mount Pleasant, Maryland, about 2,000 feet above the mouth of Israel Creek and 3,000 feet below the mouth of Tuscarora Creek. It is described in Water-Supply Paper No. 35, page 93. Records of discharge measurements for 1899 will be found in the Twenty-first Annual Report, Part IV, page 98. During 1900 the following measurements were made by Mr. Paul:

June 29: Gage height, 4.10 feet; discharge, 191 second-feet. September 20: Gage height, 3.80 feet; discharge, 88 second-feet.

Daily gage height, in feet, of Monocacy River near Frederick, Maryland, for 1900.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1	$5.40 \\ 5.40$	$5.10 \\ 5.10$	13.45 12.00	$5.40 \\ 5.70$	$4.70 \\ 4.70$	$4.40 \\ 4.40$	$4.00 \\ 4.00$	$\frac{4.00}{3.90}$	$3.90 \\ 3.80$	$3.90 \\ 3.80$	$3.70 \\ 3.70$	$5.20 \\ 4.30$
3 4	$5.40 \\ 5.20 \\ 5.00$	5.10 5.10	9.50 8.20	5.50 5.50	$4.70 \\ 4.90$	$4.40 \\ 4.40$	3.90 3.90	3.90 3.80	$3.80 \\ 3.70 \\ 2.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ 5.70 \\ $	3.80 3.80	$3.70 \\ 4.10 \\ 10$	$     \begin{array}{r}       4.30 \\       7.20 \\       12 10     \end{array} $
6 		5.20 5.10 5.30	$7.30 \\ 7.10 \\ 8.00$	5.50 5.40 5.30	4.80 4.60 4.50	4.40 4.30 4.20	3.90 3.90 3.80	$3.70 \\ 3.70 \\ 3.70 \\ 3.70$	$3.70 \\ 3.70 \\ 3.70$	3.80 3.70 3.70	4.10 4.00 4.00	12.10 6.00 5.50
8 9	4.50 4.50	$\begin{array}{c} 6.90 \\ 7.55 \\ e.90 \end{array}$	$\begin{array}{c} 7.50 \\ 6.50 \\ e 20 \end{array}$	5.20 5.10 5.10	4.40 4.40	$4.20 \\ 4.20 \\ 4.10$	3.80 3.70 2.70	3.70 3.70 2.70	3.70 3.70 2.60	3.70 3.70 2.70	4.00 3.90	5.20 4.90
$\begin{array}{c}10\\11\\12\\\ldots\end{array}$		5.30 5.50	6.30 5.90	$5.00 \\ 5.00 \\ 5.00$	4.40 4.40 4.40	4.10 4.10 4.10	$     \begin{array}{r}       3.70 \\       3.70 \\       3.70     \end{array} $	3. 60 3. 60 3. 60	3.60 3.60 3.60	$     \begin{array}{r}       3.70 \\       3.70 \\       3.70     \end{array} $	a. 90 3. 90 3. 90	4.30 4.20
13 14 15	$9.20 \\ 5.40 \\ 4.90$	15.10 12.85 7.00	5.70 5.60 5.50	$5.00 \\ 5.00 \\ 5.00 \\ 5.00$	$     \begin{array}{r}       4.30 \\       4.30 \\       4.30     \end{array} $	4.10 4.10 4.40	3.70 3.70 3.70	$3.50 \\ 3.50 \\ 3.50$	3.60 3.60 3.60	3.70 3.90 4.10	3.90 3.90 3.90	4.00
16 17	$4.80 \\ 4.60 \\ 4.60$	$     \begin{array}{r}       6.50 \\       5.90 \\       \hline       5.90 \\       \hline       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\       7.00 \\    $	5.40 5.40 5.40	$4.90 \\ 4.90 \\ 1.90 $	4.30 4.30	$4.80 \\ 5.00$	3.60 3.60	3.50 3.60	3.90 3.90	4.10	3.90 3.90	4.00
18 19 20	4.00 4.90 9.00	5.90 5.80 5.50	5.40 5.40 13.50	5.10 5.20 5.10	$     \begin{array}{r}       4.30 \\       6.50 \\       7.00     \end{array} $	$     \begin{array}{r}       5.80 \\       6.00 \\       5.10     \end{array} $	3.60 3.70 4.60	$3.90 \\ 3.80 \\ 3.80$	3.90 3.90 3.80	3.90 3.80 3.70	3.80 3.80 3.80	$ \begin{array}{c} 4.00 \\ 3.90 \\ 3.90 \end{array} $
21 22 23	9.50 7.05 6.50	5.50 17.15 15.00	10.20 9.10 8.20	$5.00 \\ 5.00 \\ 5.50$	6.50 5.90	4.90 4.50	4.60 3.80	$3.80 \\ 4.80 \\ 4.70$	3.80 3.70 2.60	3.70 3.70 2.80	3.80 3.80	$3.90 \\ 4.00 \\ 4.00$
24 25	$6.00 \\ 5.70$	10.50 8.50	6.50 6.10	$5.60 \\ 5.40$	4.80 4.70	4.20	5.50 4.80	4.10 4.70	3.50 3.50 3.50	3.80 3.80 3.80	3.90 3.90 3.90	4.10
20 27 28	$     \begin{array}{r}       5.50 \\       5.10 \\       4.90     \end{array} $	$   \begin{array}{c}     7.10 \\     6.50 \\     6.50   \end{array} $	$     \begin{array}{r}       6.00 \\       5.90 \\       5.70     \end{array} $	$4.90 \\ 4.80 \\ 4.80$	$     4.60 \\     4.50 \\     4.50 $	4.20 4.20 4.10	$4.20 \\ 4.20 \\ 4.10$	4.00 3.90 5.50	3.50 3.50 3.60	$     \begin{array}{r}       3.70 \\       3.70 \\       3.70 \\       3.70 \\     \end{array} $	$9.20 \\ 7.30 \\ 7.10$	$     \begin{array}{r}       4.10 \\       4.10 \\       4.10     \end{array} $
29 30 31	4.60 4.50 4.50		5.50 5.50 6.50	4.80 4.70	$     4.50 \\     4.50 \\     4.50 $	$4.10 \\ 4.00$	$4.00 \\ 4.00 \\ 4.00$	5.30 4.30 4.00	$3.70 \\ 4.00$	3.70 3.70 3.70	6.90 6.30	4.00
	2.00		0.00				1.00,	1.00		0.10		

ROCK CREEK AT ZOOLOGICAL PARK, DISTRICT OF COLUMBIA.

The first station on Rock Creek was established in 1892, at the request of the Commissioners of the District of Columbia. On January 18, 1897, a new station was established on the bridge of the Zoological Park. This bridge was rebuilt in November, 1900, and the gage was destroyed. A new station will be established in 1901. During 1900 one measurement was made by E. G. Paul, as follows:

April 24: Gage height, 2.75 feet; discharge, 77 second-feet.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oet.	Nov.
1	2.45	2.43	3. 30	2.75	2.60	2.45	2.35	2.35	2.15	2.40	2.10
2	2.43 2.43	$\frac{2.43}{2.38}$	3.25 2.88	$2.70 \\ 2.70$	$\frac{2.60}{2.60}$	2.73 2.60	$\frac{2.35}{2.35}$	$2.28 \\ 2.30$	2.13 2.10	$\frac{2.30}{2.20}$	-2.15 -2.15
4	2.40	2.40	2.78	2.70	2.60	2.55	2.40	2.28	2.10	2.20	2.28
5	2.38	3.03	2.75	2.68	2.60	2.50	2.38	2.25	2.10	2.20	2.35
0	2.40 2.40	$\frac{2.00}{2.53}$	$\frac{2.80}{2.85}$	2 65	2.55	2,40	2.38	2 23	$\frac{2.10}{2.10}$	$\frac{2.20}{2.15}$	2.28
8	2. 40	2.83	2.73	2.65	2.55	2.58	2.35	2.20	2.10	2.25	2.40
9	2.40	2.95	2.70	2.63	2.60	2.45	2.33	2.20	2.10	2.25	2.48
10	2.40	$\frac{2.68}{2.60}$	$\frac{2.68}{2.65}$	2.60	2.63	2.45	2.30	2.20	2.10 2.10	2.20	2.43
12	3.60	2.68	2.70	2.80	2.55	2.35	2.30	2.15	$\tilde{2}.10$	2.20	
13	3.03	3.88	2.70	2.75	2.53	2.45	2.30	2.18	2.10	2.23	
14	2.88	3.00	2.70	2.68	2.50	2.48	2.30	2.15	2.10	2.35	
18	2.53	2.75	$\frac{2.08}{2.70}$	2.65	2.50	2.65	2.30	2.15	$\frac{2.15}{2.65}$	2.30	
17	2.80	2.70	2.78	2.70	2.50	4.30	2.30	2.15	2.40	2.25	
18	2.80	2.70	2.80	2.70	2.50	3.45	2.30	2.15	2.20	2.20	
19 90	2.83	2.10	$\frac{2.80}{3.75}$	3.10	2.90	2.78	2.30	2.10	2.17	2.20	
21	3.13	2.73	3.18	2.73	2.55	2.58	2.40	2.18	2.15	2.20	
22	2.88	5.20	2.85	2.80	2.50	2.55	2.48	2.28	2.15	2.20	
23	2.80	3.30	2.80	2.80	2.50	2.50	2.40	2.23	2.15	2.20	
25	2.68	$\begin{bmatrix} 2.90\\ 2.90\end{bmatrix}$	2.73	2.70	2.50	2.50	2.48	2.48	2.15	2.23	
26	2.60	3.08	2.75	2.70	2.50	2.48	2.35	2.28	2.15	2.18	
27	2.58	3.05	2.80	2.70	2.45	2.48	2.38	2.20	2.15	2.15	
29	2.48	A. 10	2.80	2,60	2.45	2.35	2.30	2.20	2.40	2.10	
30	2.48		2.80	2.60	2.45	2.35	2.30	2.20	2.60	2.10	
31	2.55		2.80		2.40		2.50	2.15		2.10	
					1			1			1

Daily gage height, in feet, of Rock Creek at Zoological Park, District of Columbia, for 1900.

#### APPOMATTOX RIVER AT MATTOAX, VIRGINIA.

This station was established in August, 1900, at the crossing of the Southern Railway, 27 miles southwest of Richmond. The gage rod, which is on the guard rail of the bridge, is laid off to feet and tenths, graduations being indicated by brass nails. The zero of the rod is 58.1 feet from the west end of the bridge, on the upstream side. The outer rim of the pulley is 0.9 foot from the zero of the rod; the distance from the end of the weight to the pointer on the wire rope is 48.75 feet. When the gage reading is 1 foot the water level is 45.6 feet below the top surface of the upper chord of the bridge, upstream side, and at the zero of the gage.

The river here is straight for a considerable distance above the station, but there is an abrupt bend about 100 feet below the bridge. The river is very narrow, and at the low stage at which the gage was placed the current velocity is not very well distributed, there being practically no current for several feet next to the west bank. It was possible, however, to secure a good gaging, and old residents stated that the river was at the lowest stage it had reached in fourteen years. The Mattoax railroad station is located on the west bank of the river, and J. C. Carter, the station agent, is the observer. During 1900 the following measurements were made by E. W. Myers:

August 25: Gage height, 1 foot; discharge, 196 second-feet. November 1: Gage height, 0.85 foot; discharge, 177 second-feet. Daily gage height, in feet, of Appomattox River at Mattoax, Virginia, for 1900.

Day.	Aug.	Sept.	Oct.	Nov.	Dec.	Day.	Aug.	Sept.	Oct.	Nov.	Dec.
1		$\begin{array}{c} 1.25 \\ .50 \\ .35 \\ .38 \\ .05 \\ .13 \\ .15 \\ .15 \\ .17 \\ .17 \\ .13 \\ .03 \\ .06 \\ .06 \\ .03 \\ .03 \\ .06 \\ .03 \\ .03 \\ .06 \\ .03 \\ .03 \\ .06 \\ .03 \\ .05 \\ .03 \\ .03 \\ .05 \\ .03 \\ .03 \\ .03 \\ .05 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 \\ .03 $	$\begin{array}{c} 0.73 \\ .68 \\ .98 \\ .98 \\ .95 \\ .83 \\ .88 \\ 1.60 \\ .95 \\ .83 \\ .88 \\ 1.20 \\ .85 \\ .78 \\ .95 \\ .95 \\ .95 \\ .95 \\ .95 \end{array}$	$\begin{array}{c} 0.80 \\ .90 \\ 1.40 \\ 2.05 \\ 2.90 \\ 2.00 \\ 1.40 \\ 1.20 \\ 1.15 \\ 1.10 \\ 1.00 \\ .95 \\ 1.00 \\ .97 \\ .97 \end{array}$	$\begin{array}{c} 1.10\\ 1.60\\ .99\\ 1.70\\ 5.05\\ 6.50\\ 3.10\\ 2.20\\ 1.95\\ 1.45\\ 1.45\\ 1.25\\ 1.30\\ 1.25\\ 1.30\\ 1.25\\ 1.15\\ \end{array}$	17         18         19         20         21         22         23         24         25         26         27         28         29         29         20         21         22         23         24         25         26         27         28         29         30         31	0.50 0.50 .45 .30 .55 2.50	$\begin{array}{c} 3.75\\ 2.25\\ 1.00\\ .78\\ .60\\ .60\\ .60\\ .73\\ .90\\ .85\\ .60\\ .65\\ .55\\ .65\end{array}$	$\begin{array}{c} 0.90\\ .85\\ .85\\ .750\\ .65\\ .65\\ .70\\ .80\\ 1.65\\ .80\\ .80\\ .75\\ .80\\ .85\end{array}$	$\begin{array}{c} 1.00\\ .86\\ .99\\ .96\\ .93\\ .99\\ 1.05\\ .94\\ .90\\ 1.00\\ 1.90\\ 2.93\\ 1.70\\ 1.20\\ \end{array}$	$\begin{array}{c} 1.\ 00\\ .\ 75\\ 1.\ 75\\ 1.\ 50\\ 1.\ 45\\ 1.\ 00\\ 1.\ 42\\ 3.\ 00\\ 3.\ 92\\ 4.\ 50\\ 3.\ 00\\ 3.\ 30\\ 2.\ 05\\ 2.\ 00\\ 2.\ 35\\ \end{array}$

NORTH (OF JAMES) RIVER AT GLASGOW, VIRGINIA.

This station, which was established August 21, 1895, by C. C. Babb and D. C. Humphreys, is at the East Glasgow county bridge about 1 mile above the mouth of the river. It is described in Water-Supply Paper No. 35, pages 95 and 96. Records of measurements made in 1899 will be found in the Twenty-first Annual Report, Part IV, page 107. During 1900 the following measurements were made by D. C. Humphreys:

March 5: Gage height, 2.18 feet; discharge, 1,234 second-feet. June 26: Gage height, 1.45 feet; discharge, 600 second-feet. August 4: Gage height, 0.71 foot; discharge, 252 second-feet. December 19: Gage height, 1.08 feet; discharge, 398 second-feet.

Daily gage height, in feet, of North (of James) River at Glasgow, Virginia, for 1900.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oet.	Nov.	Dec.
1	0.98	1.20	6.35	2.04	1.40	1.30	1.25	0.78	0.41	0.95	0.90	1.60
3	. 92	1.20	3.75	1.87	1.40	1.40	1.13	:70	.40	. 55	. 90	1.48
4	.95	1.25 1 10	3.25	1.82 1.72	1.35 1.39	1.30	1.10	. 68	.41	. 53	. 95	a 2.89
6	. 90	1.40	$2.50 \\ 2.65$	1.65	1.30	1.00	1.05	. 55	.40	. 50	. 90	3.85
7	. 90	1.30	2.50	1.60	1.22	1.00	1.00	. 52	. 40	. 50	. 86	3.45
9	.09	2.00 2.00	$2.30 \\ 2.28$	1.53 1.50	$1.20 \\ 1.20$	1.00	. 90	. 51	. 34	. 50	. 85	$\frac{5.10}{2.00}$
10	. 90	1.90	2.50	1.45	1.20	1.00	.88	. 50	. 30	. 50	. 85	1.70
12	1.45	1.62	$2.10 \\ 2.06$	1.43	1.10	1.00	. 89 . 80	. 50	. 30	. 50	. 82	$1.58 \\ 1.50$
13	1.75	5.50	1.95	1.40	1.10	2.00	. 75	. 50	.40	. 50	. 80	1.40
14	1.53	+. +0 3. 25	$1.75 \\ 1.65$	1.32 1.32	$1.10 \\ 1.00$	1.40	. 19	. 50	. 40	. 48	. 80	1.33
16	1.35	2.85	1.85	1.28	1.00	4.40	. 70	. 50	2.40	. 45	. 80	1.20
18	1.33 1.36	a 2.40	$\frac{2.03}{1.90}$	1.20	1.00	4.00	$.70 \\ .72$	. əu . 50	$1.10 \\ .60$	. 40	. 18	1.10
19	2.50	2.00	1.90	2.60	2.52	3.30	. 20	. 48	.50	. 48	. 72	1.05
20	6.02	1.93 1.95	4.40	$a \frac{2.52}{2.00}$	1.48	$\frac{2.60}{2.30}$	. 49	.48 .50	. 40	. 40	. 10	1.02 1.00
20	3.21	6.40	3.85	1.45	1.35	1.95	1.30	. 50	. 52	. 46	. 75	1.00
$\frac{23}{24}$	2.15	4.80	$\frac{3.10}{2.82}$	$\frac{3.00}{2.65}$	$1.25 \\ 1.28$	$1.75 \\ 1.50$	1.50 1.10	.48	. 64	1.15	. 76	1.00 1.00
25	1.95	2.95	2.72	2.35	2.50	1.45	. 85	.50	. 60	2.55	.78	. 98
$\frac{26}{27}$	1.76	2.80 2.60	$\frac{2.50}{2.50}$	$\frac{2.15}{2.15}$	$\frac{2.00}{1.65}$	$1.40 \\ 1.35$	1.15 1.30	. 50	.60	-1.45 -1.20	6.35	. 98
28	1.50	2.35	2.38	2.10	1.50	1.25	1.05	. 50	. 52	1.15	2.90	. 95
29	1.55 1.35	•••••	$\frac{2.28}{2.20}$	$\frac{2.00}{1.75}$	1.52	1.22 1.18	. 95	. 50	1.25	1.00	2.25	. 93
31	1.45		2.12		1.30		.88	.45		. 90		. 90

a Interpolated.

#### JAMES RIVER AT BUCHANAN, VIRGINIA.

This station, which was established August 18, 1895, by C. C. Babb and D. C. Humphreys, is located about 20 miles above the mouth of North River and a half mile above the mouth of Purgatory Creek. It is described in Water-Supply Paper No. 35, page 97. Records of measurements for 1899 will be found in the Twenty-first Annual Report, Part IV, page 108. During 1900 the following measurements were made by D. C. Humphreys:

March 30: Gage height, 4.62 feet; discharge, 4,453 second-feet. June 28: Gage height, 2.80 feet; discharge, 1,043 second-feet. August 4: Gage height, 2.25 feet; discharge, 523 second-feet. August 21: Gage height, 1,85 feet; discharge, 374 second-feet. December 20: Gage height, 2.93 feet; discharge, 1,197 second-feet.

Daily gage height, in feet, of James River at Buchanan, Virginia, for 1900.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
Day. 2 3 4 5 6 7 8 9 10	Jan. 2.20 2.20 2.10 2.10 2.10 2.00 2.00 2.0	Feb. 2.40 2.30 2.35 2.55 2.55 2.50 2.95 3.65 3.80	Mar. 6.80 9.25 6.80 5.50 4.90 4.55 4.40 4.40 4.60 4.35	$\begin{array}{c} \textbf{Apr.}\\ \hline \\ 4.40\\ 4.15\\ 4.00\\ 3.90\\ 3.80\\ 3.70\\ 3.60\\ 3.50\\ 3.35\\ 3.20\end{array}$	May. 3.10 3.00 2.90 2.85 2.80 2.80 2.70 2.65 2.50 2.55	June. 2.85 2.75 3.30 5.05 2.90 2.80 2.70 2.70 2.60 2.50	July. 2.70 2.60 2.60 2.50 2.50 2.50 2.40 2.40 2.30 2.20	Aug. 2.40 2.30 2.25 2.10 2.10 2.00 2.00 2.00 1.90	Sept. 1.90 1.90 2.15 2.90 2.80 2.20 1.95 1.80 1.80	Oct. 2.20 2.20 2.20 2.10 2.10 2.10 2.10 2.10 2.10	Nov. 2.50 2.50 2.80 3.45 3.55 3.25 2.95 2.80 2.70 2.60	4.20 3.80 3.70 6.05 9.30 6.25 5.35 4.95 4.75 4.40
11 12 13 14 15 16 17 18 19 20	$\begin{array}{c} 2.40\\ 3.10\\ 4.20\\ 3.55\\ 3.15\\ 2.95\\ 2.80\\ 2.80\\ 3.75\\ 9.30\\ \end{array}$	$\begin{array}{c} 3.50\\ 3.35\\ 6.85\\ 9.20\\ 6.10\\ 5.50\\ 4.55\\ 4.30\\ 3.60\\ 3.35\end{array}$	$\begin{array}{c} 4.20\\ 4.05\\ 3.90\\ 3.75\\ 3.60\\ 3.60\\ 3.50\\ 3.40\\ 3.50\\ 9.50\\ 9.50\end{array}$	$\begin{array}{c} 3.10\\ 3.00\\ 3.00\\ 3.00\\ 2.90\\ 2.80\\ 2.95\\ 4.15\\ 4.90\end{array}$	$\begin{array}{c} 2.50\\ 2.50\\ 2.50\\ 2.40\\ 2.40\\ 2.30\\ 2.25\\ 2.90\\ \end{array}$	$\begin{array}{c} 2.50\\ 2.50\\ 3.10\\ 2.80\\ 4.60\\ 6.30\\ 6.90\\ 4.65\\ 4.65\end{array}$	$\begin{array}{c} 2.20\\ 2.30\\ 2.30\\ 2.20\\ 2.20\\ 2.10\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\$	$\begin{array}{c} 1.90\\ 1.90\\ 1.90\\ 1.90\\ 1.90\\ 1.90\\ 1.90\\ 1.80\\ 1.80\\ 1.80\\ 1.70\\ 1.70\\ \end{array}$	$\begin{array}{c} 1.80\\ 1.70\\ 1.70\\ 1.70\\ 2.10\\ 3.15\\ 3.35\\ 2.60\\ 2.35\\ 2.20\\ 10\end{array}$	$\begin{array}{c} 2.10\\ 2.10\\ 2.10\\ 2.10\\ 2.35\\ 2.70\\ 2.60\\ 2.45\\ 2.30\\ 2.20\\ \end{array}$	$\begin{array}{c} 2.60\\ 2.50\\ 2.50\\ 2.50\\ 2.50\\ 2.40\\ 2.40\\ 2.40\\ 2.40\\ 2.30\\ \end{array}$	$\begin{array}{c} 3.95\\ 3.95\\ 3.80\\ 3.65\\ 3.50\\ 3.35\\ 3.20\\ 3.10\\ 3.10\\ 3.00\\ 2.90\end{array}$
21 22 23 24 25 26 27 27 28 29 29 30 31	$\begin{array}{c} 8.15 \\ 5.60 \\ 4.55 \\ 3.95 \\ 3.30 \\ 3.20 \\ 2.75 \\ 2.55 \\ 2.40 \\ 2.40 \end{array}$	$     \begin{array}{r}       3.30 \\       8.00 \\       7.45 \\       6.40 \\       5.60 \\       4.80 \\       4.35 \\       4.15 \\       \hline     \end{array} $	$\begin{array}{c} 10,30\\ 7,40\\ 5,95\\ 5,20\\ 4,95\\ 4,85\\ 4,80\\ 4,90\\ 4,75\\ 4,60\\ 4,60\\ \end{array}$	$\begin{array}{r} 4.65 \\ 4.70 \\ 5.45 \\ 4.85 \\ 4.40 \\ 4.25 \\ 3.85 \\ 3.70 \\ 3.25 \\ 3.15 \end{array}$	$\begin{array}{c} 2.85\\ 2.65\\ 2.50\\ 2.65\\ 4.50\\ 4.00\\ 3.45\\ 3.20\\ 3.10\\ 3.00\\ 3.00\\ \end{array}$	$\begin{array}{r} 4.15\\ 3.90\\ 3.25\\ 3.05\\ 3.00\\ 2.90\\ 2.80\\ 2.70\\ 2.70\\ 2.70\\ 2.70\end{array}$	$\begin{array}{c} 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.10\\ 3.10\\ 3.20\\ 3.15\\ 3.30\\ 2.75\\ 2.55\end{array}$	$\begin{array}{c} 1.70 \\ 1.70 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.90 \\ 1.90 \\ 1.90 \\ 1.90 \\ 1.90 \\ 1.90 \\ 1.90 \end{array}$	$\begin{array}{c} 2.10 \\ 2.10 \\ 2.20 \\ 2.10 \\ 2.20 \\ 2.10 \\ 2.10 \\ 2.20 \\ 2.20 \\ 2.20 \\ 2.20 \end{array}$	$\begin{array}{c} 2.20 \\ 2.30 \\ 2.95 \\ 10.45 \\ 5.65 \\ 4.10 \\ 2.90 \\ 2.70 \\ 2.60 \\ 2.60 \\ 2.60 \end{array}$	$\begin{array}{c} 2.30 \\ 2.30 \\ 2.30 \\ 2.65 \\ 4.25 \\ 18.60 \\ 12.20 \\ 6.85 \\ 5.50 \\ 4.85 \\ \end{array}$	$\begin{array}{c} 2.90\\ 2.90\\ 2.80\\ 3.05\\ 3.05\\ 3.00\\ 2.90\\ 2.90\\ 2.80\\ 2.80\\ 2.80\end{array}$

#### JAMES RIVER AT CARTERSVILLE, VIRGINIA.

This station, which was established January 1, 1899, by D. C. Humphreys, is located at the highway bridge crossing the James at Cartersville, a half mile from the railroad station and 50 miles above Richmond, Virginia. It is described in Water-Supply Paper No. 35, page 98, together with a number of other gages that have been installed on this river. Records of measurements for the year 1899

#### VIRGINIA.

will be found in Paper No. 35, page 99. During 1900 the following measurements were made by D. C. Humphreys:

April 2: Gage height, 4,74 feet; discharge, 9,469 second-feet. June 30: Gage height, 2.34 feet; discharge, 4,049 second-feet. August 8: Gage height, 0.97 foot; discharge, 1,515 second-feet. August 24: Gage height, 1.00 foot; discharge, 1,405 second-feet. December 22: Gage height, 2.08 feet; discharge, 3,360 second-feet.

Daily gage height, in feet, of James River at Cartersville, Virginia, for 1900.

	Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
	Day.	Jan. 2.00 2.20 2.42 2.42 2.42 2.20 2.10 1.85 1.60 3.65 4.40 4.10 4.10 4.00 3.40 2.80 2.40 4.30 3.40 4.30 3.40 3.40 3.40 4.42 3.42 3.42 3.42 3.42 3.42 3.42 3.42 3.42 3.42 3.42 3.42 3.42 3.42 3.42 3.42 3.42 3.42 3.42 3.42 3.42 3.42 3.42 3.42 3.42 3.42 3.42 3.42 3.42 3.42 3.42 3.42 3.42 3.42 3.42 3.42 3.42 3.42 3.42 3.42 3.42 3.42 3.42 3.42 3.42 3.42 3.42 3.42 3.42 3.42 3.42 3.42 3.42 3.42 3.42 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40	Feb. 2.10 1.75 1.50 2.25 4.35 4.00 3.15 2.90 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.40 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50	$\begin{array}{c} \text{Mar.} \\ \hline \\ 7.80 \\ 15.65 \\ 12.90 \\ 9.50 \\ 7.55 \\ 6.40 \\ 5.10 \\ 5.10 \\ 5.10 \\ 5.10 \\ 5.05 \\ 4.80 \\ 4.40 \\ 4.00 \\ 3.60 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.60 \\ 4.90 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ 3.40 \\ $	Apr. 4.95 4.73 4.73 4.20 4.00 3.50 3.40 3.10 3.10 3.10 3.10 3.10 3.10 3.10 3.10 3.10 3.10 3.10 3.10 3.10 3.10 3.10 3.10 3.10 3.10 3.10 3.10 3.10 3.10 3.10 3.10 3.10 3.10 3.10 3.10 3.10 3.10 3.10 3.10 3.10 3.10 3.10 3.10 3.10 3.10 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2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.55 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1.95\\ 1.95\\ 1.70\\ 1.55\\ 1.70\\ 1.55\\ 1.48\\ 1.47\\ 1.27\\ 1.27\\ 1.25\\ 1.20\\ 1.10\\ 1.10\\ 1.10\\ 1.10\\ \end{array}$	Aug. 1.75 1.53 1.22 1.30 1.15 1.10 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.75 .83 .82 .82 .74 .73 .74 .65 .65 .65 .65 .65 .65 .75 .65 .75 .75 .75 .75 .75 .75 .75 .7	Sept. 0.90 .85 .60 .60 .60 .60 .60 .60 .60 .60	Oct. 1.00 1.00 1.20 1.20 1.20 1.05 1.05 1.05 1.05 1.05 1.05 1.05 1.05 1.05 1.02 1.00 2.30 1.55 1.20 1.20 1.20 1.20 1.20 1.20 1.20 1.20 1.20 1.20 1.20 1.20 1.20 1.20 1.20 1.20 1.20 1.20 1.20 1.20 1.20 1.20 1.20 1.20 1.20 1.20 1.20 1.20 1.20 1.05 1.05 1.05 1.05 1.20 1.20 1.05 1.05 1.20 1.05 1.20 1.05 1.05 1.20 1.20 1.05 1.20 1.05 1.05 1.20 1.20 1.05 1.20 1.20 1.05 1.20 1.20 1.05 1.20 1.20 1.05 1.20 1.20 1.05 1.20 1.20 1.05 1.20 1.20 1.20 1.20 1.05 1.05 1.20 1.20 1.20 1.20 1.20 1.20 1.20 1.20 1.20 1.20 1.20 1.20 1.20 1.20 1.20 1.20 1.20 1.20 1.20 1.20 1.20 1.20 1.20 1.20 1.20 1.20 1.20 1.20 1.20 1.20 1.20 1.20 1.20 1.20 1.20 1.20 1.20 1.20 1.20 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1.20 1.20 1.20 1.20 1.20 1.20 1.20 1.20 1.20 1.20 1.20	Nov. 1.85 1.70 3.03 2.30 2.215 2.000 1.702 1.677 1.553 1.552 1.487 1.447 1.447	Dec. 6.65 3.88 3.33 9.50 11,30 11,15 8.00 5.90 5.55 5.05 4.00 3.52 3.30 3.15 3.10 2.90 2.50 2.237
12222222222233	9 9 1 2 2 3 4 4 5 5 6 7 7 8 9 9 0 1 	$\begin{array}{r} 4.30\\ 13.08\\ 13.00\\ 11.60\\ 7.50\\ 6.10\\ 5.00\\ 4.20\\ 3.65\\ 3.25\\ 3.25\\ 3.00\\ 2.55\\ 2.35\end{array}$	$\begin{array}{c} 4.50 \\ 4.00 \\ 3.80 \\ 8.30 \\ 11.80 \\ 11.25 \\ 9.05 \\ 7.00 \\ 6.00 \\ 5.10 \\ \hline \end{array}$	$\begin{array}{r} 4.20\\ 6.00\\ 10.50\\ 11.75\\ 9.30\\ 7.00\\ 6.00\\ 5.50\\ 5.40\\ 5.30\\ 5.20\\ 5.00\\ 5.30\end{array}$	$\begin{array}{c} 8.20 \\ 7.50 \\ 7.40 \\ 8.50 \\ 7.73 \\ 7.50 \\ 6.40 \\ 5.50 \\ 5.33 \\ 4.57 \\ 4.10 \\ 3.80 \end{array}$	$\begin{array}{c} 2.40\\ 2.75\\ 2.68\\ 2.58\\ 2.50\\ 2.40\\ 3.40\\ 3.35\\ 4.40\\ 3.60\\ 3.10\\ 2.95\\ 2.73\\ 1\end{array}$	$\begin{array}{c} 9.00\\ 7.50\\ 5.50\\ 4.48\\ 3.85\\ 3.50\\ 3.20\\ 3.25\\ 3.10\\ 2.65\\ 2.35\\ \end{array}$	$\begin{array}{c} 1.\ 10\\ 1.\ 21\\ 1.\ 14\\ 1.\ 07\\ 1.\ 17\\ 1.\ 80\\ 1.\ 70\\ 1.\ 40\\ 2.\ 80\\ 2.\ 30\\ 2.\ 25\\ 1.\ 95\\ \end{array}$	$\begin{array}{c} .82\\ .65\\ .70\\ .75\\ .95\\ 1.00\\ 1.25\\ .95\\ .80\\ 1.15\\ 1.10\\ .82\\ 1.03\\ \end{array}$	$\begin{array}{c} 2.17\\ 2.00\\ 1.30\\ 1.15\\ 1.00\\ 1.05\\ 1.03\\ 1.02\\ 1.00\\ 1.00\\ 1.00\\ 1.00\\ \end{array}$	$\begin{array}{c} 1.25\\ 1.15\\ 1.10\\ 1.00\\ 1.20\\ 1.70\\ 10.90\\ 6.98\\ 4.70\\ 3.70\\ 2.75\\ 2.75\\ 2.40\\ \end{array}$	$\begin{array}{c} 1.44\\ 1.40\\ 1.38\\ 1.37\\ 1.34\\ 1.30\\ 1.30\\ 3.40\\ 15.15\\ 18.10\\ 8.00\\ 7.65\\ \end{array}$	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$

#### JAMES RIVER AT HOLCOMB ROCK, VIRGINIA.

This station was established by the Willson Aluminum Company, of Holcomb Rock, Virginia, in 1899, in connection with measurements to determine the horsepower available at that point. During 1899 the records were fragmentary, but at the commencement of 1900 daily records were taken, which have been furnished to the Geological Survey through the courtesy of T. R. Ragland, general manager of the company. The gage consists of a copper float 8 by 8 by 8 inches, with a vertical rod 1[±]/₂ inches square attached to it, the rod, which extends up through the power-house floor, being scaled to tenths of a foot. The copper float is inclosed in a 12-inch by 12-inch by 12-foot box, which rests solidly on the bottom of the river. The box is perforated, so that the water in it will always stand at the same level as the water in the river, while the float, being inclosed, is not in danger of being broken by floating timber. The fluctuations of the river are read directly from the rod, which moves up or down with the float as it responds to the variations in the height of the river. Measurements of discharge are not made at this point.

Daily gage height, in feet, of James River at Holcomb Rock, Virginia, for 1900.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1	$1.40 \\ 1.40$	$1.70 \\ 1.50$	$7.90 \\ 9.85$	$3.60 \\ 3.45$	$2.30 \\ 2.20$	$1.90 \\ 1.80$	$1.65 \\ 1.70$	$1.00 \\ 1.00$	0.60	0.60 .60	$1.35 \\ 1.30$	$2.40 \\ 2.25$
3 4 5	$1.30 \\ 1.30 \\ 1.10$	$1.50 \\ 1.60 \\ 1.80$	$7.70 \\ 5.65 \\ 4.75$	$   \begin{array}{r}     3.15 \\     3.05 \\     2.75   \end{array} $	2.20 2.00 2.00	3.50 2.10 1.80	$1.55 \\ 1.60 \\ 1.45$	. 95 . 95 95	.60 .60 .60	.60 .65 .60	1.30 1.30 2.20	$2.15 \\ 4.60 \\ 9.30$
6	$1.28 \\ 1.30 \\ 1.25$	1.60 1.50 1.50	4.10 3.85 2.05	2.60 2.50 2.40	$     \begin{array}{c}             2.00 \\             1.95 \\             1.80         \end{array}     $	1.70 1.70 1.70	1.40 1.40 1.40 1.20	1.05 .90	. 60 . 60 . 60	$.60 \\ .70 \\ .75$	1.80 1.60	5.70
9 10	1.28 1.28 1.23	$   \begin{array}{c}     1.65 \\     2.43 \\     2.50 \\     9.50   \end{array} $	3.85 3.60	2.35 2.20 2.10	1.80 1.80 1.80 1.80	1.60 1.60 1.65 1.65	1.30 1.20 1.20	.90	. 60 . 60 . 60	.70 .90	1.40 1.40 1.30 1.95	3.35 3.10
11 12 13	$1.28 \\ 1.75 \\ 2.58 \\ $	2.50 5.30 10.45	3. 30 3. 30 2. 95	2.10 2.10 2.05	$     \begin{array}{c}       1.70 \\       1.70 \\       1.70     \end{array} $	1.00 1.40 2.35	$1.15 \\ 1.15 \\ 1.20$	. 80 . 80 . 85	. 60 . 60 . 50	. 80 . 80 . 80	$1.50 \\ 1.20 \\ 1.20$	2.45
14 15 16	2.65 2.30 2.03		2.80 2.60 2.65	$     \begin{array}{r}       2.00 \\       1.80 \\       1.80     \end{array} $	1.75 1.60 1.60	$2.40 \\ 2.05 \\ 4.50$	$1.10 \\ 1.10 \\ 1.00$	. 80 . 70 . 55	.30 .30 2.15	$1.00 \\ 1.00 \\ 1.30$	$1.20 \\ 1.10 \\ 1.10$	$   \begin{array}{c}     2.15 \\     2.00 \\     1.85   \end{array} $
$17 \\ 18 \\ 19 \\ \\ 19 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ \\ 10 \\ .$	$     \begin{array}{r}       1.83 \\       1.70 \\       3.50     \end{array} $	$ \begin{array}{r} 4.10 \\ 3.30 \\ 2.80 \end{array} $	$2.60 \\ 2.55 \\ 2.60$	$     \begin{array}{r}       1.80 \\       3.55 \\       4.35     \end{array} $	$     \begin{array}{r}       1.60 \\       1.60 \\       1.85     \end{array} $	$\begin{array}{c c} 6.10 \\ 6.90 \\ 6.15 \end{array}$	. 90 . 90 . 90	.50 .45 .40	$     \begin{array}{r}       1.90 \\       1.30 \\       .95     \end{array} $	$1.15 \\ 1.05 \\ 1.00$	$     \begin{array}{r}       1.10 \\       1.10 \\       1.10     \end{array} $	$     \begin{array}{c}       1.80 \\       1.70 \\       1.60     \end{array} $
20 · · · · · · · · · · · · · · · · · · ·	9,85 9,30 6,00	2.55 2.40 8.10	$7.95 \\ 11.00 \\ 8.00$	$4.70 \\ 4.80 \\ 5.85$	$     \begin{array}{r}       1.90 \\       2.25 \\       1.80     \end{array} $	5.35 3.40 2.75	. 90 . 90 . 90	.70 .45 .60	.60 .50 .50	$1.00 \\ 1.00 \\ 1.00$	$ \begin{array}{c c} 1.10 \\ 1.00 \\ 1.00 \end{array} $	$     \begin{array}{r}       1.60 \\       1.50 \\       1.50     \end{array} $
23 24 25	$\frac{4.33}{3.45}$	9.35 7.05 5.65	5.95 4.90 4.45	$5.45 \\ 4.60 \\ 1.00$	$1.65 \\ 1.80 \\ 2.95$	$2.45 \\ 2.40 \\ 2.30$	1.10 1.10 1.35	$.75 \\ .60 \\ .70$	.60 .70 .55	$1.00 \\ 10.10 \\ 5.55$	.95 .90 .90	1.50 1.50 1.50
26 27 20	2.50	$\frac{4.65}{3.90}$	4.40 4.15 4.10	3.55 3.20	$     \begin{array}{c}       3.45 \\       2.95 \\       2.35     \end{array} $	1.95 1.80 1.75	$1.90 \\ 1.60 \\ 1.80$	.70	. 60 . 60 . 60			1.50 1.55 1.60
29 30 21	1.90 1.55 1.60	0.00	4.10	2.50 2.50 2.50	2.20 2.20 2.20 1.05	$1.70 \\ 1.55$	1.60 1.60 1.50 1.25	. 60 . 60	. 50 . 50 . 50	1.90 1.55 1.50	4.20 3.25	1.50 1.50 1.50 1.50
01	1.00		ə. 40		1,95		1.55	. 00		1.00		1.50

#### ROANOKE RIVER AT ROANOKE, VIRGINIA.

This station, which was established by D. C. Humphreys, July 11, 1896, is located at the edge of the city of Roanoke, on the Walnut street car line. It is described in Water-Supply Paper No. 36, page 107, and record of discharge measurements for 1899 will be found in the Twenty-first Annual Report, Part IV, page 110. During 1900 the following measurements were made by D. C. Humphreys:

March 29: Gage height, 2.07 feet: discharge, 879 second-feet. May 5: Gage height, 1.30 feet; discharge, 298 second-feet. June 26: Gage height, 2.16 feet; discharge, 639 second-feet. July 30: Gage height, 0.91 foot; discharge, 149 second-feet. August 21: Gage height, 0.65 foot; discharge, 92 second-feet. December 19: Gage height, 1.28 feet; discharge, 307 second-feet.
## VIRGINIA AND NORTH CAROLINA.

Daily gage height, in feet, of Roanoke River at Roanoke, Virginia, for 1900.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oet.	Nov.	Dec.
1	1.70	1.10	3.80 3.10	1.85	1.50	1.20 1.13	1.50	0.90	0.65	0.80	1.40 1.50	1.58
3	1.80 1.80	1.10	3.10 2.50	1.72	1.40 1.45	$1.15 \\ 1.15$	$1.40 \\ 1.30$	. 85	. 65	1.00	1.65	1.50
4	1.70	1.05	2.10	1.65	1.40	1.10	1.70	.80	. 65	1.10	1.75	4.43
ð 6	1.15	1.20	$\frac{2.00}{1.88}$	$1.58 \\ 1.50$	1.54	$1.00 \\ 1.03$	1.89 1.60	. 80	. 00 65	$1.13 \\ 1.10$	1.49	-3.10 -2.60
7	. 80	1.15	1.77	1.45	1.22	1.03	1.40	. 75	. 65	1.05	1.20	2.20
8	. 75	1.10	1.70	1.45	1.20	1.10	1.25	. 70	. 65	1.05	1.15	2.00
9	. 10 85	$1.10 \\ 1.10$	1.95	1.40	1.20 1.35	1.20 1.15	1.19 1.10	. 70	- 60 - 60	1.00	$1.10 \\ 1.07$	1.80 1.72
11	.90	1.30	a 1.80	1.38	1.20	1.10	1.05	. 65	. 60	. 90	1.05	1.62
12	1.20	1.45	1.75	1.40	1.18	1.15	1.00	. 65	. 60	. 85	1.05	1.55
13	1.35	$\frac{4.60}{3.08}$	1.70	1.40	1.15	1.40 1.85	1.00 .97	. 63	. 60	1.80	1.03	1.48
15	1.20	2.32	1.75	1.30	1.08	1.35	. 95	. 63	1.10	1.35	1.00	1.38
16	1.15	1.95	1.72	1.27	1.05	1.60	. 95	. 60	2.00	1.15	1.00	1.34
18	• 1.10 • 1.10	1.48 1.60	1.40	1.30	1.03 1.03	2.15	. 95	. 60	1.00	1.00	1.00	1.30 1.31
19	1.20	1.48	2.05	3.75	b1.05	1.75	. 90	. 65	.80	. 95	1.00	1.25
20	4.10	1.40	4.45	2.65	b1.05 b1.10	1.55	. 90	. 65	. 70	.90	1.00	1.21 1.25
22 22	$\frac{2.00}{2.00}$	3.80	2.75	2.95	b1.10 b1.10	$1.40 \\ 1.30$	.87	. 65	. 80	. 85	1.00	1.29
23	1.72	2.85	2.35	2.55	b1.50	1.30	. 90	. 65	1.15	. 90	1.00	1.27
24	1.55	1.40	2.15 1.05	2.25	$\frac{2.40}{1.85}$	1.30	1.05	. 65	. 95	4.75	$1.00 \\ 05$	1.42
26	1.40 1.30	$\tilde{1}.90$	2.05	1.90	$1.05 \\ 1.45$	$\frac{1.60}{2.60}$	$1.05 \\ 1.25$	. 70	.80	1.95	8.20	1.35
27	1.20	1.75	2.25	1.78	1.30	1.45	1.05	. 65	. 75	1.75	2.90	1.30
28	1.10 1.10	1.65	2.40	1.65 1.60	$\frac{1.25}{2.00}$	2.45	1.00	. 65	. 70	1.55 1.50	1 95	$1.28 \\ 1.28$
30	1.08		2.03	1.55	$\tilde{1.60}$	1.70	. 90	. 65	. 60	1.45	1.75	1.24
31	1.05		1.98		1.35		. 90	. 65		1.40		1.28
			1						1			

a Interpolated.

b Estimated; repairing bridge.

This station is described in Water-Supply Paper No. 36, page 109. The river bed is muddy and is likely to cut out in seasons of high water, and both banks are subject to overflow, sometimes covering the flood plain of the river to a depth of 10 or more feet and reaching at times a width of nearly 2 miles. The highest recorded water at this station occurred on March 23, 1899, when the gage reached a height of 30 feet and the discharge was probably 83,000 second-feet; the lowest recorded water was from September 19 to 22, 1897, when the gage read 0.00 and the discharge was probably 2,000 second-feet, making the maximum flow  $41\frac{1}{2}$  times the minimum flow. The drainage area above the station is 8,817 square miles, largely forest covered and including a variety of topographic forms, from the mountains of the upper part of Dan and Staunton rivers to the extensive swamps to be found along the lower part of the basin. The stream is subject to sudden rises and falls, but the period of high water lasts several days. The observer is the bridge watchman, W. M. Adams, of Kelford, North Carolina. Records of measurements will be found as follows: For 1896, Eighteenth Annual Report, Part IV, page'48; for 1897, Nineteenth Annual Report, Part IV, page 181; for 1898, Twentieth Annual Report, Part IV, page 142; for 1899, Twenty-first Annual Report, Part IV, page

ROANOKE RIVER AT NEAL, NORTH CAROLINA.

111. During 1900 the following measurements were made by E. W. Myers:

February 10: Gage height, 9.70 feet; discharge, 9,361 second-feet. April 10: Gage height, 7.10 feet; discharge 6,266 second-feet. April 11: Gage height, 6.90 feet; discharge, 6,002 second feet. April 24: Gage height, 25.60 feet: discharge, 49,896 second-feet. May 11: Gage height, 4.69 feet; discharge, 5,503 second-feet. June 30: Gage height, 10.12 feet; discharge, 9,530 second-feet. August 10: Gage height, 1.40 feet; discharge, 2,342 second-feet. November 2: Gage height, 3.18 feet; discharge 3,734 second-feet.

Daily gage height, in feet, of Roanoke River at Neal, North Carolina, for 1900.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1	2.10	7.80	16.40	12.20	12.90	5.80	9.15	7.40	2.15	1.80	3. 70	8.70
9	2.10	6.70 5.00	18.50	11.60 11 10	11.50 10.40	5.40 5.20	$\frac{8.10}{7.20}$	$\frac{4.80}{3.30}$	2.50	2.60	$\frac{3.20}{2}$	6.50
4	2.20	4.30	23.10	10.20	9.60	4.80	6.30	2.70	1.20	1.20	4.00	4.60
5	2.20	4.60	24.65	9.50	8.80	4.50	5.30	2.60	. 70	1.25	6.40	4.70
6	3.50	6.80	23.80	9.00	8.10	4.20	4.50	2.25	. 40	1.45	7.80	11.75
7	$\frac{4.30}{1.20}$	12.70	$\frac{21.50}{10.00}$	8.50	7.60	$\frac{4.50}{4.50}$	$\frac{4.00}{2.70}$	1.90	. 40	1.40	9.00	20.75
0 Q	4.30	11 10	17.30	$\frac{0.10}{7.50}$	7 00	4.30	3 70	1.00	30	1.00	6.50	14 60
10	4.50	9.75	17.70	7.20	7.10	4.20	3.40	1.30	.70	2.90	5.10	11.80
11	5.10	9.90	18.10	6.90	7.00	4.10	3.00	1.20	. 50	3,50	4.20	9.40
12	7.00	11.10	18.30	6.90	6.60	4.20	2.90	1.00	. 20	3.20	3.70	7.70
13	12.00	13.10	17.30 15.20	8.50	6.30 5.00	4.15	3.10	. 90	. 10	3.20	3,40 2 10	6.60
1±	19.00	22 50	13.60	10.20	5.50	4 10	2.50	. 60	. 30	2.10	2.85	5.80
16	17.60	23.88	12.70	9.70	5.20	7.60	2.30	.40	.40	1.70	2.80	4.70
17	14.30	23.90	12.10	8.50	4.80	9.90	2.80	. 40	.10	2.80	2.70	4.30
18	11.70	22.80	13.40	1.50	4.70	11.20	2.50	. 60	1.80	3.90	2.50	4.20
19	10.20	19.70 17.00	14.40	1.10	4.95	17.40 16.10	2.00	. 40	12.40	3.70	2.40	3.85
20	9.00	14 20	14.10 13.40	23 40	$\frac{5.10}{7.80}$	10.10 12.90	1.50	. 40	9.20	2.90	2.25	3.70
90 20	21.25	13.60	13.90	24.63	7.60	9.80	1.40	.40	3.80	1.70	2.20	4.40
23	23.40	14.60	15.80	25.95	6.70	8.00	1.40	. 40	2.50	1.50	2.28	4.90
24	23.50	21.65	15.30	25.55	5.90	6.70	1.50	. 70	1.30	1.35	2.35	5.40
25	21.60	22.30	13.50	24.20	6.00	6.30	6.00	.90	1,45	1.20	2.50	6,40
20 97	15.00	20.95	13.70	20.00	14 70	15.20	9.60	2.10	1.00	0,00 15 40	2.00	8 20
28	18.10	18,80	14.30	18,40	13.70	13.00	10.45	1.50	$\frac{1.60}{2.40}$	11.80	3.00	7.90
29	11.70		14.20	16.00	10.40	12.00	13.60	1.10	2.50	8.50	11.60	6.95
30	10.40		13.40	14.30	8.00	10.45	13.45	1.10	2.50	6.10	11.40	5.90
31	9.10		13.30		6.70		10.40	1.40		4.60		5,90
	1		1	1	U.		12		1			

## DAN RIVER AT SOUTH BOSTON, VIRGINIA.

This station, which was established August 27, 1900, by E. W. Myers, is located in the town of South Boston, Virginia, on the railroad bridge of the Norfolk and Western Railroad which crosses the river at that place. The gage rod is laid off on the downstream guard rail of the bridge, the graduations being indicated by brass nails driven into the rail. The zero of the rod is exactly over the center of the first span from the north end of the bridge. The distance between the zero of the rod and the outer rim of the pulley is 2.39 feet, and the distance between the end of the weight and the pointer on the wire rope is 36.44 feet. When the gage reading is 1 foot the water surface is 31.06 feet below the top of the head of the nut on the pin connecting the two tension rods with the lower chord of the bridge, this pin being on the lower side of the bridge and exactly opposite the zero of the gage. This is a very good station for

#### VIRGINIA.

the gaging of all except the very highest stages of flow. At extreme heights the river spreads out over a flood plain of considerable width. The trestle connecting the bridge with the embankment on the south side of the river is a curve of rather high degree. The bed of the stream is of coarse sand and probably shifts only slightly. R. M. Taliaferro, South Boston, Virginia, is the observer. During 1900 the following measurements were made by E. W. Myers:

August 27: Gage height, 1.00 foot; discharge, 1,046 second-feet. October 31: Gage height, 2.20 feet; discharge, 1,576 second-feet.

Daily gage height, in feet, of Dan River at South Boston, Virginia, for 1900.

Day.	Sept.	Oct.	Nov.	Dec.	Day.	Sept.	Oct.	Nov.	Dec.
1	$\begin{array}{c} 0.62\\ .55\\ .95\\ .95\\ .95\\ .96\\ .97\\ .90\\ .37\\ .90\\ .40\\ .50\\ .40\\ .45\\ .40\\ 4.90 \end{array}$	$\begin{array}{c} 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.40\\ 1.90\\ 2.40\\ 2.40\\ 2.20\\ 2.30\\ 2.00\\ 2.00\\ 2.00\\ \end{array}$	$\begin{array}{c} 2.00\\ 2.20\\ 2.00\\ 2.40\\ 2.50\\ 2.50\\ 2.50\\ 2.50\\ 2.40\\ 2.00\\ 2.00\\ 1.90\\ 1.90\\ 1.80\end{array}$	$\begin{array}{c} 3,00\\ 3,00\\ 4,00\\ 4,00\\ 4,10\\ 8,00\\ 3,80\\ 3,80\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\ 3,20\\$	17         18         19         20         21         22         23         24         25         26         27         28         29         30         31	$\begin{array}{c} 8,55\\ 3,600\\ 2,000\\ 1,65\\ 1,25\\ 1,55\\ 1,30\\ 1,70\\ 1,70\\ 1,50\\ 1,60\\ 1,40\\ 1,30\\ 1,30\\ \end{array}$	$\begin{array}{c} 2.\ 40\\ 2.\ 40\\ 2.\ 00\\ 1.\ 90\\ 2.\ 00\\ 2.\ 00\\ 2.\ 30\\ 4.\ 50\\ 3.\ 50\\ 2.\ 50\\ 2.\ 50\\ 2.\ 00\\ 2.\ 00\\ 2.\ 00 \end{array}$	$\begin{array}{c} 1.70\\ 1.70\\ 1.70\\ 1.70\\ 1.70\\ 1.60\\ 1.60\\ 1.60\\ 2.20\\ 5.60\\ 3.20\\ 3.20\\ 3.00\\ \end{array}$	$\begin{array}{c} 3,00\\ 3,00\\ 2,90\\ 3,00\\ 3,10\\ 3,10\\ 3,10\\ 3,00\\ 3,00\\ 3,00\\ 3,00\\ 2,70\\ 2,80\end{array}$

#### STAUNTON RIVER AT RANDOLPH, VIRGINIA.

This station, which was established August 27, 1900, by E. W. Myers, is about five-eighths of a mile southwest of Randolph station, on the line of the Southern Railway from Richmond to Danville, on the railroad bridge which crosses the river at that place. The rod is laid off on the guard rail of the bridge on the downstream side, the graduations to feet and tenths being indicated by brass tacks. The zero of the gage rod is over the center of the fifth floor beam of the second span from the north end of the bridge. The distance between the zero of the rod and the outer rim of the pulley is 3.66 feet; the distance between the end of the weight and the pointer on the wire rope is 41.13 feet. When the gage reading is 1 foot the water surface is 34.85 feet below the top surface of the fifth floor beam, directly under the zero of the gage. The river is straight for a long distance above and below the bridge, and the velocity of the current is very well distributed. It is said that the rise at this point is about 25 feet. It is not probable that the channel changes to any degree during high water. The observer at this station is Justin Field, station agent at Randolph. During 1900 the following measurements were made by E. W. Myers:

August 27: Gage height, 1.00 foot; discharge, 1,349 second-feet. October 31: Gage height, 2.75 feet; discharge, 2,304 second-feet.

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Daily gage height, in feet, of Staunton River at Randolph, Virginia, for 1900.

Day.	Sept.	Oct.	Nov.	Dec.	Day.	Sept.	Oct.	Nov.	Dec.
1	$\begin{array}{c} 1.00\\ 1.00\\ 75\\ .70\\ .75\\ 2.00\\ 1.00\\ .80\\ .70\\ .50\\ .50\\ .40\\ .30\\ .30\\ 1.00\\ .910\end{array}$	$\begin{array}{c} 1.30\\ 1.35\\ 1.60\\ 1.55\\ 2.00\\ 1.80\\ 1.60\\ 1.80\\ 1.60\\ 1.80\\ 2.00\\ 1.65\\ 1.00\\ 1.55\\ 2.05\\ 2.05\\ 2.05\\ 2.55\\ 2.05\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\ 2.55\\$	$\begin{array}{c} 2.60\\ 2.50\\ 2.80\\ 4.40\\ 4.60\\ 3.195\\ 2.555\\ 2.60\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2.555\\ 2$	$\begin{array}{c} 3.\ 70\\ 3.\ 30\\ 3.\ 05\\ 4.\ 75\\ 15.\ 50\\ 10,\ 50\\ 4.\ 80\\ 4.\ 35\\ 4.\ 00\\ 3.\ 75\\ 3.\ 60\\ 3.\ 40\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 30\\ 3.\ 3$	17           18           20           21           22           23           24           25           26           27           28           29           30           31	$\begin{array}{c} 6.90\\ 3.30\\ 2.05\\ 1.60\\ 1.35\\ 1.30\\ 1.40\\ 1.35\\ 2.50\\ 2.00\\ 1.50\\ 1.40\\ 1.55\\ 1.40\\ \end{array}$	$\begin{array}{c} 2.05\\ 1.70\\ 1.50\\ 1.45\\ 1.40\\ 1.35\\ 1.50\\ 6.10\\ 15.15\\ 6.10\\ 4.50\\ 3.30\\ 3.00\\ 2.75\end{array}$	$\begin{array}{c} 2.30\\ 2.30\\ 2.25\\ 2.30\\ 2.33\\ 2.35\\ 2.30\\ 2.25\\ 3.10\\ 12.40\\ 6.50\\ 4.75\\ 4.00\\ \end{array}$	$\begin{array}{c} 3.00\\ 3.00\\ 3.00\\ 3.05\\ 3.15\\ 3.50\\ 3.70\\ 5.70\\ 4.80\\ 4.80\\ 3.50\\ 3.50\\ 3.50\\ 3.30\\ 3.95\end{array}$

#### TAR RIVER AT TARBORO, NORTH CAROLINA.

This station is described in Water-Supply Paper No. 36, page 110. Extensive sand bars have formed in the channel during periods of extreme low water, and they modify very materially the relation between the gage height and the discharge at low stages of the river. The highest recorded flood was on February 11, 1899, when the gage height was 25 feet and the discharge was probably 19,850 second-feet. The lowest recorded flow was on November 2, 1900, the discharge being 87 second-feet, the maximum flow thus being about 218 times the minimum flow. The observer is R. H. Williams, who reads the gage once a day during ordinary stages of the river, but oftener during floods. Measurements of discharge are made at the station and occasionally at the highway bridge crossing the stream about 200 yards above, as the lower section is sometimes obstructed by rafts of logs. Records of flow during 1899 will be found in the Twentyfirst Annual Report, Part IV, page 112. During 1900 the following measurements were made by E. W. Myers:

April 11: Gage height, 4.48 feet; discharge, 1,915 second-feet. April 23: Gage height, 14.90 feet; discharge, 10.237 second-feet. May 18: Gage height, 2.18 feet; discharge, 1,003 second-feet. June 30: Gage height, 2.30 feet, discharge, 1,030 second-feet. August 9: Gage height, 0.40 foot, discharge, 371 second-feet. November 2: Gage height, -0.30 foot; discharge, 87 second-feet. November 21: Gage height, 0.50 foot; discharge, 412 second-feet.

#### NORTH CAROLINA.

Daily gage height, in feet, of Tar River at Tarboro, North Carolina, for 1900.

$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1           2           3           4           5           6           7           8           9           10           11           12           13           14           15           16           17           18           19           20           21           22           23           24           25           26           27           28           29           30	$\begin{array}{c} 3.709.6564543433745532976568903452333443333905536899034506556891097655644526689109765554452668910976555445266891097655568910976555689109765556891097655568910976555689109765556891097655568910976555689109765556891097655568910976556891097655689109765556891097655568910976556891097655689109765556891097655689109766556891097665668910976655668910976656689109766566891097665668910976656689109666666666666666666$	$\begin{array}{c} 4.0\\ 3.8\\ 3.7\\ 3.6\\ 3.5\\ 4.8\\ 6.0\\ 5.9\\ 5.4\\ 5.0\\ 6.1\\ 7.8\\ 10.6\\ 12.8\\ 17.0\\ 6\\ 12.8\\ 15.8\\ 17.0\\ 16.5\\ 13.7\\ 9.80\\ 10.0\\ 11.5\\ 9.80\\ 13.9\\ 13.7\\ 12.6\\ 6\\ 11.9\\ \end{array}$	$\begin{array}{c} 10.0 \\ 10.5 \\ 12.3 \\ 13.5 \\ 14.5 \\ 13.0 \\ 10.5 \\ 3.7 \\ 9.0 \\ 11.2 \\ 4.5 \\ 9.5 \\ 7.5 \\ 12.2 \\ 4.5 \\ 9.5 \\ 7.5 \\ 1.5 \\ 6.0 \\ 1 \\ 6.3 \\ 9.5 \\ 10.0 \\ 9.1 \\ 0 \\ 10.5 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ $	$\begin{array}{c} \textbf{8.6}\\ \textbf{9.01}\\ \textbf{8.7.6}\\ \textbf{9.01}\\ \textbf{8.5.5}\\ \textbf{5.30}\\ \textbf{5.30}\\ \textbf{5.5.0}\\ \textbf{5.5.0}\\ \textbf{5.5.0}\\ \textbf{5.5.0}\\ \textbf{5.5.0}\\ \textbf{5.5.0}\\ \textbf{8.7.2}\\ \textbf{6.04}\\ \textbf{10.82}\\ \textbf{5.8}\\ \textbf{11.06}\\ \textbf{8.7.2}\\ \textbf{6.04}\\ \textbf{10.82}\\ \textbf{5.6}\\ \textbf{6.4}\\ \textbf{10.82}\\ \textbf{5.6}\\ \textbf{6.6}\\ \textbf{4} \end{array}$	$\begin{array}{c} 0 \\ 5.4.56 \\ 4.4.30 \\ 7.4.4.4.03 \\ 3.3.3.60 \\ 1.8.5.4.2.00 \\ 3.3.2.2.2.2.4.50 \\ 4.5.4.4.33 \\ 4.5.5.4.33 \\ 3.4.5.5.4.33 \\ 3.3.4.5.5.4.33 \\ 3.3.4.5.5.4.33 \\ 3.3.4.5.5.4.33 \\ 3.3.4.5.5.4.33 \\ 3.3.4.5.5.4.33 \\ 3.3.4.5.5.4.33 \\ 3.3.4.5.5.4.33 \\ 3.3.4.5.5.4.33 \\ 3.3.4.5.5.4.33 \\ 3.3.4.5.5.4.33 \\ 3.3.4.5.5.4.33 \\ 3.3.4.5.5.4.33 \\ 3.3.4.5.5.4.33 \\ 3.3.4.5.5.4.33 \\ 3.3.4.5.5.4.33 \\ 3.3.4.5.5.4.33 \\ 3.3.4.5.5.4.33 \\ 3.3.4.5.5.4.33 \\ 3.3.4.5.5.4.33 \\ 3.3.4.5.5.4.33 \\ 3.3.4.5.5.4.33 \\ 3.3.4.5.5.4.33 \\ 3.3.4.5.5.4.33 \\ 3.3.4.5.5.4.33 \\ 3.3.4.5.5.4.33 \\ 3.3.4.5.5.4.33 \\ 3.3.4.5.5.4.33 \\ 3.3.4.5.5.4.33 \\ 3.3.4.5.5.4.33 \\ 3.3.4.5.5.4.33 \\ 3.3.4.5.5.4.33 \\ 3.3.4.5.5.4.33 \\ 3.3.4.5.5.4.33 \\ 3.3.4.5.5.4.33 \\ 3.3.4.5.5.4.33 \\ 3.3.4.5.5.4.33 \\ 3.3.4.5.5.4.33 \\ 3.3.4.5.5.4.33 \\ 3.3.4.5.5.4.33 \\ 3.3.4.5.5.4.33 \\ 3.3.4.5.5.4.33 \\ 3.3.4.5.5.4.33 \\ 3.3.4.5.5.4.33 \\ 3.3.4.5.5.4.33 \\ 3.3.4.5.5.4.33 \\ 3.3.4.5.5.4.33 \\ 3.3.4.5.5.4.33 \\ 3.3.4.5.5.4.33 \\ 3.3.4.5.5.4.33 \\ 3.3.5.4.5.5.4.33 \\ 3.3.5.5.4.33 \\ 3.3.5.5.4.33 \\ 3.3.5.5.4.33 \\ 3.3.5.5.5.4.33 \\ 3.3.5.5.5.4.33 \\ 3.3.5.5.5.4.33 \\ 3.3.5.5.5.5.5.5.5.5 \\ 3.3.5.5.5.5.5.5.5.5 \\ 3.3.5.5.5.5.5.5.5.5 \\ 3.3.5.5.5.5.5.5.5.5 \\ 3.3.5.5.5.5.5.5.5.5.5.5 \\ 3.3.5.5.5.5.5.5.5.5.5.5 \\ 3.3.5.5.5.5.5.5.5.5.5.5.5.5.5.5 \\ 3.3.5.5.5.5.5.5.5.5.5.5.5.5.5.5.5.5.5.5$	$\begin{array}{c} 2.6\\ 2.10\\ 1.132\\ 1.35\\ 1.255\\ 1.32\\ 1.35\\ 1.40\\ 1.455\\ 5.435\\ 5.53\\ 4.55\\ 4.35\\ 5.5\\ 4.35\\ 5.45\\ 5.5\\ 4.3\\ 2.6\\ 5.5\\ 4.3\\ 2.6\\ 5.5\\ 5.5\\ 4.3\\ 2.6\\ 5.5\\ 5.5\\ 3.2\\ 5.5\\ 5.5\\ 5.5\\ 5.5\\ 5.5\\ 5.5\\ 5.5\\ 5$	$\begin{array}{c} 2.03\\ 1.35\\ 1.60\\ 1.11\\ .76\\ .76\\ .43\\ .22\\ .164\\ .32\\ .164\\ .32\\ .10\\ .00\\ .00\\ .00\\ .50\\ 1.25\\ .32\\ .10\\ .00\\ .00\\ .00\\ .00\\ .00\\ .00\\ .00$	$\begin{array}{c} 1.7\\ 1.3\\ 1.6\\ 1.8\\6\\5\\1\\ 0\\0\\0\\0\\0\\0\\0\\ $	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} -0.323\\ -0.323\\ -1.77\\ 33455\\ 3.455\\ 3.455\\ -1.43\\ 0.6\\ -4.42\\ -2.77\\ -4.2\\ -3.4\\ -3.3\\ -1.3\\ -3.4\\ -3.3\\ -1.3\\ -3.4\\ -3.3\\ -1.3\\ -3.4\\ -3.3\\ -3.4\\ -3.3\\ -3.4\\ -3.3\\ -3.4\\ -3.3\\ -3.4\\ -3.3\\ -3.4\\ -3.3\\ -3.4\\ -3.3\\ -3.4\\ -3.3\\ -3.4\\ -3.3\\ -3.4\\ -3.3\\ -3.4\\ -3.3\\ -3.4\\ -3.3\\ -3.4\\ -3.3\\ -3.4\\ -3.3\\ -3.4\\ -3.3\\ -3.4\\ -3.3\\ -3.4\\ -3.3\\ -3.4\\ -3.3\\ -3.4\\ -3.3\\ -3.4\\ -3.3\\ -3.4\\ -3.3\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -3.4\\ -$	$\begin{array}{c} 0.88\\ .77\\ .63\\ .32\\ .12\\ .30\\ .21\\ .12\\ .22\\ .22\\ .22\\ .22\\ .22\\ .22$

### NEUSE RIVER AT SELMA, NORTH CAROLINA.

This station is described in Water-Supply Paper No. 36, page 111. The maximum flood of which there is any record was on February 9, 1899, when the water reached a height of 21 feet on the gage, with a probable discharge of 12,000 second-feet. The minimum flow occurred during the very severe drought of 1897, the lowest gage height being -0.4 foot, on October 17 and 18, and the discharge 75 second-feet, making the maximum flow about 160 times the minimum flow. The drainage area above the station is 1,175 square miles. Records of flow during 1899 will be found in the Twenty-first Annual Report, Part IV, page 114. During 1900 the following measurements were made by E. W. Myers:

February 8: Gage height, 3.40 feet; discharge, 1,117 second-feet. April 12: Gage height, 3.80 feet; discharge, 1,076 second-feet. April 24: Gage height, 17.05 feet; discharge, 9,027 second-feet. May 17: Gage height, 1.70 feet; discharge, 461 second-feet. June 27: Gage height, 3.00 feet; discharge, 590 second-feet. August 10: Gage height, 0.61 foot; discharge, 139 second-feet. November 6: Gage height, 4.60 feet; discharge, 1,278 second-feet. November 22: Gage height, 0.90 foot; discharge, 243 second-feet. 135

Daily gage height, in feet, of Neuse River at Selma, North Carolina, for 1900.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
Day. 1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 13 14 15 11 12 13 14 15 12 13 14 15 12 12 13 14 15 12 12 13 14 15 12 12 13 14 15 12 12 12 12 12 12 12 12 12 12	$Jan.\\ 1.4\\ 1.9\\ 2.15\\ 1.4\\ 1.5\\ 1.4\\ 1.0\\ 1.1\\ 3.0\\ 9.7\\ 10.5\\ 3.2\\ 8\\ 4.2\\ 5.5\\ 3.2\\ 8\\ 4.5\\ 5.5\\ 4.5\\ 5.5\\ 3.5\\ 3.5\\ 3.5\\ 5.5\\ 3.5\\ 5.5\\ 3.5\\ 5.5\\ 3.5\\ 5.5\\ 3.5\\ 5.5\\ 3.5\\ 5.5\\ 3.5\\ 5.5\\ 5$	Feb. 1.8 1.7 1.5 2.0 2.5 1.3 0 3.0 3.3 3.3 5.6 9.8 6 17.0 17.0 16.0 17.0 16.0 4.0 5.0 17.0 1.5 1.7 1.5 1.7 1.5 1.7 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5	Mar. 8.7 1255 12.5 1 13.1 1 8.4 7.0 6.4 7.2 8.4 7.0 8.4 7.0 8.4 7.0 8.4 7.0 8.4 7.0 8.4 7.5 8.4 7.0 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.4 7.5 8.5 8.5 8.5 8.5 8.5 8.5 8.5 8.5 8.5 8	Apr. 3.86 3.55 3.54 3.34 3.33 3.32 3.53 3.44 3.33 3.32 3.53 3.54 3.55 3.54 11.25 8.24 11.00 12.455 17.22 18.45 9 12.455 17.20 8	May. 6.3 5.5.6 4.6 8.3 2.2 3.2 4.0 2.2 2.10 1.87 1.88 3.00 7.56 3.40 2.25 2.55 5.55 5.55 5.55 5.55 5.55 5.5	June. 1.551.43 1.521.43 1.221.33 1.461.76 1.551.44 1.37 1.44 1.37 1.48 1.58 1.44 1.37 1.48 1.57 1.44 1.57 1.44 1.57 1.58 1.54 1.44 1.57 1.58 1.54 1.55 1.54 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.5	$\begin{matrix} \textbf{July.} \\ \hline \\ \textbf{4.7} \\ \textbf{3.2} \\ \textbf{2.08} \\ \textbf{1.54} \\ \textbf{.1.3} \\ \textbf{1.32} \\ \textbf{1.10} \\ \textbf{.1.21} \\ \textbf{1.10} \\ \textbf{1.44} \\ \textbf{1.21} \\ \textbf{1.10} \\ \textbf{.88} \\ \textbf{1.68} \\ \textbf{.88} \\ \textbf{1.68} \\ \textbf{.88} \\ \textbf{1.88} \\ \textbf{.86} \\ \textbf{26} \end{matrix}$	Aug. 2.0 1.8 1.3 1.2 1.0 .9 .9 .9 .9 .9 .9 .6 .65 .55 .55 .55 .55 .55 .55 .55 .55	Sept. 1.851.080.7665.5544444444444444444444444444444444	$\begin{array}{c c} Oct. \\ \hline 0.77.6 \\ .54 \\ .33 \\ .45 \\ .66 \\ .77 \\ .88 \\ .66 \\ .54 \\ .44 \\ .55 \\ \end{array}$	Nov. 0.1 2.2 1.4 4.2 6.0 3.1 2.37 1.5 4 1.4 4 1.3 2.37 1.5 4 1.4 4 1.32 1.2 1.1 1.0 9 .99 .88 88 80 100 100 100 100 100 100 100 100	Dec. 1.09 1.09 1.04 4.43 5.22 3.66 2.00 1.65 1.32 2.00 1.65 1.32 2.22 3.42 5.22 3.42 5.22 3.42 5.22 3.42 5.22 3.42 5.22 3.42 5.22 5.22 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.23 5.35 5.35 5.35 5.35 5.35 5.35 5.35 5.35 5.35 5.35 5.35 5.35 5.35 5.35 5.35 5.35 5.35 5.35 5.35 5.35 5.35 5.35 5.35 5.35 5.35 5.35 5.35 5.35 5.35 5.35 5.35 5.35 5.35 5.35 5.35 5.35 5.35
26 27 28 29 30 31	$     \begin{array}{r}       3.1 \\       2.8 \\       2.8 \\       2.2 \\       2.0 \\       1.9 \\       \end{array} $	8.6 6.8 5.1	$ \begin{array}{c} 4.7 \\ 4.9 \\ 4.7 \\ 4.5 \\ 4.3 \\ 4.0 \\ \end{array} $	13. 5 8. 5 4. 7 3. 8 3. 4 3. 3	$     \begin{array}{r}       3.5 \\       2.8 \\       2.5 \\       2.2 \\       2.0 \\       1.9 \\       1.7 \\       \end{array} $	5.7 4.3 3.2 2.7 3.7	$     \begin{array}{r}       3.3 \\       8.4 \\       12.0 \\       7.8 \\       4.2 \\       2.9 \\       2.6 \\       \end{array} $	$     \begin{array}{r}             .7 \\             .7 \\           $	.7 .7 .7 .7 .7		$     \begin{array}{r}       1.0 \\       2.0 \\       4.5 \\       3.2 \\       2.1 \\       1.6 \\       \end{array} $	2.2 1.8 1.6 1.0 2.0 4.3

### DEEP RIVER AT CUMNOCK, NORTH CAROLINA.

This station was established June 29, 1900, by E. W. Myers. It is 300 yards northwest of the railroad station at Cumnock. The wire gage, which is graduated to feet and tenths, is nailed to the guard rail of the bridge. The water surface is 37.41 feet below the top of the lower chord at the side of the tension rod supporting the floor beam opposite the gage. The initial point of sounding is at the northwest end of the bridge. The channel is straight for several hundred feet above and below the bridge, but the current is rather sluggish during low water. The bed of the stream is muddy, with some bowlders. The observer is J. A. Rollins, a watchman at Cumnock. During 1900 the following measurements were made by E. W. Myers:

June 29: Gage height, 3.00 feet; discharge, 540 second-feet. August 11: Gage height, 1.30 feet; discharge, 112 second-feet. November 5: Gage height, 4.55 feet: discharge, 1,118 second-feet. December 19: Gage height, 1.70 feet; discharge, 199 second-feet. Daily gage height, in feet, of Deep River at Cunnock, North Carolina, for 1900.

Day.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Day.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
$\begin{array}{c} 1 \\ 2 \\ 3 \\ 3 \\ 4 \\ 5 \\ 5 \\ 6 \\ 7 \\ 8 \\ 9 \\ 10 \\ 11 \\ 12 \\ 22 \\ 13 \\ 14 \\ 15 \\ 16 \\ 16 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10$	$\begin{array}{c} 2.24\\ 2.04\\ 1.85\\ 2.95\\ 2.14\\ 1.87\\ (a)\\ (a)\\ (a)\\ (a)\\ (a)\\ (a)\\ (a)\\ (a)$	$\begin{array}{c} 1.54\\ 1.54\\ 1.65\\ 1.37\\ 1.35\\ 1.53\\ 1.53\\ 1.34\\ 1.13\\ 1.18\\ 1.29\\ 1.30\\ 1.20\\ 1.27\\ 1.30\\ 1.43\\ 1.37\\ \end{array}$	$\begin{array}{c} 2.02\\ 1.79\\ 1.69\\ 1.47\\ 1.34\\ 1.36\\ 1.27\\ 1.37\\ 1.37\\ 1.32\\ 1.37\\ 1.45\\ 1.50\\ 8.52 \end{array}$	$\begin{array}{c} 1.31\\ 1.35\\ 1.14\\ 1.21\\ 1.10\\ 1.16\\ 1.00\\ 1.28\\ 1.50\\ 1.77\\ 1.82\\ 1.60\\ 1.46\\ 1.32\\ 2.11\\ 2.11\\ \end{array}$	$\begin{array}{c} 1.32\\ 1.24\\ 1.39\\ 9.19\\ 5.43\\ 2.89\\ 1.88\\ 1.83\\ 1.60\\ 1.50\\ 1.40\\ 1.34\\ 1.33\\ 1.62\end{array}$	$\begin{array}{c} 1.58\\ 1.70\\ 2.94\\ 6.96\\ 9.99\\ 4.66\\ 3.17\\ 2.26\\ 2.13\\ 1.90\\ 1.72\\ 1.74\\ 1.85\\ 1.70\\ 1.50\\ 1.66\\ \end{array}$	17 18 19 20. 21 22. 23 24 25. 26 27. 28. 29. 29. 30. 31 31 28. 29. 30. 31. 28. 29. 30. 31. 29. 29. 29. 29. 29. 29. 29. 29	$\begin{array}{c} (a) \\ (a) \\ (a) \\ 1.24 \\ .96 \\ 1.25 \\ 1.85 \\ 1.50 \\ 4.27 \\ 3.39 \\ 2.35 \\ 1.90 \\ 1.54 \end{array}$	$\begin{array}{c} 1.75\\ 1.20\\ .85\\ 1.14\\ 1.10\\ 1.12\\ 1.45\\ 2.34\\ 1.76\\ 1.46\\ 1.41\\ 1.34\\ 1.25\\ 2.35\\ 2.59\end{array}$	$\begin{array}{c} 4.40\\ 2.04\\ 1.92\\ 1.78\\ 1.67\\ 1.45\\ 1.53\\ 1.55\\ 1.56\\ 1.51\\ 1.55\\ 1.50\\ 1.21\\ \end{array}$	$\begin{array}{c} 1.95\\ 1.66\\ 1.57\\ 1.39\\ 1.34\\ 1.38\\ 1.43\\ 1.50\\ 1.36\\ 1.28\\ 1.34\\ 1.14\\ 1.30\\ 1.33\\ 1.40\\ \end{array}$	$1.69 \\ 1.39 \\ 1.80 \\ 1.72 \\ 1.71 \\ 1.80 \\ 1.39 \\ 1.44 \\ 1.28 \\ 1.82 \\ 1.82 \\ 1.55 \\ 1.45 \\ 1.80 \\ 1.55 \\ 1.45 \\ 1.80 \\ 1.55 \\ 1.45 \\ 1.80 \\ 1.55 \\ 1.45 \\ 1.80 \\ 1.55 \\ 1.80 \\ 1.55 \\ 1.80 \\ 1.55 \\ 1.80 \\ 1.55 \\ 1.80 \\ 1.55 \\ 1.80 \\ 1.55 \\ 1.80 \\ 1.55 \\ 1.80 \\ 1.55 \\ 1.80 \\ 1.55 \\ 1.80 \\ 1.55 \\ 1.80 \\ 1.55 \\ 1.80 \\ 1.55 \\ 1.80 \\ 1.55 \\ 1.80 \\ 1.55 \\ 1.80 \\ 1.55 \\ 1.80 \\ 1.55 \\ 1.80 \\ 1.55 \\ 1.80 \\ 1.55 \\ 1.80 \\ 1.55 \\ 1.80 \\ 1.55 \\ 1.80 \\ 1.55 \\ 1.80 \\ 1.55 \\ 1.80 \\ 1.55 \\ 1.80 \\ 1.55 \\ 1.80 \\ 1.55 \\ 1.80 \\ 1.80 \\ 1.55 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ 1.80 \\ $	$\begin{array}{c} 1.58\\ 1.38\\ 1.70\\ 5.77\\ 8.23\\ 4.63\\ 3.31\\ 3.31\\ 3.195\\ 2.28\\ 2.23\\ 5.2\\ 9.22\end{array}$

a No record.

### CAPE FEAR RIVER AT FAYETTEVILLE, NORTH CAROLINA.

This station is described in Water-Supply Paper No. 36, page 115. The maximum flood of which there is any record occurred on January 12, 1895, when the river reached a height of 58 feet on the gage, and the discharge was at the rate of about 91,000 cubic feet per second. The lowest stage of flow was on October 8 and 9, 1897, when the gage height was 0.2 foot and the discharge 340 second-feet. The maximum discharge is therefore about 270 times the minimum flow. The drainage area above the station is 44.93 square miles.

Moneure station on Haw River was abandoned January 1, 1900. A measurement was made on June 28, however, when the gage read 2.68 feet; the area of the section was 611 square feet, the mean velocity 1.25 feet per second, and the discharge 769 second-feet. Discharge measurements for 1898 and 1899 will be found in the Twenty-first Annual Report, Part IV, page 115.

Moneure station on Deep River was also abandoned January 1, 1900. Measurement was made on June 27, when the gage read 3.67 feet; the area of section was 600 square feet, the mean velocity 1.14 feet per second, and the discharge 687 second-feet. Measurements for 1898 and 1899 will be found in the Twenty-first Annual Report, Part IV, page 117.

Records of flow during 1899 will be found in the Twenty-first Annual Report, Part IV, page 119. During 1900 the following measurements were made by E. W. Myers:

February 9: Gage height, 6.90 feet: discharge, 3,748 second-feet. April 12: Gage height, 6.10 feet; discharge, 2,686 second-feet. April 25: Gage height, 25,30 feet; discharge, 13,479 second-feet. May 17: Gage height, 3.80 feet; discharge, 1,596 second-feet. June 29: Gage height, 5.80 feet; discharge, 2,331 second-feet. August 11: Gage height, 0.70 foot; discharge, 415 second-feet. November 3: Gage height, 0.75 foot; discharge, 416 second-feet.

Daily ga	ge height,	, in feet	, $of$	Cape	Fear	River	at	Fayetteville,	North	Carolina,	for
					1	900.					Č.

$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
00	1           2           3           4           5           6           7           8           9           10           11           12           13           14           15           16           17           18           20           21           22           23           24           25           26           27           28           29           30	$\begin{array}{c} 5.0\\ 4.9.3\\ 4.4.2\\ 4.4.2\\ 4.4.2\\ 4.4.2\\ 4.4.2\\ 1.3.9\\ 3.4.8\\ 9.1.3\\ 21.0\\ 3.4.8\\ 9.1.3\\ 21.7.3\\ 0.17.5\\ 1.2.5\\ 1.2.5\\ 1.2.5\\ 1.2.5\\ 5.5\\ 5.5\\ 5.5\\ 5.5\\ 5.5\\ 5.5\\ 5.5\\$	$\begin{array}{c} 5.2\\ 5.0\\ 4.6\\ 4.4\\ 5.3\\ 10.0\\ 8.0\\ 8.2\\ 5.8\\ 30.0\\ 24.7\\ 36.0\\ 35.8\\ 30.0\\ 24.7\\ 36.8\\ 30.0\\ 24.7\\ 18.4\\ 13.7\\ 9.0\\ 23.0\\ 18.4\\ 13.7\\ 9.1\\ 18.4\\ 13.7\\ 9.1\\ 18.4\\ 13.7\\ 9.1\\ 18.4\\ 13.7\\ 9.1\\ 18.4\\ 13.7\\ 18.4\\ 13.7\\ 18.4\\ 13.7\\ 18.4\\ 13.7\\ 18.4\\ 13.7\\ 18.4\\ 13.7\\ 18.4\\ 13.7\\ 18.4\\ 13.7\\ 18.4\\ 13.7\\ 18.4\\ 18.2\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ 18.4\\ $	$\begin{array}{c} 12.0\\ 27.0\\ 3.9\\ 29.0\\ 22.3\\ 0\\ 15.0\\ 15.0\\ 15.0\\ 15.0\\ 15.0\\ 19.0\\ 15.0\\ 19.0\\ 15.0\\ 19.0\\ 15.0\\ 19.0\\ 15.0\\ 19.0\\ 15.0\\ 19.0\\ 15.0\\ 19.0\\ 15.0\\ 19.0\\ 15.0\\ 19.0\\ 15.0\\ 19.0\\ 11.6\\ 8.5\\ 7.6\\ 0\\ 9.8\\ 14.0\\ 11.6\\ 8\end{array}$	$\begin{array}{c} 9.0\\ 7.7\\ 6.9\\ 9.1\\ 9.2\\ 6.7\\ 9.1\\ 10.0\\ 9.2\\ 6.6\\ 5.8\\ 5.6\\ 18.0\\ 14.4\\ 10.2\\ 7.0\\ 6.0\\ 38.0\\ 22.0\\ 14.4\\ 0\\ 38.0\\ 22.0\\ 12.2\\ 10.0\\ 8.3\\ \end{array}$	$\begin{array}{c} 8.3\\ 9.7\\ 7.69\\ 6.6\\ 5.50\\ 4.55\\ 5.50\\ 4.7\\ 4.8\\ 8.80\\ 18.0\\ 10.4\\ 7.5\\ 5.5\\ 5.5\\ 5.5\\ 5.5\\ 5.5\\ 5.5\\ 5.5$	$\begin{array}{c} 3.2\\ 3.20\\ 3.20\\ 2.8\\ 2.7\\ 2.7\\ 2.5\\ 3.9\\ 4.20\\ 2.5\\ 3.0\\ 2.5\\ 5.0\\ 14.0\\ 12.4\\ 4.0\\ 12.0\\ 4.0\\ 12.0\\ 4.0\\ 12.5\\ 5.0\\ 16.0\\ 5.5\\ 0\end{array}$	$\begin{array}{c} 5.0\\ 4.30\\ 3.3.16\\ 3.3.16\\ 3.3.1\\ 3.6\\ 2.2.8\\ 1.64\\ 1.8\\ 5.05\\ 2.50\\ 1.5\\ 1.3\\ 1.0\\ 1.9\\ 5.8\\ 5.05\\ 2.50\\ 1.5\\ 1.3\\ 1.0\\ 1.0\\ 9.5\\ 8.8\\ 5.0\\ 9.6\\ 8\end{array}$	68228844298777786555984776522377299	$\begin{array}{c} 5.0\\ 4.5\\ 3.8\\ 2.5\\ 1.8\\ 2.5\\ 1.8\\ 2.5\\ 1.8\\ 2.5\\ 1.8\\ 2.5\\ 1.8\\ 1.8\\ 1.8\\ 1.8\\ 1.0\\ 1.8\\ 1.0\\ 1.1\\ 1.0\\ 1.8\\ 1.0\\ 1.0\\ 1.0\\ 1.0\\ 1.0\\ 1.0\\ 1.0\\ 1.0$	$\begin{array}{c} 0.9\\ .87\\ .69\\ .22\\ 1.08\\ .79\\ .88\\ 1.63\\ .1.49\\ .88\\ .1.49\\ .1.29\\ .88\\ .77\\ .88\\ .66\\ .77\\ .88\\ .66\\ .67\\ .88\\ .77\\ .88\\ .67\\ .88\\ .67\\ .88\\ .67\\ .88\\ .67\\ .88\\ .67\\ .88\\ .67\\ .88\\ .67\\ .88\\ .67\\ .88\\ .67\\ .88\\ .67\\ .88\\ .67\\ .88\\ .67\\ .88\\ .67\\ .88\\ .67\\ .88\\ .67\\ .88\\ .67\\ .88\\ .67\\ .88\\ .67\\ .88\\ .67\\ .88\\ .67\\ .88\\ .67\\ .88\\ .67\\ .88\\ .67\\ .88\\ .67\\ .88\\ .67\\ .88\\ .67\\ .88\\ .67\\ .88\\ .67\\ .88\\ .88\\ .88\\ .88\\ .88\\ .88\\ .88\\ .8$	$\begin{array}{c} 0.6\\ 5.7\\ 2.5\\ 5.12\\ 5.5\\ 10.5\\ 5.2\\ 2.5\\ 4.0\\ 4.9\\ 2.2\\ 4.0\\ 1.8\\ 1.1\\ 1.1\\ 1.1\\ 1.1\\ 1.5\\ 5.3\\ 2.2\\ 1.8\\ 1.1\\ 1.1\\ 1.1\\ 1.1\\ 1.5\\ 5.3\\ 2.2\\ 1.2\\ 3.1\\ 1.1\\ 1.1\\ 1.1\\ 1.1\\ 1.1\\ 1.1\\ 1.1$	$\begin{array}{c} 2.8\\ 2.2\\ 2.1\\ 1.4\\ 0\\ 0\\ 9.2\\ 2.1\\ 1.4\\ 0\\ 0\\ 9.2\\ 4.8\\ 1.4\\ 0\\ 0\\ 9.2\\ 1.4\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\$

### YADKIN RIVER AT SILOAM, NORTH CAROLINA.

On August 2, 1900, a temporary station was established on Yadkin River at Siloam, North Carolina, by Cleveland Abbe, jr., and N. C. Curtis. Many miscellaneous measurements were also made on the upper tributaries of the Yadkin in connection with the general hydrographic study of the southern Appalachian region, records of which will be found in Water-Supply Paper No. 49.

The gaging station at Siloam is located on the north bank of the river, in a clump of overhanging trees, 50 yards above Hall's ferry and one-third of a mile south of the Siloam station, on the Wilkesboro division of the Southern Railroad. The gage rod, which is graduated to feet and tenths, is securely braced in a clump of trees. The gage is referred to a bench mark on the south bank in a clump of three sycamores at the water's edge, 25 feet above the ferry landing. A notch cut on the outermost tree is 8 feet from the root, and the bench mark is the top of the knot opposite this notch. The reading of the gage on August 2, 1900, was 2.7 feet, equal to 9.6 feet on the old gage, referred to the bench mark across the river, measuring to the surface of the water. The river is said to rise not more than 9 feet in ordinary freshets, but in 1898, as shown by flood marks and according to verbal accounts, it must have risen to about 16 feet on the present The initial point of sounding is on the right bank, at the gage. outer edge of the first stake on the upstream side of the rod. The banks are high and rarely are submerged. The bed of the stream is

gravel and sand, slightly shifting. The drainage area of the river at this station is 1,219 square miles. The observer is C. E. Scott, of Siloam. During 1900 the following measurements were made by N. C. Curtis:

July 11: Gage height, 2.9 feet; discharge, 1,367 second-feet. August 3: Gage height, 2.6 feet; discharge, 1,218 second-feet. October 31: Gage height, 3.1 feet; discharge, 1,469 second-feet.

Daily gage height, in feet, of Yadkin River at Siloam, North Carolina, for 1900.

		1					1	-	1	1		1
	Day.	Aug.	Sept.	Oct.	Nov.	Dec.	Day.	Aug.	Sept.	Oct.	Nov.	Dec.
-												
1			2.00	2.10	2.50	2.60	17	2.10	(a)	2.30	2.50	2.60
2			2.00	2.10	2.50	2.60	18	2.10	(a)	2.30	2.50	2.60
3		2.10	2.00	2.20	2.80	2.70	19	2.10	(a)	2.30	2.50	2.60
4		2.05	2.00	2.20	2.60	2.70	20	2.10	(a)	2.30	2.50	2.60
5		2.00	2 00	2.30	2.40	2 60	21	2 60	(a)	2.30	2.60	2 70
6		1 95	2.00	2 30	2 40	2 60	99	3 05	(a)	2 60	2 60	2 70
77		1 00	2 00	2 30	2 40	2 60	92	2 05	(a)	3 10	2 50	2 70
0		1.00	0.00	9.40	2.40	0.00	94	2.00	(u)	11 + 90	2.00	0.10
0		1.90	2.00	A. 40	2.00	A. 00	6t	3.00	(a)	11.40	4.00	4.10
9		1.90	2.00	2.30	2.50	2.60	25	2.90	(a)	4.50	2.80	2.60
10		1.80	2.00	2.30	2.40	2.70	26	2.75	(a)	3.60	11.30	2.60
11.		1.80	2.00	2.30	2.40	2.70	27	2.70	(a)	3.40	10.80	2.70
12		1.80	2.00	2.30	2.40	2.70	28	2.00	(a)	3.20	10.60	2.70
13		1.85	2.00	2.60	2.40	2.60	29	2.00	(a)	2.60	9.00	2.70
14		2 05	2 05	2 40	2 40	2.60	30	2.00	(a)	2 60	2.80	3 10
15		2 10	2 20	2 30	2 40	2 60	31	2.00	()	2 60		3 20
16		2 10	(a)	2 30	9 50	2 60	01	1.00		12.00		0.40
10		A. 10	(11)	A. 00	A. 00	10.00						
								1			1	

a No record.

YADKIN RIVER AT SALISBURY, NORTH CAROLINA.

This station is described in Water-Supply Paper No. 36, page 116. Owing to the inconvenient location of the railroad bridge from which the measurements were made and its height above the water, the gaging station was moved June 1, 1899, to the new iron highway bridge about 300 yards above the railroad bridge, the new gage reading the same as the old. In its new position the 10-foot mark on the rod is opposite the center of the first strut from the west end of the second span from the west end of the bridge, on the downstream side. The rod is of pine, 3 inches wide, well painted, graduated to feet and tenths, and securely nailed to the inner surface of the guard rail, the top of the rod being flush with the top of the rail. The distance between the zero of the rod and the outer rim of the pullev is 2.13 feet, and between the end of the weight and the pointer on the wire 26.75 feet. The observer is J. T. Yarbrough, keeper of the bridge. The stream here is about the same width as at the railroad bridge, and the section is a fairly good one for gaging purposes, the bottom for the greater part of the width of the stream being hard and rocky. At times the current is very materially modified by large quantities of driftwood lodging against the piers, but it is thought better results can be obtained than at the old station. Although this stream is subject to periods of comparatively low flow, the minimum run-off is large. The lowest recorded flow was 900 second-feet, occurring in September and October, 1897. The highest flood of which there is any record occurred on March 20,

1899, the gage height being 18.80 feet and the measured discharge 115,000 cubic feet per second, showing the maximum discharge to be nearly 128 times the minimum discharge.

Records of flow during 1899 will be found in the Twenty-first Annual Report, Part IV, page 120. During 1900 the following measurements were made by E. W. Myers:

February 13: Gage height, 7.43 feet; discharge, 26,682 second-feet. April 14: Gage height, 2.50 feet; discharge, 3,962 second-feet. May 19: Gage height, 2.45 feet; discharge, 4,042 second-feet. May 25: Gage height, 3.82 feet; discharge, 7,930 second-feet. August 18: Gage height, 1.95 feet; discharge, 1,447 second feet. November 9: Gage height, 2.30 feet; discharge, 2,095 second-feet. December 17: Gage height, 2.45 feet; discharge, 3,025 second-feet.

Daily gage height, in feet, of Yadkin River at Salisbury, North Carolina, for 1900.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
Day. 1	Jan. 1,50 1,60 1,60 1,60 2,00 2,30 2,50 4,30 3,90 2,50 3,90 2,50 2,30 2,50 4,30 3,00 2,50 2,30 2,50 4,30 3,00 2,50 3,00 2,50 3,00 2,50 3,00 2,50 3,00 2,50 3,00 2,50 3,00 2,50 3,00 2,50 3,00 2,50 4,30 3,00 2,50 4,30 3,00 2,50 4,30 4,30 4,30 4,30 4,30 4,30 4,30 4,30 4,30 4,30 4,30 4,30 4,30 4,30 4,30 4,30 4,30 4,30 4,30 4,30 4,30 4,30 4,30 4,30 4,30 4,30 4,30 4,30 4,30 4,30 4,30 4,30 4,30 4,30 4,30 4,300 2,50 4,300 2,500 4,300 2,500 4,300 2,500 2,500 4,300 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500 2,500	Feb. 1.50 1.50 1.70 2.80 2.30 2.30 2.30 2.30 2.30 2.30 2.90 3.90 4.10 6.00 9.10 6.00 4.10 3.20 2.80	$\begin{array}{c} \textbf{Mar.} \\ \hline \\ 4.60 \\ 9.50 \\ 6.90 \\ 4.40 \\ 3.50 \\ 2.90 \\ 2.90 \\ 4.30 \\ 4.40 \\ 4.20 \\ 3.50 \\ 3.30 \\ 3.00 \\ 2.70 \\ 4.50 \\ 6.10 \\ 4.60 \end{array}$	Apr. 2.60 2.50 2.60 2.30 2.30 2.30 2.30 2.30 2.20 2.70 2.60 2.70 2.60 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.30 2.20 2.40 2.30 2.20 2.20 2.20 2.20 2.20 2.20 2.20 2.20 2.20 2.20 2.20 2.20 2.20 2.20 2.20 2.20 2.20 2.20 2.20 2.20 2.20 2.20 2.20 2.20 2.20 2.20 2.20 2.20 2.20 2.20 2.20 2.20 2.20 2.20 2.20 2.20 2.20 2.20 2.20 2.20 2.20 2.20 2.20 2.20 2.20 2.20 2.20 2.20 2.20 2.20 2.20 2.20 2.20 2.20 2.20 2.20 2.20 2.20 2.20 2.20 2.20 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2.300 2.305 2.305 2.355 2.255 2.2550 2.2550 2.2550 2.250 2.250 2.2550 2.2550 2.2550 2.2550 2.2550 2.2550 2.2550 2.355 2.2550 2.355 2.2550 2.355 2.2550 2.355 2.2550 2.355 2.2550 2.355 2.355 2.355 2.355 2.355 2.355 2.355 2.355 2.355 2.355 2.355 2.355 2.355 2.355 2.355 2.355 2.355 2.355 2.355 2.355 2.355 2.355 2.355 2.355 2.355 2.355 2.355 2.355 2.355 2.355 2.355 2.355 2.355 2.355 2.355 2.355 2.355 2.355 2.355 2.355 2.355 2.355 2.355 2.355 2.355 2.355 2.355 2.355 2.355 2.355 2.355 2.355 2.355 2.355 2.355 2.355 2.355 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 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2.25555555 2.25	Aug. 2.35 2.20 2.10 2.10 2.20 1.95 1.95 1.95 1.95 1.95 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.90 2.00	Sept. 2.10 1.90 1.90 1.90 1.85 1.80 1.75 1.70 1.85 1.70 1.65 1.65 4.10 4.95 2.80	Oct. 2.60 2.10 1.90 1.90 2.20 2.10 2.30 2.60 2.20 2.05 2.05 2.20 2.20 2.20 2.05 2.20 2.20 2.05 2.20 2.20 2.05 2.20 2.00 2.20 2.05 2.20 2.05 2.20 2.05 2.20 2.05 2.20 2.05 2.20 2.05 2.20 2.05 2.20 2.05 2.20 2.05 2.20 2.05 2.20 2.05 2.20 2.05 2.20 2.05 2.20 2.05 2.20 2.05 2.20 2.05 2.20 2.05 2.20 2.05 2.20 2.05 2.20 2.05 2.20 2.05 2.20 2.05 2.20 2.05 2.20 2.05 2.20 2.05 2.20 2.05 2.20 2.05 2.20 2.05 2.20 2.05 2.20 2.05 2.20 2.05 2.20 2.05 2.20 2.05 2.20 2.05 2.20 2.05 2.20 2.05 2.20 2.05 2.20 2.05 2.05 2.05 2.00 2.00 2.05 2.05 2.05 2.00 2.00 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 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2.70 2.60 2.50 3.60 6.63 4.80 5.55 2.50 2.50 2.50 2.50 2.50 2.50 2.5
18 19 20 21 22 23 23 24 25 26 27	$\begin{array}{c} 2.30 \\ 2.30 \\ 4.90 \\ 5.50 \\ 4.90 \\ 3.60 \\ 2.60 \\ 2.40 \\ 2.90 \\ 2.90 \end{array}$	$\begin{array}{c} 2.30\\ 2.40\\ 2.30\\ 2.40\\ 5.60\\ 6.30\\ 4.30\\ 3.80\\ 3.50\\ 2.90\end{array}$	$\begin{array}{c} 4.60\\ 4.60\\ 3.70\\ 4.60\\ 3.80\\ 3.20\\ 3.00\\ 2.80\\ 3.90\\ 3.90\\ \end{array}$	$\begin{array}{c} 2.30\\ 9.95\\ 10.60\\ 6.00\\ 7.00\\ 6.70\\ 4.50\\ 3.90\\ 3.50\\ 2.20\end{array}$	$\begin{array}{c} 2.40\\ 2.50\\ 2.40\\ 2.30\\ 2.10\\ 2.10\\ 2.10\\ 4.00\\ 3.20\\ 2.70\end{array}$	$\begin{array}{c} 4.52\\ 4.52\\ 3.47\\ 2.95\\ 2.65\\ 3.57\\ 7.00\\ 4.68\\ 4.40\\ 4.25\end{array}$	$\begin{array}{c} 2.00 \\ 1.90 \\ 2.00 \\ 2.00 \\ 2.45 \\ 2.30 \\ 2.65 \\ 2.55 \\ 2.55 \end{array}$	$\begin{array}{c} 2.00 \\ 1.90 \\ 1.85 \\ 1.85 \\ 1.90 \\ 2.60 \\ 3.05 \\ 2.25 \\ 2.30 \\ 2.10 \end{array}$	$\begin{array}{c} 2.30\\ 2.20\\ 2.00\\ 2.00\\ 2.00\\ 2.25\\ 2.10\\ 2.00\\ 1.90\\ 1.90\end{array}$	$\begin{array}{c} 2.00\\ 2.00\\ 2.00\\ 1.90\\ 2.00\\ 4.55\\ 6.81\\ 3.45\\ 9.90\\ \end{array}$	$\begin{array}{c} 2.13\\ 2.15\\ 2.20\\ 2.35\\ 2.30\\ 2.25\\ 2.20\\ 2.20\\ 4.08\\ 7.95\end{array}$	$\begin{array}{c} 2.39\\ 2.40\\ 2.40\\ 2.70\\ 3.30\\ 3.30\\ 3.30\\ 3.20\\ 2.90\\ 2.90\\ 2.90\end{array}$
27 28 29 30 31	$\begin{array}{c} 2.30 \\ 2.20 \\ 2.20 \\ 2.00 \\ 1.90 \end{array}$	2.90	$\begin{array}{c} 5.80\\ 3.40\\ 3.00\\ 2.90\\ 2.80\\ \end{array}$	3. 30 3. 10 2. 90 2. 70	$\begin{array}{c} 2.70 \\ 2.30 \\ 2.30 \\ 2.10 \\ 2.10 \end{array}$	4. 55 3. 45 3. 55 3. 50	$     \begin{array}{r}       3.30 \\       3.05 \\       2.55 \\       2.30 \\       2.20 \\     \end{array} $	$\begin{array}{c} 2.10 \\ 2.00 \\ 1.90 \\ 1.90 \\ 2.05 \end{array}$	1.90 1.90 1.90 1.75	2.90 2.60 2.50 2.30 2.35	1,85 3,90 3,20 2,80	2.70 2.60 2.55 2.55 3.25

# YADKIN RIVER AT NORWOOD, NORTH CAROLINA.

This station was abandoned January 1, 1900, and no measurements have been made since that date. A description of the station and records of discharge measurements will be found in Water-Supply Paper No. 36, page 118; also in the Twenty-first Annual Report, Part IV, page 121.

CATAWBA RIVER NEAR MORGANTON, NORTH CAROLINA.

During the summer of 1900 a hydrographic investigation was made of the southern Appalachian region. For the purpose of the study, temporary stations were established on Catawba River near Morganton, on John River near Morganton, and on Linville River near Bridgewater. Many miscellaneous measurements were also made on the headwaters of the Catawba and its tributaries, as well as of other streams, records of which will be found in Water-Supply Paper No. 49.

The Morganton station was established June 19, 1900, at the highway bridge near Morganton, on the road from Morganton to Hartland. The wire gage is suspended from the bridge, and is read on a horizontal scale graduated to feet and tenths and nailed on the guard rail. The river is straight for a distance of 200 feet above and below the station. The banks are high and have never overflowed. The highest flood of the Catawba rose to the floor of the bridge at this station, a height of about 28 feet. The bed is silt and mud and shifts slightly during floods. The drainage area is 757.8 square miles. Upper Creek flows into the Catawba about 200 feet above the station. The observer is J. W. Kincaid, a farmer living about 200 yards from the station. During 1900 the following measurements were made:

June 13: Gage height, 1.33 feet; discharge, 1,393 second-feet. June 18: Gage height, 2.50 feet; discharge, 4,030 second-feet. July 6: Gage height, 1.30 feet; discharge, 1,164 second-feet. August 8: Gage height, 0.60 foot; discharge, 558 second-feet. September 24: Gage height, 0.50 foot; discharge, 525 second-feet. November 7: Gage height, 1.50 feet; discharge, 1,374 second-feet.

Daily gage height, in feet, of Catawba River near Morganton, North Carolina, for 1900.

	Day.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1			1.53	0.97	0.60	0.50	1.25	1.35
2			1.78	. 83	. 55	. 50	1.25	1.25
ŝ			1.60	.78	. 60	. 58	2.70	1.65
4			1.48	. 75	. 53	1 00	1.70	2.40
E			1.43	. 75	. 55	1.20	1.45	2.30
6			1.30	. 70	. 50	1.10	1.70	1.97
7	·		1.23	. 70	. 45	.80	1.55	1.60
8			1.20	. 65	. 50	. 85	1.25	1.45
6	)		1.10	. 63	. 45	.80	1.35	1.50
10	)		1.50	. 60	. 45	. 75	1.20	1.40
11			1.00	. 58	. 33	. 65	1.20	1.25
12	2		1.00	. 57	. 35	. 60	1.20	1.20
1:	}		1.25	. 65	. 33	. 55	1.10	1.10
14			1.00	. 65	1.55	.58	1.25	1.05
12	j		. 95	. 63	2.50	.53	1.25	
16			. 90	. 55	2.15	.53	1.25	
17			.87	. 63	1.25	.53	1.25	
18	}		.87	. 63	1.15	.53	1.00	
19	}	2.50	. 83	. 53	. 80	.53	1.50	
2	)	1 60	.85	.45	.68	.53	1.25	
21		1.60	.87	45	. 63	.50	1.00	
2	)	3 37	83	65	43	50	1.50	
2	}	3.05	80	73	55	8 55	95	
2		3.87	. 00	58	. 53	6.48	1.50	
$\overline{2}$		3 60	1 23	. 80	.55	4 15	1.90	
2	1	3.00	1.25	. 60	.53	2.95	4 30	
2	7.	2.30	2.63	. 63	.53	1.80	3 20	
25		2.28	1 05	53	48	1 60	2 30	
29	}	1.95	1 10	. 55	55	1.60	1 60	
30	)	1 70	1 45	60	53	1 40	1.52	
3	· · · · · · · · · · · · · · · · · · ·	1.10	1 43	. 00	, 00	1 35	1.00	
			1. 10	. 00		1.00		
		1						

LINVILLE RIVER NEAR BRIDGEWATER, NORTH CAROLINA.

This station, one of the temporary stations established in connection with the hydrographic investigations of the southern Appalachian region, was established July 3, 1900. It is located at Poole's mill, just above the ford on the road between Morganton and Marion. The gage is near the tailrace of the mill, and the gagings are made about 200 feet farther down. The bed is extremely rough and rocky, the current being swift during high water. There are no bridges across this stream, and high-water measurements are therefore difficult to obtain. The bench mark is a cross cut on the rocky cliff on the left bank of the stream. The initial point of sounding is at the end of a log sunk in the sandy right bank. The drainage area at this station is 86.2 square miles. The observer is J. A. Cooper, miller. The following measurements were made during 1900:

June 14: Gage height, 9.92 feet; discharge, 104 second-feet. July 3: Gage height, 9.54 feet; discharge, 216 second-feet. July 10: Gage height, 9.90 feet; discharge, 116 second-feet. August 17: Gage height, 10.15 feet; discharge, 78 second-feet. September 21: Gage height, 9.8 feet; discharge, 55 second-feet.

Daily gage height, in feet, of Linville River near Bridgewater, North Carolina, for 1900.

$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	Day.         July.         Aug.         Sept.         Oct.         Day.         July.         Aug.         Sept.           1         9.83         10.17         9.75         17         9.83         10.13         9.67           2         9.92         10.17         9.67         18         9.83         10.13         9.67           3         9.54         9.88         10.21         9.58         19         10.04         10.08         10.09	Oct.
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	
	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	

JOHN RIVER NEAR MORGANTON, NORTH CAROLINA.

This station was established June 17, 1900, by H. A. Pressey and E. W. Myers, at the highway bridge on the road from Morganton to Lenoir. A wire gage is suspended from the bridge, and the readings are made on a gage rod nailed to the guard rail on the downstream side of the bridge. The river channel is straight for 200 feet above and 300 feet below the station. The banks are high and the bed is rocky and permanent in section. The drainage area at this station is 212.8 square miles. The observer is W. A. Clontz, a farmer living about a third of a mile from the bridge. The following measurements were made during 1900:

June 13: Gage height, 2.64 feet; discharge, 465 second-feet. June 19: Gage height, 3.50 feet; discharge, 1,202 second-feet. July 6: Gage height, 2.63 feet; discharge, 511 second-feet. August 8: Gage height, 1.90 feet; discharge, 135 second-feet. September 24: Gage height, 1.90 feet; discharge, 148 second-feet.

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November 7: Gage height, 2.32 feet: discharge, 367 second-feet.

Daily gage height, in feet, of John River near Morganton, North Carolina, for 1900.

-	Dav	June	July	Ang	Sent	Oet	Nov	Dec
	Day .	o uno.	ourj.	Arug.	sope.	000.	11011	Dec.
-	•							
	1	1		9.10		1 20	0.90	a 90
	1		9.60	2.10		1.00	A. 00	2.02
			2.00	4.00		1.00	4.00	a - o o
	9		4.00	2.00		1.90	2.00	2.32
	<u>4</u>		2.38	2.15		2.45		3.38
	5		2.70	1 1.90		2.38	2.60	3.20
	6		2.58	1.88		2.28	2.35	2.85
	7		2.45	1.93		2.10	2.35	2.67
	8			1.90		2.03	2.30	2.62
	9		2.38	1.90		1.93	2.25	
1	0		2.30	1.90	1.70	1.90	2.25	2.50
1	1		2.25	1.90	1.70	1.90		2.35
1	2		2.25		1.70	1.95	2.20	2.32
1	3		2.30	1.98	1.70	1.90	2.20	2.35
1	<b>+</b>		2.25	1.88	1.80		2.15	2.30
1	5			1.93	2.90	1.90	2.15	2.28
1	6		2.15	1.93		1.88	2.10	
1	7		2.13	1.93	2.20	1.83	2.05	2.25
1	8		2.10	1.93	2.03	1.78		2.20
1	9	3, 50	2.10	(a)	1.95	1.73	2.12	2.18
2	0	3.25	2.15		1.90	1.73	2.15	2.22
<b>2</b>	1	2.80	2.45		1.90		2.12	3.08
2	2	3.28			1.90	1.88	2.10	2.92
2	3	3.20	2.10			14.72	2.08	
2	4		2.28		1.90	5.60	2.08	2.78
2	5	3.75	2.35		1.85	3, 45		2.68
2	6	3.58	2.30		1.83	2.98	4.55	2.48
2	7	3 23	2.23		1.83	2.70	3.00	2.32
2	8	3 20	2 20		1.80		2.65	2.32
2	9	2.95	14.140		1.83	2.45	2.52	2.28
3	0	2.85	2.20			2.30	9 49	10.140
3	1	N. 00	2 13			2.30	14. IN	2.90
								N.00

"No record from August 19 to September 9, inclusive.

#### CATAWBA RIVER AT CATAWBA, NORTH CAROLINA.

This station was originally established in July, 1896, but was abandoned December 31, 1899. On June 13, 1900, it was reestablished as a temporary station to assist in the study of the hydrography of the southern Appalachian region. The measurements are made from the Southern Railway bridge about a fourth of a mile east of the railway station. The wire gage is suspended from the bridge and is referred to the painted gage rod, which is divided into feet and tenths and nailed to the guard rail. The initial point of sounding is on the west end of the bridge. The channel is straight above and below the station, and the current is moderately swift. The banks are high, and the bed is composed of gravel and fine sand. The observer is C. A. Reed, jr., clerk in the post-office at Catawba. During 1900 the following measurements were made by E. W. Myers:

July 3: Gage height, 3.45 feet; discharge, 3,372 second-feet. August 14: Gage height, 2.10 feet: discharge, 914 second-feet. November 7: Gage height, 2.95 feet: discharge, 2,083 second-feet. December 18: Gage height, 2.59 feet: discharge, 2,139 second-feet.

Day.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1		3.15	2.80	(a)	3.55	3.70	2.85
2		2.65	2.70	(a)	3.60	3.50	2.85
3		3.35	2.55	1.80	3.65	3.10	3.40
4		3.15	2.40	1.72	3.70	4.10	4.50
5		3.10	2.40	1.75	3.70	3.20	4.10
6		3.00	2.40	1.90	4.20	3.10	3.85
7		2.90	2.40	1.85	3.90	3.10	3.45
8		2.90	2.35	1.80	3.85	2.95	3.15
9		2.80	2.30	1.78	3.80	2.75	3.00
10		2.75	2.30	1.72	3.75	2.75	2.95
11		2.65	2.30	1.70	3.75	2.75	2.95
12		2.60	2.25	1.75	3.75	2.15	2.80
13	2.35	2.60	2.25	1.75	3.70	2.75	2.85
14	2.80	2. 55	2.20	1.00	3.60	2.70	2 80
10	3.15	2.50	(a)	1.80	3.60	2.70	2.70
16	4.80	2.50	(a)	5.00	3.60	2.00	2.79
17	8.00	2.50	(a)	5.70	3.60	2.60	2.45
18	7.50	2.50	(a)	4.40	3.63	2.50	2.60
19	5.05	2.50	(a)	0.00 2.10	3.70	2.05	2.60
20	4.00	2. 50	(a)	0.10	0.00	2.00 9.00	3.10
81	0.40 4 mm	2.00	(a)	0.00	0.00	2.00	4.80
ών	4.70	2 00 9 20	(4)	0.00	0.70	A. 00 9.50	5.20
20	0.14	2.00	(a)	0,00	4.10	2.50	4. (0
θ#	0.10	2.70	(u)	9,00	7 40	9 co	4.40
40	5.05	2.10	( <i>a</i> )	2.45	5 70	0.10	0.00
40	4 15	2.90	(a)	3 40	4 00	5.00	0.00
99	9.65	2 00	(a)	3.28	4.70	4 10	3.10
90	3.45	2 70	(a)	3 30	4 45	3 60	3.10
80 80	3 30	2 70	$\left( a \right)$	3 40	4 35	3 25	3 35
81	0.00	3.00	(a)	0.40	3 90	0.40	4 05
······································		0.00	(10)		0.00		1.00

Daily gaye height, in feet, of Catawba River at Catawba, North Carolina, for 1900.

#### a No record.

# CATAWBA RIVER AT ROCKHILL, SOUTH CAROLINA.

This station, which is described in Water-Supply Paper No. 36, page 121, was established September 3, 1895. During the last year a dam has been constructed across the river about 6 miles above the gaging station, and it is probable that this will modify the flow to some extent, particularly at low stages. The maximum flood of which there is any record at this station occurred March 20, 1899, the water reaching a height of 17.25 feet on the gage, with a probable discharge of about 72,000 second-feet. The lowest stage of flow occurred in September of 1895 and 1896, when a gage height of 1.0 foot was reached, the probable discharge being 1,300 second-feet. During 1900 the following measurements were made by E. W. Myers:

February 21: Gage height, 2.63 feet; discharge, 3,803 second-feet. February 22: Gage height, 5.28 feet; discharge, 16,791 second-feet. April 13: Gage height, 2.75 feet; discharge, 4,703 second-feet. April 21: Gage height, 9.07 feet; discharge, 31,610 second-feet. May 21: Gage height, 2.42 feet; discharge, 3,703 second-feet July 4: Gage height, 2.86 feet; discharge, 5,623 second-feet. August 16: Gage height, 1.70 feet; discharge, 1,936 second-feet. October 26: Gage height, 3.30 feet; discharge, 8,843 second-feet.

Daily gage height, in feet, of Catawba River at Rockhill, South Carolina, for 1900.

-													
	Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oet.	Nov.	Dec.
	l	1.80 1.80	$2.10 \\ 2.00$	$\begin{array}{r} 4.60\\11.90\end{array}$	$2.80 \\ 2.70$	(a)	$2.30 \\ 2.30$	$3.00 \\ 2.90$	$2.20 \\ 2.10$	$1.80 \\ 1.80$	$1.40 \\ 1.40$	$1.90 \\ 1.80$	$2.20 \\ 2.00$
A. 4. 4.	3	2.70 2.70 2.30	$\begin{array}{c} 2.00 \\ 2.10 \\ 2.20 \end{array}$	$7.90 \\ 4.50 \\ 3.70$	2.60 2.50 2.80	(a) (a) (a)	2.20 2.50 2.50	2.80 2.80 2.50	2.00 1.90 1.90	$1.80 \\ 1.80 \\ 1.70$	1.40 1.40 1.40	$1.80 \\ 3.40 \\ 3.00$	2.00 3.20 4.20
ere		2.20 2.00	2.40 2.40 2.00	3.30 3.10	2.80 2.60	(a) (a) (a)	2.40 2.30	2.40 2.40 2.40	1.80 1.80 1.80	1.70 1.70 1.70	1.40 1.70 1.70	2.50 2.10	4.10
10	)	$     \begin{array}{c}       2.00 \\       2.00 \\       2.00 \\       1.00     \end{array} $	2.00 2.00 2.60 2.00	3.80 4.10 2.50	2.60 2.60 2.50 2.50	(a) (a)	2.30 2.40 2.40	2.30 2.20 2.20	1.80 1.80 1.80 1.80	1.70 1.60 1.60 1.60	1.40 1.80 1.60	2.00 2.00 1.90	2.40 2.20 2.20 2.20
12 12		$1.90 \\ 3.20 \\ 4.70$	3.80 3.80 6.30	3.70 3.40 3.20	2.50 2.20 2.70	(a) 2.40 2.30	2.40 2.30 2.20	2.20 2.10 2.10	$ \begin{array}{c} 1.70 \\ 1.70 \\ 1.70 \\ 1.70 \end{array} $	$     \begin{array}{r}       1.50 \\       1.50 \\       1.50 \\       1.50 \\       \end{array} $	$1.60 \\ 1.60 \\ 1.60$	$     \begin{array}{c}       1.80 \\       1.70 \\       1.70     \end{array} $	$2.20 \\ 2.20 \\ 2.00 $
14 15 16		$     \begin{array}{r}       3.59 \\       2.80 \\       2.50     \end{array} $	$12.30 \\ 7.50 \\ 4.30$	$     \begin{array}{r}       3.10 \\       2.90 \\       5.80     \end{array} $	$2.60 \\ 2.50 \\ 2.50$	$2.30 \\ 2.30 \\ 2.30 \\ 2.30$	$2.20 \\ 2.60 \\ 2.55$	$\begin{array}{c} 2.10 \\ 2.10 \\ 2.10 \\ 2.10 \end{array}$	$     \begin{array}{r}       1.70 \\       1.70 \\       1.70 \\       1.70 \\       \end{array} $	$     \begin{array}{c}       1.50 \\       1.60 \\       1.60     \end{array} $	$     \begin{array}{r}       1.50 \\       1.50 \\       1.50 \\       1.50 \\       \end{array} $	$ \begin{array}{c c} 1.70 \\ 1.70 \\ 1.70 \\ 1.70 \\ \end{array} $	$     \begin{array}{r}       1.90 \\       1.90 \\       1.90     \end{array} $
$17 \\ 18 \\ 19 \\ 19 \\ 19 \\ 19 \\ 19 \\ 19 \\ 19$		2.40 2.20 2.00	$     \begin{array}{r}       3.40 \\       3.00 \\       2.90     \end{array} $	$\begin{array}{r} 6.70 \\ 4.50 \\ 3.60 \end{array}$	$2.50 \\ 2.40 \\ 10.00$	$2.25 \\ 2.30 \\ 4.60$	$     \begin{array}{r}       3.90 \\       6.75 \\       6.30     \end{array} $	2.10 2.10 2.10 2.10	$   \begin{array}{c}     2.00 \\     2.00 \\     1.90   \end{array} $	$\begin{array}{c} 3.20 \\ 2.70 \\ 2.10 \end{array}$	$     \begin{array}{r}       1.50 \\       1.50 \\       1.40     \end{array} $	$     \begin{array}{c}       1.70 \\       1.70 \\       1.70 \\       1.70 \\       \hline     \end{array} $	$     \begin{array}{c}       1.90 \\       1.80 \\       1.80     \end{array} $
20 21 22		2.90 3.30 3.20	$   \begin{array}{c}     2.60 \\     2.60 \\     4.90   \end{array} $	3.30 3.80 3.70	(a) (a) (a)	2.60 2.40 2.20	$     \begin{array}{r}       4.40 \\       3.30 \\       2.90     \end{array} $	2.00 1.90 1.90	$     \begin{array}{r}       1.90 \\       1.70 \\       1.60     \end{array} $	$     \begin{array}{r}       1.80 \\       1.80 \\       1.70     \end{array} $	1.40 1.40 1.35	1.70 1.70 1.70	$1.80 \\ 4.20 \\ 3.80$
23		2.70 2.50 2.40	5.40 4.00 3.40	3.30 2.30 2.00	(a) (a) (a)	2.20 2.20 2.40	5.80 6.50 5.00	$     \begin{array}{r}       1.00 \\       2.10 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       2.60 \\       $	$     \begin{array}{r}       1.00 \\       2.30 \\       2.10 \\       1.80     \end{array} $	1.70 1.40 1.40	1.40 7.75 11.20	1.70 1.70 1.70 1.70	4.20
2020		2.40 2.40 2.30	3.30 3.00	3.00 3.10 3.70 2.50	(a) (a) (a)	3.60 2.80	4.90 4.00 2.50	2.00 2.20 2.30 2.50	$     \begin{array}{c}       1.80 \\       2.00 \\       1.90 \\       1.80     \end{array} $	1.40 1.30 1.30 1.20	$     \begin{array}{r}       11.50 \\       3.40 \\       2.50 \\       9.90 \\     \end{array} $	1.70 1.80 6.10 2.00	$     \begin{array}{r}       2.80 \\       2.70 \\       2.50 \\       2.20     \end{array} $
28 29 30		2.20 2.10 2.10	2.80	$3.50 \\ 3.20 \\ 3.10$	(a) (a) (a)	2.60 2.50 2.40	5.50 3.20 3.10	2.50 2.30 2.90	1.80 1.80 2.00	$1.30 \\ 1.30 \\ 1.30 \\ 1.30$	2.20 2.10 2.00	5.90 2.60 2.30	2.30 2.20 2.20
31	•••••	2.10		3.00		2.30		2.20	1.80		2.00		2.60

a Gage broken; no record.

# BROAD RIVER (OF THE CAROLINAS) AT DELLINGER, SOUTH CAROLINA.

The station at Gaffney, South Carolina, was abandoned on account of its poor section, and the station at Dellinger was established August 30, 1900, by N. C. Curtis, in connection with the hydrographic investigations of the southern Appalachian region. The gage is a 4-inch by 4-inch timber, 13 feet long, spiked to a tree on the left bank of the river at Ellis's ferry, Dellinger, 1 mile below the North Carolina-South Carolina State line and 10 miles south of Shelby, North Carolina. The gage is graduated to feet and tenths and reads direct. The initial point of sounding is a stake in the center of the roadway, used for securing ferryboats to the bank. The channel is straight, the current rather rapid, and the bed of the stream sandy and slightly shifting. The right bank is about 10 feet high, and is not subject to overflow; the left bank rises to a considerable height. It has been observed that the surface of the water in the river is about 4 inches higher in the evening than in the morning. This may probably be accounted for by the fact that there are two cotton mills on Second Broad River which close their gates at night, in order to allow the ponds to fill, and cut off nearly all of the discharge of Second Broad River during low water. The observer is J. S. Gramling, ferryman. During 1900 N. C. Curtis made one measurement at this station, as follows:

August 30: Gage height, 0.8 foot; discharge, 1,430 second-feet.

Daily gage height,	in feet, o	of B	Broad H	River (of	the C	Carolinas)	at	Dellinger,	South
			Caroli	na, for 1	900.				

Day.	Sept.	Oct.	Nov.	Dec.	Day.	Sept.	Oct.	Nov.	Dec.
$\begin{array}{c} 1 \\ 2 \\ 3 \\ 4 \\ 4 \\ 5 \\ 5 \\ 6 \\ 7 \\ 7 \\ 8 \\ 9 \\ 9 \\ 10 \\ 11 \\ 12 \\ 13 \\ 14 \\ 15 \\ 16 \\ 15 \\ 16 \\ 10 \\ 11 \\ 15 \\ 16 \\ 10 \\ 11 \\ 11 \\ 12 \\ 11 \\ 12 \\ 11 \\ 11$	$\begin{array}{c} \hline \hline \\ 0.60 \\ .70 \\ .70 \\ .60 \\ .60 \\ .60 \\ .50 \\ .30 \\ .50 \\ .50 \\ .50 \\ .50 \\ .50 \\ .40 \\ .40 \\ .20 \\ 2.90 \\ \end{array}$	$\begin{array}{c} 0.55\\ .60\\ .50\\ .50\\ .50\\ .60\\ .60\\ .70\\ 1.00\\ .80\\ .60\\ .60\\ .60\\ .30\\ .75\\ .30\\ \end{array}$	$\begin{array}{c} 0.80\\ .70\\ .70\\ .90\\ .90\\ .90\\ .60\\ .60\\ .60\\ .60\\ .60\\ .70\\ .70\\ .70\\ .70\\ .70\\ .70\\ .70\end{array}$	$\begin{array}{c} 1,35\\ 1,20\\ 1,30\\ 2,50\\ 3,15\\ 2,00\\ 1,70\\ 1,55\\ 1,20\\ 1,30\\ 1,20\\ 1,15\\ 1,15\\ 1,15\\ 1,15\\ 1,15\\ 1,15\\ .80\\ \end{array}$	17	$\begin{array}{c} 1.50\\ 1.00\\ .70\\ .60\\ .60\\ .70\\ .60\\ .70\\ .60\\ .50\\ .50\\ .50\\ .50\\ .50\\ .50\\ \end{array}$	$\begin{array}{c} 0.30\\ .30\\ .30\\ .20\\ .40\\ 1.00\\ 5.50\\ 2.50\\ 2.50\\ 1.28\\ 1.00\\ .90\\ .80\\ \end{array}$	$\begin{array}{c} 0.\ 70\\ .\ 50\\ .\ 70\\ .\ 70\\ .\ 70\\ .\ 70\\ .\ 70\\ .\ 70\\ .\ 90\\ 6.\ 15\\ 2.\ 80\\ 1.\ 90\\ 1.\ 60\\ 1.\ 50\\ \end{array}$	$\begin{array}{c} 1.\ 00\\ .\ 90\\ .\ 90\\ .\ 90\\ 5.\ 00\\ 3.\ 25\\ 2.\ 30\\ 2.\ 50\\ 2.\ 50\\ 2.\ 50\\ 1.\ 70\\ 1.\ 60\\ 1.\ 75\\ 2.\ 50\\ \end{array}$

BROAD RIVER (OF THE CAROLINAS) NEAR ALSTON, SOUTH CAROLINA.

This.station is described in Water-Supply Paper No. 36, page 125. The river is straight for a long distance above and below the station, but the current is at an angle with the bridge. The current velocity is ample and is very uniform throughout the section. The observer is G. M. Heron, a farmer living near the station. The maximum flood at this station was on April 22, 1900, when the gage height was 23.80 feet and the probable discharge about 92,000 second-feet. The minimum flow was reached October 3, 1899, the discharge being 1,485 second-feet. The maximum discharge is, therefore, about 62 times the minimum flow. During 1900 the following discharge measurements were made by E. W. Myers:

February 26: Gage height, 5.40 feet; discharge, 8,913 second-feet. April 18: Gage height, 6.28 feet; discharge not measured. April 20: Gage height, 13.60 feet; discharge, 44,456 second-feet. May 22: Gage height, 3.40 feet; discharge, 4,406 second-feet. July 5: Gage height, 4.25 feet; discharge, 5,962 second-feet. August 17: Gage height, 2,80 feet; discharge, 2,840 second-feet.

#### SOUTH CAROLINA.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oet.	Nov.	Dec.
1		2.99	8.20	4.64	5.00	3.45	5.54	$\frac{4.00}{2.85}$	3.15	2.55	2.95	3.60
3		$ \begin{bmatrix} 2.00 \\ 2.72 \\ 2.74 \end{bmatrix} $	$ \begin{array}{r} 14.20 \\ 12.47 \\ 8.20 \end{array} $	4.17 4.24	4.60	$3.48 \\ 4.05$	4.50 5.45 5.45	3.00 3.40 3.30	$     \begin{array}{r}       3.20 \\       2.80 \\       2.50     \end{array} $	2.60 2.60 2.60		3.40 3.25 7.83
5 6		- 3.33 - 3.52 - 2.00	$6.10 \\ 5.52 \\ 5.01$	4.58 4.54 4.08	4.25 4.15 4.10	$4.45 \\ 3.90 \\ 3.70$	4.25 5.90	3.20 3.10 2.80	2.70 2.60 2.50	3.05 3.35 3.20	$7.20 \\ 5.00 \\ 2.75$	9.20 6.50 1.95
8 9	3.30 3.45	3.45 3.50 3.50	$5.04 \\ 5.16 \\ 8.98$	4.05	$     \begin{array}{r}       4.10 \\       3.90 \\       3.90     \end{array} $	$5.05 \\ 4.45$	$3.65 \\ 4.76$	$3.03 \\ 3.05$	2.50 2.48	$3.10 \\ 2.70$	$3.50 \\ 3.15$	4.25 3.90
$10 \dots 11 \dots 12$	3.60 3.80 6.30	$ \begin{array}{c c} 3.58 \\ 8.48 \\ 9.81 \\ \end{array} $	$8.30 \\ 6.63 \\ 5.43$	3.90 3.88 4.50	$   \begin{array}{c}     3.70 \\     3.60 \\     3.60   \end{array} $	$4.45 \\ 4.20 \\ 3.85$	$3.74 \\ 3.40 \\ 3.30$	2.90 2.82 2.80	2.30 2.05 2.30	3.25 3.15 2.90	$   \begin{array}{r}     3.05 \\     2.90 \\     2.80   \end{array} $	3.60 3.55 3.45
13 14	7.50 5.00	14.48 19.95	$5.07 \\ 4.66$	$     \begin{array}{r}       4.70 \\       4.41 \\       4.41     \end{array} $	$3.65 \\ 3.64 \\ 9.64$	$3.60 \\ 4.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ $	$3.20 \\ 4.80 $	$2.85 \\ 2.60 \\ 0.60 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ 0.61 \\ $	2.35 2.38 2.38	2.85 3.10	2.70 3.00	3.35
$15 \\ 16 \\ 17 \\ \\ \\ \\ \\ $	3.80 3.20 2.78	16.90 11.11 7.47	$     \begin{array}{r}       4.40 \\       11.68 \\       12.80     \end{array} $	$     \begin{array}{r}             4.40 \\             3.90 \\             3.70         \end{array}     $	3.64 3.54 3.50	$4.32 \\ 4.20 \\ 10.00$	$     \begin{array}{r}       4.40 \\       3.70 \\       3.50     \end{array} $	2.95 2.90 2.80	$     \begin{array}{r}       2.65 \\       5.30 \\       6.12     \end{array} $	$   \begin{array}{r}     3.00 \\     2.50 \\     2.85   \end{array} $	2.90 2.85 2.90	3.70 3.30 3.05
$     18 \dots 19 \dots 20 $	2.38 2.36 2.00	5.57 4.92 4.51		$\begin{array}{c} 6.40 \\ 17.20 \\ 11.60 \end{array}$	3.40 4.80 4.20	12.33 8.60 6.00	3.40 3.25 3.10	2.95 2.85 2.75	4.10 3.20 3.05	2.70 2.70 2.60	2.95 2.95 2.75	3.10 3.20 3.30
21 22	3. 87 3. 52	4.20 9.25	$6.83 \\ 5.84$	15.50 23.40	3.60 3.47	$5.00 \\ 4.50$	$3.10 \\ 2.98$	$2.35 \\ 2.60$	2.85 2.65	2.65 2.60	3.55 3.35	7.20 8.55
23 24 25	3. 38 3. 73 3. 58	9.50 6.64 7.50	$5.39 \\ 5.08 \\ 7.20$	$   \begin{array}{r}     18.10 \\     11.80 \\     10.00   \end{array} $	$3.42 \\ 3.25 \\ 6.50$	$10.55 \\ 13.98 \\ 10.00$	$3.40 \\ 3.10 \\ 3.42$	$     \begin{array}{c}       2.55 \\       3.50 \\       3.35     \end{array} $	$2.58 \\ 2.40 \\ 2.50$	$2.35 \\ 6.95 \\ 8.40$	$3.20 \\ 3.15 \\ 3.05$	$7.20 \\ 5.15 \\ 4.80$
26 27 29	3.38 3.29 2.10	5.50 5.00	10.80 8.40	7.40 7.30 6.10	$6.20 \\ 5.55 \\ 4.10$	8.00 6.85 6.25	3,25 4.32 4.29	2.80 3.10 2.60	2.80 2.65 2.50	5.85 3.90 2.55	3.90 10.13	4.45 4.20 2.00
29 30	3.10           2.90           2.84	4. 00	$     \begin{array}{r}       6.54 \\       5.60 \\       5.11     \end{array} $	$5.65 \\ 5.50$	4.40 3.85 3.70	$     \begin{array}{r}       0.55 \\       5.95 \\       6.15     \end{array}   $	4.33     4.35     4.45	2.00 2.75 2.90	2.30 2.45 2.45	a. aa 3. 30 3. 00	$     \begin{array}{r}       6.39 \\       4.65 \\       3.85     \end{array}   $	5.80 3.70 3.95
31	. 3. 10		4.78		3.55		4.95	3.10		3.15		6.30

Daily gage height, in feet, of Broad River (of the Carolinas) near Alston, South Carolina, for 1900.

#### SALUDA RIVER AT WATERLOO, SOUTH CAROLINA.

This station is described in Water-Supply Paper No. 36, page 126. Records of flow during 1899 will be found in the Twenty-first Annual Report, Part IV, page 129. During 1900 the following measurements were made by E. W. Myers:

February 23: Gage height, 7.33 feet; discharge, 3,347 second-feet. April 19: Gage height, 9.91 feet; discharge, 5,415 second-feet. May 22: Gage height, 3.35 feet; discharge, 757 second-feet. July 5: Gage height, 5.10 feet; discharge, 1,486 second-feet. August 17: Gage height, 4.10 feet; discharge 917 second-feet. November 10: Gage height, 4.42 feet; discharge, 854 second-feet.

Daily gage height, in feet, of Saluda River at Waterloo, South Carolina, for 1900.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1 2 3 4 5 6	3.60 4.00 4.55 4.50 4.30 4.05	4.00 4.10 4.80 3.95 4.60 5.25	$\begin{array}{c} 10.20\\ 11.95\\ 10.70\\ 7.20\\ 6.35\\ 6.00 \end{array}$	$6.00 \\ 5.55 \\ 5.05 \\ 5.10 \\ 5.35 \\ 5.15 $	$\begin{array}{c} 6.40\\ 6.10\\ 5.70\\ 5.70\\ 5.70\\ 5.70\\ 5.95\end{array}$	$\begin{array}{r} 4.50 \\ 4.20 \\ 4.40 \\ 5.45 \\ 4.90 \\ 5.10 \end{array}$	7.40 5.85 6.45 6.25 5.90 5.65	4.35 4.50 4.95 4.70 4.65	$\begin{array}{r} 4.70 \\ 4.90 \\ 4.00 \\ 4.00 \\ 4.10 \\ 4.05 \end{array}$	3.10 3.90 4.10 4.80 4.40 4.60	$\begin{array}{r} 4.35 \\ 4.40 \\ 6.60 \\ 7.75 \\ 4.70 \\ 5.60 \end{array}$	5.45 4.90 4.60 7.85 7.90 $7.90$
7 8 9 10 11		5.29 5.30 5.20 4.25 6.75 7.80 10.90	$\begin{array}{c} 0.00\\ 5.65\\ 8.80\\ 10.05\\ 8.30\\ 7.40\\ 2.05\end{array}$	5.15 5.35 5.45 4.35 4.85 5.50	5.55 5.00 4.90 4.85 4.95 4.65	$\begin{array}{c} 5.10 \\ 8.10 \\ 10.90 \\ 10.00 \\ 6.90 \\ 6.00 \end{array}$	5.03 5.20 5.20 5.40 4.85 4.70	$     \begin{array}{r}       3.05 \\       4.05 \\       4.15 \\       5.15 \\       3.95 \\       5.00 \\       5.00 \\       \end{array} $	$     \begin{array}{r}       4.05 \\       4.00 \\       4.65 \\       3.70 \\       3.00 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\      4.28 \\       4.28 \\       4.28 \\       4.28 \\       4.28 \\       4$	$\begin{array}{c} 4.00 \\ 3.80 \\ 3.10 \\ 4.10 \\ 5.00 \\ 4.25 \\ 4.25 \end{array}$	5.00 5.40 4.50 4.55 5.15 4.20	5.95 5.80 5.55 5.05 4.30 5.40
$\begin{array}{c} 12 \\ 13 \\ 14 \\ 15 \\ 16 \\ 17 \end{array}$	9.55 7.80 5.65 5.05 5.30 5.05	$\begin{array}{c} 10.30\\ 16.40\\ 20.00\\ 17.00\\ 8.40\\ 7.00 \end{array}$	$     \begin{array}{r}       6.05 \\       5.85 \\       5.70 \\       5.80 \\       11.05 \\       10.70 \\     \end{array} $	5.90 5.40 5.70 5.05 5.00 4.90	5.40 5.00 5.00 4.65 4.83 4.45	5.80 5.25 6.20 7.00 6.55 10.25	$\begin{array}{r} 4.55 \\ 4.75 \\ 5.80 \\ 6.10 \\ 4.90 \\ 4.60 \end{array}$	$\begin{array}{c} 3.80 \\ 3.65 \\ 3.90 \\ 4.00 \\ 4.55 \\ 4.50 \end{array}$	$\begin{array}{r} 4.00 \\ 3.95 \\ 4.10 \\ 4.75 \\ 8.75 \\ 6.10 \end{array}$	$\begin{array}{r} 4.10 \\ 4.90 \\ 3.95 \\ 3.20 \\ 4.60 \\ 4.40 \end{array}$	$\begin{array}{c} 3.45 \\ 5.10 \\ 5.15 \\ 5.05 \\ 4.40 \\ 4.70 \end{array}$	5.35 5.45 4.90 5.45 4.20 4.25
18 19 20 21 22 23	$\begin{array}{r} 4.90\\ 5.15\\ 5.20\\ 5.45\\ 4.00\\ 5.20\end{array}$	$6.45 \\ 5.90 \\ 5.50 \\ 6.10 \\ 8.50 \\ 7.70 $	$\begin{array}{c} 8.00\\ 6.90\\ 8.10\\ 7.40\\ 6.65\\ 6.10\end{array}$	$\begin{array}{r} 8.65 \\ 9.55 \\ 8.80 \\ 13.40 \\ 16.80 \\ 14.40 \end{array}$	$5.10 \\ 5.75 \\ 5.35 \\ 4.55 \\ 5.20 \\ 4.40$	$\begin{array}{c} 8.70 \\ 7.00 \\ 6.50 \\ 5.95 \\ 6.10 \\ 8.55 \end{array}$	$\begin{array}{r} 4.60 \\ 4.50 \\ 4.45 \\ 5.30 \\ 4.20 \\ 5.05 \end{array}$	$\begin{array}{r} 4.10 \\ 4.00 \\ 3.30 \\ 3.85 \\ 4.10 \\ 4.05 \end{array}$	$\begin{array}{r} 4.25 \\ 4.20 \\ 5.20 \\ 4.00 \\ 4.95 \\ 4.15 \end{array}$	$\begin{array}{r} 4.65 \\ 4.20 \\ 4.55 \\ 5.80 \\ 3.05 \\ 4.20 \end{array}$	$\begin{array}{c} 4.10 \\ 3.50 \\ 4.60 \\ 4.45 \\ 4.50 \\ 5.25 \end{array}$	5.25 4.50 5.20 5.20 5.65 5.15
24 25 26 27 28	$\begin{array}{c} 4.90 \\ 5.00 \\ 4.95 \\ 5.00 \\ 3.95 \\ 3.95 \end{array}$	5.55 6.90 5.80 5.70 5.20	$\begin{array}{c} 6.90 \\ 9.15 \\ 8.15 \\ 7.80 \\ 6.85 \end{array}$	$\begin{array}{c} 12.55\\ 9.30\\ 7.70\\ 7.40\\ 7.00\\ \end{array}$	$\begin{array}{c} 8.50 \\ 7.35 \\ 6.45 \\ 6.10 \\ 4.50 \end{array}$	$\begin{array}{c} 11.80\\ 10.70\\ 10.80\\ 8.25\\ 8.25\\ 8.25\end{array}$	$5.30 \\ 4.35 \\ 5.30 \\ 4.40 \\ 5.40 $	$\begin{array}{c} 4.15 \\ 5.20 \\ 4.00 \\ 3.75 \\ 4.40 \end{array}$	$\begin{array}{c} 3.55 \\ 4.10 \\ 4.00 \\ 4.05 \end{array}$	$\begin{array}{c} 8.30 \\ 8.10 \\ 6.70 \\ 5.35 \\ 4.70 \end{array}$	$5.10 \\ 4.50 \\ 10.20 \\ 9.90 \\ 8.40$	5.00 5.45 4.85 4.60 4.45
29 30 31	$     \begin{array}{r}       4.15 \\       4.05 \\       4.00 \\     \end{array} $		$     \begin{array}{r}       6.30 \\       6.10 \\       6.05     \end{array} $	6.55 6.30	$5.30 \\ 4.60 \\ 5.30$	7.35 8.30	$\begin{array}{c} 4.95 \\ 4.70 \\ 5.30 \end{array}$	$   \begin{array}{r}     4.00 \\     4.60 \\     4.95   \end{array} $	4.80 3.80	$\begin{array}{c} 3.90\ 5.20\ 5.25 \end{array}$	5.20 5.55	$5.35 \\ 5.55 \\ 5.70$

#### TALLULAH RIVER AT TALLULAH FALLS, GEORGIA.

This station was established August 29, 1900, and records of gage heights were obtained until October 19, 1900, when the observer left Tallulah Falls, and no readings have been made since that time. Measurements are made from the wagon bridge across the river about a half mile above the head of the falls. The bridge is a single iron span about 100 feet long. The gage is a vertical rod 10 feet long, graduated to feet and tenths, nailed to a 2-inch by 4-inch pine timber, and the whole spiked to a tree on the left bank of the river about 50 feet above the bridge. The observer is T. A. Robinson, proprietor of the Robinson Hotel. During 1900 the following measurements were made by Max Hall and J. C. Conn:

August 29: Gage height, 1 foot: discharge, 252 second-feet. December 21: Gage height, 2 feet; discharge, 963 second-feet.

Daily gage height, in feet, of Tallulah River at Tallulah Falls, Georgia, for 1900.

Day.	Aug.	Sept.	Oct.	Day.	Aug.	Sept.	Oct.	Day.	Aug.	Sept.	Oct.
1 2 3 5 6 7 8 9 11		$\begin{array}{c} 1.50\\ 1.40\\ 1.10\\ 1.00\\ 1.00\\ 1.00\\ 1.00\\ 1.00\\ 1.00\\ .90\\ .90\\ .90\end{array}$	$\begin{array}{c} 1.03\\ 1.03\\ 1.02\\ 1.01\\ 1.01\\ 1.03\\ 1.03\\ 1.03\\ 1.02\\ 1.02\\ 1.01\\ 1.01 \end{array}$	12 13 14 16 17 18 19 20 21 22 22 22		$\begin{array}{r} .85\\ .80\\ 1.20\\ 1.95\\ 2.90\\ 1.95\\ 1.70\\ 1.40\\ 1.35\\ 1.30\\ 5.40\end{array}$	$\begin{array}{c} 1. \ 01 \\ 1. \ 01 \\ 1. \ 00 \\ 1. \ 00 \\ 1. \ 00 \\ 1. \ 00 \\ 1. \ 00 \\ 1. \ 00 \\ \end{array}$	23	$     1.00 \\     .95 \\     1.60   $	$\begin{array}{c} 1.25\\ 1.20\\ 1.20\\ 1.19\\ 1.17\\ 1.10\\ 1.09\\ 1.04\\ \end{array}$	

# TUGALOO RIVER NEAR MADISON, SOUTH CAROLINA.

This station, established July 19, 1898, at Cook's ferry, about a half mile from Madison, South Carolina, 1 mile below the Southern Railway bridge over Tugaloo River and 2 miles above the mouth of Chauga Creek, is described in Water-Supply Paper No. 36, page 127. Results of measurements are given in the Twentieth Annual Report, Part IV, page 162, and in the Twenty-first Annual Report, Part IV, page 131. During 1900 the following measurements were made by Max Hall and others:

February 21: Gage height, 4.25 feet; discharge, 2,243 second-feet. August 30: Gage height, 1.71 feet; discharge, 872 second-feet. December 25: Gage height, 3.60 feet; discharge, 1,717 second-feet. December 27: Gage height, 2.80 feet; discharge, 1,414 second-feet.

Daily gage height, in feet, of Tugaloo River near Madison, South Carolina, for 1900.

	Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
-125450789011121411011192222222222222222222222222		$\begin{array}{c} 1.333222465335109859441994422199\\ 1.1.1.1.1.1.53322211.99\\ 2.1.1.465322211.99\end{array}$	$\begin{array}{c} 1.6\\ 1.68\\ 1.75\\ 3.31\\ 2.22\\ 3.05\\ 4.60\\ 1.99\\ 9.22\\ 5.45\\ 3.55\\ 4.0\\ 8.355\\ 5.0\\ 4.0\\ 8.355\\ 3.51\\ 4.0\\ 8.355\\ 3.51\\ 4.0\\ 8.35\\ 3.51\\ 1.0\\ 1.0\\ 1.0\\ 1.0\\ 1.0\\ 1.0\\ 1.0\\ 1.$	$\begin{array}{c} 4 \cdot 5 \cdot 9 \cdot 9 \cdot 7 \cdot 5 \cdot 8 \cdot 8 \cdot 6 \cdot 1 \cdot 5 \cdot 2 \cdot 9 \cdot 7 \cdot 6 \cdot 1 \cdot 0 \cdot 6 \cdot 7 \cdot 2 \cdot 0 \cdot 4 \cdot 2 \cdot 1 \cdot 2 \cdot 8 \cdot 8 \cdot 3 \cdot 1 \\ 9 \cdot 5 \cdot 3 \cdot 3 \cdot 3 \cdot 3 \cdot 3 \cdot 3 \cdot 4 \cdot 6 \cdot 5 \cdot 4 \cdot 4 \cdot 3 \cdot 3 \cdot 3 \cdot 5 \cdot 4 \cdot 3 \cdot 3 \cdot 6 \cdot 5 \cdot 4 \cdot 4 \cdot 4 \cdot 5 \cdot 4 \cdot 4 \cdot 5 \cdot 4 \cdot 4$	5446743211818482091654833259697 3333333333344333355574733866554444	21130 0 87 6 4 4 3 21 1 0 9 9 8 8 3 8 7 6 5 3 9 9 7 1 5 5 4 4 4 4 3 3 3 3 3 3 3 3 3 3 3 3 3 2 2 2 2	$\begin{array}{c} 3\ 6\ 8\ 2\ -\ 9\ 9\ 5\ 5\ -\ 5\ 6\ 8\ 3\ 3\ 3\ 3\ 5\ 9\ 5\ 5\ 5\ 5\ 5\ 5\ 5\ 5\ 5\ 5\ 5\ 5\ 5\$	1 6 1 6 2 9 8 6 8 6 7 6 9 9 7 6 2 1 0 9 8 8 1 9 7 6 2 8 1 5 5 5 4 4 8 8 8 6 7 6 9 9 7 6 2 1 0 9 8 8 1 9 7 6 2 8 1	1 8 1 - 5 5 4 3 3 2 1 1 1 - 2 0 3 1 3 1 0 9 8 8 1 3 - 2 9 8 7 - 3 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	$\begin{array}{c} 5581\\2221\\1.876\\1.1555446\\1.16130\\963221\\00981\\222222222222222222222222222222222222$	1.0.7.7.9.2.8.85.7.6.6.8.6.6.5.5.4.4.4.6.4.8.9.9.9.6.5 1.1.1.1.3.1.1.1.1.2.1.1.1.1.1.1.4.6.4.8.9.9.9.6.5	11 222229322200991199 11988877777789000999243310 111111112000999243310	$\begin{array}{c} 2;543366841109965543332221110332230461282\\ 2;243366844109965222111033229211103229612822\\ 2;254336022211102222211103220322216612822266128222661282226661282226661282226661282226661282226661282226661282226661282226661282226661282226661282226661282226661282226661282226661282226661282226661282226661282226661282226661282226661282226661282226661282226661282226661282226661282226661282226661282226661282226661282226661282226661282226661282226661282226661282226661282226661282226661282226661282226661282226661282226661282226661282226661282226661282226661282226661282226661282226661282226661282226661282226661282226661282226661282226661282226661282226661282226661282226661282226661282226661282226661282226661282226661282226661282226661282226661282226661282226661282226661282226661282226661282226661282226661282226661282226661282222666128222266612822226661282222266666666$
3	1	1.8		3.9 3.7	*.*	2.3	0.1	*. 2 3. 3	2.8	1. (	2.2	0. <del>4</del>	4.0

#### SAVANNAH RIVER NEAR CALHOUN FALLS, SOUTH CAROLINA.

This station was established August 4, 1896, on the Seaboard Air Line bridge across Savannah River, above the mouth of Beaverdam Creek, below Rocky River, and about 3 miles west of the town of Calhoun Falls, South Carolina. It is described in Water-Supply Paper No. 36, page 129. More than four-fifths of the drainage area of this river in the Blue Ridge Mountains in North Carolina, South Carolina, and Georgia is covered with the original oak forest. Records of flow during 1899 will be found in the Twenty-first Annual Report,

IRR 48-01-4

Part IV, page 134. During 1900 the following measurement was made by Max Hall:

March 1: Gage height, 5.47 feet; discharge, 13,803 second-feet.

Daily gage height, in feet, of Savannah River near Calhoun Falls, South Carolina, for 1900.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1	9.9		5.9	3.6	4.0		3.6	2.9	2.9	91	2.0	3.0
2	$3.2 \\ 3.2$	$2.8 \\ 2.8$		3.5 3.5	$3.9 \\ 4.2$	$2.7 \\ 3.1$	3.2 3.0	$3.0 \\ 3.0$	3.7 3.3	$2.0 \\ 2.0 \\ 2.0$		$2.9 \\ 2.8$
4 5 	$3.1 \\ 3.0 \\ 3.0$	$2.7 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 $	$4.2 \\ 3.9 \\ 3.8$	3.7 3.6 3.4	4.0 3.9 3.7	2.9 3.5 3.4	3.0 2.9 2.9	$2.9 \\ 2.9 \\ 2.8$	3.0 3.0 2.0	$2.1 \\ 2.1 \\ 3.0$	$4.3 \\ 4.0 \\ 3.8$	3.9 3.8 3.8
7 8	$2.9 \\ 2.9 \\ 2.9$	2.9 2.9	$3.6 \\ 4.0$	3.3 3.4	$3.6 \\ 3.4$	$3.9 \\ 11.0$	$2.8 \\ 2.7$	$2.8 \\ 2.7$	$2.8 \\ 2.6$	$2.7 \\ 2.6$	$3.7 \\ 3.4$	3.7 3.6
9 10 11	2.9 3.0 3.2	$3.0 \\ 3.2 \\ 5.2$	$4.9 \\ 4.3 \\ 3.9$	$3.4 \\ 3.3 \\ 3.6$	$3.3 \\ 3.1 \\ 3.1$	5.0 3.5 3.0	$2.7 \\ 2.6 \\ 2.5$	$2.6 \\ 2.4 \\ 2.3$	$2.5 \\ 2.3 \\ 2.3 \\ 2.9$	$2.5 \\ 2.4 \\ 2.4$	3.3 3.2 3	$3.4 \\ 3.4 \\ 3.3$
$\begin{array}{c} 11\\ 12\\ 13\\ \end{array}$	4.0 3.9	$9.3 \\ 15.5$	3.8 3.6	$4.0 \\ 3.8$	$3.0 \\ 3.0 \\ 3.0$	3.0 3.1	2.4 2.4	12121		$2.6 \\ 3.9$	$3.0 \\ 2.9$	3.3 3.4
14 15 16	$3.7 \\ 3.6 \\ 3.5$	$     \begin{array}{r}       19.4 \\       8.0 \\       5.5     \end{array} $	$3.4 \\ 3.3 \\ 4.6$	3.6 3.6 3.5	3.0 2.9 2.9	$3.0 \\ 3.0 \\ 3.3$	$2.5 \\ 2.4 \\ 2.3$	$2.6 \\ 2.5 \\ 2.5 \\ 5$	$2.0 \\ 4.7 \\ 6.9$	$3.0 \\ 2.9 \\ 2.8$	$2.7 \\ 2.7 \\ 2.6$	3.7 3.6 3.4
17 18	3.3 3.3	$4.9 \\ 4.7$	4.5 4.0	$3.5 \\ 3.9$	$2.9 \\ 2.8$	$5.6 \\ 6.1$	2.2	$2.6 \\ 2.6 \\ 2.6$	$5.0 \\ 3.2$	$2.6 \\ 2.5$	$     \begin{array}{c}       2.6 \\       2.6     \end{array}   $	3.4 3.3
19 20 21	$3.4 \\ 3.9 \\ 3.8$	4.4	$3.8 \\ 4.2 \\ 4.0$	$5.0 \\ 5.1 \\ 8.0$	$3.0 \\ 3.0 \\ 2.9$	$4.9 \\ 4.0 \\ 3.7$	2.1 2.1 2.1	$2.4 \\ 2.3 \\ 2.9$	3.0 2.9 2.9	$2.5 \\ 2.4 \\ 2.4$	2.6 3.0 2.9	$3.3 \\ 3.6 \\ 3.7$
22 23	$3.6 \\ 3.5$	$5.4 \\ 4.7$	3.9 3.8	$10.4 \\ 5.5$	$     \begin{array}{c}             2.9 \\             3.0         \end{array}     $	3.6 4.0	$2.0 \\ 2.2$	$2.0 \\ 2.0 \\ 2.0$	$2.7 \\ 2.7 \\ 2.7$	$2.4 \\ 2.5$	$2.8 \\ 2.8$	$3.5 \\ 3.4$
24 25 26	$3.4 \\ 3.2 \\ 3.2 \\ 3.9$	$4.4 \\ 4.2 \\ 4.0$	$4.0 \\ 5.6 \\ 5.7$	$     \begin{array}{r}       6.9 \\       6.0 \\       4.9     \end{array} $	$4.9 \\ 4.2 \\ 3.9$	$12.7 \\ 12.0 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.8 \\ 7.$	2.3	1.9 2.5 2.0	$2.6 \\ 2.4 \\ 2.4$	$5.0 \\ 4.0 \\ 3.9$	2.6 2.6 3.6	$3.4 \\ 3.3 \\ 3.3$
27 28	$3.1 \\ 3.0$	3.9 3.9 3.9	$5.0 \\ 4.8$	4.2 4.0	$3.0 \\ 3.0 \\ 3.0$	$5.0 \\ 4.5$	$2.3 \\ 3.4$	$2.5 \\ 2.7 \\ 2.9$	2.2 2.0	$3.7 \\ 3.5$	$3.4 \\ 3.2$	3.3 3.2
29 30 21	3.0 3.0 2.0		$\frac{4.2}{3.9}$	$4.2 \\ 4.0$	2.9 2.9	$3.9 \\ 3.8$	3.2 3.4 2.1	2.3 2.2 9 1	$2.0 \\ 2.1$	$3.3 \\ 3.1 \\ 2.0$	$3.1 \\ 3.0$	3.2 3.3
01 10	4.9	******	0.1		<i>w.</i> 0		0.1	<i>i</i> . 1		4.9		0.0

### SAVANNAH RIVER AT AUGUSTA, GEORGIA.

**v**e

Observations of river heights have been maintained at the highway bridge in the city of Augusta since 1875. The station is described in Water-Supply Paper No. 36, page 130. The gage heights as published are the average of four daily readings reduced to feet and hundredths. Discharge measurements are made at the North Augusta highway bridge. Records of flow during 1899 will be found in the Twenty-first Annual Report, Part IV, page 135. During 1900 one measurement was made by B. M. Hall, as follows:

August 28: Gage height, 7.30 feet; discharge, 5,968 second-feet.

#### GEORGIA.

Daily gage height, in feet, of Savannah River at Augusta, Georgia, for 1900.

-												1	
	Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
_													
			0.07	17 07	0.00	11 50	* **0	71.10	11 00	~ 0*	0.10	P 00	~ ~~
1		7.12	0.87	17.07	9.98	11.00	7.10	14.40	11.29	1.01	0.18	7.20	7.90
ŝ		0.94	0.01	12 97	9.09	10.70	7.50	19.95	9.40	0.35	0.00	7.70	7 75
0		6 42	6 52	11 06	0.54	10.70	8 30	11 66	7 76	7 22	6 16	13 80	0.18
45		6 50	8 33	11 44	9 65	10.60	10.20	10.60	7 73	7.00	6 40	12.00	15 31
6		6.67	9 10	10 60	9.63	9 60	9.50	9.62	7.33	6.85	6 65	9.30	14 44
7		6.39	8.89	10.37	9.20	9.30	11.70	9.27	7.27	6.44	7.65	8.00	11.22
8		6.65	8.08	10.64	9.00	9.00	19.70	8.96	7.19	6.20	7.41	7.70	9.32
ğ		6.71	8.12	17.35	8.75	9.00	19.90	8.79	7.13	6.27	7.35	7.50	8.50
10		6.71	10.04	17.60	8.90	8.80	19.90	8.39	7.09	5.89	7.50	7.40	8.40
11		7.12	20.58	14.35	9.15	8.70	10.80	8.52	7.06	6.16	6.30	6.90	8.06
12		10.40	27.19	12.21	11.10	8.60	9.50	8.22	6.57	6.06	6.75	7.00	7.90
13		15.00	29.60	10.96	11.35	8,40	9.20	8.68	6.62	6.08	6.85	7.10	7.80
14		12.79	32.31	10.39	10.77	8.30	9.30	8.94	7.31	5.99	7.48	7.00	8.80
15		9.37	30.08	10.08	9.47	8.30	9.90	9.60	7.17	7.40	7.14	7.00	11.56
$16_{10}$		8.65	22.08	15.25	9.16	8.20	9.70	9.37	6.77	14.49	6.62	6,80	9.81
17	****	8.12	16.29	17.21	8.88	7.80	15.00	8.64	7.67	14.24	6.56	6.80	8,60
$18 \\ 10$		7.67	12.70	14.21	12.10	8.40	19.80	8.07	1.31	10.00	0.41	0.00	7.91
19		7.94	11. 59	11.43	23.89	9.70	18.40	8.19	0.18	8,30	0.40	0.80	6.44
20 91		0.94	10.40	15.08	24.70	10.80	10.50	7 80	0.04	7 97	5.05	7.50	0.10
41 99		10.20	14 70	13.70	26 72	8 00	0.60	7 30	6.48	7 19	6.30	7 40	12,10
$\frac{66}{23}$		0 11	15 44	11 85	24 73	8.40	11 70	8.00	6 50	6 02	6.32	7 30	11 12
24		8 44	12.89	11 73	18 27	10 40	21 80	8 20	6.56	6.35	12 66	7 40	9 35
$\tilde{25}$		8.12	12.96	14 10	14.75	13 00	29 20	8.92	6.77	6 75	16 72	7.00	9.40
$\tilde{26}$		7.96	12.37	19.65	17.08	11.00	26.80	8.32	7.77	6.50	12.30	10.00	9.20
27		7.73	10.98	18.37	13.73	9.10	23.00	9.23	7.12	6.67	10.60	14.90	8.72
28		7.19	10.31	14.79	12.50	8.50	19.60	11.12	7.20	6.46	9.72	11.80	8.40
29		7.22		12.67	11.81	8.10	16.70	10.20	6.69	6.50	8.52	9.10	8.25
30		7.20		11.46	11.20	7.90	14.60	11.88	6.62	6.19	7.95	8.30	8.40
31		7.08		10.69		7.80		13.35	7.08		7.60		15.22
_			1										

# BROAD RIVER (OF GEORGIA) NEAR CARLTON, GEORGIA.

This station, established May 27, 1897, is located on the bridge of the Seaboard Air Line 3 miles east of Carlton, Georgia, and 3 miles above the mouth of the South Fork. A description of the station is given in Water-Supply Paper No. 36, page 131. The gage was last verified on October 17, 1900. Records of flow for 1899 will be found in the Twenty-first Annual Report, Part IV, page 132. During 1900 the following measurements were made by Max Hall:

February 16: Gage height, 4.25 feet; discharge, 2,088 second-feet. March 30: Gage height, 3.30 feet; discharge, 1,480 second-feet. May 3: Gage height, 4.49 feet; discharge, 2,562 second-feet. October 17: Gage height, 2.22 feet; discharge, 661 second-feet.

Daily	gage	height,	in	feet,	of	Broad	River	(of	Georgia)	n ear	Carlton,	Georgia,
						1	for 1900	).				

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1	2.40	2.30	5.50	3.10	3.40	2.60	3. 50	3.70	2.30	2.10	2.40	2.40
2	2.40	2.30 2.30	$\frac{4.90}{3.85}$	3.10 3.00	$\frac{3.20}{4.70}$	2.50	$\frac{3.30}{3.40}$	3.80	2.50 2.50	2.10 2 10	2.40	2.40
4	2.35	2.30	3.30	3.10	3.90	2.90	3.20	3.60	2.30 2.30	2.20	3.50	4.20
5	$\frac{2.35}{2.30}$	$\frac{3.30}{2.95}$	$\frac{3.15}{3.00}$	3.00 3.00	$\frac{3.20}{3.10}$	$\frac{2.90}{3.00}$	$\frac{3.00}{2.90}$	2.50 2.50	$\frac{2.20}{2.20}$	$2.30 \\ 2.50$	$\frac{2.80}{2.60}$	5.00 3.80
7	2.30	2.70	3.00	2.90	3.00	4.30	2.80	2.50	2.10	3.00	2.50	3.20
8	$\frac{2.30}{2.30}$	$\frac{2.65}{2.80}$	6.50 6.80	2.80 2.80	3.00 2.90	$7.70 \\ 7.60$	$\frac{2.80}{2.80}$	$\frac{2.40}{2.40}$	$\frac{2.10}{2.10}$	$2.60 \\ 2.50$	$\frac{2.40}{2.40}$	$2.80 \\ 2.70$
10	2.40	4.00	5.10	2.70	2.90	3.80	2.70	2.30	2.10	2.40	2.40	2.60
$11$ $12$ $\dots$	2.90 5.85	10.50	a. 80 3. 30	a. au 3. 90	2.90	3.20 3.10	2.00	2.30	$\frac{2.10}{2.00}$	$\frac{2.30}{2.30}$	2.40	2.50
13	$\frac{4.90}{3.30}$	22.20 16 90	3.20 3.10	3,90	$\frac{2.80}{2.80}$	3.10	$\frac{3.05}{3.55}$	$\frac{4.00}{2.50}$	2.00 2 10	2.70 2.60	2.30	2.50
15	2.95	8.00	3.00	3.10	2.70	3.10	3.00	2.40	5.50	2.40	2.30	2.60
$     16 \dots 17 $	$\frac{2.75}{2.65}$	$\frac{4.30}{3.70}$	$\frac{4.20}{3.80}$	$\frac{3.00}{2.90}$	$2.70 \\ 2.70$	$3.50 \\ 4.30$	$\frac{2.90}{2.80}$	2.40 2.50	$5.00 \\ 4.00$	$2.30 \\ 2.20$	2.30 2.30	2.50 2.40
18	3.15	3.30	3.30	3.90	2.70	5.60	2.70	2.50	2.80	2.20	2.30	2.40
19 20	$\frac{5.60}{3.75}$	3.20 3.10	4. 60	6.70	3.00 2.90	$\frac{4.90}{3.50}$	$\frac{2.60}{2.60}$	2.60	2.30 2.40	$\frac{2.20}{2.20}$	$\frac{2.40}{2.40}$	2.40
21	$\frac{3.70}{2.85}$	3.10	$\frac{4.10}{2.70}$	8.00	2.70	$\frac{3.10}{2.00}$	2.50 2.50	2.30	2.30	2.20	2.40 2 50	$\frac{3.80}{2.20}$
23	2.70	3.60 3.65	3.40	5.80	2.70	4.20	2.50 2.50	2.30	2.30 2.30	4.20	2.40	3.00
24 25	$\frac{2.60}{2.50}$	$3.20 \\ 3.65$	$\frac{3.60}{4.70}$	6.50 7 30	$\frac{4.00}{3.20}$	$13.00 \\ 12.60$	$\frac{3.00}{2.70}$	$2.20 \\ 2.20$	$\frac{2.30}{2.20}$	5.00 3.10	$2.40 \\ 3.60$	2.90 2.80
26	2.45	3.60	6.50	5.10	2.90	7.00	2.90	2.60	2.20	4.00	3.60	2.60
28	2.45 2.40	3.20 3.00	$\frac{5.30}{4.00}$	$3.90 \\ 3.70$	$\frac{2.80}{2.70}$	5.60 4.60	$\frac{3.40}{3.70}$	$2.50 \\ 2.20$	$\frac{2.20}{2.20}$	$3.80 \\ 3.10$	$\frac{2.80}{2.60}$	$2.50 \\ 2.50$
29	2.40		3.50	3.50	2.70	4.00	3.40	2.20	2.20	2.70	2.50	2.50
31	2.30 2.30		$\frac{0.00}{3.25}$	0.00	2.60	4.00	a. 50 3. 90	2.20	<i>A</i> . 10	2.50	4.00	2. 30 3. 80

# OCONEE RIVER NEAR DUBLIN, GEORGIA.

This station was established by the United States Weather Bureau in 1894, was discontinued on April 30, 1897, and was reestablished by the Georgia geological survey on February 11, 1898. Since October 15, 1898, the station has been maintained by the United States Weather Bureau. It is located about a half mile east of Dublin, Georgia, and is described in Water-Supply Paper No. 36, page 133. Records of measurement will be found as follows: For 1898, Twentieth Annual Report, Part IV, page 170; for 1899, Twenty-first Annual Report, Part IV, page 136. During 1900 the following measurements of Oconee River at Dublin were made by B. M. Hall and his assistants:

April 12: Gage height, 4.25 feet; discharge, 4,680 second-feet. December 7: Gage height, 7.30 feet; discharge, 7,991 second-feet.

#### GEORGIA.

Daily gage height, in feet, of Oconee River near Dublin, Georgia, for 1900.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
Jacy           1           2           3           4           5           6           7           8           9           10           12           13           14           15           16           17           18           19           20           21           22           23           24           25           26           28	$\begin{array}{c} 4 \\ 2 \\ 2 \\ 1 \\ 1 \\ 1 \\ 1 \\ 6 \\ 6 \\ 1 \\ 1 \\ 1 \\ 2 \\ 4 \\ 3 \\ 4 \\ 5 \\ 5 \\ 4 \\ 3 \\ 2 \\ 2 \\ 2 \\ 2 \\ 2 \\ 2 \\ 2 \\ 2 \\ 2$	$\begin{array}{c} 1.7\\ 1.6\\ 1.6\\ 1.6\\ 1.6\\ 1.6\\ 1.6\\ 1.6\\ 1.6$	$\begin{array}{c} 8.0\\ 9.6\\ 10.4\\ 11.0\\ 9.0\\ 6.6\\ 5.8\\ 7.0\\ 8.5\\ 8.7.0\\ 8.5\\ 8.7.4\\ 8.7\\ 8.0\\ 7.14\\ 8.7\\ 8.9\\ 9.5\\ 8.3\\ 8.9\\ 9.5\\ 9.6\\ 8.5\\ 7.4\\ 8.3\\ 8.9\\ 9.5\\ 9.6\\ 8.5\\ 8.3\\ 8.9\\ 9.5\\ 9.6\\ 8.5\\ 8.3\\ 8.9\\ 9.5\\ 9.6\\ 8.5\\ 8.3\\ 8.9\\ 9.5\\ 9.6\\ 8.5\\ 8.3\\ 8.9\\ 9.5\\ 9.6\\ 8.5\\ 8.3\\ 8.9\\ 9.5\\ 9.6\\ 8.5\\ 8.3\\ 8.9\\ 9.5\\ 9.6\\ 8.5\\ 8.5\\ 8.5\\ 8.5\\ 8.5\\ 8.5\\ 8.5\\ 8.5$	$\begin{array}{c} 8.8\\ 8.5\\ 5.5\\ 5.3\\ 4.8\\ 4.5\\ 4.2\\ 4.2\\ 4.2\\ 4.2\\ 4.2\\ 4.2\\ 4.2\\ 4.2$	$\begin{array}{c} 8.3\\ 8.3\\ 4.6\\ 6.7\\ 3.7\\ 7.5\\ 7.5\\ 7.5\\ 7.5\\ 7.5\\ 7.5\\ 7.5\\ 7$	$\begin{array}{c} 1.6\\ 1.4\\ 1.3\\ 1.2\\ 1.9\\ 2.8\\ 4.1\\ 1.2\\ 1.9\\ 2.8\\ 4.1\\ 5.0\\ 6.2\\ 5.7\\ 3.0\\ 2.9\\ 7.5\\ 8.0\\ 9.9\\ 10.6\\ 100.2\\ 7.9\\ 8.0\\ 9.9\\ 11.6\\ 7\end{array}$	$\begin{array}{c} 19.0\\ 16.9\\ 14.87\\ 10.15\\ 8.05\\ 5.3.9\\ 3.26\\ 2.86\\ 6.61\\ 5.57\\ 4.18\\ 2.33\\ 2.08\\ 1.52\\ 1.00\\ 2.48\\ 1.52\\ 1.00\\ 2.11\\ 2.17\\ 1.7\end{array}$	$\begin{array}{c} & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\$	$\begin{array}{c} & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\$	$\begin{array}{c} -0.1 \\ -0.3 \\ -3.3 \\32 \\08 \\32 \\08 \\32 \\11 \\ 1.22 \\08 \\66 \\65 \\52 \\11 \\00 \\77 \\66 \\65 \\52 \\11 \\00 \\77 \\56 \\55 \\53 \\00 \\55 \\53 \\00 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\55 \\$	$\begin{array}{c} 1.0\\ 0.9\\ 3.7\\ 5.5\\ 5.5\\ 6.6\\ 4.8\\ 3.9\\ 2.6\\ 1.3\\ 1.2\\ 1.0\\ 1.0\\ 9\\ .8\\ 7\\ 7\\ 1.1\\ 2\\ .8\\ .7\\ 1.5\\ 5\end{array}$	$\begin{array}{c} 2.3\\ 2.3\\ 1.8\\ 6.4\\ 2.3\\ 2.3\\ 2.3\\ 2.3\\ 2.3\\ 2.3\\ 2.3\\ 2.3$
29 30 31	$2.0 \\ 1.8 \\ 1.7$		$10.2 \\ 10.4 \\ 10.2$	13.6 11.4	$3.0 \\ 2.2 \\ 1.9$	20.0 20.8	$     \begin{array}{r}       1.7 \\       5.9 \\       5.2 \\       5.2 \\       \end{array} $	.5 .5 .8	2 0.0	$     \begin{array}{c}       2.1 \\       1.9 \\       1.3     \end{array}   $	5.3 3.4	$3,4 \\ 3.3 \\ 8.4$

### YELLOW RIVER AT ALMON, GEORGIA.

This station, which was established September 12, 1897, is described in Water-Supply Paper No. 36, page 134. During the year 1900 the bridge was washed away and a new bridge was built, but the gage was preserved and a new gage was referred to the same datum. It is attached to the post of a bridge bent near the left bank, and is referred to a bench mark on a sycamore tree on the left bank 40 yards above the bridge, a railroad spike in the tree being 7 feet above the zero of the gage. The gage was verified December 22, 1900. Records of measurements at this station during 1899 will be found in the Twentyfirst Annual Report, Part IV, page 137. During 1900 the following measurements of the discharge at Almon were made by B. M. Hall and his assistants:

April 19: Gage height, 9 feet; discharge, 3,295 second-feet. November 30: Gage height, 2.40 feet; discharge, 341 second-feet. December 22: Gage height, 4.50 feet; discharge, 966 second-feet. 153

Daily gage height, in feet, of Yellow River at Almon, Georgia, for 1900.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
$     \begin{array}{c}       1 \\       2 \\       3 \\       4 \\       5 \\       \dots \\       5     \end{array} $	$2.1 \\ 1.9 \\ 1.9 \\ 1.9 \\ 2.0 $	2.0 2.0 2.0 2.0 2.0 2.5		3.1 3.0 3.0 3.0 3.0 3.0	3.7 3.8 7.2 6.9 4.0	2.4 2.4 2.4 2.4 3.4	$\begin{array}{r} 4.0\\ 5.0\\ 5.0\\ 4.7\\ 4.0\end{array}$	3.4 2.7 2.5 2.3 2.3	3.0 3.0 2.5 2.3 2.1	2.0 2.0 2.0 2.5 2.5	$2.0 \\ 2.0 \\ 2.0 \\ 4.3 \\ 4.0$	2.4 2.3 2.3 7.5 7.0
6 7 8 9 10 11	2.0 2.0 2.0 2.0 2.3 2.9	2.7 2.5 2.5 3.5 5.7 5.9	$\begin{array}{c} 3.0\\ 3.0\\ 4.7\\ 10.0\\ 6.0\\ 4.0\end{array}$	3.0 2.9 2.9 2.9 2.9 2.9 2.9 3.9	$     \begin{array}{r}       3.6 \\       3.4 \\       3.2 \\       3.1 \\       3.0 \\       3.0 \\       3.0 \\       \end{array} $	$\begin{array}{c} 4.0\\ 3.4\\ 6.7\\ 4.4\\ 3.3\\ 3.1\end{array}$	$     \begin{array}{r}       3.5 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       3.0 \\       $	2.2 2.1 2.0 2.0 2.0 1.9	2.1 2.0 2.0 2.0 2.0 2.0 2.0 2.0	$2.8 \\ 3.5 \\ 4.0 \\ 3.0 \\ 2.7 \\ 2.4$	$   \begin{array}{c}     3.0 \\     2.5 \\     2.0 \\     2.0 \\     2.0 \\     2.0 \\     2.0 \\   \end{array} $	5.0 3.5 3.0 2.9 2.8 2.8
12 13 14 15 16	$     \begin{array}{r}                                     $	$\begin{array}{c} 15.0 \\ 20.0 \\ 15.0 \\ 7.0 \\ 5.0 \end{array}$	3.8 3.6 3.4 3.3 3.8	$\begin{array}{c} 4.7 \\ 4.0 \\ 3.4 \\ 3.0 \\ 2.0 \end{array}$	3.0 2.9 2.8 2.8 2.8 2.8	2.9 2.8 3.2 3.0 4.0	3.0 3.0 3.0 3.0 2.8	$     \begin{array}{r}       1.9 \\       1.9 \\       1.9 \\       2.5 \\       2.3 \\       2.3 \\       \end{array} $	$ \begin{array}{c} 2.0 \\ 2.0 \\ 3.0 \\ 8.0 \\ 7.0 \end{array} $	2.4 2.4 2.3 2.3 2.2	2.0 2.0 2.0 2.0 2.0 2.0 2.0	2.9 2.7 4.0 3.5 3.2
17 18 19 20 21 22 22	2.4 3.4 4.0 4.3 3.6 3.0	$4.9 \\ 4.7 \\ 3.6 \\ 4.7 \\ 3.9 \\ 3.8 $	$     \begin{array}{r}       3.4 \\       3.0 \\       3.4 \\       5.0 \\       4.3 \\       3.7 \\     \end{array} $	3.0 8.0 9.0 6.8 12.0 10.0	$2.8 \\ 2.7 \\ 3.5 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.6 \\ 2.6 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 $	$6.0 \\ 5.0 \\ 4.0 \\ 3.5 \\ 3.2 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 $	2.7 2.6 2.5 2.0 2.0 2.0	$2.2 \\ 2.0 \\ 2.0 \\ 2.0 \\ 2.0 \\ 2.5 $	$\begin{array}{r} 4.0 \\ 3.0 \\ 2.5 \\ 2.0 \\ 2.0 \\ 2.0 \\ 2.0 \end{array}$	2.1 2.0 2.0 2.0 2.0 2.0 2.0 2.0	2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0	3.0 2.8 2.8 5.0 6.5 4.5
23 24 25 26 27	$   \begin{array}{c}       3.0 \\       2.8 \\       2.6 \\       2.5 \\       2.4 \\       2.3   \end{array} $	3.7 3.7 3.8 3.8 3.8	$3.4 \\ 3.7 \\ 5.5 \\ 8.0 \\ 6.0$	$ \begin{array}{r} 10.0\\ 6.0\\ 7.2\\ 12.0\\ 6.8\\ 6.0\\ \end{array} $	2.6 4.0 3.0 2.8 2.6	$\begin{array}{c} 7.5 \\ 11.0 \\ 11.0 \\ 12.0 \\ 9.0 \end{array}$	$     \begin{array}{r}       2.0 \\       2.0 \\       2.5 \\       2.0 \\       3.0 \\     \end{array} $	2.5 2.4 2.3 2.0 2.0	$\begin{array}{c} 2.0 \\ 2.0 \\ 2.0 \\ 2.0 \\ 2.0 \\ 2.0 \\ 2.0 \end{array}$	$     \begin{array}{r}       2.0 \\       3.0 \\       3.0 \\       2.5 \\       2.3 \\       2.0 \\       \end{array} $	2.0 2.0 2.0 4.5 3.5	3.5 3.5 3.5 3.0 3.0
28 29 30 31	$2.2 \\ 2.1 \\ 2.0 \\ 2.0 $	3.8	$4.4 \\ 4.0 \\ 3.5 \\ 3.2$	5.8 $5.4$ $4.3$	2.4 2.4 2.4 2.4 2.4	$9.5 \\ 6.3 \\ 5.0$	$3.5 \\ 3.5 \\ 5.0 \\ 4.0$	$2.0 \\ 2.0 \\ 2.0 \\ 5.0 $	2.0 2.0 2.0 2.0	2.0 2.0 2.0 2.0 2.0	2.5 2.4 2.4	$2.9 \\ 2.9 \\ 4.0 \\ 7.5$

# TOWALIGA RIVER NEAR JULIETTE, GEORGIA.

This station was established on the Southern Railway bridge  $2\frac{1}{2}$  miles north of Juliette, Georgia, May 5, 1899, but observations of gage heights were not started until November 2, 1899. A description of the station will be found in Water-Supply Paper No. 36, page 136. Bench mark No. 1 is an iron girder 40 feet from the left end of the bridge and is 37.30 feet above gage datum. W. L. Jackson, a farmer living near the station (post-office address, Berner, Georgia), is the observer. Records of measurements made during 1899 will be found in Water-Supply Paper No. 36, page 136. During 1900 the following measurements were made by B. M. Hall and his assistants:

February 17: Gage height, 6.35 feet; discharge, 1,025 second-feet. April 3: Gage height, 2.60 feet; discharge, 348 second-feet. December 8: Gage height, 2.75 feet; discharge, 468 second-feet.

#### GEORGIA.

Daily gage height, in feet, of Towaliga River near Juliette, Georgia, for 1900.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1	2220099999783210182395322101 2222211199978321018239532210101	$\begin{array}{c} 2.0\\ 1.9\\ 2.17\\ 2.6\\ 2.37\\ 1.4\\ 2.73\\ 1.8\\ 1.4\\ 1.8\\ 1.6\\ 3.3\\ 2.4\\ 0\\ 3.32\\ 2.4\\ 0\\ 3.29\\ 2.4\\ 0\\ 2.9\\ 2.4\\ 0\\ 3.29\\ 2.4\\ 0\\ 3.29\\ 2.4\\ 0\\ 3.29\\ 2.4\\ 0\\ 3.29\\ 2.4\\ 0\\ 3.29\\ 2.4\\ 0\\ 3.29\\ 2.4\\ 0\\ 3.29\\ 2.4\\ 0\\ 3.29\\ 2.4\\ 0\\ 3.29\\ 2.4\\ 0\\ 3.29\\ 2.4\\ 0\\ 3.29\\ 2.4\\ 0\\ 3.29\\ 2.4\\ 0\\ 3.29\\ 2.4\\ 0\\ 3.29\\ 2.4\\ 0\\ 3.29\\ 2.4\\ 0\\ 3.29\\ 2.4\\ 0\\ 3.29\\ 2.4\\ 0\\ 3.29\\ 2.4\\ 0\\ 3.29\\ 2.4\\ 0\\ 0\\ 2.29\\ 0\\ 0\\ 2.2\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\$	931844494833011001311313274068441 24322232313113113132274068441	$\begin{array}{c} 1.66886576555470988778888888816642232\\ 2.222355470987778888888816642232\\ 1.1472554416423333\\ 3.333332\\ \end{array}$	169316655554443332222222222118955444211	$\begin{array}{c} 0 \\ 0 \\ 1 \\ 1 \\ 1 \\ 7 \\ 9 \\ 1 \\ 2 \\ 2 \\ 2 \\ 2 \\ 2 \\ 2 \\ 2 \\ 2 \\ 2$	$\begin{array}{c} 0.0\\ 4.4.05\\ 3.3.51\\ 4.4.0\\ 3.3.4.4.0\\ 3.3.4.4.3\\ 3.3.4.4.3\\ 3.2.2.1\\ 1.00\\ 0.05\\ 1.52\\ 9.6\\ 4.50\\ 1.4\\ 5.2\\ 1.4\\ 5.3\\ 1.4\\ 5.3\\ 1.4\\ 5.3\\ 1.4\\ 5.3\\ 1.4\\ 5.3\\ 1.4\\ 5.3\\ 1.4\\ 5.3\\ 1.4\\ 5.3\\ 1.4\\ 1.5\\ 1.5\\ 1.2\\ 1.4\\ 1.5\\ 1.2\\ 1.4\\ 1.4\\ 1.5\\ 1.5\\ 1.4\\ 1.4\\ 1.5\\ 1.5\\ 1.4\\ 1.4\\ 1.5\\ 1.5\\ 1.4\\ 1.4\\ 1.5\\ 1.5\\ 1.4\\ 1.4\\ 1.5\\ 1.4\\ 1.4\\ 1.5\\ 1.5\\ 1.4\\ 1.4\\ 1.5\\ 1.5\\ 1.4\\ 1.4\\ 1.5\\ 1.5\\ 1.4\\ 1.4\\ 1.5\\ 1.5\\ 1.4\\ 1.4\\ 1.5\\ 1.5\\ 1.4\\ 1.4\\ 1.5\\ 1.5\\ 1.4\\ 1.4\\ 1.5\\ 1.4\\ 1.4\\ 1.5\\ 1.4\\ 1.4\\ 1.5\\ 1.5\\ 1.4\\ 1.4\\ 1.5\\ 1.5\\ 1.4\\ 1.4\\ 1.5\\ 1.5\\ 1.4\\ 1.4\\ 1.5\\ 1.5\\ 1.4\\ 1.4\\ 1.5\\ 1.5\\ 1.4\\ 1.5\\ 1.5\\ 1.4\\ 1.5\\ 1.5\\ 1.4\\ 1.5\\ 1.5\\ 1.4\\ 1.5\\ 1.5\\ 1.4\\ 1.5\\ 1.5\\ 1.4\\ 1.5\\ 1.5\\ 1.4\\ 1.5\\ 1.5\\ 1.4\\ 1.5\\ 1.5\\ 1.4\\ 1.5\\ 1.5\\ 1.4\\ 1.5\\ 1.5\\ 1.4\\ 1.5\\ 1.5\\ 1.5\\ 1.4\\ 1.5\\ 1.5\\ 1.4\\ 1.5\\ 1.5\\ 1.4\\ 1.5\\ 1.5\\ 1.5\\ 1.5\\ 1.5\\ 1.5\\ 1.5\\ 1.5$	$\begin{array}{c} 22277375322211111111107532103652652111111111111111111$	$\begin{array}{c} 4.55\\ 1.59\\ 1.65\\ 1.32\\ 1.00\\ 1.00\\ 1.00\\ 1.00\\ 1.00\\ 1.00\\ 1.00\\ 1.00\\ 1.00\\ 1.00\\ 1.0\\ 1.$	$\begin{array}{c} 9904146987556775431111114659153221123322113322112332211322211233222113222112332221132222$	$\begin{array}{c} 1.3\\ 2.2\\ 0.8\\ 2.2\\ 7.6\\ 4\\ 3.5\\ 2.21\\ 2.0\\ 2.0\\ 9\\ 1.9\\ 1.8\\ 2.0\\ 9\\ 1.8\\ 1.8\\ 0\\ 1.9\\ 1.8\\ 1.9\\ 2.5\\ 4.1\\ 2.3\\ 1.9\\ \end{array}$	$\begin{array}{c} 1,99\\ 1,97\\ 4,00\\ 3,20\\ 4,30\\ 0,22\\ 3,00\\ 4,40\\ 6,30\\ 0,44\\ 4,30\\ 0,22\\ 3,00\\ 4,06\\ 6,43\\ 5,55\\ 2,85\\ 2,25\\ 3,43\\ 3,43\\ 3,14\\ 3,16\\ 2,25\\ 3,55\\ 2,25\\ 3,43\\ 3,43\\ 3,14\\ 3,16\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\ 2,15\\$

### OCMULGEE RIVER AT MACON, GEORGIA.

This station was established by the United States Weather Bureau January 21, 1893, and measurements were begun by the United States Geological Survey in 1895. The station is described in Water-Supply Paper No. 36, page 136. During the year 1900 Mr. T. S. Collins, of the United States Weather Bureau, put in a new gage on the center pier of the bridge on which the old gage was placed, and referred it to the same datum as the old gage. The old gage is still in place, is in good condition, and is still used except during low water, when mud accumulates around its base at a higher level than the river. The new gage was put in to save cleaning away the mud from the bottom of the old gage. Records of measurements for 1899 will be found in the Twenty-first Annual Report, Part IV, page 139. During 1900 the following measurements were made by B. M. Hall and his assistants:

April 13: Gage height, 7.38 feet; discharge, 4,855 second-feet. November 20: Gage height, 2.40 feet: discharge, 1,369 second-feet. December 6: Gage height, 8.65 feet; discharge, 5,698 second-feet. December 21: Gage height, 12.82 feet; discharge, 9,621 second-feet. 155

Daily gage height, in feet, of Ocmulgee River at Macon, Georgia, for 1900.

Day.	Jan.	Feb.	Mar.	Ap <b>r</b> .	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
Day.  1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22 22	Jan. 1.65 1.52 1.22 1.25 1.4 1.43 1.39 2.20 2.20 2.29 3.86 3.91	Feb. 1.6 1.5 1.5 2.9 2.3 3.2 3.2 3.2 3.2 1.5 1.5 1.5 2.5 3.2 3.2 3.2 3.2 3.2 3.2 1.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 5	Mar. 9,2 9,7,7 6,2 5,5 5,5 5,5 5,5 5,5 5,5 5,5 7,0 7,8 8,1 6,8 5,5 3,5 8,1 6,8 8,5 5,5 8,5 7,0 7,8 7,8 7,8 7,8 7,7 7,6 8,8 9,7,7 7,6 8,8 9,9,4 8,9,9,4 8,9,9,4 8,5 7,7 7,7 7,6 8,8 9,6 7,7 7,7 7,6 8,8 9,7,7 7,7 7,8 7,8 7,7 7,8 7,7 7,7 7,8 7,7 7,8 7,7 7,8 7,7 7,8 7,7 7,8 7,7 7,8 7,7 7,8 7,7 7,8 7,7 7,8 7,7 7,8 7,7 7,8 7,7 7,8 7,7 7,8 7,7 7,8 7,7 7,8 7,7 7,8 7,7 7,8 7,7 7,8 7,7 7,8 7,7 7,8 7,7 7,8 7,7 7,8 7,7 7,8 7,7 7,8 7,7 8,8 9,7,7 7,8 7,7 8,8 7,7 7,8 7,7 8,8 7,7 7,8 7,7 7,8 7,8	$\begin{array}{c} \text{Apr.} \\ \hline \\ 5.29 \\ 4.8 \\ 4.65 \\ 4.53 \\ 4.3 \\ 4.1 \\ 4.3 \\ 7.06 \\ 6.1 \\ 5.38 \\ 4.3 \\ 4.1 \\ 4.3 \\ 7.06 \\ 15.6 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 \\ 18.0 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2.265 2.264 2.265 2.265 2.265 2.265 2.265 2.265 2.265 2.265 2.265 2.265 2.265 2.265 2.265 2.265 2.265 2.265 2.265 2.265 2.265 2.265 2.265 2.265 2.265 2.265 2.265 2.265 2.265 2.265 2.265 2.265 2.265 2.265 2.265 2.265 2.265 2.265 2.265 2.265 2.265 2.265 2.265 2.265 2.265 2.265 2.265 2.265 2.265 2.265 2.265 2.265 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 2.255 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Oct. 1.881.7221 4.605.0665.0652.2254 2.2542.2254 2.25422.221 2.2091.991	Nov. 2.022832 12.22832 12.22843324554332222211 2.224322222211 2.2244 2.22222211 2.20442 2.22442	$\begin{array}{c} \text{Dec.} \\ \hline \\ 2.7 \\ 2.6 \\ 2.5 \\ 8.4 \\ 11.5 \\ 9.3 \\ 0.4 \\ 4.8 \\ 4.2 \\ 3.7 \\ 3.3 \\ 3.2 \\ 3.0 \\ 8.5 \\ 12.5 \\ 8.5 \\ 4.6 \\ 4.4 \\ 3.9 \\ 4.0 \\ 12.8 \\ 12.1 \\ \end{array}$
23 24 25 26 27 28 29 30 31	$\begin{array}{c} 5.1 \\ 2.7 \\ 2.5 \\ 2.2 \\ 2.0 \\ 2.0 \\ 1.9 \\ 1.7 \\ 1.6 \end{array}$	$ \begin{array}{c} 7.7\\ 6.4\\ 7.3\\ 6.5\\ 5.9\\ 5.5\\ \end{array} $	$\begin{array}{c} 5.6 \\ 7.3 \\ 7.9 \\ 10.5 \\ 10.9 \\ 7.8 \\ 7.4 \\ 6.6 \\ 5.8 \end{array}$	$\begin{array}{c} 13.9\\ 13.2\\ 13.0\\ 12.4\\ 9.8\\ 7.6\\ 7.0\\ 6.3\end{array}$	$\begin{array}{c} 3.3 \\ 4.6 \\ 4.8 \\ 4.2 \\ 3.8 \\ 3.3 \\ 3.1 \\ 3.0 \\ 2.9 \end{array}$	$\begin{array}{c} 4.0\\ 16.0\\ 20.2\\ 20.0\\ 16.4\\ 14.0\\ 12.7\\ 10.4\\ \end{array}$	$     \begin{array}{r}       3.4 \\       3.9 \\       3.4 \\       3.3 \\       4.2 \\       4.5 \\       5.6 \\       6.3 \\       8.0 \\     \end{array} $	$\begin{array}{c} 2.2 \\ 3.6 \\ 4.1 \\ 4.3 \\ 3.8 \\ 2.7 \\ 2.4 \\ 2.3 \\ 3.8 \end{array}$	2.4 2.3 2.3 2.2 2.0 2.0 2.0 1.9	$\begin{array}{c} 2.1 \\ 8.3 \\ 4.2 \\ 3.7 \\ 2.9 \\ 2.5 \\ 2.4 \\ 2.3 \\ 2.1 \end{array}$	2.5 2.7 2.5 7.1 5.5 4.3 3.2 2.9	$\begin{array}{c c} 8.0\\ 6.5\\ 5.5\\ 4.8\\ 4.1\\ 3.9\\ 3.8\\ 7.8\\ 7.5\end{array}$

# FLINT RIVER AT ALBANY, GEORGIA.

This station, which is described in Water-Supply Paper No. 36, page 138, was originally established by the United States Weather Bureau on April 10, 1893, and has been maintained from that date to the present time. In 1898 the gage was washed out by a freshet, but soon afterwards it was replaced. The present rod is located at the foot of Broad street, just below the county bridge. It is a pine board, and is in two sections. The first section, which reads from 0 to 18.6 feet, is spiked to a cypress stump which stands at the edge of the water; the second section, which reads from 18.7 feet to 30 feet, is spiked to a cypress pole. The bench marks are as follows: (1) The top of the rail at the railroad station of the Plant System, being 42.2 feet above the zero of the gage and 184 feet above mean sea level, making the elevation of the zero of the rod 141.8 feet above sea level; (2) a cut in the lower iron pier of the county bridge 10 feet above gage datum and 151.8 feet above mean sea level; and (3) a spike in the corner of Mase & Company's warehouse, corner of Broad and Front streets, 53.8 feet above gage datum. The highest water recorded was on March 25, 1897, when the height of 31.6 feet was reached, and the lowest point recorded since the commencement of the record was on October 9, 1895, when the reading was -0.9 foot. The danger line is at 20 feet. Discharge measurements are made at the county highway bridge in Albany, a steel structure in two spans of 130 feet each, with two approaches of 315 and 205 feet, respectively.

#### GEORGIA.

Kinchafoonee and Muckalee creeks are two important tributaries of Flint River. They unite about 2 miles north of Albany, forming Big Muckalee Creek, which enters Flint River on the west side within the city limits. There is a wagon bridge over the Kinchafoonee about 1 mile above its junction with the Muckalee, and a similar bridge on the Muckalee  $1\frac{3}{4}$  miles above its mouth and about 300 yards below the mouth of the Kinchafoonee. Measurements will be made at these bridges whenever Flint River is measured at Albany. No discharge measurements were made at this point during 1900 or in previous years, but measurements will be made during 1901.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1	$\begin{array}{c} 4.430339663773222773883199889903347552009\\ 1.11112223332229093347552009\\ 1.12223332223332223333332222209\\ 1.33333322222209\\ 1.333333333333333333333333333333333333$	$\begin{array}{c} 1.8\\ 1.9\\ 2.3\\ 2.6\\ 2.9\\ 3.4\\ 4.8\\ 6.4\\ 9.8\\ 14.3\\ 18.1\\ 20.0\\ 21.3\\ 4.8\\ 26.0\\ 29.0\\ 22.4\\ 26.0\\ 29.0\\ 28.1\\ 1.2\\ 20.0\\ 28.1\\ 1.2\\ 9.0\\ 9.0\\ \end{array}$	$\begin{array}{c} 9.1\\ 9.2\\ 9.3\\ 9.5\\ 9.6\\ 9.2\\ 9.2\\ 9.2\\ 9.1\\ 9.2\\ 9.2\\ 9.2\\ 9.2\\ 9.2\\ 9.2\\ 9.2\\ 9.2$	$\begin{array}{c} 11.1\\ 10.0\\ 9.13\\ 7.2\\ 6.1\\ 5.9\\ 5.4\\ 7.4\\ 3.3\\ 4.3\\ 4.3\\ 4.5\\ 7.4\\ 3.3\\ 4.5\\ 7.8\\ 6\\ 10.7\\ 2\\ 12.1\\ 6\\ 14.3\\ 14.9\\ 15.2\\ 12.1\\ 12.1\\ 6\\ 14.3\\ 14.9\\ 9.0\\ 8.9 \end{array}$	$\begin{array}{c} 9.4\\ 10.2\\ 11.1\\ 0\\ 9.6\\ 2.2\\ 3.3\\ 9.5\\ 4.8\\ 3.4\\ 9.5\\ 5.2\\ 1.4\\ 3.3\\ 1\\ 2.6\\ 4.8\\ 3.1\\ 1.2\\ 2.0\\ 0\\ 1.7\\ 4.1\\ 1.2\\ 2\\ 1.0\\ 1.0\\ \end{array}$	$\begin{array}{c} 1.332 \\ 1.1332 \\ 47112 \\ 1.122 \\ 2.233 \\ 3334 \\ 4014 \\ 444 \\ 452 \\ 2.233 \\ 3334 \\ 4014 \\ 444 \\ 453 \\ 2.22 \\ 2.23 \\ 2.23 \\ 333 \\ 455 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 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1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2 \\ 1.2$	$\begin{array}{c} 15.8\\ 16.0\\ 16.2\\ 2\\ 18.0\\ 0\\ 2.0\\ 1\\ 5.4\\ 9\\ 0\\ 3.4\\ 4.9\\ 0\\ 5.4\\ 6\\ 1\\ 1.5\\ 6\\ 4.5\\ 1\\ 1.5\\ 6\\ 4.5\\ 1\\ 1.5\\ 6\\ 1\\ 1.5\\ 6\\ 3.2\\ 3\\ 9\end{array}$	$\begin{array}{c} 4.22\\ 4.423\\ 8.84\\ 2.26\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.02\\ 1.08\\ 1.02\\ 1.08\\ 1.02\\ 1.08\\ 1.02\\ 1.08\\ 1.02\\ 1.08\\ 1.02\\ 1.08\\ 1.02\\ 1.08\\ 1.02\\ 1.08\\ 1.02\\ 1.08\\ 1.02\\ 1.08\\ 1.02\\ 1.08\\ 1.02\\ 1.08\\ 1.02\\ 1.08\\ 1.02\\ 1.08\\ 1.02\\ 1.08\\ 1.02\\ 1.08\\ 1.02\\ 1.08\\ 1.02\\ 1.08\\ 1.02\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 1.08\\ 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$	$\begin{array}{c} 0.90\\ 1.02\\ 1.122\\ 3.3\\ 1.1\\ 1.22\\ 3.3\\ 3.4\\ 4.4\\ 2.3\\ 3.3\\ 3.4\\ 4.4\\ 4.4\\ 3.3\\ 3.3\\ 3.1\\ 1.4\\ 4.4\\ 4.4\\ 3.3\\ 3.3\\ 3.1\\ 1.1\\ 1.2\\ 2.3\\ 1.1\\ 1.2\\ 2.3\\ 1.1\\ 1.2\\ 2.3\\ 1.1\\ 1.2\\ 2.3\\ 1.2\\ 1.2\\ 1.2\\ 1.2\\ 1.2\\ 1.2\\ 1.2\\ 1.2$	$\begin{array}{c} 3.0479\\ 3.379\\ 4.5679\\ 1.1322\\ 1.1322\\ 1.1322\\ 1.1572\\ 4.778\\ 2.2778\\ 1.1572\\ 2.2778\\ 2.2778\\ 2.222\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 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2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ 2.22\\ $	$\begin{array}{c} 2.5\\ 1.9\\ 1.8\\ 2.3\\ 7\\ 2.9\\ 4\\ 3.8\\ 4.1\\ 7.2\\ 2.9\\ 4\\ 3.8\\ 4.1\\ 7.4\\ 4\\ 7.7\\ 8\\ 8.2\\ 8\\ 9\\ 9\\ 1\\ 1\\ 9.0\\ 0\\ 8\\ 7\\ 7\\ 8\\ 8\\ 9\\ 9\\ 4\\ 10.3\\ \end{array}$

Daily gage height, in feet, of Flint River at Albany, Georgia, for 1900.

# FLINT RIVER AT WOODBURY, GEORGIA.

Measurements of the flow of Flint River were made during 1897 and 1898 at Molina, Georgia, but the river bed was so shifting that the station was discontinued on June 2, 1898. Records of the measurements made at Molina will be found as follows: For 1897, Nineteenth Annual Report, Part IV, page 234; for 1898, Twentieth Annual Report, Part IV, page 233. A gage has been maintained at Albany, Georgia, by the United States Weather Bureau, as described in Water-Supply Paper No. 36, page 138. Two measurements were made in 1899 at the Macon and Birmingham bridge near Woodbury, Georgia, 5 miles below the Molina station. On March 29, 1900, a gage was put in near this bridge, and the station was reestablished. The gage is a vertical rod fastened to a willow tree on the left bank of the river about 300 feet above the bridge, and is referred to the bench mark (the top of the iron girder under the cross-ties at a point 12 feet to the left of the center pier), which is 27 feet above the zero of the gage, the zero of the gage being 659.6 feet above sea level. This gage was maintained by the Georgia geological survey until November 1, 1900, when it was adopted by the United States Weather Bureau as a half-year station, instead of the one at Reynolds, Georgia. During 1900 the following measurements were made by B. M. Hall and his assistants:

March 29: Gage height, 2.20 feet; discharge, 2,329 second-feet. May 2: Gage height, 2.85 feet; discharge, 3,220 second-feet. December 12: Gage height, 0.85 foot; discharge, 998 second-feet. December 21: Gage height, 4.35 feet; discharge, 5,423 second-feet.

Daily gage height, in feet, of Flint River at Woodbury, Georgia, for 1900.

Day. Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1	$\begin{array}{c} 1.3\\ 1.2\\ 1.2\\ 1.1\\ 1.1\\ 1.1\\ 1.1\\ 1.1\\ 1.0\\ 1.0\\ 1.0$	$\begin{array}{c} 1.9\\ 1.53\\ 1.4\\ 1.20\\ .98\\ .77\\ .66\\ .55\\ .65\\ 1.08\\ .77\\ .66\\ .55\\ .65\\ 1.08\\ .77\\ .55\\ 1.05\\ 1.5\\ 1.5\\ .55\\ .65\\ .55\\ .65\\ .55\\ .65\\ .55\\ .5$	$\begin{array}{c} 0.6\\ .5\\ .6\\ .1.0\\ 1.4\\ 1.6\\ 1.5\\ 1.4\\ 1.8\\ 1.8\\ 1.8\\ 1.6\\ 1.0\\ .7\\ .65\\ .5\\ 1.0\\ 4.1\\ 4.0\\ 3.8\\ 0\\ 5.0\\ 2.4\\ 0\\ 8.5\\ 8.0\\ 7.0\\ 5.9\\ 5.1\\ 1.4\\ 1\end{array}$	$\begin{array}{c} 2.9\\ 2.85\\ 4.37\\ 4.3.7\\ 4.84\\ 1.10\\ 1.65\\ 1.63\\ 1.00\\ .87\\ .65\\ .65\\ 1.18\\ 1.00\\ 1.26\\ .55\\ 1.18\\ 1.02\\ 1.26\\ .55\\ 1.18\\ 1.02\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 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1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26\\ 1.26$	$\begin{array}{c} & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & & \\ & & & \\ & & & \\ & & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ &$	$\begin{array}{c} 0.4\\ 0.4\\ .7\\ .6\\ .4\\ .32\\ .22\\ .1\\ .13\\ 1.6\\ 1.53\\ 1.18\\ .33\\ .22\\ .22\\ .22\\ .22\\ .22\\ .22\\ .22$	$\begin{array}{c} 0.2\\\\\\\\\\\\\\\\$	$\begin{array}{c} 0.4\\ 1.2\\ 2.3\\ 3.3\\ 2.3\\ 2.3\\ 2.3\\ 3.2\\ .5\\ .65\\ .5\\ .5\\ .5\\ .65\\ .5\\ .5\\ .65\\ .6$	$\begin{array}{c} 0.76 \\531 \\882 \\8231 \\843 \\843 \\843 \\843 \\843 \\8327 \\133 \\133 \\133 \\133 \\133 \\133 \\133 \\133 \\133 \\133 \\133 \\133 \\133 \\133 \\133 \\133 \\133 \\133 \\133 \\133 \\133 \\133 \\133 \\133 \\133 \\133 \\133 \\133 \\133 \\133 \\133 \\133 \\133 \\133 \\133 \\133 \\133 \\133 \\133 \\133 \\133 \\133 \\133 \\133 \\133 \\133 \\133 \\133 \\133 \\133 \\133 \\133 \\133 \\133 \\133 \\133 \\133 \\133 \\133 \\133 \\133 \\133 \\133 \\133 \\133 \\133 \\133 \\133 \\133 \\133 \\133 \\133 \\133 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\\133 \\133 \\133 \\133 \\133 \\133 $

# CHATTAHOOCHEE RIVER AT OAKDALE, GEORGIA.

Two gaging stations are maintained on Chattahoochee River, one at Oakdale, 8 miles northwest of Atlanta, and the other at West Point, Georgia, where the river reaches the Alabama State line. The station at Oakdale was established October 17, 1895, and is described in Water-Supply Paper No. 36, page 139. The results of measurements during 1899 will be found in the Twenty-first Annual Report, Part IV, page 140. During 1900 the following measurements were made by B. M. Hall and his assistants:

January 4: Gage height, 1.53 feet; discharge, 1,784 second-feet. March 27: Gage height, 5.85 feet; discharge, 5,504 second-feet. July 6: Gage height, 4 feet; discharge, 3,886 second-feet. September 12: Gage height, 1.08 feet; discharge, 1,456 second-feet. November 29: Gage height, 2.32 feet; discharge, 2,334 second-feet. Daily gage height, in feet, of Chattahoochee River at Oakdale, Georgia, for 1900.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
Day.  Day.  Day.  Day.  2.  2.  2.  2.  2.  3.  4.  5.  5.  6.  7.  8.  9  10  11  12  13  14  15  16  17  18  19  20  21  22  23  24  24  25  25  25  25  25  25  25  25	Jan. 1.0 .7 .5 .9 1.2 1.3 1.2 1.3 1.2 1.3 1.2 1.3 1.2 1.7 1.2 1.7 1.2 1.7 1.2 1.7 1.2 1.7 1.2 1.7 1.2 1.2 1.3 1.2 1.2 1.7 1.2 1.7 1.2 1.7 1.2 1.7 1.2 1.3 1.2 1.7 1.2 1.3 1.2 1.7 1.2 1.3 1.2 1.7 1.2 1.3 1.2 1.7 1.2 1.3 1.2 1.3 1.2 1.5 1.2 1.5 1.2 1.5 1.2 1.5 1.2 1.5 1.2 1.5 1.2 1.5 1.2 1.5 1.5 1.2 1.5 1.2 1.5 1.2 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5	Feb. 1.0 9 9 2.9 3.8 4.3 8.0 1.5 20.7 16.4 4.8 3.5 3.1 3.0 4.23 4.23 4.24 4.24 4.24 4.24 4.25 3.45 3.45 3.45 3.45 3.45 3.45 3.45 3.45 3.45 3.45 3.45 3.45 3.45 3.45 3.45 3.45 3.45 3.45 3.45 3.45 3.45 3.45 3.45 3.45 3.45 3.45 3.45 3.45 3.45 3.45 3.45 3.45 3.45 3.45 3.45 3.45 3.45 3.45 3.45 3.45 3.45 3.45 3.45 3.45 3.45 3.45 3.45 3.45 3.45 3.45 3.45 3.45 3.45 3.45 3.45 3.45 3.45 3.45 3.45 3.45 3.45 3.45 3.45 3.45 3.45 3.45 3.55 3.45 3.45 3.45 3.55 3.45 3.45 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3.55	Mar. 4.5 5.9 4.5 3.6 3.3 1 3.0 8.8 8.6 3.3 1 3.0 8.8 7.9 6.5 5 4.0 1 3.2 3.0 0 3.6 3.0 8.5 5.5 4.0 1 3.2 5.0 9 4.5 5.5 9 4.5 5.5 9 4.5 5.5 8 4.5 8 5.5 8 5.5 8 5.5 8 5.5 8 5.5 8 5.5 8 5.5 8 5.5 8 5.5 8 5.5 8 5.5 8 5.5 8 5.5 8 5.5 8 5.5 8 5.5 8 5.5 8 5.5 8 5.5 8 5.5 8 5.5 8 5.5 8 5.5 8 5.5 8 5.5 8 5.5 8 5.5 8 5.5 8 5.5 8 5.5 8 5.5 8 5.5 8 5.5 8 5.5 8 5.5 8 5.5 8 5.5 8 5.5 8 5.5 8 5.5 8 5.5 8 5.5 8 5.5 8 5.5 8 5.5 8 5.5 8 5.5 8 5.5 8 5.5 8 5.5 8 5.5 8 5.5 8 5.5 8 5.5 8 5.5 8 5.5 8 5.5 8 5.5 8 5.5 8 5.5 8 5.5 5 5.5 5 5.5 5 5.5 5 5.5 5 5.5 5 5.5 5 5.5 5 5.5 5 5.5 5 5.5 5 5.5 5 5.5 5 5.5 5 5.5 5 5.5 5 5.5 5 5.5 5 5.5 5 5.5 5 5.5 5 5.5 5 5.5 5 5.5 5 5.5 5 5.5 5 5.5 5 5.5 5 5.5 5 5.5 5 5.5 5 5.5 5 5.5 5 5.5 5 5.5 5 5.5 5 5.5 5 5.5 5 5.5 5 5.5 5 5.5 5 5.5 5 5.5 5 5.5 5 5.5 5 5.5 5 5.5 5 5.5 5 5.5 5 5.5 5 5.5 5 5.5 5 5 5.5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	$\begin{array}{c} \textbf{Apr.} \\ \hline \\ \\ \hline \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\$	May. 5.0 4.85 4.0 3.0 0 3.0 0 3.0 0 3.0 0 2.9 9 2.8 7 2.26 2.66 2.66 2.55 3.77 3.0 1 3.27 3.9 2.9 9 2.9 2.9 2.9 2.9 2.9 2.9 2.9 2.9 2.9 2.9	$\begin{array}{c} {\tt June.}\\ \hline \\ \hline \\ \hline \\ \\ \hline \\ \\ \hline \\ \\ \\ \\ \\ \\ \\ \\$	$\begin{array}{c} July.\\ \hline \\ 5.0 \\ 4.5 \\ 6.0 \\ 7.5 \\ 7.5 \\ 7.5 \\ 7.5 \\ 6.4 \\ 6.5 \\ 8 \\ 5.7 \\ 5.5 \\ 5.4 \\ 2 \\ 5.0 \\ 4.4 \\ 4.3 \\ 4.3 \\ 4.1 \\ 4.0 \\ 3.9 \\ 3.8 \\ 7 \\ 3.7 \\ 0 \end{array}$	Aug. 5.0 4.5 4.0 4.0 4.0 4.0 4.0 3.5 3.5 3.5 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0	Sept. 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.	$\begin{array}{c} \text{Oct.} \\ \hline \\ 2.1 \\ 2.1 \\ 2.1 \\ 3.0 \\ 3.8 \\ 4.0 \\ 4.0 \\ 3.9 \\ 3.5 \\ 3.9 \\ 4.2 \\ 4.0 \\ 3.6 \\ 3.4 \\ 3.5 \\ 3.9 \\ 4.2 \\ 3.0 \\ 3.6 \\ 3.4 \\ 3.2 \\ 8 \\ 3.0 \\ 3.6 \\ 3.3 \\ 3.0 \\ 3.3 \\ 3.0 \\ 3.3 \\ 3.0 \\ 3.3 \\ 3.0 \\ 3.3 \\ 3.0 \\ 3.3 \\ 3.0 \\ 3.3 \\ 3.0 \\ 3.3 \\ 3.0 \\ 3.3 \\ 3.0 \\ 3.3 \\ 3.0 \\ 3.3 \\ 3.0 \\ 3.3 \\ 3.0 \\ 3.3 \\ 3.0 \\ 3.3 \\ 3.0 \\ 3.3 \\ 3.0 \\ 3.3 \\ 3.0 \\ 3.3 \\ 3.0 \\ 3.3 \\ 3.0 \\ 3.3 \\ 3.0 \\ 3.3 \\ 3.0 \\ 3.3 \\ 3.0 \\ 3.3 \\ 3.0 \\ 3.3 \\ 3.0 \\ 3.3 \\ 3.0 \\ 3.3 \\ 3.0 \\ 3.3 \\ 3.0 \\ 3.3 \\ 3.0 \\ 3.3 \\ 3.0 \\ 3.3 \\ 3.0 \\ 3.3 \\ 3.0 \\ 3.3 \\ 3.0 \\ 3.3 \\ 3.0 \\ 3.3 \\ 3.0 \\ 3.3 \\ 3.0 \\ 3.3 \\ 3.0 \\ 3.3 \\ 3.0 \\ 3.3 \\ 3.0 \\ 3.3 \\ 3.0 \\ 3.3 \\ 3.0 \\ 3.3 \\ 3.0 \\ 3.3 \\ 3.0 \\ 3.3 \\ 3.0 \\ 3.3 \\ 3.0 \\ 3.3 \\ 3.0 \\ 3.3 \\ 3.0 \\ 3.3 \\ 3.0 \\ 3.3 \\ 3.0 \\ 3.3 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\ 3.0 \\$	Nov. 2.4 2.4 3.00 2.25 5.25 5.25 2.55 2.24 2.4 2.4 2.4 2.21 2.21 2.21 2.21 2.	Dec. 2.2 2.2 2.2 2.1 2.3 4.1 4.0 3.8 7 3.5 2.1 2.0 2.3 2.2 2.1 2.1 2.3 2.2 2.1 2.1 2.3 2.2 2.1 2.1 2.3 2.2 2.2 2.2 2.1 2.3 2.2 2.2 2.2 2.2 2.2 2.2 2.2 2.2 2.2
26 27 28 28 29 29 30 31	$     \begin{array}{r}       2.0 \\       1.9 \\       1.7 \\       1.5 \\       1.5 \\       1.4 \\       1.3 \\     \end{array} $	4.1 4.0 3.3 3.0	$\begin{array}{c} 1.1 \\ 7.5 \\ 6.0 \\ 4.5 \\ 4.0 \\ 3.8 \\ 3.5 \\ \end{array}$	$     \begin{array}{r}       4.5 \\       6.0 \\       5.5 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       5.0 \\       $	$     \begin{array}{r}       3.5 \\       3.4 \\       3.2 \\       3.0 \\       2.5 \\       2.4 \\       \end{array} $	$     \begin{array}{r}       17.5 \\       11.4 \\       10.5 \\       7.5 \\       6.0 \\       5.5 \\       \end{array} $	$\begin{array}{c} 4.0\\ 5.0\\ 6.0\\ 6.5\\ 7.4\\ 10.0\\ 6.0\end{array}$	2.7 2.6 2.5 3.0 3.0 2.7	2.5 2.0 2.0 1.8 1.5 1.5	$     \begin{array}{r}       3.0 \\       3.9 \\       2.8 \\       2.6 \\       2.4 \\       2.4     \end{array} $	1.8 1.8 5.6 3.3 2.3 2.0	2.7 2.5 2.3 2.3 3.0 3.8

## CHATTAHOOCHEE RIVER AT WEST POINT, GEORGIA.

This station was established July 30, 1896, on the highway bridge in West Point, Georgia, about 500 feet below the railroad bridge. It is described in Water-Supply Paper No. 36, page 142. The gage was last verified December 4, 1900. The observer is C. E. Melton. The results of measurements during 1899 will be found in the Twenty-first Annual Report, Part IV, page 141. During 1900 the following measurements were made by B. M. Hall and his assistants:

January 20: Gage height, 4.65 feet; discharge, 6,574 second-feet. February 24: Gage height, 4.92 feet; discharge, 7,158 second-feet. August 22: Gage height, 2.80 feet; discharge, 2,755 second-feet. December 4: Gage height, 3.93 feet; discharge, 5,224 second-feet. 159

Daily gage height, in feet, of Chattahoochee River at West Point, Georgia, for 1900.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1	3.00	2.80	5.90	4.10	4.90	3.40	6.30	6.40	4.10	2.60	2.80	3.70
3	$\frac{2.80}{2.50}$	$\frac{2.60}{2.40}$	$\frac{4.70}{4.60}$	$4.10 \\ 4.05$	$\frac{4.80}{4.60}$	3.30 3.30	9.40 7.80	5.70 5.00	6.10 4.50	$2.50 \\ 2.50$	$\frac{2.70}{4.60}$	$\begin{bmatrix} 3.20 \\ 3.10 \end{bmatrix}$
4	2.50	3.00	5.00	4.05	4.40	3.60	7.00	4.50	3.20	2.60	4.20	3.90
5	2.40	3.00	4.80	4.00	4.30	5.00	6.50	4.00	3.00	3.80	4.30	4.50
⁶ / ₇	2.80	$\frac{4.60}{4.50}$	4.50	3.95	4.20	4.80	6.20 5.40	3.60	2.90	$\frac{4.00}{4.90}$	3.60	5.00
8	2.80	4.20	5.00	3.90	3.80	$\frac{4.50}{5.10}$	5.40 5.00	3.20	2.70	3.70	3.20	4.60
9	2.80	4.60	8.10	3.85	3.60	8.10	5.10	3.10	2.60	3.50	3.10	3.90
10	2.70	7.30	7.50	3.80	3.60	8.50	4.20	3.00	2.50	3.40	3.00	3.60
10	3.40	8.60	6.30	4.90	3.50	5.80	4.00	2.90	2.40	3,40	3.00	3,30
12	4.70	19.12	3.00	6.70	3.40	4.00	5.40	2.80	2.00	3.00	2.90	3.10
14	4.70	19.50	4.50	6.00	3.40	3,90	5.00	3.80	2.30	3.70	2.80	4.90
15	4.90	18.50	4.30	5.50	3.30	4.20	4.80	3.00	9.20	3.20	2.80	4.20
16	4.60	12.40	4.50	4.20	3.30	6.40	4.50	3.00	12.60	3.00	2.70	3.70
17	3.70	5.90	$\frac{4.30}{4.10}$	$\frac{4.00}{6.00}$	3.20	6.00	$\frac{4.30}{4.10}$	2.90	8.80	3.00	2.70	3.50
10	3 90	4 70	5 00	7 70	3 70	8 40	4 00	2.80	5 70	2 90	2 70	3.00
20	4.60	4.50	5.20	8.50	3.60	6,00	3, 80	2.80	4.30	2.80	2.70	5.80
21	4.80	4.60	5.20	7.40	3.50	4.50	3.60	2.80	3.20	2.80	2.60	6.50
22	5.10	4.60	6.30	7.00	3.40	3.80	3.50	2.80	3.00	3.00	2.80	6.40
60 DA	4.20	4.70	5.80	7.00	5.40	4.60	3.80	2.90	2.90	4.00	3.90	5 30
25	3.70	4.80	6.10	9.20	4,40	17.80	3.60	3.80	2.80	4.90	3.20	4.80
26	3.30	5.00	6.50	8.00	4.20	14.60	3.60	3.40	2.70	3.40	3.80	4.20
27	3.20	4.60	5.80	6.00	4.00	12.20	4.00	3.20	2.70	3.20	4.50	4.10
28	3.00	4.90	5.40	4.80	3.60	8.40	6.10	3.00	2.70	3.00	4.00	3.90
89	2.00		5.30 5.10	4.00	0.00 3.40	5.00 6.70	12 60	2.90	2 60	2.80	<b>5.00</b> 4.60	3.60
31	2.90		4.50	0.40	3.40	0.10	9.20	3.90	2.00	2.80	+,00	7.20
			1.00		0.10		0.140	0.00				

#### ETOWAH RIVER AT CANTON, GEORGIA.

This station was established by the United States Weather Bureau March 12, 1892. It is located on the iron highway bridge about 1,000 feet north of the Atlanta, Knoxville and Northern Railway station at Canton and about a half mile north of Canton Creek. The gage is a vertical timber attached to the upstream side of the left-bank pier of the bridge, and is graduated to feet and tenths. Owing to high water at the time the gage was put in it was set 1 foot higher than intended. Recognizing the error, the gage-height records were begun by adding 1 foot to the actual readings. It was the intention to lower the gage as soon as the water went down, but this has not been done, so that all of the gage heights and discharge measurements have been based on the rod with the zero point set 1 foot lower than the actual rod. The gage will probably be lowered to its proper place during the year 1901. This station is described in Water-Supply Paper No. 36, page 143. Records of measurements during 1899 will be found in the Twentyfirst Annual Report, Part IV, page 145. During 1900 the following measurements were made by B. M. Hall and his assistants:

February 27: Gage height, 0.80 foot; discharge, 1,113 second-feet. May 19: Gage height, 1.05 feet; discharge, 1,351 second-feet. December 1: Gage height, 0.55 foot; discharge, 816 second-feet.

#### GEORGIA.

Daily gage height, in feet, of Etowah River at Canton, Georgia, for 1900.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1           2           3           4           5           7           8           9           10           11           12           13           14           15           16           17           18           19           20           23           24           25           26           27           28           29           30	$\begin{array}{c} 0.66 \\ .66 \\ .66 \\ .66 \\ .66 \\ .66 \\ .66 \\ .66 \\ .66 \\ .44 \\ .40 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 \\ .44 $	0.6 8 1.0 1.2 1.2 2.5 1.8 2.7 2.5 1.4 2.0 3.1 1.5 1.5 1.0 1.0 1.0 1.0 1.0 1.0 1.5 1.5 1.5 1.6 8 .0 1.0 1.5 1.5 1.0 1.0 1.5 1.0 1.5 1.0 1.0 1.2 2.5 8 1.0 1.0 1.2 2.5 8 1.0 1.0 1.2 2.5 8 1.0 1.0 1.2 2.5 8 1.0 1.0 1.2 2.5 8 1.0 1.0 1.2 2.5 8 1.0 1.0 1.2 2.5 8 1.0 1.0 1.2 2.5 8 1.0 1.0 1.2 2.5 8 1.0 1.0 1.0 2.5 1.0 1.0 2.5 1.0 1.0 2.5 1.0 1.0 2.5 1.0 1.0 2.5 1.0 1.0 2.5 1.0 1.0 2.5 1.0 1.0 2.5 1.0 1.0 2.5 1.0 1.0 2.5 1.0 1.0 2.5 1.0 1.0 2.5 1.0 2.5 1.0 1.0 2.5 1.0 2.5 1.0 1.0 2.5 1.0 2.5 1.0 2.5 1.0 1.0 2.5 1.0 2.5 1.0 2.5 1.0 2.5 1.0 2.0 1.0 2.5 1.0 2.5 1.0 2.5 1.0 2.5 1.0 2.0 1.0 2.5 1.0 2.0 1.0 2.0 1.0 2.0 1.0 2.0 1.0 2.0 1.0 2.0 1.0 2.0 1.0 2.0 1.0 2.0 1.0 2.0 1.0 2.0 1.0 2.0 1.0 2.0 1.0 2.0 1.0 2.0 1.0 2.0 1.0 2.0 1.0 2.0 1.0 2.0 1.0 2.0 1.0 2.0 1.0 2.0 1.0 2.0 1.0 2.0 1.0 2.0 1.0 2.0 1.0 2.0 1.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2	0.888.888 .888.888. .888.888. .888.442 .1099.999.999. .536888816 .888.1600 .888.9999. .536888816 .888.1600 .888.1600 .888.1600 .888.1600 .888.1600 .888.1600 .888.1600 .888.1600 .888.1600 .999.1000 .536.888.1600 .532.2000 .532.2000 .532.2000 .532.2000 .532.2000 .532.2000 .532.2000 .532.2000 .532.2000 .532.2000 .532.2000 .532.2000 .532.2000 .532.2000 .532.2000 .532.2000 .532.2000 .532.2000 .532.2000 .532.2000 .532.2000 .532.2000 .532.2000 .532.2000 .532.2000 .532.2000 .532.2000 .532.2000 .532.2000 .532.20000 .532.2000 .532.2000 .532.2000 .532.2000 .532.2000 .532.2000 .532.2000 .532.2000 .532.2000 .532.2000 .532.2000 .532.2000 .532.2000 .532.2000 .532.2000 .532.2000 .532.2000 .532.2000 .532.2000 .532.2000 .532.2000 .532.2000 .532.2000 .532.2000 .532.2000 .532.2000 .532.2000 .532.2000 .532.2000 .532.2000 .532.2000 .532.2000 .532.2000 .532.2000 .532.2000 .532.2000 .532.2000 .532.2000 .532.2000 .532.2000 .532.2000 .532.2000 .532.2000 .532.2000 .532.2000 .532.2000 .532.2000 .532.2000 .532.2000 .532.2000 .532.20000000000000000000000000000000000	1.4 1.4 1.4 1.0 .8 .8 .8 .8 .8 .8 .8 .8 .8 .8	$\begin{array}{c} 1.2\\ 1.2\\ 1.2\\ 1.2\\ 1.2\\ 1.2\\ 1.2\\ 1.2\\$	$\begin{array}{c} 1.4\\ 1.4\\ 2.4\\ 2.0\\ 3.0\\ 3.0\\ 6.0\\ 4.0\\ (a)\\ (a)\\ (a)\\ (a)\\ (a)\\ (a)\\ (a)\\ (a)$	$\begin{array}{c} 1.7\\ 1.7\\ 1.8\\ 1.8\\ 1.8\\ 2.2\\ 1.0\\ 1.0\\ 1.0\\ 1.0\\ 1.0\\ 1.0\\ 1.0\\ 1.0$	$\begin{array}{c} \hline \\ \hline $	$\begin{array}{c} 0.6\\ .66\\ .66\\ .66\\ .66\\ .66\\ .66\\ .66\\$	$\begin{array}{c} 0.322\\ \cdot & \cdot \\ \cdot & \cdot \\ 1.533210\\ \cdot & \cdot \\ 2.22222\\ \cdot & \cdot \\ 1.100\\ \cdot & \cdot \\ 2.22222\\ \cdot & \cdot \\ 1.100\\ \cdot & \cdot \\ 2.55750\\ \cdot & \cdot \\ 2.2222\\ \cdot & \cdot \\ 1.100\\ \cdot & \cdot \\ 1.000\\ \cdot & \cdot \\ 2.55750\\ \cdot & \cdot \\ 2.2222\\ \cdot & \cdot \\ 1.1222\\ \cdot & \cdot \\ 1.1222\\ \cdot & \cdot \\ 2.2222\\ \cdot & \cdot \\ 1.1222\\ \cdot & \cdot \\ 2.2222\\ \cdot & \cdot \\ 1.1222\\ \cdot & \cdot \\ 2.2222\\ \cdot & \cdot \\ 2.22222\\ \cdot & \cdot \\ 2.222222\\ \cdot & \cdot \\ 2.222222\\ \cdot & \cdot \\ 2.222222\\ \cdot & \cdot \\ 2.2222222\\ \cdot & \cdot \\ 2.2222222\\ \cdot & \cdot \\ 2.22222222\\ \cdot & \cdot \\ 2.222222222\\ \cdot & \cdot \\ 2.22222222222222\\ \cdot & \cdot \\ 2.222222222222222222222222222222222$	$\begin{array}{c} 1.3\\ 1.4\\ 1.6\\ 1.4\\ 1.4\\ 1.4\\ 1.4\\ 1.4\\ 1.4\\ 1.4\\ 1.4$	$\begin{array}{c} 0.66\\55\\528\\28\\26\\528\\28\\26\\528\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\28\\$

a No record.

#### COOSAWATTEE RIVER AT CARTERS, GEORGIA.

This station was established August 15, 1896, at the iron highway bridge at Carters, Murray County, Georgia, about 20 miles northeast of Calhoun. The gage was last verified November 17, 1900. The station is described in Water-Supply Paper No. 36, page 144. Records of measurements during 1899 will be found in the Twenty-first Annual Report, Part IV, page 146. During 1900 the following measurements were made by O. P. Hall and Max Hall:

April 28: Gage height, 2.60 feet; discharge, 1,075 second-feet.
May 11: Gage height, 2.15 feet; discharge, 811 second-feet.
May 24: Gage height, 2.05 feet; discharge, 781 second-feet.
August 13: Gage height, 1.58 feet; discharge, 576 second-feet.
September 7: Gage height, 1.25 feet; discharge, 423 second-feet.
November 17: Gage height, 1.37 feet; discharge, 458 second-feet.
November 26: Gage height, 4.08 feet; discharge, 1,899 second-feet.
December 22: Gage height, 2.70 feet; discharge, 1,132 second-feet.

Daily gage height, in feet, of Coosawattee River at Carters, Georgia, for 1900.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Nov.	Dec.
1	1.20	1.40	3.00	2.40	2.70	1.90	3.50	2.00	<i>(a)</i>	1.40
2	1.20 1.10	$1.40 \\ 1.30$	$\frac{3.10}{2.70}$	$\frac{2.40}{2.50}$	$\frac{2.60}{2.50}$	$\frac{2.00}{2.00}$	$\frac{3.50}{5.00}$	2.00	$\begin{pmatrix} (a) \\ (a) \end{pmatrix}$	$1.40 \\ 1.50$
4	1.10	1.40	2.80	2.60	2.40	2.00	4.80	1.90	1.50	1.60
5	1.00	1.50	4.75	2.50	2.30	2.10	4.00	1.80	1.40	1.80
0 7	1.00	1.70 1.80	$\frac{4.75}{4.90}$	$\frac{2.00}{2.60}$	2.20	$\frac{2.20}{5.00}$	3.80	$1.70 \\ 1.70$	1.50 1.50	1.70
8	1.10	2.00	5.20	2.50	$\tilde{2}.10$	3.00	3.50	1.70	1.60	1.60
9	1.20	4.10	5,00	2.60	2.40	5.00	3.40	1.60	1.60	1.60
10	4.00	2.50 2.50	4.60	$\frac{2.70}{4.00}$	$\frac{2.20}{2.00}$	4.50	3.50 3.40	$1.00 \\ 1.60$	1.50	1.50 1.40
12	7.00	8.50	2.90	5.00	1.90	2.20	3.30	1.60	1.40	1.40
13	3.50	20.50	3.00	3.00	1.70	2.00	3.00	1.50	1.40	1.50
14	2.00	5.40	2.90	2.50	$1.70 \\ 1.80$	$\frac{2.40}{2.60}$	2.80	1.50 1.40	1.30 1.30	1.60 1.70
16	1.70	3.20	2.50	2.70	1.80	3.00	2.60	1.40	1.30	1.60
17	1.70	2.80	2.50	2.80	2.10	3.00	2.40	1.50	1.40	1.80
18	$\frac{2.00}{4.30}$	2.70 2.50	$\frac{3.00}{7.50}$	3.00	2.00 1.00	$\frac{3.40}{5.00}$	$\frac{2.20}{2.00}$	1.50 1.50	1.40	2.00
20	4.00	2.30 2.20	4.00	3.70	1.80 1.80	5.60	$\tilde{2.00}$	1.60	1.30	4.00
21	2.50	3.00	3.50	4.50	1.70	4.20	2.00	1.60	1.30	3.20
99 99	2.20	3.20	3,00	3.50	1.70	$\frac{4}{4}.70$	1.90	1.80	1.40	2.60
24	2.00	3.10 3.05	$\frac{2.50}{2.50}$	2,90	1.90	4.00	$\frac{1.60}{3.00}$	$2.00 \\ 2.50$	1.40 1.60	2.60
25	1.90	3.00	2.00	2.80	2.00	5.00	2.20	1.90	3.50	2.50
26	1.80	3.00	5.00	2.70	2.10	6.00	$\frac{3.50}{5.90}$	(a)	5.00	2.50
28	1.80	$2.90 \\ 2.50$	3.60 3.50	3,00	1.90	5,00	3.20 3.20	(a)	$\frac{4.00}{2.50}$	2.40 2.30
29	1.60		3.10	3.10	1.80	4.50	2.40	(a)	1.50	2.40
30	1.50		3.00	3.00	1.80	4.00	2.30	(a)	1.50	2.50
31	1.50		2.80		1.90		2.20	<i>(a)</i>		2.60

a No record August 26 to November 3.

### OOSTANAULA RIVER AT RESACA, GEORGIA.

This station was established July 27, 1896, on the iron bridge of the Western and Atlantic Railroad in the town of Resaca, Georgia, 1,000 feet from the railroad station. It is described in Water-Supply Paper No. 36, page 146. Records of measurements during 1899 will be found in the Twenty-first Annual Report, Part IV, page 147. During 1900 the following measurements were made by O. P. Hall:

April 30: Gage height, 8 feet; discharge, 5,118 second-feet. May 15: Gage height, 3.60 feet; discharge, 1,466 second-feet. May 25: Gage height, 3.75 feet; discharge, 1,539 second-feet. December 11: Gage height, 4.30 feet; discharge, 1,919 second-feet.

#### GEORGIA.

Daily gage height, in feet, of Oostanaula River at Resaca, Georgia, for 1900.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	Nov.	Dec.
1         2         3         4         5         6         7         8         9         11         12         33         4         15         6         17         18         9         20         21         22         23         24         25         26         27         28         29         30         31         32         33         34         35         36         37         38         39         30         31         32         33         34         35         36         37         38         39         30         31         32         33         34         35         36	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 3.1\\ 3.0\\ 3.0\\ 3.1\\ 4.3\\ 3.5\\ 5.6\\ 9.1\\ 7.3\\ 20.3\\ 23.5\\ 20.3\\ 23.5\\ 20.8\\ 23.5\\ 20.8\\ 23.5\\ 5.5\\ 5.2\\ 5.3\\ 9.1\\ 8.9\\ 7.0\\ 6.0\\ 5.5\\ 5.5\\ 3.4\\ 9.1\\ 8.9\\ 7.0\\ 6.5\\ 5.5\\ 5.2\\ 5.5\\ 5.2\\ 5.5\\ 5.2\\ 5.5\\ 5.2\\ 5.5\\ 5.2\\ 5.5\\ 5.5$	$\begin{array}{c} 6.0\\ 7.3\\ 6.8\\ 5.9\\ 5.1\\ 1.5\\ 1.3\\ 15.5\\ 1.4\\ 2\\ 11.1\\ 1\\ 7.6\\ 6.0\\ 5.6\\ 7.3\\ 6.0\\ 16.9\\ 17.2\\ 8\\ 8.8\\ 7.7\\ 8.0\\ 12.2\\ 8\\ 8.8\\ 7.2\\ 6.6\\ 2\end{array}$	$\begin{array}{c} 5.8\\ 5.8\\ 5.3\\ 5.6\\ 6.3\\ 5.0\\ 6.2\\ 5.0\\ 4.8\\ 6.2\\ 5.0\\ 4.8\\ 4.6\\ 7.2\\ 6.2\\ 5.8\\ 11.9\\ 12.0\\ 10.4\\ 11.8\\ 9.7\\ 7.2\\ 6.2\\ 5.5\\ 5.8\\ 5.6\\ 5.5\\ 7.8\\ \end{array}$	$\begin{array}{c} 6.87\\ 5.5538\\ 4.464\\ 0.9887\\ 6.5638\\ 3.3664\\ 4.4338\\ 3.389\\ 8.766\\ 7.80\\ 3.366\\ 4.43\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.38\\ 3.3$	$\begin{array}{c} 3.3\\ 3.5\\ 3.5\\ 4.0\\ 5.0\\ 7.7\\ 7.9\\ 13.0\\ 10.5\\ 5.6\\ 5.8\\ 6.6\\ 6.8\\ 6.6\\ 6.8\\ 10.9\\ 7.0\\ 6.5\\ 8\\ 9.9\\ 12.8\\ 9.9\\ 12.8\\ 9.9\\ 12.8\\ 9.9\\ 12.8\\ 9.9\\ 12.8\\ 14.0\\ 15.0\\ 17.2\\ 17.5\\ 13.0\\ 9.6\\ \end{array}$	$\begin{array}{c} 8 & 9 \\ 2 & 2 \\ 3 \\ 3 \\ 4 \\ 4 \\ 6 \\ 5 \\ 7 \\ 5 \\ 0 \\ 9 \\ 8 \\ 8 \\ 8 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7$	$\begin{array}{c} 4.52\\ 4.400\\ 8.606\\ 8.306\\ 5.508\\ 4.400\\ 4.009\\ 3.554\\ 4.409\\ 9.35\\ 4.409\\ 9.807\\ 7.666\\ 4.5427\\ 5.77\end{array}$

*a* Frozen. NOTE.—This is a half-year Weather Bureau station.

#### COOSA RIVER AT ROME, GEORGIA.

This station is described in Water-Supply Paper No. 36, page 148. Measurements of flow are made at Rome, also at Riverside, 120 miles farther downstream. The measurements at Rome are made on the Oostanaula and the Etowah just above their junction to form the Coosa. Etowah River is measured at the Second avenue bridge, and Oostanaula River at the Fifth avenue bridge, and the results added together give the flow of Coosa River at Rome. Results of measurements during 1899 will be found in the Twenty-first Annual Report, Part IV, page 149. During 1900 the following measurements were made by Max Hall and others:

February 21: Gage height, 4.80 feet; discharge, 8,115 second-feet. May 19: Gage height, 2.30 feet; discharge, 4,496 second-feet. September 13: Gage height, 0.90 foot; discharge, 1,992 second-feet. December 8: Gage height, 3.73 feet; discharge, 6,066 second-feet. Daily gage height, in feet, of Coosa River at Rome, Georgia, for 1900.

Day.	Jan.	Feb.	Mar.	Apr,	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1	2.0	2.0	$\frac{4.2}{5.8}$	$\frac{4.4}{4.2}$	6.2	2.4	10.5	3.4	1.5	1.2	2.1	3.2
3	$1.0 \\ 1.5$	1.6	5.6	4.0	4.0	2.8	8.0	3.0	1.7	1.0	2.0	2.6
4 5	$\frac{1.5}{1.5}$	$\frac{2.0}{3.0}$	$\frac{4.4}{4.1}$	$\frac{4.0}{4.0}$	4.0	4.2	7.0	2.8	1.7 1.5	1.0	2.3	3.5 7 4
6	1.5	3.8	3.8	4.0	3.7	4.2	4.2	2.5	$1.5 \\ 1.5$	. 9	2.1	6.8
7	1.5	2.8	5.0	3.8	3.6	4.8	3.8	2.2	1.4	. 9	2.1	5.2
9	1.5	4.0	5. 2 15. 0	ə. ə 3. 6	ə. 4 3. 0	$13.0 \\ 12.6$	a. 8 4. 0	$2.2 \\ 2.0$	$1.0 \\ 1.0$	5.9	1.9	
10	1.5	6.9	13.4	3.5	3.0	8.0	4.3	2.0	.8	2.6	1.8	3.2
11 12	$\frac{2.0}{7.0}$	6.4	10.3 7.5	6.0	3.0	$5.9 \\ 5.0$	3.8	1.8	.8	2.0	1.8	$\frac{2.8}{2.6}$
13	9.0	22.6	5.5	7.4	2.5	5.2	3.8	1.8	.8	2.5	1.5	2.6
14	$\frac{7.2}{5.5}$	27.2	4.8	5.5	2.4	$\frac{5.3}{4.2}$	$\frac{3.4}{3.4}$	$\frac{1.7}{2.0}$	.8	$\frac{3.2}{3.0}$	$1.5 \\ 1.5$	2.4
16	3.5	21.2	5.3	5.6	2.4	3.8	3.3	1.7	11.1	2.0	1.5	2.2
17	3.0	18.0	5.6	6.2	2.4	4.8	$\frac{3.1}{3.0}$	1.6	7.0	1.6	1.5	2.2
19	$5.0^{9}{5.0}$	5.0	5.2	11.0	2.9	6.5	2.8	$\frac{1.0}{2.2}$	2.3	1.5	1.4	2.0
20	11.3	4.0	15.9	11.4	3.0	7.2	2.6	2.0	2.0	1.4	$\frac{1.6}{1.0}$	2.8
$\frac{21}{22}$	10.6	$\frac{4.1}{6.8}$	17.5 14.6	13.0 12.7	$\frac{2.0}{2.5}$	4.2	2.5	$1.0 \\ 1.6$	1.8	1.8	$\frac{1.8}{2.1}$	8.0
23	5.8	7.6	10.4	10.5	2.3	5.5	2.4	1.6	1.6	1.6	2.1	7.0
24	4.0	6.0 5.8	8.8	8.6	2.9	14.2 18.2	2.4	$1.9 \\ 2.4$	$1.6 \\ 1.5$	$1.6 \\ 1.5$	$\frac{2.0}{5.0}$	6.6
26	3.1	5.2	13.0	6.5	2.7	17.0	2.8	2.0	1.5	1.5	11.0	5.6
27	2.8	4.6	12.1	$5.3 \\ 4.8$	$\frac{2.6}{2.5}$	15.5 15.6	$6.2 \\ 6.8$	1.8	l.4 14	$\frac{1.4}{2.2}$	11.5	4.0
29	2.4		5.8	4.3	2.4	14.2	6.2	1.5	1.3	2.2	7.0	3.6
30	$\frac{2.1}{2.0}$		5.7	6.0	$\frac{2.9}{3.0}$	10.0	4.5	$1.5 \\ 1.5$	1.3	2.1	4.0	3.5
01	~.0		0.0		5.0		4.0	1.0		A.1		0.0

COOSA RIVER NEAR RIVERSIDE, ALABAMA.

This station, established September 25, 1896, is at the bridge of the Southern Railway near Riverside. It is described in Water-Supply Paper No. 36, page 149. Records of measurements during 1899 will be found in the Twenty-first Annual Report, Part IV, page 150. During 1900 the following measurements were made by Max Hall and others:

February 10: Gage height, 5.03 feet; discharge, 13,493 second-feet. March 21: Gage height, 12.50 feet; discharge, 43,759 second-feet. May 5: Gage height, 4.15 feet; discharge, 11,196 second-feet. August 21: Gage height, 2.32 feet; discharge, 5,609 second-feet. December 28: Gage height, 4.25 feet; discharge, 11,335 second-feet. Daily gage height, in feet, of Coosa River near Riverside, Alabama, for 1900.

	Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1234567		$\begin{array}{r} 3.50 \\ 3.00 \\ 2.50 \\ 2.40 \\ 2.15 \\ 2.05 \\ 1.95 \end{array}$	$\begin{array}{c} 2.\ 70\\ 2.\ 65\\ 2.\ 60\\ 2.\ 50\\ 2.\ 60\\ 2.\ 80\\ 2.\ 95 \end{array}$	$\begin{array}{c} 6.90\\ 7.55\\ 6.90\\ 6.25\\ 5.40\\ 5.00\\ 4.90 \end{array}$	$\begin{array}{r} 6.65\\ 6.25\\ 6.00\\ 5.60\\ 5.10\\ 4.90\\ 4.75\end{array}$	$5.00 \\ 5.30 \\ 5.30 \\ 4.75 \\ 4.30 \\ 4.20 \\ 4.00$	2.752.802.902.602.703.453.90	$11.60 \\ 10.10 \\ 8.90 \\ 8.20 \\ 7.50 \\ 6.45 \\ 5.50$	$\begin{array}{r} 4.70\\ 3.90\\ 3.00\\ 2.75\\ 2.55\\ 2.40\\ 2.25\end{array}$	1.852.002.202.102.001.801.70	$\begin{array}{c} 1.55\\ 1.55\\ 1.50\\ 1.50\\ 1.50\\ 1.45\\ 1.40\end{array}$	$\begin{array}{r} 2.30\\ 2.25\\ 2.50\\ 2.50\\ 2.50\\ 2.40\\ 2.40\end{array}$	5.75 4.35 3.75 3.40 3.30 4.35 6.05
		$\begin{array}{c} 1.95\\ 2.00\\ 2.00\\ 2.10\\ 3.50\\ 6.00\\ 7.40\\ 7.00\end{array}$	$\begin{array}{c} 3.\ 00\\ 3.\ 75\\ 4.\ 25\\ 5.\ 80\\ 6.\ 50\\ 13.\ 30\\ 15.\ 30\\ 15.\ 20\end{array}$	$\begin{array}{c} 6.00\\ 8.75\\ 10.00\\ 10.55\\ 10.05\\ 8.75\\ 7.50\\ 5.60\\ \end{array}$	$\begin{array}{r} 4.40 \\ 4.35 \\ 4.30 \\ 6.50 \\ 12.40 \\ 12.90 \\ 11.70 \\ 9.50 \end{array}$	$\begin{array}{c} 3.65\\ 3.40\\ 3.30\\ 3.15\\ 2.95\\ 2.70\\ 2.70\\ 2.65\end{array}$	$\begin{array}{r} 4.20 \\ 7.05 \\ 8.30 \\ 8.00 \\ 7.70 \\ 6.70 \\ 4.30 \\ 4.50 \end{array}$	$\begin{array}{r} 4.70 \\ 5.00 \\ 4.30 \\ 4.20 \\ 4.10 \\ 5.65 \\ 4.65 \\ 3.75 \end{array}$	$\begin{array}{c} 2.15\\ 2.10\\ 2.00\\ 2.00\\ 1.90\\ 2.25\\ 2.00\\ 1.90\end{array}$	$\begin{array}{c} 1.60\\ 1.50\\ 1.45\\ 1.35\\ 1.30\\ 1.25\\ 1.20\\ 2.25\end{array}$	$\begin{array}{c} 1.50\\ 2.20\\ 2.35\\ 3.85\\ 3.60\\ 3.80\\ 3.80\\ 3.00 \end{array}$	$\begin{array}{c} 2.35\\ 2.30\\ 2.30\\ 2.15\\ 2.10\\ 2.10\\ 2.00\\ 1.90\end{array}$	5.40 4.80 4.00 3.60 3.15 2.95 2.80 3.70
$15 \\ 16 \\ 17 \\ 18 \\ 19 \\ 20 \\ 21 \\ 20 \\ 21 \\ 20 \\ 21 \\ 20 \\ 21 \\ 20 \\ 21 \\ 20 \\ 21 \\ 20 \\ 21 \\ 20 \\ 21 \\ 20 \\ 21 \\ 20 \\ 21 \\ 20 \\ 21 \\ 20 \\ 21 \\ 20 \\ 21 \\ 20 \\ 21 \\ 20 \\ 21 \\ 20 \\ 21 \\ 20 \\ 21 \\ 20 \\ 21 \\ 20 \\ 21 \\ 20 \\ 21 \\ 20 \\ 21 \\ 20 \\ 21 \\ 20 \\ 21 \\ 20 \\ 21 \\ 20 \\ 21 \\ 20 \\ 21 \\ 20 \\ 21 \\ 20 \\ 21 \\ 20 \\ 21 \\ 20 \\ 21 \\ 20 \\ 21 \\ 20 \\ 21 \\ 20 \\ 21 \\ 20 \\ 21 \\ 20 \\ 21 \\ 20 \\ 21 \\ 20 \\ 21 \\ 20 \\ 21 \\ 20 \\ 21 \\ 20 \\ 21 \\ 20 \\ 21 \\ 20 \\ 21 \\ 20 \\ 21 \\ 20 \\ 21 \\ 20 \\ 21 \\ 20 \\ 21 \\ 20 \\ 21 \\ 20 \\ 21 \\ 20 \\ 21 \\ 20 \\ 21 \\ 20 \\ 21 \\ 20 \\ 21 \\ 20 \\ 21 \\ 20 \\ 21 \\ 20 \\ 21 \\ 20 \\ 21 \\ 20 \\ 21 \\ 20 \\ 21 \\ 20 \\ 21 \\ 20 \\ 21 \\ 20 \\ 21 \\ 20 \\ 21 \\ 20 \\ 21 \\ 20 \\ 21 \\ 20 \\ 21 \\ 20 \\ 21 \\ 20 \\ 21 \\ 20 \\ 21 \\ 20 \\ 21 \\ 20 \\ 21 \\ 20 \\ 21 \\ 20 \\ 21 \\ 20 \\ 20$		$\begin{array}{c} 7.00 \\ 6.40 \\ 5.10 \\ 4.00 \\ 4.25 \\ 8.00 \\ 9.70 \\ 10.00 \end{array}$	$\begin{array}{c} 15.20 \\ 14.50 \\ 14.00 \\ 13.25 \\ 12.80 \\ 12.10 \\ 9.00 \\ 7.80 \end{array}$	$\begin{array}{c} 5.60 \\ 6.00 \\ 6.30 \\ 6.00 \\ 6.50 \\ 10.00 \\ 12.20 \\ 12.85 \end{array}$	$\begin{array}{r} 9.50 \\ \overline{7.20} \\ 12.40 \\ 18.10 \\ 17.55 \\ 15.65 \\ 13.95 \\ 13.15 \end{array}$	$\begin{array}{c} 2.65 \\ 2.65 \\ 2.60 \\ 2.60 \\ 2.60 \\ 2.60 \\ 2.60 \\ 2.65 \\ 3.20 \end{array}$	$\begin{array}{r} 4.50 \\ 4.70 \\ 5.00 \\ 4.90 \\ 6.90 \\ 6.45 \\ 6.10 \end{array}$	$     \begin{array}{r}       3.75 \\       3.60 \\       3.50 \\       3.35 \\       3.10 \\       3.00 \\       2.90 \\       2.70 \\       70 \\       \end{array} $	$ \begin{array}{r} 1.90\\ 1.85\\ 2.00\\ 2.60\\ 2.26\\ 2.10\\ 2.20\\ 2.00 \end{array} $	$     \begin{array}{r}       3.35 \\       6.00 \\       7.00 \\       7.50 \\       6.00 \\       4.35 \\       3.20 \\       2.50 \\     \end{array} $	$\begin{array}{c} 3.00 \\ 2.90 \\ 2.80 \\ 2.65 \\ 2.50 \\ 2.40 \\ 2.30 \\ 2.90 \end{array}$	$   \begin{array}{r}     1.90 \\     1.80 \\     1.75 \\     1.70 \\     1.80 \\     2.00 \\     2.50 \\     1.00 \\   \end{array} $	2.70 2.65 2.55 2.55 3.00 3.30 5.20
232425 26 27 28 20	•	$ \begin{array}{r} 10.00\\ 9.40\\ 8.75\\ 7.75\\ 6.00\\ 4.10\\ 3.60\\ 2.30 \end{array} $	$\begin{array}{c} 7.80 \\ 6.80 \\ 7.20 \\ 6.90 \\ 6.50 \\ 5.25 \\ 5.00 \end{array}$	12,80 12,60 11,80 10,60 10,30 10,20 9,85 9,50	$\begin{array}{c} 13.15\\ 12.65\\ 12.20\\ 10.80\\ 9.15\\ 7.90\\ 6.50\\ 5.70\end{array}$	$\begin{array}{c} 3.20 \\ 2.90 \\ 3.00 \\ 3.25 \\ 3.10 \\ 3.20 \\ 3.00 \\ 3.00 \\ 3.00 \\ 3.00 \end{array}$	$\begin{array}{c} 0, 10 \\ 7, 00 \\ 11, 35 \\ 12, 50 \\ 14, 10 \\ 14, 42 \\ 14, 60 \\ 13, 80 \end{array}$	$\begin{array}{c} 2.40 \\ 2.45 \\ 2.50 \\ 2.60 \\ 2.50 \\ 2.60 \\ 3.70 \\ 5.70 \end{array}$	2.00 2.00 1.95 1.90 2.20 2.10 2.00 1.95	$\begin{array}{c} 2.50 \\ 2.00 \\ 1.90 \\ 1.85 \\ 1.80 \\ 1.60 \\ 1.65 \\ 1.60 \end{array}$	$\begin{array}{c} 2.20 \\ 2.15 \\ 3.00 \\ 5.25 \\ 7.50 \\ 5.00 \\ 3.80 \\ 3.00 \end{array}$	$\begin{array}{r} 4.00\\ 3.80\\ 3.20\\ 3.10\\ 3.00\\ 4.35\\ 6.40\\ 9.20\end{array}$	5.20 7.00 7.30 6.90 6.35 5.90 4.90 1.30
29 30 31		5. 50 3. 00 2. 70		$   \frac{9.50}{8.50}   \frac{7.20}{7.20} $	5.35	$     \begin{array}{c}       2.80 \\       2.70 \\       2.60     \end{array}   $	13.80	$5.30 \\ 5.90$	$     \begin{array}{r}       1.95 \\       1.90 \\       1.90 \\       1.90 \\     \end{array}   $	1.55	3.00 2.65 2.50	5.20 8.20	$\frac{4.00}{6.50}$

# COOSA RIVER AT LOCKS NOS. 4 AND 5, ALABAMA.

Records of gage heights at these stations are kept by the United States Engineer Corps, who have kindly furnished copies to the Geological Survey. Records of gage heights at Lock No. 5 during the year 1900 are not available. The records for Lock No. 4 are given in the accompanying table. Discharge measurements are not made at either of these stations. The stations are described in Water-Supply Paper No. 36, page 150.

IRR 48—01—5

Day.	Jan.	Feb.	Mar.	Ap <b>r</b> .	May.	June.	July.	Aug.	Sept.	Oet.	Nov.	Dec.
1	$\begin{array}{c} 33.0\\ 33.0\\ 2.7\\ 4\\ 2.19\\ 1.99\\ 2.00\\ 1.99\\ 2.5.0\\ 6\\ 6.2\\ 1.6\\ 9\\ 5.16\\ 6.2\\ 1.99\\ 10.5\\ 11.99\\ 10.5\\ 4.5\\ 5.5\\ \end{array}$	$\begin{array}{c} & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\$	$\begin{array}{c} 7.9\\ 8.4\\ 7.9\\ 8.4\\ 7.9\\ 6.5\\ 6.0\\ 7.8\\ 6.8\\ 6.8\\ 6.8\\ 6.8\\ 6.8\\ 6.8\\ 6.8\\ 7.2\\ 7.0\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2\\ 11.2$	$\begin{array}{c} 6.9\\ 6.1\\ 5.5\\ 5.3\\ 5.4\\ 4.6\\ 4.9\\ 7.4\\ 4.6\\ 4.9\\ 7.4\\ 13.9\\ 14.5\\ 0.0\\ 8\\ 99.4\\ 6\\ 20.3\\ 18.0\\ 0\\ 16.0\\ 14.4\\ 8\\ 12.2\\ 20.3\\ 18.0\\ 0\\ 16.0\\ 14.4\\ 8\\ 12.2\\ 2\\ 9.22\\ \end{array}$	$= \frac{8}{56024} + \frac{1207}{56024} + 120$	3322828445700 3322828445700 9.00 9.00 9.00 9.00 9.00 9.00 9.00 9	$\begin{array}{c} & \\ & \\ & \\ & \\ & \\ & \\ & \\ & \\ & \\ & $	$\begin{array}{c} \textbf{A} \textbf{u}\textbf{g},\\ \hline \textbf{5}, \textbf{7}, \textbf{4}, \textbf{3}, \textbf{6}, \textbf{2}, \textbf{3}, \textbf{5}, \textbf{2}, \textbf{2},$	$\begin{array}{c} & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\$	322223049722447322719763566622 1.122233444433332211165556622	$\begin{array}{c} 664477778953098777766511335440610\\ 222222222222222222222222222222222222$	$\begin{array}{c} 7.7332977.532977.76877.76877.76877.76877.768777.768778.777.687784298533299822865855548422855554881155988811559888115598881155988811559888115598881155988811559888115598881155988811559888115598881155988811559888115598881155988811559888115598881155988811559888115598881155988811559888115598881155988811559888115598881155988811559888115598881155988811559888115598881155988811559888115598881155988811559888115598881155988811559888115598881155988811559888115598881155988811559888115598881155988811559888115598888115598881155988811559888115598881155988811559888115598881155988811559888115598881155988811559888115598881155988811559888811559888115598881155988881155988881155988881155988888888$
48 29 30 31	$\frac{4.0}{3.8}$ 3.3 3.0	6.2	$11.8 \\ 11.0 \\ 9.9 \\ 8.0$	$     \begin{array}{r}       4.8 \\       6.8 \\       6.0 \\     \end{array} $	$     \begin{array}{r}       3.0 \\       3.0 \\       2.8 \\       2.8 \\       2.8     \end{array} $	17.0 15.2 14.5	$     \begin{array}{r}       4.2 \\       5.6 \\       6.3 \\       6.8 \\       6.8     \end{array} $	$2.3 \\ 1.9 \\ 2.0 \\ 1.9$	$     \begin{array}{r}       1.6 \\       1.5 \\       1.5 \\       1.5 \\       \dots \end{array} $	$     \begin{array}{r}       5.2 \\       4.5 \\       2.9 \\       2.6 \\     \end{array} $	$10.2 \\ 10.0 \\ 8.7$	$     \begin{array}{r}       6.0 \\       5.1 \\       4.5 \\       6.0 \\     \end{array} $

Daily gage height, in feet, of Coosa River at Lock No. 4, Alabama, for 1900.

### TALLAPOÓSA RIVER NEAR SUSANNA, ALABAMA.

This station was established July 27, 1900, by J. R. Hall. It is located at the mouth of Blue Creek, which is 10 feet above the east landing of McCarty's ferry, 13 miles southwest of Dadeville, and 3 miles from Susanna, the nearest post-office. The rod is graduated to feet and tenths; it is 18 feet long, and is nailed vertically to a tree overhanging the water on the south side of the creek at the junction of the creek and the river. The gage is referred to a bench mark on a white hickory tree about 40 feet from the rod on the south bank of the creek, and is 376.67 feet above tide water. Discharge measurements are made from a boat held in place by a wire stretched across the river, upon which the distances from the initial point are tagged. The section is an exceptionally good one, depth and current being almost uniform the entire width of the stream. The observer is T. A. Walls, a farmer who lives 1 mile from the station. During 1900 the following measurements were made by James R. Hall:

July 27: Gage height, 1.80 feet; discharge, 2,309 second-feet. August 9: Gage height, 1.55 feet; discharge, 1,900 second-feet. September 28: Gage height, 1.50 feet; discharge, 1,809 second-feet. November 24: Gage height, 2.40 feet; discharge, 3,629 second-feet.
Daily gage height, in feet, of Tallapoosa River near Susanna, Alabama, for 1900.

Day.	July.	Aug.	Sept.	Oet.	Nov.	Dec.	Day.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
$\begin{array}{c} 1 \\ 2 \\ 3 \\ 3 \\ 5 \\ 5 \\ 6 \\ 7 \\ 7 \\ 8 \\ 9 \\ 10 \\ 11 \\ \end{array}$		$5.80 \\ 4.00 \\ 2.00 \\ 1.80 \\ 1.80 \\ 2.10 \\ 2.20 \\ 1.70 \\ 1.55 \\ 1.50 \\ 1.40 $	$\begin{array}{c} 2.40\\ 3.80\\ 4.80\\ 4.20\\ 2.25\\ 1.50\\ 1.45\\ 1.45\\ 1.45\\ 1.35\\ 1.35\end{array}$	$\begin{array}{r} 1.40\\ 1.40\\ 1.40\\ 1.35\\ 1.30\\ 2.80\\ 3.00\\ 2.50\\ 1.85\\ 1.80\\ 1.75\\ \end{array}$	$\begin{array}{c} 1.80\\ 1.70\\ 1.70\\ 1.65\\ 1.65\\ 1.65\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\$	$\begin{array}{c} 2.00\\ 2.00\\ 2.10\\ 2.20\\ 2.30\\ 2.50\\ 2.40\\ 2.40\\ 2.40\\ 2.30\\ 2.10\\ \end{array}$	17 18 19 20 21 22 23 24 24 25 26 27	1.80	$\begin{array}{c} 1.95\\ 1.95\\ 1.80\\ 1.75\\ 1.70\\ 1.70\\ 1.70\\ 1.90\\ 2.00\\ 2.05\\ 2.50\\ 2.15\\ \end{array}$	$\begin{array}{c} 8.40\\ 4.80\\ 3.00\\ 2.50\\ 1.80\\ 1.80\\ 1.80\\ 1.70\\ 1.60\\ 1.50\\ 1.50\end{array}$	$\begin{array}{c} 2.35\\ 2.30\\ 2.20\\ 2.10\\ 1.90\\ 1.70\\ 3.90\\ 6.00\\ 5.00\\ 4.30\\ 4.10\end{array}$	$\begin{array}{c} 1.75\\ 1.75\\ 1.80\\ 1.85\\ 1.85\\ 1.90\\ 2.40\\ 2.40\\ 2.40\\ 3.00\\ 4.90\\ 4.20 \end{array}$	$\begin{array}{c} 2.60\\ 2.50\\ 2.40\\ 4.50\\ 5.80\\ 4.50\\ 4.00\\ 4.00\\ 3.70\\ 3.20\\ 2.80\end{array}$
12 13 14 15 16	· · · · · · · · · · · · · · · · · · ·	$     \begin{array}{r}       1.40 \\       1.40 \\       1.40 \\       1.40 \\       1.90 \\       \end{array} $	$1.35 \\ 1.35 \\ 1.30 \\ 1.35 \\ 11.70$	$\begin{array}{c} 1.70\\ 1.90\\ 2.40\\ 2.45\\ 2.40\end{array}$	$     \begin{array}{r}       1.55 \\       1.55 \\       1.60 \\       1.60 \\       1.60 \\       \end{array} $	$\begin{array}{c} 2.00 \\ 1.90 \\ 3.80 \\ 3.90 \\ 2.80 \end{array}$	28 29 30 31	$     \begin{array}{r}       1.90 \\       1.80 \\       4.00 \\       6.80     \end{array} $	2.00 1.90 1.80 2.25	$     \begin{array}{r}       1.50 \\       1.45 \\       1.45 \\       \dots \end{array} $	$2.30 \\ 2.20 \\ 1.90 \\ 1.85$	3.90 3.00 2.80	2.70 2.60 2.70 2.90

#### TALLAPOOSA RIVER NEAR STURDEVANT, ALABAMA.

This station was established July 19, 1900, by J. R. Hall. It is located at the Columbus and Western Railroad bridge a fourth of a mile west of Sturdevant. The gage rod is 20 feet high, and is graduated to feet and tenths. It is in two sections and is fastened vertically, the shorter section to a post at the edge of the water on the east bank about 20 feet below the bridge, and the longer section to the first stone pier from the east bank. It is so set that when the water rises above the short section it is on the long section, and the readings are made as from one continuous rod. The initial point of sounding is the east end of the bridge. The section is broken by three piers and by some large rocks below the bridge. The gage is referred to a bench mark consisting of a nail in the southwest corner of pier No. 2, east side of river, 455.70 feet above tide water and 14.20 feet above the zero of the gage. The observer is B. F. Neighbors, farmer and postmaster at Sturdevant, who lives a fourth of a mile from the station. During 1900 the following measurements were made by James R. Hall:

July 20: Gage height, 2.85 feet; discharge, 2,603 second-feet. August 13: Gage height, 1.95 feet; discharge, 1,887 second-feet.

Daily gage height, in feet, of Tallapoosa River near Sturdevant, Alabama, for 1900.

Day.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Day.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1		$\begin{array}{c} 4.30\\ 3.40\\ 2.80\\ 2.50\\ 2.40\\ 2.35\\ 2.25\\ 2.20\\ 2.10\\ 2.00\\ 1.95\\ 1.90\\ 2.00\end{array}$	$\begin{array}{c} 3.40\\ 6.10\\ 4.20\\ 2.90\\ 2.50\\ 2.20\\ 2.00\\ 1.90\\ 1.80\\ 1.60\\ 1.60\\ 1.60\end{array}$	$\begin{array}{c} 1.80\\ 1.70\\ 1.60\\ 3.30\\ 3.00\\ 3.00\\ 2.90\\ 3.10\\ 3.20\\ 3.30\\ 3.40\\ 3.50\\ \end{array}$	$\begin{array}{c} 2.50\\ 3.40\\ 4.70\\ 3.60\\ 3.30\\ 2.90\\ 2.70\\ 2.60\\ 2.40\\ 2.40\\ 2.40\end{array}$	2.90 2.80 2.70 3.20 3.20 3.20 3.20 2.80 2.80 2.60 2.60 2.70	17 18 19 20 21 22 23 24 25 26 27 28 29 29 29 29 29 29 29 29 21 21 21 22 23 24 25 26 27 28 29 29 21 21 24 25 26 27 28 28 29 29 29 20 21 22 23 24 25 26 27 28 28 29 29 29 20 21 22 23 24 25 27 28 27 28 27 28 27 28 27 27 28 27 28 27 28 27 27 28 27 28 27 29 29 27 29 29 20 21 21 22 23 24 25 27 29 29 29 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20	$\begin{array}{c} 2.95\\ 2.80\\ 3.05\\ 2.75\\ 2.65\\ 2.55\\ 2.65\\ 2.60\\ 2.50\\ 2.70\\ 6.50\\ \end{array}$	$\begin{array}{c} 3.00\\ 2.80\\ 4.00\\ 2.90\\ 2.40\\ 2.30\\ 2.40\\ 2.70\\ 2.50\\ 2.80\\ 2.60\\ 2.50\\ 2.40\end{array}$	$\begin{array}{c} 7.90\\ 5.00\\ 3.80\\ 3.00\\ 2.70\\ 2.50\\ 2.40\\ 2.30\\ 2.20\\ 2.10\\ 2.00\\ 2.00\\ 2.00\end{array}$	$\begin{array}{c} 2.60\\ 2.20\\ 2.10\\ 2.00\\ 1.90\\ 2.10\\ 5.00\\ 7.30\\ 6.40\\ 5.40\\ 4.20\\ 3.60\\ 2.90\end{array}$	$\begin{array}{c} 2.30\\ 2.20\\ 2.20\\ 2.50\\ 3.50\\ 3.50\\ 3.50\\ 4.80\\ 5.90\\ 5.40\\ 3.40\\ 3.20\end{array}$	$\begin{array}{c} 3.20\\ 3.10\\ 3.00\\ 5.20\\ 6.80\\ 5.30\\ 4.90\\ 5.60\\ 4.70\\ 4.20\\ 3.90\\ 3.60\\ 3.40\end{array}$
14 15 16		$2.10 \\ 2.60 \\ 3.40$	$1.80 \\ 8.80 \\ 12.00$	$3.50 \\ 3.00 \\ 2.60$	2.30 2.30 2.30 2.30	$\begin{array}{c} 4.70 \\ 3.00 \\ 3.70 \end{array}$	30 31	$7.60 \\ 5.00$	2.30 2.80	1.90	2.70 2.60	3.10	$3.50 \\ 7.50$

#### TALLAPOOSA RIVER NEAR MILSTEAD, ALABAMA.

This station was established August 7, 1897, at the bridge of the Tallassee and Montgomery Railway, about a fourth of a mile from Milstead. It is described in Water-Supply Paper No. 36, page 152. The gage was last verified December 3, 1900. Records of discharge measurements for 1899 will be found in the Twenty-first Annual Report, Part IV, page 151. During 1900 the following measurements were made by Max Hall:

February 23: Gage height, 9.20 feet: discharge, 9,956 second-feet. March 5: Gage height, 6.70 feet: discharge, 7,088 second-feet. December 3: Gage height, 2.95 feet: discharge, 3,031 second-feet.

Daily gage height, in feet, of Tallapoosa River near Milstead, Alabama, for 1900.

		1										
Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1	2.70	2.50	13.20	5.50	6.30	2.60	9.00	6.50	2.70	1.80	2 50	3 30
2	2.60	2.40	13.10	5.30	5.90	2.70	9.10	4.50	8.00	1.60	3.30	3.30
3	2.40	2.30	10.70	5.00	5.40	$-\frac{3.00}{2.50}$	10.60	3.50	8.10	1.50	6.10	3.30
4	$\frac{2.30}{2.30}$	4, 50	6.80	5.30 4.80	$\frac{4.90}{1.70}$	3,90	- 7.10 - 8.00	2.80	4.40	1.80	6.50	3.50
6	$\frac{2.30}{2.30}$	4.30	6.10	4.70	3.90	3. 50	5.20	2.50	-2.40	6.40	5.50	3.90
7	2.20	4.40	5.60	4.60	3.80	3,30	4.40	2.30	2.20	3.40	4.10	3.80
8	2.20	3.80	10.90	4.60	3.70	5.90	4.00	2.20	-2.00	3.20	3.50	3.80
9	2.20	5.20	13.80*	$\frac{4.50}{4.60}$	$\frac{3.60}{2.50}$	9.70	$\frac{3.50}{2}$	2.10	1.80 1.50	2.60	3.00	-3.10
10	2.30	8,90	10.00	$\frac{4.60}{5.50}$	3.30	5.60	5.50	1.90	1.70 1.70	3.00	$\frac{2.90}{2.70}$	2.80
12	7.30	30.00	7.90	10.60	3.20	4.60	4.10	1.90	1.60	2.80	2.60	2.80
13	6.00	43.25	6.60	11.50	-3.10	5.30	4.70	1.80	1.50	3.40	2.60	2.80
14	4.50	42.00	5.90	9,00	3.00	4.00	6.70	1.90	1.50	3.30	2.50	7.70
10	$\frac{4.00}{2.40}$	31.90	5.40	6,60	$\frac{2.90}{2.00}$	3.80	6.00	2.20	14.00 25.00	3,30	2.50	9.10
10	3.00	13 50	$\frac{7.00}{7.20}$	3. 30 4. 70	2.80	$\frac{0.00}{4.50}$	$\frac{0.10}{3.80}$	3 10	18 00	2 70	$\frac{2.50}{2.50}$	-4.30 5.20
18	2.90	8,90	5.60	13.90	2.80	5,90	3, 80	2.50	11.00	2.20	2.50	4.20
19	3.70	7.00	-5.40	17.06	-2.80	-5.00	3,60	4.00	-5,30	2.10	2.50	4.00
20	9.50	6.10	6.00	15.00	-2.90	5.90	-3.10	4.20	3.60	2.00	2.50	8.60
21	6.00	0.00	11.40 10.50	10.90 12.20	$\frac{2.80}{2.00}$	5,90	3.00	2.00	3.00	1.90	2.50	17.00 12.50
66 23	4.60	9.50	7.60	10.30	3.10	5.40	2.70	2.00	2.30	4.80	4.00	10.40
24	3.90	8,90	15.50	13.20	3.40	20.00	2.60	2.30	2.20	12.10	3.90	11.30
25	3.50	8.40	15.20	12.50	3.50	25.04	2.50	3.30	2.00	10.50	3.50	8.70
26	3.10	8.00	16.00	9.40	5.00	20.00	2.50	$\frac{3.40}{2.60}$	2.00	9.00	10.50	6.60
41 98	0.00 2.80	6.00	10.70	6 40	4.00	18 00	2.90	3.00	2.00	4.20	6.70	5.00
29	2.70	0.00	8.70	6.20	2.70	13.80	3.20	2.60	2.00	2.20	4.50	4.60
30	2.60		7.10	6.10	3.00	9.00	8.10	2.10	1.90	2.90	3.70	4.30
31	2.50		6.20		2.50		10.60	3.20		2.70		11.60

ALABAMA RIVER AT MONTGOMERY, ALABAMA.

This station was established by the United States Engineer Corps a number of years ago, at the Montgomery wharf, near the union passenger station at the foot of Commerce street. The readings are now taken by the Weather Bureau, and copies are furnished to the Geological Survey. The station is described in Water-Supply Paper No. 36, page 153. No measurements were made in 1899 or previous years. During 1900 one measurement was made by Max Hall, as follows:

March 6: Gage height, 11.40 feet; discharge, 29,470 second-feet.

#### ALABAMA.

Daily gage height, in feet, of Alabama River at Montgomery, Alabama, for 1900.

	Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1 2 3 4 5 6 7 8 9 10 11 2 3 14 5 6 7 8 9 10 11 2 3 14 5 6 7 8 9 21 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	Day.	$\begin{array}{c} \text{Jan.}\\ \hline\\ 4.9\\ 4.3\\ 3.9\\ 9\\ 2.5\\ 2.2\\ 2.2\\ 2.2\\ 2.2\\ 2.2\\ 2.2\\ 2.2$	$\begin{array}{c} \text{Feb.} \\ \hline 6.0 \\ 5.8 \\ 5.3 \\ 5.0 \\ 6.1 \\ 6.1 \\ 6.1 \\ 6.1 \\ 8.0 \\ 14.2 \\ 21.2 \\ 31.3 \\ 31.8 \\ 48.4 \\ 44.5 \\ 44.5 \\ 44.5 \\ 37.5 \\ 33.5 \\ 528.0 \\ 228.0 \\ 228.0 \\ 221.0 \\ 18.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12.2 \\ 12$	$\begin{array}{c} \textbf{Mar.} \\ \hline 12.4 \\ 17.6 \\ 19.0 \\ 19.4 \\ 14.8 \\ 10.1 \\ 10.1 \\ 10.5 \\ 318.6 \\ 19.5 \\ 18.5 \\ 19.5 \\ 10.5 \\ 11.7 \\ 11.9 \\ 10.6 \\ 19.3 \\ 223.5 \\ 25.1 \\ 223.5 \\ 25.1 \\ 223.5 \\ 28.1 \\ 27.6 \\ \end{array}$	$\begin{array}{c} {\rm Apr.} \\ \hline \\ 14.0 \\ 10.8 \\ 9.2 \\ 8.6 \\ 8.1 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ $	$\begin{array}{c c} \textbf{May.} \\ \hline \\ \textbf{May.} \\ \hline \\ \textbf{10.2} & 9.6 \\ 9.23 \\ 9.23 \\ 7.2 \\ 6.6 \\ 6.5 \\ 5.6 \\ 5.5 \\ 6.5 \\ 5.6 \\ 5.3 \\ 5.0 \\ 5.0 \\ 5.6 \\ 5.3 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 4.4 \\ 4.0 \\ 4.0 \\ 4.0 \\ 4.0 \\ 4.0 \\ 4.0 \\ 4.0 \\ 4.0 \\ 4.0 \\ 4.0 \\ 4.0 \\ 5.2 \\ 5.0 \\ 5.2 \\ 5.0 \\ 4.7 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\ 1.0 \\$	$\begin{array}{c} {\rm June},\\ \\ 3.5\\ 3.5\\ 3.5\\ 3.5\\ 4.4\\ 4.4\\ 4.5\\ 0\\ 10.0\\ 11.0\\ 0\\ 12.0\\ 10.0\\ 12.0\\ 10.0\\ 12.0\\ 10.0\\ 12.0\\ 10.0\\ 12.0\\ 10.0\\ 12.0\\ 10.0\\ 12.0\\ 10.0\\ 27.4\\ 14.2\\ 227.4\\ 230.8\\ \end{array}$	$\begin{matrix} \textbf{July.} \\ \hline \textbf{29,0} \\ \textbf{24,8} \\ \textbf{220,2} \\ \textbf{217,2} \\ \textbf{17,28} \\ \textbf{12,2} \\ \textbf{20,22} \\ \textbf{17,28} \\ \textbf{12,28} \\ \textbf{12,28}$	Aug. 10,6 9,9 6,6 5,3 4,5 3,9 8,3 3,0 2,6 2,5 2,5 2,5 2,5 2,5 3,1 3,0 2,6 2,5 2,5 3,1 3,0 2,6 2,5 3,0 2,5 3,0 2,6 3,0 2,6 3,0 3,0 2,6 3,0 3,0 3,0 3,0 3,0 3,0 3,0 3,0	$\begin{array}{c} \text{Sept.} \\ \hline 3.0 \\ 3.5 \\ 5.5 \\ 5.7 \\ 5.0 \\ 4.4 \\ 9 \\ 2.5 \\ 2.0 \\ 1.6 \\ 1.6 \\ 1.4 \\ 1.6 \\ 1.4 \\ 1.6 \\ 1.2 \\ 7.0 \\ 1.5 \\ 8.0 \\ 4.5 \\ 3.0 \\ 2.4 \\ 2.3 \\ 2.0 \\ \end{array}$	$\begin{array}{c} \text{Oct.} \\ \hline \\ 1.7 \\ 1.6 \\ 1.4 \\ 1.5 \\ 0.4 \\ 1.4 \\ 1.5 \\ 0.4 \\ 1.4 \\ 1.5 \\ 0.4 \\ 1.4 \\ 2.0 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5$	Nov. 373,744,26610,82200,77000,77000000000000000000000000	$\begin{array}{c} \text{Dec.} \\ \hline \\ $
29 30 31		$     \begin{array}{r}       6.8 \\       6.4 \\       6.3     \end{array}   $		$23.2 \\ 20.5 \\ 17.5$	$14.6 \\ 11.2$	$4.5 \\ 4.3 \\ 3.8$	32.8 31.8	7.0 9.2 11.6	$3.3 \\ 3.0 \\ 2.9$	2.0 1.7		$     \begin{array}{r}       13.4 \\       11.5 \\     \end{array}   $	8.8 9.0 10.0

#### ALABAMA RIVER AT SELMA, ALABAMA.

This station was originally established by the United States Engineer Corps; readings are now taken by the United States Weather Bureau. The gage, which is attached to the iron highway bridge, the floor of which is about 60 feet above low water, is in two sections. The lower section, which reads from -3.0 feet to +2.30 feet, is secured to the pile on the lower side of the cofferdam on the draw pier; the upper section, which reads from 2.30 feet to 48 feet, is spiked to the highway bridge. The bench mark, which is an iron bolt driven into the face of a rock bluff 182.3 feet from the first bridge pier, on the road ascending to the city, is 26 feet above the zero of the gage and 87.30 feet above mean sea level. The top of the coping stone of the pivot pier at the highway bridge to which gage is attached is 56 feet above the zero of the gage and 117.30 feet above mean sea level. Graduations extend from -3.0 feet to +48 feet. During 1900 the following measurements were made:

April 14: Gage height, 23.60 feet; discharge, 66,607 second-feet. May 26: Gage height, 6.10 feet; discharge, 17.049 second-feet. August 24: Gage height, 3.10 feet; discharge, 9,879 second-feet.

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Daily gage height, in feet, of Alabama River at Selma, Alabama, for 1900.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1	$7.2 \\ 6.6 \\ 4.3$	$\frac{4.8}{3.6}$	$17.2 \\ 19.7 \\ 29.9 $	$19.8 \\ 16.8 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ $	15.4 13.9 12.0	$4.8 \\ 4.6 \\ 4.4$	$   \begin{array}{c}     34.8 \\     33.0 \\     20.8   \end{array} $	$14.0 \\ 13.0 \\ 11.0$	3.9 3.9	0.8 .7	2.0 2.0 4.0	$     \begin{array}{c}       16.0 \\       14.0 \\       11.0     \end{array} $
4 5 6	3.3 3.0 3.0	$     \begin{array}{r}       3.9 \\       4.7 \\       6.2     \end{array} $	22.0 20.6 17.8	$     \begin{array}{r}       14.0 \\       12.0 \\       10.9 \\       8.0     \end{array}   $	$     \begin{array}{r}       13.0 \\       12.0 \\       11.8 \\       10.2     \end{array}   $	$4.2 \\ 5.6 \\ 5.0$	$     \begin{array}{r}       25.6 \\       26.5 \\       23.5 \\       20.2 \\       \end{array} $	9.0 7.0 6.0	$     \begin{array}{r}       4.5 \\       5.4 \\       5.0 \\     \end{array}   $	.6 .5 1.0	9.0 14.0 13.5	9.0 8.0 7.5
7 8 9 10	$3.0 \\ 3.0 \\ 2.7 \\ 2.7 \\ 2.7$	$8.2 \\ 8.4 \\ 8.5 \\ 10.7$	$15.0 \\ 13.9 \\ 14.9 \\ 18.8$	7.8 8.9 9.6 9.5	9.6 8.8 8.0 7.8	$4.6 \\ 4.2 \\ 6.8 \\ 11.6$	$17.0 \\ 14.0 \\ 11.5 \\ 10.0$	5.5 5.0 4.8 4.5	$4.5 \\ 4.1 \\ 3.3 \\ 1.8$	$     \begin{array}{r}       1.8 \\       2.5 \\       4.0 \\       4 2     \end{array} $	$9.4 \\ 6.3 \\ 4.0 \\ 2.0$	7.0 7.0 9.0 9.4
11 12 13	3.3 7.7 12.4	$   \begin{array}{r}     16.0 \\     22.2 \\     29.9   \end{array} $	$\begin{array}{c} 20.9 \\ 22.2 \\ 22.0 \end{array}$	$\begin{array}{c} 9.8 \\ 12.0 \\ 17.7 \end{array}$	7.5 7.3 7.0	$     \begin{array}{r}       13.5 \\       14.0 \\       13.9 \\       13.9     \end{array} $	$     \begin{array}{r}       10.0 \\       9.8 \\       10.2 \\       10.0 \\       10.0 \\       \end{array} $	3.2 3.0 2.8	1.0 .7 .6	2.0 2.0 2.5	2.0 1.9 1.6	$6.0 \\ 5.0 \\ 2.0$
$ \begin{array}{c} 14 \\ 15 \\ 16 \\ 17 \\ \end{array} $	$13.5 \\ 14.7 \\ 14.0 \\ 13.2$	$38.6 \\ 41.0 \\ 47.0 \\ 48.0$	19.9 19.0 16.9 15.3	23.4 25.5 25.0 22.5	$     \begin{array}{r}       6.6 \\       6.4 \\       6.0 \\       5.7 \\     \end{array} $	$12.8 \\ 11.0 \\ 9.0 \\ 8.9$	9.9 9.9 10.0 9.9	$2.5 \\ 2.5 \\ 2.4 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 \\ 2.8 $	$1.0 \\ 1.6 \\ 11.0 \\ 18.0$	$4.3 \\ 6.7 \\ 6.0 \\ 5.2$	$     \begin{array}{c}       1.6 \\       1.0 \\       1.0 \\       1.0 \\       1.0 \\       \end{array} $	$3.2 \\ 9.0 \\ 11.0 \\ 11.0$
18 19 20	12.0 11.1 11.1	$\begin{array}{c} 47.9 \\ 47.0 \\ 44.1 \end{array}$	$     \begin{array}{r}       13.9 \\       14.3 \\       14.6 \\       14.6     \end{array} $	$\begin{array}{c} 23.5 \\ 29.0 \\ 34.8 \end{array}$	$5.5 \\ 5.2 \\ 5.1$		9.0 7.0 7.0	$2.7 \\ 2.7 \\ 2.5 \\ 2.5$	$     \begin{array}{r}       19.0 \\       19.4 \\       16.0 \\     \end{array} $	$2.5 \\ 1.0 \\ 1.0$	$     \begin{array}{r}       1.0 \\       1.0 \\       1.0 \\       1.0 \\       \end{array} $	$     \begin{array}{r}       10,0 \\       6,0 \\       5.1     \end{array} $
21 22 23 24	$13.4 \\ 16.9 \\ 18.5 \\ 18.3$	$\begin{array}{c} 41.6 \\ 36.9 \\ 33.2 \\ 22.6 \end{array}$	$     \begin{array}{r}       18.8 \\       23.0 \\       25.5 \\       29.0 \\     \end{array} $	$     39.0 \\     39.8 \\     41.0 \\     40.0 $	$5.0 \\ 5.0 \\ 4.8 \\ 5.5$	10.9 12.0 12.9 14.0		$2.3 \\ 2.6 \\ 3.6 \\ 3.8$	$     \begin{array}{r}       12.5 \\       10.0 \\       6.0 \\       3.0 \\     \end{array} $		$     \begin{array}{c}       1.0 \\       1.6 \\       6.0 \\       9.0 \\     \end{array} $	$9.0 \\ 14.5 \\ 17.0 \\ 17.2$
25 26 27	$17.0 \\ 14.7 \\ 13.0 $	$\begin{array}{c} 22.6 \\ 21.1 \\ 19.0 \end{array}$	30.2 32.7 33.3			17.6 24.5 29.0	$5.8 \\ 5.0 \\ 4.5$	4.0 3.5 3.5 3.5	$     \begin{array}{c}       1.9 \\       1.6 \\       1.0     \end{array}   $	$     \begin{array}{r}       11.5 \\       12.0 \\       11.5     \end{array} $	$9.8 \\ 9.9 \\ 13.0$	17.6 18.0 17.0
28 29 30 31	$     \begin{array}{r}       11.2 \\       8.4 \\       6.5 \\       4.8     \end{array} $	16.9	32.5 30.5 27.7 91.1	$28.5 \\ 23.0 \\ 18.0$		32.0 33.5 35.0	4.4 7.5 8.0 11.8	$3.4 \\ 3.5 \\ 4.0 \\ 1.2$	$1.0 \\ .9 \\ .8$	$12.3 \\ 13.0 \\ 11.0 \\ 5.0$	$16.0 \\ 16.8 \\ 17.0$	$14.5 \\ 12.9 \\ 11.2 \\ 11.0 \\ 11.0 \\ 11.0 \\ 11.0 \\ 11.0 \\ 11.0 \\ 11.0 \\ 11.0 \\ 11.0 \\ 11.0 \\ 11.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ 10.0 \\ $

#### BLACK WARRIOR RIVER AT TUSCALOOSA, ALABAMA.

A continuous record of the gage heights at Tuscaloosa has been kept by the United States Engineer Corps since 1889. During 1895 and 1896 a number of discharge measurements were made, from which a rating table was established. Since that time measurements of flow and computations of the discharge have been made regularly by the United States Geological Survey. The station is described in Water-Supply Paper No. 36, page 156. The records are furnished by R. C. McCalla, jr., United States assistant engineer. Records of measurements during 1899 will be found in the Twenty-first Annual Report, Part IV, page 153. No measurements were made during the year 1900. Daily gage height, in feet, of Black Warrior River at Tuscaloosa, Alabama, for 1900.

Day. Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$\begin{array}{c} {\rm Feb.} \\ {\rm 6,92} \\ {\rm 6,00} \\ {\rm 5,000} \\ {\rm 5,100} \\ {\rm 5,100} \\ {\rm 9,580} \\ {\rm 11,590} \\ {\rm 12,230} \\ {\rm 20,604} \\ {\rm 41,376} \\ {\rm 445,733} \\ {\rm 40,234} \\ {\rm 45,592} \\ {\rm 21,000} \\ {\rm 22,380} \\ {\rm 22,380} \\ {\rm 21,000} \\ {\rm 22,380} \\ {\rm 22,380}$	$\begin{array}{c} {\rm Mag} \\ {\rm is, 14} \\ {\rm 35, 14} \\ {\rm 35, 00} \\ {\rm 32, 329} \\ {\rm 32, 20, 23, 20, 23, 20, 23, 20, 23, 20, 23, 20, 23, 20, 23, 20, 23, 20, 23, 20, 23, 20, 23, 20, 23, 20, 23, 20, 23, 20, 23, 20, 23, 20, 23, 20, 23, 20, 23, 20, 23, 20, 23, 20, 23, 20, 23, 20, 23, 20, 23, 20, 23, 20, 23, 20, 23, 20, 23, 20, 23, 20, 23, 20, 23, 20, 23, 20, 23, 20, 23, 20, 23, 20, 23, 20, 23, 23, 23, 23, 23, 23, 23, 23, 23, 23$	$\begin{array}{c} {\rm Apr.} \\ 21,55 \\ 18,60 \\ 15,80 \\ 12,27 \\ 12,17 \\ 10,297 \\ 10,58 \\ 26,359 \\ 52,79 \\ 10,58 \\ 26,359 \\ 52,79 \\ 10,58 \\ 26,359 \\ 53,409 \\ 42,30 \\ 63,00 \\ 64,057 \\ 659 \\ 357 \\ 100 \\ 64,057 \\ 659 \\ 357 \\ 94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 33,94 \\ 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#### BLACK WARRIOR RIVER NEAR CORDOVA, ALABAMA.

This station is located at the Kansas City, Memphis and Birmingham Railroad bridge three-fourths of a mile from Cordova, Alabama. The gage was established by the United States Weather Bureau, but records were discontinued by that bureau some time ago. From 12 to 55 feet the gage is a vertical timber bolted to the inside of the bridge pier on the left bank of the river. Below 12 feet the gage was sloping, but it was out of position and could not be used when the station was established by the Geological Survey on May 21, 1900, so a short new section was put in at that time. This section is a 2-inch by 10-inch plank, graduated to feet and tenths, marked with nails from -1.5 feet to +12.5 feet, and spiked to a willow tree on the right bank of the river about 200 feet below the bridge. The bench mark is the top of the stone pier on the left bank, and is 54.95 feet above the zero of the gage. Measurements are made from the railroad bridge, which is a single-span, iron, through bridge 300 feet long. The section is a good one. The observer is A. B. Logan, who lives on the right bank of the river, only a few hundred feet from the end of the bridge. During 1900 one measurement was made by Max Hall, as follows:

May 21: Gage height, 0.10 foot; discharge, 747 second-feet.

Day.	May.	June.	July.	Aug.	Sept.	Oet.	Nov.	Dec.
Day.           1           2           3           4           5           6           7           8           9           10           12           13           14           15           16           17           18           19           20           21           22           23           24           25           26           27           28           29		0.6 2.8 5.7.1 7.5 6.5 7.6 6.5 7.6 6.5 7.6 8.6 8.6 8.8 9.8 8.0 8.2 7.1 13.4 0.6 6.1 15.2 33.8 31.3 1223.9	3 $3$ $3$ $3$ $3$ $3$ $3$ $3$ $3$ $3$	Aug. 0.9 5 4 2 1 0.9 5 4 2 3 3 4 5 5 5 6 6 6 6 6 6 6 6 6 6 6 1 1 2 3 3 4 4 5 5 5 5 5 5 5 5 5 5 5 5 5	$\begin{array}{c} \text{Sept.} \\ \hline 0.5 \\ .2 \\ .1 \\ 0 \\1 \\ .2 \\ .3 \\4 \\ .5 \\ .5 \\ .5 \\ .5 \\ .6 \\6 \\ 1.5 \\ .5 \\ .1 \\ .0 \\ .1 \\ .2 \\ .3 \\ .4 \\ .4 \\ .5 \\ .5 \\ .6 \\ .6 \\ .7 \\ .6 \\ .6 \\ .7 \\ .6 \\ .6$	$\begin{array}{c} -0.8 \\ -0.8 \\9 \\9 \\ -1.0 \\ -1.1 \\ +9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\9 \\$	$\begin{array}{c} 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 $	$\begin{array}{c} 1.4 \\ 1.0 \\ .8 \\ 1.0 \\ .8 \\ 1.0 \\ 1.9 \\ 1.8 \\ 1.4 \\ 1.4 \\ 1.0 \\ .8 \\ .8 \\ .6 \\ .5 \\ .5 \\ .5 \\ .5 \\ .5 \\ .5 \\ .5$
30 31	.9 .9	16.5	$\begin{array}{c} 1.2\\ 1.5 \end{array}$	$\frac{.9}{1.0}$	.7	$^{1}_{1}$	1.9	$1.7 \\ 2.8$

Daily gage height, in feet, of Black Warrior River near Cordova, Alabama, for 1900.

#### HILLABEE CREEK NEAR ALEXANDER CITY, ALABAMA.

This station, which was established August 29, 1900, by J. R. Hall, is located 6[‡] miles northeast of Alexander City, on the road leading from that town to Newsite. The gage, which is graduated to feet and tenths and is placed vertically, is in two sections, the short section, which reads from 0 to 5.50 feet, being fastened to a post in the edge of the water on the north bank 20 feet from the upstream side of the bridge, the long section, which reads from 5,50 feet to 16 feet, being fastened to the upstream end of the first pier on the north bank, and arranged so that when water rises above the short section the readings are made from the long one, both sections being easily read from the north approach to the bridge. The initial point of sounding is on the south side of the first pier on the north bank. The gage is referred to a bench mark at the top of a chord on the downstream side of the bridge at the second pier from the north bank, and is 27.6 feet above the zero of the gage. The bridge is in three spans having a total length of 276 feet, with a north approach of 116 feet and a south approach of 124 feet, making a total, over all, of 516 feet. The observer is J. H. Chisholm, a farmer, post-office address Alexander City, Alabama. During 1900 the following measurements were made by James R. Hall:

August 29: Gage height, 1.40 feet; discharge, 184 second-feet. November 28: Gage height, 2 feet; discharge, 390 second-feet.

Daily	gage	height,	in j	feet,	of	Hillabee	Creek	near	Alexander	City,	Alabama,	for
							1900.					

Day.	Aug.	Sept.	Oct.	Nov.	Dec.	Day.	Aug.	Sept.	Oct.	Nov.	Dec.
1           2           3           4           5           6           7           8           9           10           11           12           13           14           15           16		$\begin{array}{c} 2.3\\ 2.3\\ 1.6\\ 1.4\\ 1.3\\ 1.2\\ 1.2\\ 1.1\\ 1.1\\ 1.1\\ 1.1\\ 1.1\\ 1.1$	$\begin{array}{c} 1.3\\ 1.1\\ 1.1\\ 1.1\\ 2.0\\ 2.8\\ 2.6\\ 2.4\\ 2.3\\ 1.8\\ 1.6\\ 1.4\\ 1.4\\ 1.2\end{array}$	$\begin{array}{c} 1.6\\ 2.6\\ 6.8\\ 3.2\\ 2.2\\ 1.8\\ 1.7\\ 1.8\\ 1.7\\ 1.7\\ 1.7\\ 1.7\\ 1.7\\ 1.7\\ 1.7\\ 1.6\\ \end{array}$	$\begin{array}{c} 1.9\\ 1.9\\ 1.8\\ 1.9\\ 1.8\\ 1.9\\ 1.8\\ 1.7\\ 1.7\\ 1.7\\ 1.7\\ 1.7\\ 1.8\\ 3.8\\ 2.9\\ 2.8\end{array}$	17	   1.4 1.3 1.8	$\begin{array}{c} 2.6\\ 2.22\\ 1.65\\ 1.55\\ 1.5\\ 1.4\\ 1.2\\ 1.3\\ 1.4\\ 1.3\\ 1.4\\ 1.3\\ 1.4\\ 1.3\end{array}$	$\begin{array}{c} 1.3\\ 1.3\\ 1.2\\ 1.2\\ 1.9\\ 5.9\\ 2.9\\ 2.1\\ 1.9\\ 1.8\\ 1.7\\ 1.6\\ 1.5\\ 1.5\end{array}$	$\begin{array}{c} 1.5\\ 1.4\\ 1.5\\ 1.6\\ 1.7\\ 2.1\\ 1.9\\ 5.1\\ 2.9\\ 2.4\\ 2.0\\ 1.9\\ 1.9\end{array}$	$\begin{array}{c} 2.7\\ 2.8\\ 3.0\\ 9.0\\ 4.0\\ 3.0\\ 2.9\\ 2.8\\ 2.6\\ 5.5\\ 5.7\\ 5.7\end{array}$

#### TALLADEGA CREEK AT NOTTINGHAM, ALABAMA.

This station is located on the Southern Railroad bridge a fourth of a mile from the depot at Nottingham, Alabama, and 1 mile north of Alpine, Alabama. The gage, which is graduated to feet and tenths and is 20 feet long, is fastened vertically to the north end of the bridge on the upstream side, the bottom end of the gage being nailed to an old mudsill projecting from the north bank. The initial point of sounding is at the gage. The bench mark is the top rail on the upstream side of the bridge, and is 24.13 feet above gage datum. The section is a good one and is free from piers. The observer is R. M. McClatchy, station agent at Nottingham. During 1900 the following measurements were made by James R. Hall:

August 16: Gage height, 1.10 feet; discharge, 102 second-feet. November 29: Gage height, 1.70 feet; discharge, 240 second-feet.

Daily gage height, in feet, of Talladega Creek at Nottingham, Alabama, for 1900.

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$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$

#### BIG SANDY CREEK NEAR DADEVILLE, ALABAMA.

This station, which was established by J. R. Hall August 2, 1900, is located about  $4\frac{1}{2}$  miles southwest of Dadeville, at the highway bridge on the Dadeville-Susanna road. The gage, which is graduated to feet and tenths, is 16 feet high and is fastened vertically to the first pier on the north side of the creek. The initial point of sounding is at the gage rod. The section is good for ordinary or flood measurements, but is rather wide and shoaly for low-water measurements. The latter can, however, be made a short distance from the gage. The observer is L. H. Finch, a farmer who lives 200 yards from the station, postoffice address, Dadeville, Alabama. During 1900 the following measurements were made by James R. Hall:

July 6: Gage height, 1.20 feet; discharge, 260 second-feet. August 8: Gage height, 1.00 foot; discharge, 110 second-feet. August 8: Gage height, 1.00 foot; discharge, 116 second-feet. August 25: Gage height, 1.35 feet: discharge, 281 second-feet. November 16: Gage height, 1.10 feet; discharge, 155 second-feet. December 31: Gage height, 2.00 feet; discharge, 870 second-feet.

The measurements of August 8 and November 16 were made a half mile below Smith's bridge.

Daily	gage heigh	t, in fe	pet, of $B$	ig Sandı	I Creek near	Dadeville.	Alabama,	for 1900.
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Day.	Aug.	Sept.	Oct.	Nov.	Dec.	Day.	Aug.	Sept.	Oct.	Nov.	Dec.
1	$\begin{array}{c} 1.\ 00\\ 1.\ 20\\ 1.\ 10\\ 1.\ 10\\ 1.\ 10\\ 1.\ 05\\ 1.\ 05\\ 1.\ 05\\ 1.\ 00\\ 1.\ 00\\ 9.\ 05\\ 9.\ 00\\ 1.\ 80\\ 1.\ 00\\ 1.\ 00\\ \end{array}$	$\begin{array}{c} 1.10\\ 1.10\\ 1.40\\ 1.30\\ 1.20\\ 1.05\\ 1.00\\ 1.05\\ 2.00\\ 1.80\\ 1.40\\ 1.20\\ 2.00\\ 2.20\\ \end{array}$	$\begin{array}{c} 0.95\\ .90\\ .90\\ .90\\ 3.50\\ 1.25\\ 1.20\\ 1.10\\ 1.15\\ 1.10\\ 1.20\\ 1.15\\ 1.10\\ 1.05\\ \end{array}$	$\begin{array}{c} 1.00\\ 1.30\\ 2.00\\ 1.80\\ 1.40\\ 1.20\\ 1.20\\ 1.20\\ 1.15\\ 1.15\\ 1.15\\ 1.15\\ 1.15\\ 1.15\\ 1.10\\ 1.10\\ 1.10\\ 1.10\\ \end{array}$	$\begin{array}{c} 1.\ 10\\ 1.\ 15\\ 1.\ 25\\ 1.\ 30\\ 1.\ 35\\ 1.\ 30\\ 1.\ 25\\ 1.\ 10\\ 1.\ 10\\ 1.\ 10\\ 1.\ 10\\ 1.\ 10\\ 2.\ 20\\ 1.\ 80\\ 1.\ 45\\ \end{array}$	$\begin{array}{c} 19\\ 18\\ 19\\ 20\\ 21\\ 22\\ 23\\ 23\\ 24\\ 24\\ 25\\ 24\\ 25\\ 23\\ 24\\ 25\\ 24\\ 25\\ 23\\ 25\\ 23\\ 25\\ 23\\ 25\\ 23\\ 25\\ 23\\ 25\\ 23\\ 25\\ 23\\ 25\\ 23\\ 25\\ 23\\ 25\\ 23\\ 25\\ 25\\ 25\\ 25\\ 25\\ 25\\ 25\\ 25\\ 25\\ 25$	$\begin{array}{c} 1.80\\ 1.20\\ 1.10\\ 1.00\\ 1.00\\ .90\\ .90\\ 1.70\\ 1.60\\ 1.40\\ 1.60\\ 1.15\\ 1.10\\ 1.00\\ 1.80\\ \end{array}$	$\begin{array}{c} 3.90\\ 1.50\\ 1.10\\ 1.05\\ 1.00\\ 1.00\\ 1.00\\ 1.00\\ 1.00\\ 1.00\\ 1.05\\ 1.05\\ 1.05\\ 1.00\\ .90\\ \end{array}$	$\begin{array}{c} 1.\ 10\\ 1.\ 00\\ 1.\ 05\\ 1.\ 05\\ 1.\ 00\\ 1.\ 50\\ 1.\ 45\\ 1.\ 40\\ 1.\ 20\\ 1.\ 15\\ 1.\ 10\\ 1.\ 05\\ 1.\ 05\\ 1.\ 00\\ 1.\ 05\\ \end{array}$	$\begin{array}{c} 1.05\\ 1.10\\ 1.10\\ 1.10\\ 1.10\\ 1.25\\ 1.20\\ 1.50\\ 1.90\\ 1.80\\ 1.20\\ 1.15\\ 1.10\\ \end{array}$	$\begin{array}{c} 1.45\\ 1.30\\ 2.40\\ 4.50\\ 3.50\\ 1.70\\ 1.50\\ 1.40\\ 1.35\\ 1.35\\ 1.35\\ 1.35\\ 1.35\\ 2.00\\ \end{array}$

#### TOMBIGBEE RIVER AT COLUMBUS, MISSISSIPPI.

This station is located about 1,000 feet below the highway bridge  $1\frac{1}{2}$  miles from the Southern Railway depot at Columbus. The rod, which is in three sections, is fastened vertically to the rock bluff on the left bank. It is a 3-inch by 10-inch pine timber 45 feet long, marked with brass figures and copper nails, the graduation extending from -5.0 feet to +40.0 feet. The initial point of sounding is the end of the iron bridge, right bank, downstream side. Bench mark No. 1 is 250 feet from the initial point of sounding. The bridge floor is 40.85 feet above the zero of the rod, and the top of the iron girder

#### MISSISSIPPI AND ALABAMA.

under the floor timbers is 39.85 feet above the zero. Bench mark No. 2 is the top of the rail at the depot of the Southern Railway, and is 55.2 feet above gage datum and 190.9 feet above mean sea level. The width of the river at low water is 160 feet. The maximum recorded height of the river was on April 8, 1892, when the gage registered 42 feet. The lowest recorded height was on October 26, 1893, when the gage reading was -3.9 feet. The danger line is at 33 feet. No measurements of discharge were made during 1900.

Daily gage height, in feet, of Tombigbee River at Columbus. Mississippi, for 1900.

								1				
Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oet.	Nov.	Dec.
Day. 1	$\begin{array}{c} Jan.\\ 3.5\\ -2.2\\ -2.2\\ -1.6\\ -1.6\\ -1.2\\ -1.0\\ -2.0\\ -2.0\\ -3.0\\ -2.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ -3.0\\ $	Feb. $0.43324$ 1.35553344866 3.34248667 1.098818 3.55645 3.55545 3.5455645 5.54556 5.545569	$\begin{array}{c} {\rm Mar.} \\ 7.1 \\ 6.5 \\ 6 \\ 4.8 \\ 3.4 \\ 6 \\ 14.4 \\ 15.1 \\ 3.8 \\ 11.3 \\ 9.9 \\ 6.7 \\ 4.8 \\ 5.6 \\ 18.2 \\ 4.6 \\ 9.9 \\ 15.6 \\ 18.2 \\ 19.0 \\ 19.2 \\ 11.4 \\ 8 \\ 2.7 \\ 8 \\ \end{array}$	$\begin{array}{c} {\rm Apr.} \\ 4.5 \\ 3.27 \\ 1.9 \\ 1.5 \\ 1.3 \\ 1.1 \\ .57 \\ 11.6 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8 \\ 20.8$	May. 8.0 5.5 9.4 2.8 1.5 2.3 3.6 2.3 3.6 2.3 3.6 2.3 1.6 4.7 0 	June. $1, 0$ 8.0 $10, 0, 0$ 13.4 $4$ 15.3 $17, 0, 7$ 23.6 $255, 0$ 23.6 $225, 0$ 23.6 $21, 6$ 20.0 $18, 52, 6$ 20.0 $18, 52, 6$ 21.6 $17, 8$ 17.8 $17, 8$ 17.8 $17, 8$ 15.5 $13, 8, 5$ 21.5 $24, 11, 5$ 24.1 $52, 0$	$\begin{array}{c} {\rm July.}\\ 19.7\\ 18.3\\ 17.6\\ 16.9\\ 15.9\\ 15.4\\ 515.9\\ 15.9\\ 15.4\\ 5.5\\ 10.0\\ 6.8\\ 5.5\\ 2.0\\ 1.9\\ 1.5\\ 2.0\\ 1.9\\ 1.0\\ 1.9\\ 1.0\\ 1.9\\ 1.0\\ 1.9\\ 1.0\\ 1.9\\ 1.0\\ 1.9\\ 1.0\\ 1.9\\ 1.0\\ 1.9\\ 1.0\\ 1.9\\ 1.0\\ 1.9\\ 1.0\\ 1.9\\ 1.0\\ 1.9\\ 1.0\\ 1.9\\ 1.0\\ 1.0\\ 1.0\\ 1.0\\ 1.0\\ 1.0\\ 1.0\\ 1.0$	Aug. 5.8 4.0 2.8 1.9 5 9 1.4 1.8 2.6 2.6 2.6 2.2 2.2 2.2 2.3 1.4 1.4 1.16 1.9 1.4 1.4 1.5 9	Sept. -1.2 -1.0 -1.0 -1.0 -1.0 -1.0 -1.3 -1.9 -2.3 -2.5 -2.5 -2.6 -2.7 -2.8 -2.5 -2.9 -3.0 -3.1 -3.0 -3.1 -3.0 -2.9 -2.7 -2.9 -2.7 -2.9 -2.7 -2.9 -2.7 -2.9 -2.7 -2.9 -2.7 -2.9 -2.7 -2.9 -2.7 -2.9 -2.17 -2.9 -2.2 -2.7 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-2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5 -2.5	Oct. $\begin{array}{c} -2.78 \\ -3.30 \\ -3.313 \\ -3.55 \\ -2.20 \\ -1.66 \\ +4.82 \\ +5.66 \\ +4.82 \\ +5.64 \\ +2.66 \\ +4.82 \\ +5.64 \\ +2.4 \\ +2.4 \\ -1.91 \\ -1.13 \\ -1.22 \\ +2.80 \\ +5.1 \\ -1.80 \\ +5.1 \\ -1.80 \\ +5.1 \\ -1.80 \\ +5.1 \\ -1.80 \\ +5.1 \\ -1.80 \\ +5.1 \\ -1.80 \\ +5.1 \\ -1.80 \\ +5.1 \\ -1.80 \\ +5.1 \\ -1.80 \\ +5.1 \\ -1.80 \\ +5.1 \\ -1.80 \\ +5.1 \\ -1.80 \\ +5.1 \\ -1.80 \\ +5.1 \\ -1.80 \\ +5.1 \\ -1.80 \\ +5.1 \\ -1.80 \\ -1.80 \\ -1.80 \\ -1.80 \\ -1.80 \\ -1.80 \\ 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+ $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ + $-2.33$ 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#### TOMBIGBEE RIVER NEAR EPES, ALABAMA.

A record of gage heights has been kept at this station for the last ten years by the Alabama Great Southern Railway Company. The gage is painted on the center brick pier of the railway bridge of that company across the Tombigbee a half mile east of Epes, and is referred to two bench marks, the first, the top of the iron girder at the third crossbeam at the station, 80 feet from the right-bank end of the iron bridge, is 64.70 feet above datum of gage, the second, the top of the cross-tie or the base of the rail at the station, 80 feet from the right-bank end of the iron bridge, is 65.50 feet above datum of gage. The west bank of the river is a solid wall of limestone, the east bank is flat and is subject to overflow. The trestle at the east end of the bridge is seven-eighths of a mile long. The section is good, though the water is very deep and rather swift.

Daily gage height, in feet, of Tombigbee River near Epes, Alabama, for 1900.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oet.	Nov.	Dec.
1	$\frac{8.5}{7.5}$	3.0 3.0	18.0 19.0	24.5 19.5	43.0 41.0	6.0 8.0	44.5	$14.5 \\ 12.0$	2.0 2.5	0.5	7.0	8.0
3 4 	$\begin{array}{c} 6.5 \\ 6.0 \\ 5.5 \end{array}$	3.0 3.0 5.0	18.0 17.0 15.0	16.0 12.0 10.0	39.0 33.5	15.0 21.0 24.5	44.5 44.0 42.5	10.5 8.0	$2.0 \\ 2.0 \\ 2.0 \\ 2.0$	.5	9.0 8.5	7.0
6  7	$5.0 \\ 4.5 \\ 4.5$	6.0 7.0	13.0 14.0 13.0	8.0 7.5	20.5 16.0	27.0 29.5	42.0	5.0 5.0	2.0 2.0 2.0		7.5 7.0	
8 9 10	4.0 3.5 3.5	11.5 13.5	$     \begin{array}{r}       18.0 \\       21.0 \\       23.0     \end{array} $	$7.0 \\ 7.0 \\ 6.5$	10.0 7.0 7.0	$33.0 \\ 34.5 \\ 37.0$	40.0 39.0 38.0	4.0 3.0 2.0	$2.0 \\ 2.0 \\ 2.0 \\ 2.0$	$.5 \\ .5 \\ 2.0$	$5.5 \\ 4.5 \\ 4.0$	$4.0 \\ 4.0 \\ 3.5$
$\begin{array}{c}11\\12\\13\\\ldots\end{array}$	$   \begin{array}{r}     13.0 \\     20.0 \\     23.0   \end{array} $	$     \begin{array}{r}       15.0 \\       20.5 \\       26.0     \end{array} $	24.0 24.0 23.0	20.5 26.0 29.0	$7.0 \\ 8.0 \\ 8.0$	$38.5 \\ 39.5 \\ 40.5$	$     \begin{array}{r}       34.0 \\       26.0 \\       23.0     \end{array} $	$2.0 \\ 2.0 \\ 2.0 \\ 2.0$	$     \begin{array}{r}       1.5 \\       1.5 \\       1.5 \\       1.5 \\     \end{array} $	$4.0 \\ 6.0 \\ 7.5$	$4.0 \\ 3.0 \\ 3.0 \\ 3.0$	3.0 3.0 3.5
14 15 16	23.5 22.0 21.0	$     \begin{array}{r}       28.0 \\       28.0 \\       26.0     \end{array} $	$20.0 \\ 17.5 \\ 17.0$	$     \begin{array}{r}       30.0 \\       31.0 \\       38.0     \end{array} $	$7.0 \\ 6.0 \\ 6.0$	$   \begin{array}{r}     41.0 \\     41.5 \\     42.0   \end{array} $	$15.5 \\ 13.0 \\ 8.0$	$2.0 \\ 2.0 \\ 1.5$	$2.0 \\ 1.5 \\ 1.0$	$8.5 \\ 10.0 \\ 10.5$	$2.5 \\ 2.0 \\ 2.0$	$3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 $
17 18	18.5 15.0 11.5	24.0 22.0 18.5	18.0 18.0 18.5	46.0 48.5 51.0	$5.0 \\ 4.0 \\ 3.5$	42.0 42.0 41.5	$7.0 \\ 6.0 \\ 5.0$	$1.5 \\ 1.5 \\ 1.5 \\ 1.5$	1.0 1.0 1.0	10.0 7.5 5.0	2.0 2.0 2.5	3.0 3.0 2.0
20 21	11.5 10.0 8.5	16.0 14.0	$     \begin{array}{c}       10.9 \\       26.0 \\       30.0 \\       93.0 \\     \end{array} $	51.0 51.5 52.0 52.0	0.0 3.5 3.5	41.5	6.5 7.0	$1.5 \\ 1.5 \\ 1.0 \\ 1.0$	1.0 .5 .5	4.0 3.5	2.5 2.5 3.0	
22 23 24	8.0 8.0 7.0	15.0 17.5 18.0	32.0 34.0 35.5	51.5 51.0 51.0	3.5 3.5 4.0	$ \begin{array}{c} 41.0 \\ 41.0 \\ 42.5 \end{array} $	8.0 9.0 8.0	$     \begin{array}{c}       1.0 \\       2.0 \\       1.5     \end{array} $	.ə .5 .5	$     \begin{array}{r}       3.0 \\       2.0 \\       2.0 \\       2.0 \\     \end{array} $	3.5 3.5 3.5	5.0 8.5 10.0
25 26 27	$6.5 \\ 6.0 \\ 5.0$	$17.5 \\ 17.0 \\ 16.0$	$   \begin{array}{r}     37.5 \\     38.0 \\     39.0   \end{array} $	$49.5 \\ 47.5 \\ 47.0$	$4.5 \\ 5.0 \\ 6.0$	$\begin{array}{r} 42.5 \\ 43.5 \\ 43.5 \end{array}$	$     \begin{array}{r}       6.0 \\       5.5 \\       5.0 \\       \hline     \end{array}   $	$     \begin{array}{c}       1.5 \\       1.5 \\       5.0     \end{array} $	.5 .5 .5	$3.0 \\ 4.0 \\ 4.5$	$     \begin{array}{r}       6.5 \\       8.5 \\       7.5     \end{array} $	$     \begin{array}{r}       11.5 \\       11.5 \\       12.5     \end{array} $
28 29 30	3.0 3.0 3.0	17.0	$   \begin{array}{r}     38.5 \\     35.0 \\     33.0   \end{array} $	$     46.5 \\     46.0 \\     44.5 $	7.0 7.0 6.0	$43.5 \\ 44.0 \\ 44.5$	5.5 14.0 14.5	$4.5 \\ 4.0 \\ 3.0$	.5	$7.5 \\ 9.0 \\ 8.0$	$7.5 \\ 8.0 \\ 8.5$	12.0 10.0 10.0
31	3.0		30.0		5.0		14.5	2.0		7.5		10.5

#### YOUGHIOGHENY RIVER AT FRIENDSVILLE, MARYLAND.

This station, which was established by E. G. Paul on August 17, 1898, is located at the iron highway bridge connecting the east and west portions of the village. It is described in Water-Supply Paper No. 36, page 159. Records of measurements for 1899 will be found in the Twenty-first Annual Report, Part IV, page 156. During 1900 the following measurements were made by E. G. Paul and C. R. Olberg:

February 15: Gage height, 6.2 feet; discharge, 1,816 second-feet. June 26: Gage height, 4.6 feet; discharge, 361 second-feet. September 13: Gage height, 3.8 feet; discharge, 48 second-feet.

#### MARYLAND AND WEST VIRGINIA.

Daily gage height, in feet, of Yough	hiogheny River	r at Friendsville,	Maryland, for
	1900.		

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
Day. 1 2 3 4 4 5 6 7 7 8 9 9 10 11 12 13 14 14 15 16 12 13 14 15 16 12 13 14 12 13 14 12 13 14 12 13 14 12 12 13 14 14 12 12 12 12 12 12 12 12 12 12	$\begin{array}{c c} Jan. \\ \hline \\ 5.1 \\ 5.1 \\ 5.1 \\ 5.1 \\ 5.1 \\ 5.1 \\ 5.2 \\ 5.3 \\ 5.3 \\ 5.3 \\ 5.4 \\ 6.3 \\ 6.0 \\ 5.8 \\ 6.0 \\ 5.6 \\ 5.6 \\ 6.3 \\ 6.1 \\ 5.5 \\ 4 \\ 5.5 \\ 4 \\ 5.5 \\ 5.5 \\ 4 \\ 5.5 \\ 4 \\ 5.5 \\ 5.5 \\ 4 \\ 5.5 \\ 4 \\ 5.5 \\ 4 \\ 5.5 \\ 4 \\ 5.5 \\ 4 \\ 5.5 \\ 4 \\ 5.5 \\ 4 \\ 5.5 \\ 4 \\ 5.5 \\ 4 \\ 5.5 \\ 4 \\ 5.5 \\ 4 \\ 5.5 \\ 4 \\ 5.5 \\ 4 \\ 5.5 \\ 4 \\ 5.5 \\ 4 \\ 5.5 \\ 4 \\ 5.5 \\ 4 \\ 5.5 \\ 4 \\ 5.5 \\ 5.5 \\ 4 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.5 \\ 5.$	Feb. 4.8 4.8 4.8 4.8 4.8 4.8 4.8 4.8 4.8 4.8 4.8 4.8 6.6 6.6 6.6 6.3 6.6 6.3 6.6 6.3 6.5 5.5 5.6 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5	Mar. 6.386.666.32 6.666.32 6.6.31 6.6.32 6.6.31 6.6.32 6.6.32 5.5.555 5.5.555 5.5.555 5.5.555 5.5.555 5.5.555 7.6.5 6.58 6.555 5.555 7.6.55 6.58 6.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.555 5.5555 5.5555 5.5555 5.5555 5.5555 5.55555 5.555555	Apr. 5.885.5555555555555555555555555555555	$\begin{array}{c} \textbf{May.}\\ \hline \\ 4.6\\ 4.5\\ 4.5\\ 4.5\\ 4.5\\ 4.6\\ 4.5\\ 4.6\\ 4.7\\ 4.7\\ 4.6\\ 4.5\\ 4.6\\ 4.5\\ 4.6\\ 4.5\\ 4.6\\ 4.5\\ 4.6\\ 4.5\\ 4.5\\ 4.5\\ 4.5\\ 4.5\\ 4.5\\ 4.5\\ 4.5$	June. 4.33 4.33 4.43 4.43 4.43 4.43 4.43 4.42 4.11 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.47 4.42 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.47 4.477 4.477 4.477 4.477 4.477 4.477 4.477 4.477 4.477 4.477 4.477 4.477 4.477 4.477 4.477 4.477 4.477 4.477 4.477 4.477 4.477 4.477 4.477 4.477 4.477 4.477 4.477 4.477 4.477 4.477 4.477 4.477 4.477 4.477 4.477 4.477 4.477 4.477 4.477 4.4777 4.4777 4.4777 4.47777 4.47777777777	$\begin{array}{c} {\rm July.}\\ \hline\\ & 4.8\\ 4.8\\ 4.8\\ 4.6\\ 4.4\\ 4.3\\ 4.2\\ 4.2\\ 4.2\\ 4.1\\ 4.1\\ 4.1\\ 4.1\\ 4.1\\ 4.1\\ 4.1\\ 4.1$	$\begin{array}{c c} Aug. \\ \hline \\ & 4,7,4,5,3,4,2,2,4,4,2,4,4,2,4,4,2,4,4,2,4,4,2,4,4,2,4,4,4,4,4,4,4,4,4,4,4,4,4,4,4,4,4,4,4,4$	Sept. 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.000 4.0000 4.0000 4.0000 4.0000 4.0000 4.0000 4.00000 4.00000 4.0000000000	Oct. 3.9 3.9 3.9 3.9 3.9 3.9 3.9 3.	Nov. $\begin{array}{c} & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\$	$\begin{array}{c} \hline \\ \\ \hline \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\$
27 28 29 30 31	$5.3 \\ 5.2 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 \\ 5.0 $	5.1 5.1	$5.4 \\ 5.4 \\ 5.5 \\ 5.7 \\ 5.7 \\ 5.7 \\ 5.7 \\ $	$     \begin{array}{r}       4.8 \\       4.8 \\       4.7 \\       4.7 \\       4.7 \\       4.7 \\       \hline     \end{array} $	$\begin{array}{c} 4.4 \\ 4.4 \\ 4.4 \\ 4.4 \\ 4.4 \\ 4.1 \end{array}$	$     \begin{array}{r}       4.5 \\       4.6 \\       4.8 \\       4.9 \\     \end{array} $	5.0 4.6 4.7 4.9 5.5	$\begin{array}{c} 4.1 \\ 4.1 \\ 4.2 \\ 4.1 \\ 4.1 \\ 4.1 \end{array}$	3.9 3.9 3.9 3.9 3.9	$\begin{array}{c} 4.1 \\ 4.2 \\ 4.1 \\ 4.1 \\ 4.1 \\ 4.1 \end{array}$	$8.3 \\ 6.9 \\ 5.8 \\ 5.5 $	$4.6 \\ 4.8 \\ 5.0 \\ 5.2 \\ 5.2 \\ 5.2$

#### CHEAT RIVER NEAR UNEVA, WEST VIRGINI'.

This station was established July 8, 1899. As there is no bridge at the place convenient for making measurements, a cable of 600 feet span was stretched across the stream 6 miles northwest of Morgantown, near Uneva, West Virginia. The station is described in Water-Supply Paper No. 36, page 160. During 1900 one measurement was made by E. G. Paul, as follows:

June 25: Gage height, 2.80 feet; discharge, 1,403 second-feet.

Dailg gage height, in feet, of Cheat River near Uneva, West Virginia, for 1900.

Day.	July.	Aug.	Sept	Oct.	Nov.	Dec.	Day.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1	$\begin{array}{c} 3.28\\ 2.87\\ 2.66\\ 2.43\\ 2.99\\ 2.99\\ 2.98\\ 2.55\\ 2.66\\ 2.56\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\ 2.66\\$	$\begin{array}{c} 3.2\\ 3.1\\ 2.97\\ 2.6\\ 2.4\\ 2.3\\ 2.0\\ 2.0\\ 1.8\\ 1.7\\ 1.7\\ 1.6\\ \end{array}$	$\begin{array}{c} 2.3\\ 2.1\\ 2.0\\ 1.9\\ 1.6\\ 1.5\\ 1.4\\ 1.4\\ 1.4\\ 1.4\\ 1.3\\ 1.3\\ 1.3\\ 1.4\\ \end{array}$	$\begin{array}{c} 2.1\\ 2.0\\ 1.9\\ 1.8\\ 1.7\\ 1.6\\ 1.5\\ 1.6\\ 1.7\\ 1.7\\ 1.7\\ 1.7\\ 1.6\\ 1.5\\ 1.4\\ \end{array}$	$\begin{array}{c} 1.6\\ 1.6\\ 1.7\\ 1.7\\ 1.7\\ 1.6\\ 2.0\\ 2.3\\ 2.5\\ 2.4\\ 2.2\\ 2.0\\ 1.9\\ 1.9\\ 1.9\\ 1.9\\ 2.0\\ 2.2\end{array}$	$\begin{array}{c} 4.0\\ 4.0\\ 4.3\\ 7.0\\ 7.0\\ 6.0\\ 4.4\\ 4.7\\ 3.4\\ 3.2\\ 3.0\\ 3.0\\ 3.0\\ \end{array}$	$\begin{array}{c} 17 \\ 18 \\ 19 \\ 20 \\ 21 \\ 22 \\ 23 \\ 24 \\ 25 \\ 26 \\ 27 \\ 28 \\ 29 \\ 28 \\ 29 \\ 29 \\ 30 \\ 31 \\ \ldots \\ 31 \\ \end{array}$	$\begin{array}{c} 2.99\\ 2.99\\ 2.00\\ 3.00\\ 3.95\\ 3.00\\ 2.05\\ 4.5\\ 4.5\\ 3.2\\ 3.2\\ 3.2\\ 3.2\\ 3.2\\ 3.2\\ 3.2\\ 3.2$	$\begin{array}{c} 1.6\\ 1.5\\ 1.5\\ 1.6\\ 2.0\\ 1.9\\ 1.8\\ 1.8\\ 1.8\\ 1.8\\ 1.7\\ 2.0\\ 2.3\\ 2.3\\ 2.3\\ \end{array}$	$\begin{array}{c} 1.4\\ 1.4\\ 1.4\\ 1.3\\ 1.5\\ 1.5\\ 1.5\\ 1.4\\ 1.3\\ 1.3\\ 1.3\\ 1.4\\ 1.4\\ 1.4\\ \end{array}$	$\begin{array}{c} 1.4\\ 1.4\\ 1.5\\ 1.3\\ 1.3\\ 2.3\\ 2.2\\ 2.1\\ 2.0\\ 1.8\\ 1.7\\ 1.6\\ \end{array}$	2.22 2.1 2.22 3.0 3.3 3.5 3.5 3.5 4.0	2:88677760223332211 2:0023332211 2:0023332211

#### NEW RIVER AT RADFORD, VIRGINIA.

This station, which was established by D. C. Humphreys on August 1, 1898, the gage having been erected by the United States Weather Bureau, is described in Water-Supply Paper No. 36, page 161. On account of the inaccuracies of the Weather Bureau gage, a wire gage was put in February 23, 1900, the zero being on the same level as that of the old gage. The observer is T. M. Brady. Records of measurements for 1899 will be found in Water-Supply Paper No. 36, page 162. During 1900 the following measurements were made by D. C. Humphreys:

February 23: Gage height, 2.55 feet; discharge, 11,681 second-feet. February 24: Gage height, 2.10 feet; discharge, 8,500 second-feet. March 30: Gage height, 1.78 feet: discharge, 7,709 second-feet. June 27: Gage height, 1.62 feet; discharge, 6,749 second-feet. July 28: Gage height, 1.25 feet; discharge, 5,256 second-feet. August 22: Gage height, 0.00; discharge, 1,365 second-feet. December 20: Gage height, 0.70 foot; discharge, 2,975 second-feet.

Daily gage height, in feet, of New River at Radford, Virginia, for 1900.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oet.	Nov.	Dec.
1	0.20	0.30	5.85	1.90	1.20	0.80	1.00	0.40	-0.30	0.40	0.90	1.60
3	.20	. 80	3.20	1.20 1.20	$1.40 \\ 1.00$	1.00	. 60	. 30	40	.00	.80 .80	$1.00 \\ 1.00$
4	. 20	. 80	2.10	1.10	1.30	1.00	. 70	. 30	30	. 00	1.00	-1.60
5 6	. 20	80	2.00	$\frac{1.20}{1.10}$	1.20 1.00	. 90	. 90	.30	30	.00	1.40 1.90	$-\frac{4.50}{2.00}$
7	130	1.00	1.80	1.00	1.00	. 80	. 50	.00	70	$10^{-10}_{-10}$	$1.00 \\ 1.00$	-2.00
8	. 30	1.20	2.10	1.00	. 90	. 90	. 37	20	70	.20	. 90	-2.00
9	$.40 \\ 50$	.90	2.20	. 90	1.00	. 80	. 34	40	60	. 20	. 80	-2.10
10		. 90	2.70	1.00	1.00 1.00	. 60	. 36	- : 40	- 30	20	$\frac{100}{70}$	$-\frac{2.00}{1.30}$
12	1.00	1.20	2.60	1.80	1.00	. 70	. 42	00	50	. 00	. 60	1.40
13	$\frac{3.00}{1.00}$	2.00	2.00	1.20	1.00	1.80	. 28	50	40	. 00	. 60	-1.00
14	$1.90 \\ 1.60$	$\frac{4.80}{2.80}$	1.80	1.00	. 90	$1.00 \\ 1.10$	. 14 20	= .80 70	= .40 1.00	. 20	. 50	1.00
16	1.20	1.70	1.40	.80	. 80	1.20	.28	69	2.85	. 30	.50	. 90
17	. 90	1.50	1.70	. 80	. 80	1.60	. 26	80	2.40	. 20	.40	. 80
18	1.80	$\frac{1.40}{1.20}$	$\frac{1.60}{1.20}$	. 70	. 80	$\frac{1.20}{2.00}$	. 14	80	1.20	. 10	.40	. 80
$\frac{10}{20}$	$\frac{1.00}{2.40}$	.90	$\frac{1.50}{3.95}$	$\frac{4.00}{2.60}$	. 50	1.40	. 0.5	$= :\frac{10}{70}$	. 30	.00	. 30	1.70
21	1.90	1.00	4.50	2.30	1.00	1.10	. 08	60	. 40	. 00	. 40	. 60
99 NG 111111111111111111111111111111111111	1.80	3.00	$-\frac{3.30}{9.40}$	2.70	. 90	1.00	.16	.00	. 50	. 30	.50	. 60
24	1.00 1.30	2.20	2.20	2.30	. 90	1.00	. 42	. 10	. 50	23 00	. 50	. 80
25	1.20	2.10	2.10	1.90	2.00	2.00	. 50	1.20	. 40	4.60	.50	1.00
26	1.00	1.90	1.90	1.70	1.90	1.60	. 58	. 20	. 30	2.30	7.80	. 90
24 98	.90	2.60	2.60	1.60 1.40	1.00	2.00	. 80	. 00	. 20	1.30	1.30	. 70
29	. 20		1.90	1.30	1.00	1.80	. 80	.00	30	1.20	1.90	.70
30	. 20		1.70	1.20	. 90	1.60	. 90	20	40	1.00	1.80	. 60
31	. 30		1.00		. 90		. 50	20		1.03		. 70

GREENBRIER RIVER AT ALDERSON, WEST VIRGINIA.

This station, which was established by C. C. Babb and D. C. Humphreys on August 1, 1895, is described in Water-Supply Paper No. 36, page 163. Records of measurements during 1899 will be found in the Twenty-first Annual Report, Part IV, page 159. During 1900 the following measurements were made by D. C. Humphreys:

March 31: Gage height, 4.07 feet; discharge, 5,128 second-feet. June 29: Gage height, 1.99 feet; discharge, 564 second-feet. July 24: Gage height, 1.97 feet; discharge, 493 second-feet. August 20: Gage height, 1.33 feet; discharge, 148 second-feet. December 21: Gage height, 2.24 feet; discharge, 834 second-feet.

Daily gage height, in feet, of Greenbrier River at Alderson, West Virginia, for 1900.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oet.	Nov.	Dec.
1	1.90	2.15	3.98	3.90	2.30	2.25	2.75	2.45	1.55	1.40	1.45	3.00
2	1.88	1.85	6.81	3.48	2.25	2.15	3.00	2.15	1.53	1.50	1.58	2.75
3	1.88	1.95	5.08	3.30	2.18	2.10	2.45	2.00	1.48	1.45	1.60	2.58
4	1.88	1.95	4.00	3.20	2.15	2.20	2.40	1.90	1.45	1.43	3.20	3.48
5	1.90	1.95	3.58	3.08	2.10	2.13	2.08	1.80	1.40 1.90	1.40	2.15	7.00
0	1.80	2.10	0.00 4 59	3.00	2.00	2.00	2.00	1.70	1.38 1.95	1.08	2.23	0.10
1	1.00	2.40	4.00	2.00	2.0.2	1.90	1.90	1.44	1.00	1.01	1 00	9 88
0	1.0)	2.00	4.00	2.00	1.05	1.00	1.00	1.00	1.00	1.00	1.00	2.40
10	2.05	4.95	3 70	3.02	2 10	1 88	1 78	1 55	1.00	1 27	1.80	3.40
11	2 05	3 45	3 45	2.85	2 00	1.82	1 73	1.52	1 25	1 35	1 72	3 15
12	2 17	3 10	3 17	2 65	1.95	1 75	1 65	1.48	1.23	1 35	1.75	2.92
13	4.18	7.24	3.00	2.55	1.97	1.68	1.63	1.45	1.20	1.33	1.75	2.73
14	3.15	7.90	2.90	2.50	1.92	1.70	1.60	1.40	1.20	1.45	1.85	2.65
15	2.80	5.05	2.93	2.37	1.85	2.05	1.55	1.40	1.31	1.70	1.80	2.55
16	2.53	4.00	2.87	2.30	1.83	2.28	1.52	1.40	1.88	1.70	1.78	2.45
17	2.38	3.48	2.85	2.20	1.80	-3.20	1.45	1.35	1.65	1.60	1.75	2.30
18	2.40	3.10	2.60	2.40	1.77	5.23	1.45	1.37	1.50	1.55	1.68	2.25
19	2.65	2.65	2.89	2.52	1.73	4.40	1.45	1.40	1.45	1.50	1.65	2.25
20	5.98	2.50	8.12	3.40	1.80	3.50	1.42	1.37	1.40	1.45	1.62	2.20
21	5.65	2.55	8.23	3.55	2.90	3.00	1.42	1.40	1.38	1.45	1.60	2.23
22	4.33	4.05	5.50	3.65	2.50	2.65	1.48	1.40	1.43	1.43	1.72	2.20
23	3.40	5.40	4.50	3.73	2.32	2.45	2.10	1.00	1.50	2.47	2.43	2.08
24	5.05	4.01	3.40	0.40	2.20	2.20	2.20	1.40	1.00	3.08	0.08	$\begin{bmatrix} 2.05\\ 0.10 \end{bmatrix}$
20	2. 10 0 55	0.40	4.80	0.10	2.20	2.13	0.44	1.40	$1.00 \\ 1.59$	2.60	3.08	2.18
20	2.00	0.00	4.00	9.75	2.00	2.07	2.44	1.40 1.50	1.00	2.40	18.20	2.20
100 ······	9.40	9.20	4.10	2 20	9 90	1 95	3.91	1.50	1.40	2.40	5.00	9 13
90	9 03	1.00	4 05	2 45	2 20	1 95	2 90	1.50	1 45	1 75	4 00	9 19
30	9 45		3.80	2 40	2 40	2 00	2 50	1.55	1.40	1 70	3 37	2.38
31	2 05		4.10	10	2.40	2.00	2.48	1.50	1. 10	1 63	0.01	2 35
04	1.00						. 10					A. 00

NORTH FORK OF NEW RIVER AT WEAVERSFORD, NORTH CAROLINA.

During the summer of 1900 a special investigation of the hydrographic conditions of the southern Appalachian region was made by the United States Geological Survey. Temporary stations were established on several of the largest rivers, among these being the North Fork and the South Fork of New River. A station was also established on New River near Oldtown, Virginia. The regular station on New River, which is at Fayette, West Virginia, has been continued. Descriptions of these temporary stations and the gage heights obtained are given on the following pages.

The station at Weaversford was established July 27, 1900, by Cleveland Abbe, jr., and N. C. Curtis. The nearest railroad station is at North Wilkesboro, 40 miles distant, and the Weaversford post-office is a fourth of a mile from the gaging station, which can only be reached by private conveyance. The gage rod is 12.6 feet long, and is divided into feet and tenths. It is nailed to the downstream vertical timber of the forebay of Dixon's mill. The discharge measurements are made by wading at a comparatively shallow ford, not much used and not on a public highway, located 400 yards below the house of Mr. Dixon, the owner of the mill. The initial point of sounding is on the right bank, at the outer edge of a fence post opposite the ford where measurements are made. The banks are high and have been overflowed only once, viz, in 1878. The bed of the stream is rocky and gravelly, and is constant in form. The observer is C. L. Nelson, post-office address Weaversford, Ashe County, North Carolina. The gage heights for 1900 will be published next year. During 1900 the following measurements were made by N. C. Curtis and Cleveland Abbe, jr.:

July 23: Gage height, 0.60 foot; discharge, 536 second-feet. October 27: Gage height, 0.90 foot; discharge, 708 second-feet.

#### SOUTH FORK OF NEW RIVER AT NEW RIVER, NORTH CAROLINA.

This station was established July 28, 1900, by Cleveland Abbe, jr., and N. C. Curtis. The nearest railroad station is North Wilkesboro, 30 miles distant, and the gaging station can only be reached by private conveyance. The discharge measurements are made by wading across a ford a half mile above the confluence of the North and South forks of New River and about 1 mile downstream from the gage at Warden's store. The gage is a wire cord running over a bolt driven into a locust tree, and reads on a horizontal scale divided into feet and tenths. The pointer or index on the gage wire is 10.55 feet from the extreme tip of the double window-sash weights which are attached. When the latter rest on the bottom, the index stands opposite 1 foot on the scale, which is read direct. The initial point of sounding is a notch on the stream side of the second small poplar on the left of the road going toward the stream and opposite the ford. The channel is straight, the current fairly swift, and the banks are low and seldom overflow. The bed of the stream is rocky, with bowlders and cobbles. The drainage area at this station is 326.5 square miles. The observer is F. R. Warden, a storekeeper located about 75 yards downstream from the gage. During 1900 the following measurements were made by N. C. Curtis and Cleveland Abbe, jr.:

July 28: Gage height, 2.7 feet; discharge, 751 second-feet. October 28: Gage height, 2.6 feet; discharge, 1,635 second-feet.

Daily gage height,	in feet,	of	South	Fork a	of	New	River	at	New	River,	North	Caro-
			l	ina, fo	r 1 $!$	900.						

Day.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Day.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
$\begin{array}{c} 1 \\ 2 \\ 3 \\ 4 \\ 5 \\ 6 \\ 7 \\ 8 \\ 9 \\ 10 \\ \end{array}$		$\begin{array}{r} 2.45 \\ 2.35 \\ 2.30 \\ 2.30 \\ 2.30 \\ 2.30 \\ 2.30 \\ 2.30 \\ 2.30 \\ 2.30 \\ 2.30 \\ 2.30 \\ 2.30 \end{array}$	$\begin{array}{c} 2.30\\ 2.25\\ 2.20\\ 2.20\\ 2.20\\ 2.20\\ 2.20\\ 2.20\\ 2.20\\ 2.20\\ 2.20\\ 2.20\\ 2.20\\ 2.20\end{array}$	$\begin{array}{r} 2.30\\ 2.30\\ 2.45\\ 2.80\\ 2.75\\ 2.70\\ 2.55\\ 2.50\\ 2.45\\ 2.40\end{array}$	$\begin{array}{c} 2.\ 60\\ 2.\ 60\\ 3.\ 50\\ 3.\ 80\\ 3.\ 30\\ 2.\ 80\\ 2.\ 65\\ 2.\ 60\\ 2.\ 60\\ 2.\ 60\end{array}$	$\begin{array}{c} 2.70\\ 2.70\\ 2.70\\ 3.95\\ 3.70\\ 3.20\\ 2.85\\ 2.80\\ 2.80\\ 2.75\end{array}$	17 18 19 20 21 22 23 24 25 26		$\begin{array}{c} 2.20 \\ 2.20 \\ 2.20 \\ 2.20 \\ 2.20 \\ 2.30 \\ 2.30 \\ 2.30 \\ 2.30 \\ 2.30 \\ 2.30 \\ 2.30 \\ 2.25 \end{array}$	$\begin{array}{c} 2.80 \\ 2.40 \\ 2.30 \\ 2.30 \\ 2.30 \\ 2.30 \\ 2.30 \\ 2.30 \\ 2.30 \\ 2.30 \\ 2.30 \\ 2.30 \\ 2.30 \end{array}$	$\begin{array}{c} 2.25\\ 2.20\\ 2.20\\ 2.20\\ 2.20\\ 2.20\\ 2.20\\ 7.90\\ 6.70\\ 3.75\\ 3.05\end{array}$	$\begin{array}{c} 2.40\\ 2.40\\ 2.40\\ 2.35\\ 2.30\\ 2.30\\ 2.30\\ 2.70\\ 5.20\\ \end{array}$	$\begin{array}{c} 2.60\\ 2.60\\ 2.60\\ 2.60\\ 2.60\\ 2.60\\ 2.60\\ 2.60\\ 2.60\\ 2.60\\ 2.60\\ 2.60\\ 2.60\end{array}$
$ \begin{array}{c} 11 \\ 12 \\ 13 \\ 14 \\ 15 \\ 16 \\ \end{array} $		$\begin{array}{c} 2.30 \\ 2.30 \\ 2.35 \\ 2.40 \\ 2.35 \\ 2.30 \\ 2.33 \\ 2.30 \end{array}$	$\begin{array}{c} 2.20 \\ 2.15 \\ 2.10 \\ 2.55 \\ 2.60 \\ 3.70 \end{array}$	$\begin{array}{c} 2.45\\ 2.35\\ 2.30\\ 2.30\\ 2.30\\ 2.30\\ 2.30\end{array}$	$\begin{array}{c} 2.60\\ 2.55\\ 2.50\\ 2.50\\ 2.45\\ 2.40\end{array}$	$\begin{array}{c} 2.\ 70\\ 2.\ 70\\ 2.\ 60\\ 2.\ 60\\ 2.\ 60\\ 2.\ 60\\ 2.\ 60\end{array}$	27 28 29 30 31	2.65 2.50 2.50 2.50	$\begin{array}{c} 2.20 \\ 2.20 \\ 2.50 \\ 2.45 \\ 2.35 \end{array}$	$2.30 \\ 2.30 \\ 2.30 \\ 2.30 \\$	$\begin{array}{c} 2.90 \\ 2.70 \\ 2.60 \\ 2.60 \\ 2.60 \\ 2.60 \end{array}$	$   \begin{array}{r}     3.60 \\     3.05 \\     2.95 \\     2.80 \\   \end{array} $	$\begin{array}{c} 2.60\\ 2.60\\ 2.60\\ 2.60\\ 2.80\end{array}$

#### NEW RIVER NEAR OLDTOWN, VIRGINIA.

This station, which was established by Cleveland Abbe, jr., and N. C. Curtis, July 31, 1900, is located about 2 miles west of Oldtown, and can only be reached by private conveyance. Oldtown is 30 miles from the railroad at Mount Airy, and 9 miles from a branch of the Norfolk and Western Railway. The wire gage is suspended from an overhanging tree on the left bank, 50 yards upstream from the ferry. The horizontal scale is so placed that the zero mark is next to the bank. The distance from the index on the wire to the bottom of the weight is 16.1 feet. The initial point of sounding is on the right bank, and is a notch cut in the wooden upright of the beam supporting the north end of the ferry cable. The channel above and below the station is straight and the current is fairly swift. The right bank is rather low and is subject to overflow. The left bank is rarely submerged in flood. The bed of the stream is rocky and sandy. The observer is Joshua Austin, a farmer of Oldtown. During 1900 the following measurements were made by N. C. Curtis and Cleveland Abbe, jr.:

July 31: Gage height, 6.6 feet; discharge, 1,541 second-feet. October 29: Gage height, 6.3 feet; discharge, 2,293 second-feet.

Daily gage height, in feet, of New River near Oldtown, Virginia, for 1900.

Day.	Aug.	Sept.	Oct.	Nov.	Dec.	Day.	Aug.	Sept.	Oet.	Nov.	Dec.
$\begin{array}{c} 1 \\ 2 \\$	$\begin{array}{c} 6.70\\ 6.70\\ 6.80\\ 6.90\\ 6.90\\ 6.90\\ 6.90\\ 6.90\\ 7.00\\ 7.10\\ 7.20\\ 7.20\\ 7.20\\ 6.80\\ \end{array}$	$\begin{array}{c} \hline 6.80 \\ 6.90 \\ 7.00 \\ 7.10 \\ 7.10 \\ 7.10 \\ 7.20 \\ 7.20 \\ 7.20 \\ 7.20 \\ 7.20 \\ 7.20 \\ 5.90 \\ 5.90 \\ 5.90 \\ \hline \end{array}$	$\begin{array}{c} 6.90\\ 6.80\\ 6.70\\ 6.60\\ 6.40\\ 6.50\\ 6.60\\ 6.70\\ 6.70\\ 6.70\\ 6.90\\ 6.90\\ 6.90\\ 6.90\\ 6.90\\ 6.90\\ \end{array}$	$\begin{array}{c} 6.\ 60\\ 6.\ 60\\ 5.\ 40\\ 5.\ 10\\ 5.\ 60\\ 5.\ 10\\ 6.\ 30\\ 6.\ 50\\ 6.\ 50\\ 6.\ 50\\ 6.\ 50\\ 6.\ 60\\ 6.\ 70\\ 6.\ 60\\ 6.\ 70\\ 6.\ 60\\ 6.\ 70\\ \end{array}$	$\begin{array}{c} 6.30\\ 6.30\\ 6.50\\ 5.80\\ 5.50\\ 5.90\\ 5.90\\ 6.00\\ 6.10\\ 6.30\\ 6.30\\ 6.50\\ 6.50\\ \end{array}$	17	$\begin{array}{c} 6.10\\ 7.00\\ 7.00\\ 7.10\\ 6.90\\ 6.90\\ 6.50\\ 6.60\\ 6.70\\ 6.90\\ 6.10\\ 6.10\\ 7.00\\ 6.30\\ 6.60\\ \end{array}$	$\begin{array}{c} 5.80\\ 6.50\\ 6.90\\ 6.80\\ 6.80\\ 6.80\\ 6.80\\ 6.80\\ 6.50\\ 6.90\\ 6.90\\ \hline \\ 6.90\\ \hline \end{array}$	$\begin{array}{c} 6.90\\ 6.10\\ 6.10\\ 6.10\\ 6.10\\ 1.20\\ 4.30\\ 5.40\\ 5.90\\ 6.10\\ 6.30\\ 6.30\\ 6.50\\ \end{array}$	$\begin{array}{c} 6.80\\ 6.80\\ 6.80\\ 6.80\\ 6.70\\ 6.70\\ 6.60\\ 2.40\\ 4.60\\ 5.80\\ 5.10\\ 6.20\\ \end{array}$	$\begin{array}{c} 6.50\\ 6.60\\ 6.60\\ 6.70\\ 6.50\\ 6.50\\ 6.50\\ 6.50\\ 6.70\\ 6.70\\ 6.70\\ 6.70\\ 6.70\\ 6.70\\ 6.40\\ \end{array}$

NEW RIVER AT FAYETTE, WEST VIRGINIA.

This station, which was established July 29, 1895, is just above the mouth of Wolf Creek, on the one-span highway bridge at Fayette, West Virginia. It is described in Water-Supply Paper No. 36, page 164. Records of measurements for 1899 will be found in the Twenty-first Annual Report, Part IV, page 157. During 1900 the following measurements were made by D. C. Humphreys:

March 31: Gage height, 8.49 feet; discharge, 17,387 second-feet. June 29: Gage height, 5.58 feet; discharge, 11,436 second-feet. July 25: Gage height, 2.47 feet; discharge, 4,625 second-feet. August 20: Gage height, 0.55 foot; discharge, 2,275 second-feet. December 21: Gage height, 3.40 feet; discharge, 5,915 second-feet.

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Daily gage height, in feet, of New River at Fayette, West Virginia, for 1900.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1 2 3 4 5 6 7 8 9	$\begin{array}{c} 2.95\\ 3.20\\ 3.40\\ 3.10\\ 3.10\\ 3.00\\ 3.05\\ 3.10\\ 3.40\end{array}$	$\begin{array}{r} 3.95\\ 3.60\\ 3.55\\ 3.50\\ 3.40\\ 3.45\\ 3.30\\ 3.05\\ 3.00\\ 3.05\\ 3.00\end{array}$	$\begin{array}{c} 7.80\\ 12.50\\ 8.15\\ 6.40\\ 5.55\\ 4.05\\ 4.10\\ 3.80\\ 3.50\end{array}$	$\begin{array}{c} 8,30\\ 7,50\\ 6,90\\ 6,50\\ 6,20\\ 5,70\\ 5,40\\ 5,00\\ 4,85\end{array}$	$\begin{array}{r} 4.50\\ 4.40\\ 4.10\\ 4.00\\ 4.00\\ 3.95\\ 3.85\\ 3.85\\ 3.90\end{array}$	$\begin{array}{r} 4.30\\ 3.60\\ 3.30\\ 3.00\\ 4.00\\ 3.50\\ 3.30\\ 3.00\\ 2.65\end{array}$	$\begin{array}{r} 6.60\\ 6.15\\ 5.30\\ 4.00\\ 3.10\\ 2.70\\ 2.90\\ 2.10\\ 1.80\end{array}$	$\begin{array}{r} 3.00\\ 2.20\\ 1.40\\ 1.00\\ .70\\ .50\\ .25\\ .10\\ 10 \end{array}$	0,90 .90 .90 .80 .80 .70 .70 .70 .60	$1.10 \\ .95 \\ .80 \\ .75 \\ 1.10 \\ 1.10 \\ 1.45 \\ 1.70$	3.50 3.70 3.00 2.80 2.65 2.90 3.25 3.40 3.80	$(a) \\ (a) $
$\begin{array}{c} 9 \\ 10 \\ 11 \\ 12 \\ 13 \\ 14 \\ 15 \\ 16 \\ 17 \\ 18 \end{array}$	$\begin{array}{c} 3.40\\ 3.60\\ 4.10\\ 4.44\\ 6.20\\ 5.45\\ 5.30\\ 5.00\\ 4.70\\ 4.40\end{array}$	$\begin{array}{c} 3.00 \\ 3.20 \\ 3.40 \\ 4.05 \\ 4.20 \\ 11.25 \\ 9.60 \\ 7.05 \\ 3.40 \\ 3.55 \end{array}$	$\begin{array}{c} 5.50\\ 3.45\\ 3.90\\ 4.05\\ 4.00\\ 4.00\\ 5.10\\ 5.75\\ 5.85\\ 6.20\end{array}$	$\begin{array}{r} 4.85\\ 4.95\\ 4.75\\ 4.40\\ 4.25\\ 4.30\\ 4.20\\ 3.80\\ 3.60\\ 3.40\end{array}$	$\begin{array}{c} 3.90\\ 4.00\\ 4.50\\ 4.60\\ 4.25\\ 3.85\\ 3.55\\ 3.25\\ 3.15\\ 2.90\end{array}$	$\begin{array}{c} 2.03\\ 2.50\\ 2.40\\ 2.20\\ 3.45\\ 3.60\\ 3.50\\ 8.20\\ 10.40\\ 11.00\end{array}$	$\begin{array}{c} 1.80\\ 1.45\\ 1.10\\ .90\\ .80\\ .70\\ .60\\ .60\\ .60\\ .50\end{array}$	.10 .00 .90 .60 .30 .20 .10 .10 .20 .20	$     \begin{array}{r}         & .00 \\         & .75 \\         & .80 \\         & .85 \\         & .75 \\         & .90 \\         & .80 \\         & .00 \\         & .00 \\         & .15 \\         & .80 \\         & .00 \\         & .15 \\         & .80 \\         & .80 \\         & .00 \\         & .80 \\         & .00 \\         & .80 \\         & .00 \\         & .80 \\         & .80 \\         & .00 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .90 \\         & .80 \\         & .80 \\         & .00 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\         & .80 \\   $	$\begin{array}{c} 1.40\\ -1.80\\ 1.60\\ 1.35\\ 1.40\\ 2.05\\ 2.25\\ 2.00\\ 1.85\\ 3.05 \end{array}$	$\begin{array}{c} 5.\ 60\\ 4.\ 00\\ 3.\ 75\\ 3.\ 60\\ 3.\ 45\\ 3.\ 35\\ 3.\ 10\\ 3.\ 00\\ 2.\ 70\\ 2.\ 50\end{array}$	(a) (a) (a) (a) (a) (a) (a) (a) (a) (a) (a) (a)
19	$\begin{array}{c} 4.30\\ 5.45\\ 8.75\\ 6.40\\ 4.40\\ 3.25\\ 3.60\\ 3.35\\ 3.50\\ 2.60\end{array}$	$\begin{array}{c} 4.10\\ 4.05\\ 5.10\\ 5.40\\ 7.30\\ 6.55\\ 5.60\\ 6.10\\ 5.30\\ 4.20\end{array}$	$\begin{array}{c} 7.85\\ 10.40\\ 13.60\\ 12.30\\ 9.90\\ 7.45\\ 5.95\\ 5.15\\ 4.90\\ 7.50\end{array}$	$\begin{array}{c} 3,80\\ 10,20\\ 8,50\\ 9,80\\ 9,80\\ 9,30\\ 7,85\\ 6,85\\ 6,10\\ 5,50\end{array}$	$\begin{array}{c} 4.50 \\ 4.45 \\ 4.10 \\ 4.60 \\ 4.10 \\ 3.50 \\ 4.00 \\ 6.55 \\ 6.05 \\ 5.20 \end{array}$	$\begin{array}{c} 10,50\\ 8,50\\ 6,80\\ 6,30\\ 6,00\\ 5,80\\ 5,60\\ 5,25\\ 5,00\\ 4,70\\ \end{array}$	$\begin{array}{r} .80\\ .90\\ .90\\ .75\\ .50\\ 2.10\\ 2.70\\ 2.90\\ 5.00\\ .690\end{array}$	.10 .30 .20 .40 .50 .70 1.00 1.15 .20	$\begin{array}{c} 6.00\\ 5.40\\ 5.05\\ 4.60\\ 4.30\\ 2.85\\ 2.50\\ 2.05\\ 1.40\\ 1.95\end{array}$	3.20 2.95 3.15 3.15 2.90 16.05 18.10 13.30 10.00	$ \begin{array}{r} 2.40 \\ 2.30 \\ 3.10 \\ 4.40 \\ 5.80 \\ 6.60 \\ \hline 25.00 \\ (a) \\ (c) \end{array} $	$ \begin{array}{c} (a) \\ (a) \\ (a) \\ (a) \\ (a) \\ 2.50 \\ 2.80 \\ 3.00 \\ 3.20 \\ 2.50 \end{array} $
29 	$     \begin{array}{r}       5.00 \\       3.75 \\       4.20 \\       4.05     \end{array} $		9, 65 8, 60 8, 50	5.00 4.60	$ \begin{array}{r} 5.30 \\ 4.60 \\ 4.25 \\ 4.90 \end{array} $	4.70 5.50 6.75		$     \begin{array}{r}       1.50 \\       1.50 \\       2.00 \\       1.40     \end{array} $	1.15 1.90	$5.00 \\ 4.75 \\ 4.00$	(a) $(a)$ $(a)$ $(a)$	3.90 3.90 3.90 4.10

*a* Gage broken; no record.

#### SOUTH FORK OF HOLSTON RIVER AT BLUFF CITY, TENNESSEE.

This station was originally established by the United States Weather Bureau at the highway bridge at Bluff City. Readings were begun July 17, 1900, by the United States Geological Survey, in connection with the general hydrographic investigation of the southern Appalachian region. The gage is a 4-inch by 8-inch timber bolted to the downstream side of the stone pier. The initial point of sounding is on the north end of the bridge, downstream side. The channel is straight for about 500 feet above and below the bridge, and the current is swift. The north bank is high, but the south bank is subject to overflow at the bridge. The bed is rocky and constant in section. The drainage area is 828.1 square miles. O. V. Cox is the observer. During 1900 the following measurements were made by E. W. Myers and L. V. Branch:

July 17: Gage height, 0.25 foot; discharge, 378 second-feet. August 16: Gage height, 0.25 foot; discharge, 329 second-feet. September 25: Gage height, 1.15 feet; discharge, 791 second-feet. November 8: Gage height, 0.90 foot; discharge, 681 second-feet. December 27: Gage height, 0.60 foot; discharge, 392 second-feet.

#### TENNESSEE.

Daily gage height, in feet, of	South Fork of Holston	River at Bluff City, Tennessee,
	for 1900.	

Day.	July.	Aug.	Sept.	Oet.	Nov.	Dec.	Day.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1		0.60 .45 .35 .25 .25	$\begin{matrix} 0.30 \\ .25 \\ .25 \\ .20 \\ .20 \\ .20 \\ .15 \\ .10 \\ .10 \\ .10 \\ .05 \\ 2.00 \\ 3.00 \end{matrix}$	$\begin{array}{c} 0.45 \\ .40 \\ .20 \\ .20 \\ .10 \\ .10 \\ .30 \\ .25 \\ .25 \\ .20 \\ .20 \\ .20 \\ .20 \\ .25 \end{array}$	$\begin{array}{c} 0.65\\ .60\\ .60\\ 1.70\\ 1.80\\ 1.40\\ 1.00\\ .80\\ .80\\ .80\\ .80\\ .80\\ .80\\ .60\\ .50\\ \end{array}$	$\begin{array}{c} 1.40\\ 1.20\\ 1.10\\ 2.55\\ 4.35\\ 3.20\\ 2.70\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.40\\ 1.30\\ 1.30\\ 1.20\\ \end{array}$	$\begin{array}{c} 17 \\ 18 \\ 19 \\ 20 \\ 21 \\ 22 \\ 23 \\ 23 \\ 24 \\ 25 \\ 26 \\ 27 \\ 28 \\ 27 \\ 28 \\ 29 \\ 30 \\ 31 \\ \ldots \\ \ldots \\ \end{array}$	$\begin{array}{c} 0.40\\ .40\\ .40\\ .40\\ .40\\ .40\\ .60\\ 2.00\\ 3.70\\ 1.80\\ \end{array}$	$\begin{array}{c} 0.20\\ .20\\ .20\\ .20\\ 1.00\\ 1.50\\ 1.40\\ .60\\ .35\\ .30\\ .25\\ .20\\ 1.20\\ .60\\ \end{array}$	$\begin{array}{c} 1.70\\ .90\\ .60\\ .50\\ .20\\ .90\\ 1.10\\ 1.00\\ .90\\ .70\\ .70\\ .70\\ .40\\ \end{array}$	$\begin{array}{c} 0.20\\ .10\\ .10\\ .10\\ .46\\ .45\\ 2.60\\ 1.90\\ 1.60\\ 1.30\\ 1.10\\ .70\\ .70\end{array}$	$\begin{array}{c} 0.45 \\ .40 \\ .50 \\ .555 \\ .60 \\ .90 \\ 1.30 \\ 3.70 \\ 2.50 \\ 1.90 \\ 1.60 \end{array}$	$\begin{array}{c} 1.00\\ .80\\ .80\\ .75\\ .75\\ .70\\ .70\\ .70\\ .70\\ .60\\ .60\\ .60\\ .60\\ .80\end{array}$

#### WATAUGA RIVER AT BUTLER, TENNESSEE.

In connection with the general hydrographic investigation of the southern Appalachian region, stations were established on Watauga River and on Roan Creek at Butler, Tennessee; also on Elk Creek at Lineback, Tennessee. Descriptions of these stations and records of the gage heights and discharge measurements are given on the following pages. The station on Watauga River at Butler is about 100 vards below the mouth of Roan Creek. It was established August 14, 1900. The gage rod, which is graduated to feet and tenths, is nailed to a tree on the right bank. Measurements are made from the highway bridge. The initial point of sounding is at the downstream end of the guard rail. The channel is straight above and below the station, and the current is swift. The banks are high, and the bed is sandy and rocky. The drainage area is 261 square miles. The observer is Edgar L. Shull. During 1900 the following measurements were made by E. W. Myers and L. V. Branch:

July 30: Gage height, 1.37 feet; discharge, 434 second-feet. August 7: Gage height, 0.90 foot; discharge, 214 second-feet. August 17: Gage height, 0.84 foot; discharge, 166 second-feet. October 6: Gage height, 1.12 feet; discharge, 238 second-feet. November 7: Gage height, 2.20 feet; discharge, 591 second-feet. December 28: Gage height, 1.40 feet; discharge, 311 second-feet.

Daily gage height, in feet, of Watauga River at Butler, Tennessee, for 1900.

Day.	Aug.	Sept.	Oct.	Nov.	Dec.	Day.	Aug.	Sept.	Oct.	Nov.	Dec.
1         2         3         4         5         6         7         8         9         0         1         12         13         14         16	1.30 .80 .70	$\begin{array}{c} 0.90\\ .90\\ .90\\ .90\\ .90\\ .90\\ .80\\ .80\\ .80\\ .80\\ .80\\ .80\\ .80\\ .80\\ 1.70\\ 1.70\\ 3.10 \end{array}$	$\begin{array}{c} 0.\ 90\\ .\ 90\\ .\ 90\\ .\ 90\\ .\ 90\\ .\ 90\\ .\ 90\\ .\ 90\\ .\ 90\\ .\ 90\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .\ 80\\ .$	$\begin{array}{c} 5.60\\ 5.00\\ 2.30\\ 2.10\\ 2.50\\ 2.00\\ 1.90\\ 1.90\\ 1.90\\ 1.80\\ 1.60\\ 1.50\\ 1.50\\ 1.50\\ \end{array}$	$\begin{array}{c} 2.00\\ 2.40\\ 2.40\\ 5.00\\ 4.00\\ 3.50\\ 3.00\\ 2.50\\ 2.10\\ 1.90\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ \end{array}$	$\begin{array}{c} 17. \\ 18. \\ 19. \\ 20. \\ 21. \\ 22. \\ 23. \\ 24. \\ 25. \\ 26. \\ 26. \\ 27. \\ 28. \\ 29. \\ 28. \\ 29. \\ 30. \\ 31. \\ \end{array}$	$\begin{array}{c} 0.90\\ 80\\ .80\\ 1.10\\ 1.60\\ 1.30\\ 1.20\\ .90\\ .90\\ .90\\ .80\\ 1.90\\ 1.40\\ \end{array}$	$\begin{array}{c} 4.50\\ 4.00\\ 3.20\\ 2.70\\ 1.10\\ 1.00\\ 1.00\\ .90\\ .90\\ .90\\ .90\\ .90\\ .90\end{array}$	$\begin{array}{c} 0.70\\ .70\\ .70\\ .70\\ .70\\ .70\\ 15.00\\ 9.00\\ 2.50\\ 2.00\\ 4.50\\ 2.00\\ 4.00\\ 4.00\\ 3.20\end{array}$	$\begin{array}{c} 1.50\\ 1.50\\ 1.40\\ 1.40\\ 1.40\\ 1.40\\ 1.40\\ 1.40\\ 1.40\\ 3.00\\ 3.00\\ 2.40\\ \end{array}$	$\begin{array}{c} 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\$

#### ROAN CREEK AT BUTLER, TENNESSEE.

This station was established August 8, 1900. The gage is a vertical rod nailed to a tree on the left bank of the stream, at Cole & Scott's gristmill, about a half mile above the mouth of the creek. Measurements are made from the highway bridge at the mouth of the creek, the initial point of sounding being on the right bank, at the end of the upstream guard rail. The left bank is low and is subject to overflow. The bed is composed of sand and mud. The drainage area is 163.6 square miles. The observer is W. N. Bridges, of Butler.

During 1900 the following measurements were made by E. W. Myers and L. V. Branch:

July 30: Gage height, 1.47 feet; discharge, 137 second-feet. August 7: Gage height, 1.02 feet; discharge, 65 second-feet. August 17: Gage height, 0.85 foot: discharge, 58 second-feet. October 6: Gage height, 0.86 foot; discharge, 52 second-feet. November 7: Gage height, 1.50 feet; discharge, 171 second-feet. December 28: Gage height, 1.20 feet; discharge, 82 second-feet.

Daily gage height, in feet, of Roan Creek at Butler, Tennessee, for 1900.

Day.	Aug.	Sept.	Oct.	Day.	Aug.	Sept.	Oct.	Day.	Aug.	Sept.	Oct.
$\begin{array}{c} 1 \\ 2 \\ \\ 3 \\ \\ 5 \\ \\ 6 \\ \\ 7 \\ \\ 8 \\ \\ 9 \\ \\ 10 \\ \\ 11 \\ \end{array}$	0.90 .72 .82 .78	$\begin{array}{c} 0.\ 95\\ 1.\ 00\\ .\ 83\\ .\ 83\\ .\ 83\\ .\ 81\\ .\ 80\\ .\ 76\\ .\ 75\\ .\ 75\end{array}$	$\begin{array}{c} 1.00\\ .85\\ .85\\ .85\\ .80\\ .86\\ .80\\ .89\\ .89\\ .88\\ .83\end{array}$	12 13 14 15 16 17 18 19 20 21 22	$\begin{array}{c} 0.78\\.85\\1.20\\.93\\.86\\.84\\.85\\.80\\.82\\1.05\\1.71\end{array}$	$\begin{array}{c} 0.\ 73 \\ .\ 75 \\ 1.\ 00 \\ 1.\ 65 \\ 2.\ 50 \\ 1.\ 05 \\ 1.\ 05 \\ 1.\ 00 \\ .\ 93 \\ .\ 95 \end{array}$	$\begin{array}{c} 0.87\\ .90\\ .85\\ .88\\ .82\\ .80\\ .80\\ .80\\ .80\\ .81\\ .78\\ .80\end{array}$	23 24 25 26 27 28 28 28 29 30 31	$\begin{array}{c} 1.27\\ 1.00\\ .90\\ .90\\ .84\\ .86\\ .91\\ 1.32\\ 1.05 \end{array}$	$\begin{array}{c} 1.20\\ 1.25\\ 1.05\\ .95\\ .98\\ .91\\ .95\\ 1.30\\ \end{array}$	4.80

#### ELK CREEK AT LINEBACK, TENNESSEE.

This station was established August 8, 1900. The gage rod is nailed to a tree on the left bank, 100 yards below the Lineback post-office. Gagings are made by wading. The banks are low and are subject to overflow. The channel is straight and the current is swift. The drainage area is 80.4 square miles. The observer is Dove Lineback, of Lineback, Tennessee. During 1900 the following measurements were made by E. W. Myers and L. V. Branch:

August 9: Gage height, 3.5 feet; discharge, 70 second-feet. August 17: Gage height, 3.5 feet; discharge, 56 second-feet. October 6: Gage height, 3.5 feet; discharge, 53 second-feet.

#### TENNESSEE.

Daily gage height, in feet, of Elk Creek at Lineback, Tennessee, for 1900.

	Day.	Aug.	Sept.	Oct.	Nov.	Dec.	Day.	Aug.	Sept.	Oct.	Nov.	Dec.
$\begin{array}{c} 1 \\ 2 \\ 3 \\ 4 \\ 5 \\ 5 \\ 7 \\ 8 \\ 9 \\ 10 \\ 11 \\ 12 \\ 13 \\ 14 \\ 15 \\ 16 \\ 16 \\ 16 \\ 16 \\ 16 \\ 16 \\ 16$		3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.70 3.60 3.50	$\begin{array}{c} 3.60\\ 3.50\\ 3.50\\ 3.50\\ 3.50\\ 3.40\\ 3.40\\ 3.40\\ 3.40\\ 3.30\\ 3.40\\ 3.30\\ 3.40\\ 3.80\\ 4.30\\ 4.30\\ 4.30\\ \end{array}$	$\begin{array}{c} \textbf{3.40}\\ \textbf{3.40}\\ \textbf{3.40}\\ \textbf{3.60}\\ \textbf{3.50}\\ 3.5$	$\begin{array}{c} 4.00\\ 3.90\\ 5.30\\ 5.60\\ 5.30\\ 4.50\\ 4.30\\ 4.20\\ 4.00\\ 4.00\\ 4.00\\ 4.00\\ 4.00\\ 4.00\\ 3.90\\ 3.90 \end{array}$	$\begin{array}{c} 5.30\\ 5.30\\ 5.30\\ 5.80\\ 4.60\\ 4.50\\ 4.40\\ 4.30\\ 4.20\\ 4.40\\ 4.30\\ 4.20\\ 4.40\\ 4.00\\ 4.00\\ \end{array}$	17	$\begin{array}{c} 3.50\\ 3.50\\ 3.40\\ 3.90\\ 3.90\\ 3.40\\ 3.40\\ 3.40\\ 3.40\\ 3.40\\ 3.50\\ 3.50\\ 4.00\\ 3.50\\ 4.00\\ 3.90 \end{array}$	$\begin{array}{c} 4.00\\ 3.80\\ 3.70\\ 3.60\\ 3.60\\ 3.60\\ 3.60\\ 3.60\\ 3.60\\ 3.50\\ 3.50\\ 3.50\\ 3.50\\ 3.40\\ 3.40\\ \end{array}$	$\begin{array}{c} 3.40\\ 3.40\\ 3.30\\ 3.30\\ 3.30\\ 3.30\\ 11.00\\ 5.50\\ 5.40\\ 5.30\\ 4.70\\ 4.50\\ 4.00\\ 4.00\\ \end{array}$	$\begin{array}{c} 3.90\\ 3.80\\ 3.80\\ 3.80\\ 3.80\\ 3.80\\ 3.90\\ 3.90\\ 5.90\\ 5.70\\ 4.70\\ 5.50\\ 3.60\\ \end{array}$	$\begin{array}{c} 4.\ 00\\ 4.\ 00\\ 4.\ 20\\ 4.\ 10\\ 4.\ 00\\ 4.\ 00\\ 4.\ 00\\ 4.\ 20\\ 4.\ 10\\ 4.\ 20\\ 4.\ 10\\ 4.\ 20\\ 4.\ 40\\ 4.\ 40\\ \end{array}$

NOLICHUCKY RIVER NEAR CHUCKY VALLEY, TENNESSEE.

This station was established September 6, 1900, at the highway bridge 1 mile above Chucky Valley, as an aid in the general hydrographic investigations of the southern Appalachian region made during the summer of 1900. The wire gage is suspended from the upstream side of the bridge, and is referred to a scale on the guard rail. The initial point of sounding is at the end of the lower guard rail on the left bank, downstream side. The banks are high, the current is sluggish, and the bed is sandy. The stream is straight above and below the station. The drainage area is 817 square miles. The observer is Byrd Bayless, Chucky Valley, Tennessee. During 1900 the following measurements were made by L. V. Branch and E. W. Myers:

September 5: Gage height, 2 feet; discharge, 302 second-feet. September 20: Gage height, 2.18 feet; discharge, 442 second-feet. October 15: Gage height, 2 feet; discharge, 378 second-feet. November 10: Gage height, 2.90 feet; discharge, 919 second-feet.

Daily gage height, in feet, of Nolichucky River near Chucky Valley, Tennessee, for 1900.

Day.	Sept.	Oct.	Nov.	Dec.	Day.	Sept.	Oct.	Nov.	Dec.
1	2.00 2.00 2.00 2.00 2.00 1.80 1.80 1.80 1.80 1.80 2.60 2.30 4.70	$\begin{array}{c} 1.80\\ 1.90\\ 1.90\\ 2.00\\ 3.20\\ 2.50\\ 2.30\\ 2.20\\ 2.30\\ 2.10\\ 2.10\\ 2.10\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.00 \end{array}$	$\begin{array}{c} 2.50\\ 2.60\\ 3.00\\ 5.20\\ 4.00\\ 3.50\\ 3.20\\ 2.50\\ 3.00\\ 2.90\\ 2.80\\ 2.70\\ 2.70\\ 2.70\\ 2.60\\ 2.50\\ \end{array}$	$\begin{array}{c} 3.10\\ 3.20\\ 3.00\\ 4.80\\ 3.30\\ 3.50\\ 3.40\\ 3.30\\ 3.20\\ 3.10\\ 3.00\\ 3.20\\ 3.10\\ 3.00\\ 2.90\\ 2.90\\ 2.80\\ \end{array}$	17.         18.         19.         20.         21.         22.         23.         24.         25.         26.         27.         28.         29.         30.         31.	$\begin{array}{c} 3.10\\ 2.60\\ 2.10\\ 2.00\\ 2.00\\ 2.20\\ 2.20\\ 2.10\\ 2.10\\ 2.10\\ 2.10\\ 2.10\\ 2.10\\ 2.80\\ 1.80\\ \end{array}$	$\begin{array}{c} 2,00\\ 1.90\\ 2.00\\ 1.90\\ 1.90\\ 1.90\\ 5.20\\ 3.30\\ 3.10\\ 2.90\\ 2.70\\ 2.60\\ \end{array}$	$\begin{array}{c} 2.50\\ 2.50\\ 2.40\\ 2.30\\ 2.50\\ 2.50\\ 2.50\\ 2.50\\ 2.50\\ 2.50\\ 3.40\\ 3.40\\ 3.20\\ \end{array}$	$\begin{array}{c} 2.70\\ 2.70\\ 2.60\\ 2.60\\ 2.90\\ 2.80\\ 2.90\\ 3.00\\ 3.20\\ 3.10\\ 3.00\\ 3.20\\ 3.00\\ 3.20\\ 3.20\\ \end{array}$

#### FRENCH BROAD RIVER NEAR ASHEVILLE, NORTH CAROLINA.

This station, which was established by C. C. Babb in September, 1895, is located at the Bingham School iron highway bridge, 3 miles west of Asheville, and is reached by electric car from that place. It is described in Water-Supply Paper No. 36, page 165. Records of measurements for 1899 will be found in the Twenty-first Annual Report, Part IV, page 160. During 1900 the following measurements were made by E. W. Myers, R. E. Shuford, and others:

Discharge measurements of French Broad River near Asheville, North Carolina.

Date.	Gage height.	Discharge.	Date.	Gage height.	Discharge.
1900. January 6 February 13 March 17. April 22 June 6. June 15. July 4 July 6. August 11.	$\begin{array}{c} Feet. \\ 2.52 \\ 7.95 \\ 4.20 \\ 6.80 \\ 3.30 \\ 3.60 \\ 3.675 \\ 4.05 \\ 3.10 \end{array}$	$\begin{array}{c} Secft.\\ 1,368\\ 16,967\\ 4,982\\ 13,069\\ 2,848\\ 2,258\\ 4,273\\ 3,112\\ 1,294 \end{array}$	1900.           September 6           September 13           October 13           October 23           November 20           December 14           December 30	$\begin{array}{c} Feet. \\ 3.00 \\ 2.82 \\ 3.24 \\ 3.00 \\ 8.20 \\ 3.20 \\ 3.50 \\ 3.78 \end{array}$	$\begin{array}{c} Sec.\text{-}ft.\\ 1,002\\ 710\\ 1,452\\ 997\\ 16,575\\ 1,414\\ 1,638\\ 2,135\end{array}$

Daily gage height, in feet, of French Broad River near Asheville, North Carolina, for 1900.

Dev	Ion	Fab	Man	Ann	Mor	Inno	Inhr	Aria	Sant	Oat	Nov	Dog
Day.	Jan.	reb.	mar.	Apr.	may.	June.	July.	Aug.	Bept.	Oct.	NOV.	Dec.
										-		
1	9.0*	0.00	P 40	9.40	4 50	0.07	4.05	0.05	0.00	0.05	9.50	9.00
1	2.07	2.80	6.40	-3, 40 -9, 90	4.00	0.00	4.00	0.00 0.00	- <del>0</del> , 00	2.99	3.00	- ð. 90 - e. 20
9	3.30	2.00	0.70	0.00	4. 1/	0.10	4.10	0.00	3.20	2.93	4.00	0.10
0	2.20	2.00	0.10	0.40	0.40	0.05	4.10	3.00	0.10 9.10	2.94	4.10	3.0 <del>1</del>
#	0.00	2 10	0.00	0.40	0.00	0.00	4.17	0.40	9.10	0.10	4.40	4. 50
0	0.00	0.10	9.75	0.00	0.41	0.00	4.17	0.00	9.10	0.41	4.10	4.04
0	2.47	9.50	9.10	9.15	9.17	0.00	4.20	0.00	0.10 9.05	9.10	9.05	4.00
Q	2.50	0.00	0.00 4.00	- 0, 10 - 2, 10	9.17	4.50	4.00	2.92	0.00 2.02	$\frac{0.10}{2.10}$	0.00 2.59	9.05
0	9.45	2 20	4.50	2 07	2.90	4 00	9.95	2.90	2.10	2.00	2 40	2 70
10	0 22	3.70	4.10	3.05	2.15	2.80	9.65	2 17	2.05	9.05	2.45	2.67
11	2 80	3, 10	4.10	3.20	3 10	3.70	9.67	3 15	3.00	9.85	3 47	3.55
19	4 20	3.80	3 80	3 40	3 00	3.40	2 63	3 13	9.85	3.00	3 50	3.50
18	4.95	7 05	3 60	2 20	3.00	3 45	4 80	2 95	9.80	3 13	2 47	3 47
14	3 93	7 05	3 45	3.25	2.90	3 30	4 00	3 30	3 40	3 10	3 38	3 47
15	3.80	6.55	3 37	3 00	2.85	3.20	4 03	3 17	4 65	2 90	3.35	3 49
16	4 45	5.87	3 40	3 95	2.87	7 23	3.80	3 20	5 27	2.80	3.32	3 50
17	4 10	4 95	3 50	4.30	2.85	6 10	3 70	3.35	3 90	2.85	3 30	3 47
18	3.80	4.30	3. 70	5.60	2.83	5.70	3.65	3.45	3.80	2.83	3.31	3.45
19	3.60	3.47	3.75	5.75	2.80	4.75	3.63	3.40	3.50	2.80	3.35	3.44
20	4.20	3.40	4.40	5.80	2.77	4.70	3,60	3.30	3.20	2.75	3.37	3.70
21	4.10	3.80	4.20	6.35	2.65	4.67	3.57	3.20	3.15	2.70	3,40	5.11
()4) (	4.00	4.90	4.10	7.40	2.47	4.80	3.55	3.13	3.13	3,80	3.37	4.48
23	3.80	4.70	3.70	5.10	2.30	4.93	3.65	3.15	-3.10	8.50	3,33	4.40
24	3.75	4.60	3.60	4.60	2.60	6.60	3.70	3.20	3.05	7.45	3.28	4.35
25	3.65	4.40	3.40	4.55	3.05	5.95	3.75	3.40	3.20	6.20	4.30	-4.20
26	3.45	3.50	4.30	4.43	3.10	5.80	3.87	3.35	2.70	4.80	6.45	4.12
27	3.30	3.60	4.00	4.20	3.00	5.70	4.45	3.25	2.75	4.15	5.27	3.85
28	3.20	3.80	3.85	3.90	2.80	4.65	3.85	3.20	2.80	4.00	4.70	3.80
29	2.95		3,80	3.70	2.73	4.10	3.55	3.13	2.90	3.70	4.35	3.80
30	2.90		3.60	-3.60	2.67	4.00	3.93	3.20	2.90	3.63	4.05	3.75
31	2.85		3.53		2.80		3.80	3.30		3.60		4.45

#### TENNESSEE.

#### FRENCH BROAD RIVER AT OLDTOWN, TENNESSEE.

This is one of the temporary stations established in connection with the general hydrographic study of the southern Appalachian region. Another temporary station was established on Pigeon River, a tributary of the French Broad, and many miscellaneous measurements were made on the French Broad and its tributaries, the results of which are given in Paper No. 49. The Oldtown station on the French Broad was established September 4, 1900, on the highway bridge across the river at that town, which is 2 miles north of Newport, Tennessee. The bridge is a 4-span iron structure, with wooden hand rails. The gage is securely nailed to the second span from the south end of the bridge. The 14-foot mark is the end of the rod, which is butted against the north side of the first strut from the south end of the span, on the downstream side. The outer rim of the pulley is 0.67 foot from the zero of the rod, and the distance between the end of the weight and the pointer on the wire is 25.82 feet. When the gage reads 1 foot, the water level is 20.33 feet below the top surface of the lower chord directly below the zero of the gage rod. The river is straight for a long distance above and below the bridge, and the velocity of the current is well distributed all the way across, though at the low stage at which measurement was made, some places had a velocity too small to give satisfactory results. Almost the entire distance across the bottom seems to be of fine sand. The observer is Jake Odell, Newport, Tennessee. During 1900 the following measurements were made by E. W. Myers and L. V. Branch:

September 4: Gage height, 1 foot: discharge, 867 second-feet. November 2: Gage height, 1.26 feet; discharge, 1,653 second-feet. December 15: Gage height, 1.30 feet; discharge, 1,976 second-feet. December 26: Gage height, — feet; discharge, 2,901 second-feet.

Daily gage height, in feet, of French Broad River at Oldtown, Tennessee, for 1900.

	Day.	Sept.	Oet.	Nov.	Dec.	Day.	Sept.	Oct.	Nov.	Dec.
1 2 3 4 5 5 7 8 9 10 11 13 14 15 16 10 11 13 14 15 16 10 10 11 16 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 11 13 16 16 16 16 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17		$\begin{array}{c} \hline \hline 1.00 \\ 1.00 \\ .90 \\ .90 \\ .90 \\ .80 \\ .80 \\ .80 \\ .80 \\ .80 \\ .70 \\ 1.10 \\ 1.20 \\ 2.90 \\ \end{array}$	0.80 0.80	$\begin{array}{c} 1.20\\ 1.20\\ 1.20\\ 2.20\\ 1.70\\ 1.60\\ 1.40\\ 1.30\\ 1.20\\ 1.20\\ 1.20\\ 1.20\\ 1.10\\ 1.10\\ 1.10\\ \end{array}$	$\begin{array}{c} 1.\ 60\\ 1.\ 50\\ 1.\ 40\\ 1.\ 80\\ 2.\ 80\\ 2.\ 80\\ 1.\ 80\\ 1.\ 80\\ 1.\ 60\\ 1.\ 70\\ 1.\ 60\\ 1.\ 50\\ 1.\ 40\\ 1.\ 30\\ 1.\ 30\\ 1.\ 30\\ \end{array}$	17.         18.         19.         20.         21.         22.         23.         24.         25.         26.         27.         28.         29.         23.         24.         25.         26.         27.         28.         29.         30.         31.	4.00 1.40 1.10 1.00 1.00 (a)	$\begin{array}{r} .80\\ .80\\ .80\\ .80\\ .80\\ .80\\ .220\\ 4.00\\ 3.80\\ .80\\ 3.40\\ 1.80\\ 1.50\\ 1.40\\ 1.20\\ 1.20\\ \end{array}$	$\begin{array}{c} 1.10\\ 1.10\\ 1.10\\ 1.10\\ 1.00\\ 1.00\\ 1.00\\ 1.20\\ 4.50\\ 3.00\\ 2.20\\ 1.80\\ 1.70\\ \end{array}$	1.30 1.20 1.20 1.20 2.20 2.30

a No record September 23 to October 14, inclusive.

#### 188 OPERATIONS AT RIVER STATIONS, 1900. - PART II. [NO. 48.

#### PIGEON RIVER AT NEWPORT, TENNESSEE.

This station was established September 4, 1900, on the wagon bridge at the upper end of the town of Newport, about 100 vards above the railroad bridge. The course of the river is straight for several hundred vards above and for about 50 yards below the bridge. The current at extreme low water is very sluggish. At even the lowest gage heights the water is very deep. The bottom is smooth, being of rock, in many places overlain with mud. The 15-foot mark of the rod, or the end, is abutted firmly against the east side of the first strut from the west end of the bridge, on the downstream side. The distance between the zero of the rod and the outer rim of the pulley wheel is 0.95 foot, and from the end of the weight to the pointer on the wire the distance is 32.89 feet. When the gage reading is 1 foot. the water level is 27.42 feet below the top surface of the lower chord directly beneath the zero of the gage rod. The rod is of hard pine, well painted and divided into feet and tenths. The drainage area is 655 square miles. The observer is H. M. Boyer, proprietor of a livery stable at Newport. During 1900 the following measurements were made by E. W. Myers and L. V. Branch:

September 4: Gage height, 1.00 foot: discharge, 356 second-feet. November 2: Gage height, — foot; discharge, 544 second-feet. December 15: Gage height, 1.28 feet; discharge, 691 second-feet. December 26: Gage height, 2 feet; discharge, 935 second-feet.

Daily gage height, in feet, of Pigeon River at Newport, Tennessee, for 1900.

Day.	Sept.	Nov.	Dec.	Day.	Sept.	Nov.	Dec.	Day.	Sept.	Nov.	Dec.
1 2 3 4 5 6 7 8 9 10.			$\begin{array}{c} 1.40\\ 1.50\\ 2.60\\ 3.20\\ 2.30\\ 2.10\\ 1.90\\ 1.70\\ 1.50\\ 1.50\\ \end{array}$	12 13 14 15 16 17 18 19 20 21	0. 60 . 50 1. 20 1. 60 ( <i>a</i> )	1.00 1.00	$\begin{array}{c} 1.30\\ 1.20\\ 1.40\\ 1.30\\ 1.40\\ 1.30\\ 1.30\\ 1.40\\ 1.40\\ 1.40\\ 2.40\end{array}$	23 24 25 26 27 28 28 27 28 29 30 31		$1.10 \\ 1.10 \\ 1.30 \\ 3.90 \\ 1.90 \\ 1.80 \\ 1.50 \\ 1.40$	$\begin{array}{c} 2.40\\ 2.60\\ 2.10\\ 2.00\\ 2.00\\ 2.00\\ 2.00\\ 2.10\\ 2.50\\ 2.90\end{array}$
11	60		1.30	33 77		1.00	2.00				

a No record September 16 to November 18, inclusive.

#### TUCKASEGEE RIVER AT BRYSON, NORTH CAROLINA.

This station is described in Water-Supply Paper No. 36, page 167. Results of measurements during 1899 will be found in the Twenty-First Annual Report, Part IV, page 162. During 1900 the following measurements were made by E. W. Myers and R. E. Shuford:

#### NORTH CAROLINA.

Discharge measurements of Tuckasegee River at Bryson, North Carolina.

Date.	Gage height.	Discharge.	Date.	Gage height.	Discharge.
1900. February 9 March 29 April 27 May 24 June 27 Juny 7 August 3	$\begin{matrix} Feet. \\ 2.95 \\ 2.50 \\ 2.65 \\ 1.80 \\ 2.60 \\ 2.00 \\ 1.60 \end{matrix}$	Secfeet. 3,316 2,321 2,829 1,390 2,673 1,472 920	1900. September 8 October 27 November 16 December 12 Do Do December 26	$\begin{array}{c} Feet. \\ 1.20 \\ 1.60 \\ 1.20 \\ 1.50 \\ 1.50 \\ 1.60 \end{array}$	Secfeet, 598 942 593 998 903 960

Daily gage height, in feet, of Tuckasegee River at Bryson, North Carolina, for 1900.

_													
	Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1		1.50	2.75	2.60	2.15	2.30	1.50	2.50	1.60	1.40	1.20	1.35	1.50
020		1.50	2.75	2.55	2.15	2.20	1.60 1.60	2.40	1.60 1.50	1.50 1.40	1.20	1.35	1.40
- 0 - 4		1.50 1.50	1.60	2.60	2.30	2.10	1.70	2.20	1.50	$1.40 \\ 1.30$	1.20 1.25	1 70	2.50
5		1.50	1.80	2.80	2.25	2.10	2.10	2.20	$\hat{1}.50$	1.30	1.25	1.50	2.20
6	5	1.50	1.65	3.30	2.25	2.10	2.00	2.10	1.50	1.30	1.20	1.50	2.00
7	( <b></b>	1.50	1.60	3.50	2.20	2.00	1.90	2.00	1.40	1.20	1.20	1.40	1.80
- 7		1.60	2.00	3.90	2.15	2.00	2 10	2.00	1.40 1.40	1.20	1.20	1.40 1.30	1.70
10		2.80	2.50	3.85	2.20	2.00	2.00	1.80	1.40	1.20	1.15	1.30	1.60
11		3.10	2.00	3.75	2.40	1.90	1.90	2.00	1.40	1.20	1.15	1.30	1.60
12		2.70	4.00	3.60	2.40	1.80	1.90	1.90	1.40	1.15	1.20	1.30	1.55
$13 \\ 14$		2.90	8.00	3.50	2.70	1.80	1.90 1.00	2.00	1.50	1.15	1.35	1.30 1.20	1.50
14		2.50	4.00	2.40	2.10	1.80	1.90 1.80	2.00	1.50	2.90	1.20 1.20	1.30	1.00
$16^{10}$		2.50	4.15	2.35	2.20	1.70	3.00	1.90	1.40	2.10	1.20	1.30	1.40
17		2.50	4.00	3.00	2.20	1.70	3.60	1.90	1.40	1.70	1.15	1 25	1.40
18		2.40	3.85	3.50	3.50	1.70	3.40	1.90	1.25	1.50	1.10	1.20	1.40
19		2.30	3.70	2.65	3.00	1.70	3.00	1.80	1.30	1.40 1.40	1.10	1.20	1.40
21		2.30	3.40	2.85	3.90	1.60	2.20	2.00	1.30 1.30	1.40	1.10 1.10	$1.10 \\ 1.35$	$\frac{1.80}{2.30}$
22		2.80	3.20	2.60	2.80	1.60	3.40	2.10	1.90	1.35	1.20	1.30	1.70
23	3	2.80	3.00	6.45	3.30	1.60	3.50	2.00	1.50	1.50	5.20	1.25	2.30
24		2.80	3.00	2.50	2.50	1.85	4.30	1.80	1.50	1.35	2.20	1.20	2.00
20		2.60	3,00	3.00	2.60	1.90	3.00	1.60	1.30	1.30 1.20	1.80	3.10	1.80
$\frac{20}{27}$		2.50	2.80	2.55	2.60	1.60	2.70	2.50	1.50	1.25	1.40	2.10	1.60
28	3	2.40	2.80	2.40	2.50	1.60	2.50	2.40	1.40	1.25	1.40	1.80	1.70
29		2.40		2.35	2.30	1.60	3.50	2.20	1.40	1.20	1.40	1.70	1.60
30	)	2.40		2.35	2.50	1.50	3.00	2.00	1.40	1.20	1.40	1.60	1.80
31	••••••	2.40		2.20		1.40		1,60	1.50	•••••	1.35		2.50

LITTLE TENNESSEE RIVER AT JUDSON, NORTH CAROLINA.

This station is described in Water-Supply Paper No. 36, page 168. Records of measurements for 1899 will be found in the Twenty-first Annual Report, Part IV, page 163. During 1900 the following measurements were made by E. W. Myers and R. A. Shuford:

February 10: Gage height, 4.55 feet: discharge, 3,726 second-feet. March 30: Gage height, 4.40 feet: discharge, 3,179 second-feet. April 28: Gage height, 4.55 feet; discharge, 3,785 second-feet. May 25: Gage height, 3.50 feet; discharge, 1,744 second-feet. June 28: Gage height, 5 feet; discharge, 4,644 second-feet. August 4: Gage height, 3.45 feet; discharge, 1,668 second-feet. November 17: Gage height, 2.88 feet; discharge, 1,008 second-feet. December 27: Gage height, 3.40 feet; discharge, 1,414 second-feet.

Daily	gage	height,	in	feet, of	Little	Tennessee	River	at	Judson,	North	Carolina,
						for 1900.					

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
Day. 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 14 15 16 17 18 19 20 21 22 24 24 25 24 25 24 25 24 25 26 27 27 27 27 27 27 27 27 27 27	Jan. 2366 332 2338 32 2338 22 2338 22 23 2338 22 23 23 23 23 23 23 23 23 23 23 23 23 2	Feb. 2655 2.70 2.667 2.672 2.672 2.672 2.672 2.673 2.673 2.673 2.673 2.673 2.3,72 2.673 2.673 2.3,478 3.3,333 11,358 4.583 3.3,441 3.488 3.558 3.558 3.566 3.663 3.663	$\begin{array}{c} \textbf{Mar.} \\ \hline \\ 6.33 \\ 4.42 \\ 3.78 \\ 3.70 \\ 3.84 \\ 3.93 \\ 6.40 \\ 4.30 \\ 4.430 \\ 4.58 \\ 4.58 \\ 3.98 \\ 3.98 \\ 3.98 \\ 3.98 \\ 3.98 \\ 3.98 \\ 3.99 \\ 3.99 \\ 3.99 \\ 3.99 \\ 3.99 \\ 3.99 \\ 3.99 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3$	$\begin{array}{c} {\rm Apr.} \\ \hline \\ 3.68 \\ 3.67 \\ 3.41 \\ 3.33 \\ 3.33 \\ 3.33 \\ 3.33 \\ 2.91 \\ 2.88 \\ 2.74 \\ 2.79 \\ 5.45 \\ 5.92 \\ 4.38 \\ 3.58 \\ 3.99 \\ 3.58 \\ 3.59 \\ 3.58 \\ 3.90 \\ 3.54 \\ 3.59 \\ 3.54 \\ 3.48 \\ 3.48 \\ 3.48 \\ 3.48 \\ 3.48 \\ 3.49 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9 \\ 3.9$	May. 2.93 2.93 2.84 2.70 2.68 2.69 2.68 2.68 2.68 2.68 2.68 2.53 2.53 2.58 2.59 2.71 2.70 2.68 2.67 2.53 2.58 2.67 2.53 2.54 2.90 3.35 4.42 2.90 2.90 2.93 2.93 2.93 2.93 2.93 2.93 2.93 2.93	June. 3.400 4.000 3.522 3.766 3.523 3.622 3.623 3.623 3.623 3.623 3.623 3.623 3.623 3.623 3.623 3.623 3.623 3.882 3.882 3.889 3.889 3.844 4.600 3.882 3.889 3.889 3.844 4.623 4.623 4.623 4.623 4.623 4.623 4.623 4.623 4.623 4.623 4.623 4.623 4.623 4.623 5.843 3.843 3.843 3.843 3.843 3.843 3.843 3.843 3.843 3.843 3.843 3.845 3.845 3.845 3.845 3.845 3.845 3.845 3.845 3.845 3.845 3.845 3.845 3.845 3.845 3.845 3.845 3.845 3.845 3.845 3.845 3.845 3.845 3.845 3.845 3.845 3.845 3.845 3.845 3.845 3.845 3.845 3.845 3.845 3.845 3.845 3.845 3.845 3.845 3.845 3.845 3.845 3.845 3.845 3.845 3.845 3.845 3.845 3.844 4.935 5.400 5.400 5.400 5.400 5.400 5.400 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2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 2.69 \\ 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\\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ 3.30 \\ $	$\begin{array}{c} 3.61 \\ 4.81 \\ 4.00 \\ 3.01 \\ 3.51 \\ 3.51 \end{array}$	$\begin{array}{c c} 3.\ 68\\ 3.\ 65\\ 3.\ 65\\ 3.\ 65\\ 3.\ 92\\ 3.\ 48\\ 3.\ 43\end{array}$

HIWASSEE RIVER AT MURPHY, NORTH CAROLINA.

This station is described in Water-Supply Paper No. 36, page 169. The observer is William Mingus, of Murphy. Records of measurements during 1899 will be found in the Twenty-first Annual Report, Part IV, page 165. During 1900 the following measurements were made by É. W. Myers and R. E. Shuford:

Discharge measurements of Hiwassee River at Murphy, North Carolina.

Date.	Gage height.	Discharge.	Date.	Gage height.	Discharge.
1900. February 11 February 14 April 29 May 26 June 29 July 8	$\begin{array}{c} Feet. \\ 6.10 \\ 7.95 \\ 6.10 \\ 5.52 \\ 7.10 \\ 5.90 \end{array}$	$\begin{array}{c} Sec. \textit{-ft}. \\ 1, 534 \\ 4, 567 \\ 1, 466 \\ 755 \\ 3, 405 \\ 1, 155 \end{array}$	1900. September 9 November 18 December 13 December 13 December 33	$\begin{array}{c} Feet, \\ 5.05 \\ 5.20 \\ 5.53 \\ 5.45 \\ 5.70 \end{array}$	Secft. 345 443 762 698 865

#### NORTH CAROLINA AND TENNESSEE.

Daily gage height, in feet, of Hiwassee River at Murphy, North Carolina, for 1900.

	Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1		5.50	5.12	7.00	5.90	6.10	5.40	6.80	5.80	5.35	5.00	5.20	5.40
49		5.20 5.51	5.30 5.35	6.50 6.25	5.90 5.90	6.00	5.40 5.60	6.60	5.40 5.40	5.20 5.15	4.90 5.00	5.25	5.40
4		5.30	5.40	6.10	6.70	5.90	5.80	6.40	5.40	5.10	5.10	5.60	7.20
5		5.30	5.60	6.00	6.10	5.90	5.50	6.20	5.30	5.20	5.10	5.40	6.40
-0		5.20	<b>5</b> 40	5.00 7.00	6.00	5.80	6.10	5.00	0.30 5.30	- 0, 10 - 5, 10	- 0, 00 5, 00	0.00 5.35	5.80
ŝ	}	5.20	5.40	7.50	5.90	5.70	6.10	5.80	5.20	5.05	5.30	5.30	5.75
į	)	5,20	6.72	7.40	5.85	5.70	6.10	6.20	5.20	5.05	5.10	5.25	5.60
10	)	5.20	6.02	6.90	5.80	5.70	6.30	5.70	5.20	5.00	5.05	5.25	5.60
11		5.30	6.10	6.60	6.10	5.70	6.10	5.70	5.20	5.00	5.00	5.20	5.50
$\frac{12}{13}$		5.80	12,60	6.30	6.10	5.60	6 60	5.80	5.20	5.00	4.00	5.20	5 45
14		5.60	7.70	6.12	6.00	5.60	6.10	5.70	5.20	5.05	5.10	5.25	5.45
15		5.60	7.15	6.05	6.00	5.60	5.80	5.60	5.20	7.00	5.00	5.20	5.40
16		5.50	6.50	6.30	5.90	5.50	5.80	5.60	5.10	6.45	5.00	5.15	5.40
$\frac{17}{16}$		5.40 5.45	6.20	6.00	5.80	5.40	6.20	5.60	5.30 5.20	0.70 5.45	4.90	5.20 5.15	5.40
$\frac{10}{19}$		5.90	5.90	6.85	6.70	5.70	6.30	5.50	5.10	5.35	5.00	5.20	5.30
$\hat{20}$	)	6.60	5.80	7.40	6.40	5.50	6.10	5.50	5.10	5.35	4.90	5.15	5.80
21		6.20	6.00	6.90	7.10	5.40	5.90	5.50	5.10	5.25	4.90	5.20	6.70
22		5.90	6.40	6.60	6.80	5.40	5.80	5.60	5.10	5.00	5.00	5.30	5.90
20		5.65	6.00	6 35	6.50	5 60	6.60	5.60	5.90	5.20	4.90	5 15	0.80
$\tilde{25}$		5.60	6.00	6.40	6.55	5.50	6,50	5.40	5.30	5.20	6.00	5.30	5.80
20		5.60	6.00	6.40	6.55	5.60	7.00	5.50	5.40	5.20	5.70	6.70	5.70
27		5.50	5.90	6.30	6.30	5.50	7.20	5.70	5.20	5.15	5.60	6.00	5.65
28		5.40 5.40	5.85	6.30	6.20	5.40	7.10	<b>5.90</b>	5.15	5.15	5.40 5.20	5.70	5.60
20		5.40		6.10	6.10	5.40	6.80	5.80	5.15	5.05	5 20	5.50	0.10
31		5.50		6.00		5.40		5.60	5.15		5.25		
_												1	

#### HIWASSEE RIVER AT RELIANCE, TENNESSEE.

This station was established by O. P. Hall on August 17, 1900. The gage is a vertical timber, graduated to feet and tenths, spiked to a tree on the right bank of the river about 200 feet above the Atlanta, Knoxville and Northern Railroad bridge, and very near the ferry landing. Measurements are made from the railroad bridge, a new steel structure of three spans of 140 feet each, which has recently been substituted for the old wooden bridge. Bench mark No. 1 is a nail in a hickory tree on the right bank of the river, about 100 feet above the end of the bridge and 8.56 feet above the zero of the gage. Bench mark No. 2 is the base of rail 40 feet from the right-bank end of bridge, and is 24.70 feet above the zero of the gage. At ordinary stages the river is about 350 feet wide at this point, and the section is a fairly good one, but at low stages the current becomes very sluggish. The observer is C. V. Higdon, a ferryman who lives near the gage. During 1900 the following measurements were made by O. P. Hall:

August 17: Gage height, 1.12 feet; discharge, 1.123 second-feet. September 3: Gage height, 1.16 feet; discharge, 1.159 second-feet. November 30: Gage height, 1.72 feet; discharge, 1.985 second-feet. December 19: Gage height, 1.42 feet; discharge, 1.442 second-feet. 191

Daily gage height, in feet, of Hiwassee River at Reliance, Tennessee, for 1900.

Day.	Aug.	Sept.	Oct.	Nov.	Dec.	Day.	Aug.	Sept.	Oct.	Nov.	Dec.
1		$\begin{array}{c} 1.40\\ 1.30\\ 1.20\\ 1.05\\ 1.00\\ 1.10\\ 1.05\\ 1.00\\ 1.00\\ 1.00\\ .90\end{array}$	$\begin{array}{c} 1.05\\ 1.00\\ 1.00\\ 1.00\\ 1.00\\ 1.00\\ 1.00\\ 1.00\\ 1.30\\ 1.50\\ 1.20\end{array}$	$\begin{array}{c} 1.30\\ 1.20\\ 1.80\\ 1.30\\ 1.40\\ 1.50\\ 1.40\\ 1.40\\ 1.30\\ 1.30\\ 1.30\\ 1.30\\ \end{array}$	$\begin{array}{c} 1.60\\ 1.50\\ 1.50\\ 2.80\\ 3.00\\ 2.40\\ 2.00\\ 2.00\\ 1.90\\ 1.80\\ 1.80\\ \end{array}$	17           18           19           20           21           22           23           24           25           26	$ \begin{array}{c} 1.10\\ 1.05\\ 1.05\\ 1.05\\ 1.10\\ 1.50\\ 1.40\\ 1.30\\ \end{array} $	$\begin{array}{c} 2.\ 00\\ 1.\ 60\\ 1.\ 40\\ 1.\ 30\\ 1.\ 20\\ 1.\ 20\\ 1.\ 30\\ 1.\ 30\\ 1.\ 20\\ 1.\ 10\\ \end{array}$	$ \begin{array}{c} 1.00\\ 1.00\\ .90\\ .90\\ 1.90\\ 1.00\\ 1.30\\ 4.00\\ 2.00\\ 1.50\\ \end{array} $	$\begin{array}{r} 1.20\\ 1.10\\ 1.20\\ 1.30\\ 1.40\\ 1.30\\ 1.50\\ 1.70\\ 4.50\\ \end{array}$	$1.50 \\ 1.50 \\ 1.40 \\ 1.50 \\ 2.80 \\ 2.80 \\ 2.10 \\ 2.40 \\ 2.30 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ $
11 12 13 13 14 15 16	·····	$ \begin{array}{c} .90\\.90\\.90\\1.00\\3.60\\3.50\end{array} $	$\begin{array}{c} 1.\ 10\\ 1.\ 10\\ 1.\ 20\\ 1.\ 40\\ 1.\ 10\\ 1.\ 00 \end{array}$	$ \begin{array}{c} 1.40\\ 1.30\\ 1.30\\ 1.30\\ 1.20\\ 1.20\\ \end{array} $	$\begin{array}{c} 1.\ 70\\ 1.\ 60\\ 1.\ 60\\ 1.\ 60\\ 1.\ 50\\ 1.\ 50\\ 1.\ 50\\ \end{array}$	27 28 29 30 31	$\begin{array}{c} 1.30 \\ 1.15 \\ 1.10 \\ 1.10 \\ 1.10 \\ 1.10 \\ \end{array}$	$     \begin{array}{r}       1.10 \\       1.05 \\       1.05 \\       1.05 \\       \hline       1.05       \end{array} $	$     \begin{array}{r}       1.60 \\       1.50 \\       1.50 \\       1.40 \\       1.30     \end{array} $	3. 60 2. 00 1. 80 1. 70	$ \begin{array}{c} 1.90 \\ 1.90 \\ 2.00 \\ 1.90 \\ 2.40 \end{array} $

HIWASSEE RIVER AT CHARLESTON, TENNESSEE.

This station was originally established by the United States Engineer Corps, but is now maintained as a half-year station by the United States Weather Bureau. It is described in Water-Supply Paper No. 36, pages 170 and 171, where will also be found the records of measurements made during 1899. During 1900 the following measurements were made by Max Hall:

March 14: Gage height, 3.50 feet; discharge, 6,044 second-feet. April 25: Gage height, 4 feet; discharge, 7,078 second-feet. December 8: Gage height, 2.65 feet; discharge, 4,729 second-feet.

Daily gage height, in feet, of Hiwassee River at Charleston, Tennessee, for 1900.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oet.	Nov.	Dec.
$\begin{array}{c} 1 \\ 2 \\ 3 \\ 3 \\ 4 \\ 5 \\ 5 \\ 6 \\ 7 \\ 7 \\ 7 \\ 7 \\ 8 \\ 9 \\ 9 \\ 10 \\ 11 \\ 12 \\ 13 \\ 14 \\ 14 \\ 15 \\ 16 \\ 17 \\ 18 \\ 17 \\ 18 \\ 20 \\ 21 \\ 22 \\ 23 \\ 24 \\ 24 \\ 24 \\ 24 \\ 24 \\ 24$	$\begin{array}{c} 1.0\\ 1.0\\ .9\\ .9\\ 1.1\\ 1.1\\ 1.1\\ 1.1\\ 1.4\\ 4.6\\ 0.2.4\\ 2.0\\ 1.8\\ 7\\ 2.4\\ 5.4\\ 3.7\\ 2.5\\ \end{array}$	$\begin{array}{c} 1.2\\ 1.0\\ 1.8\\ 2.3\\ 1.6\\ 1.8\\ 2.2\\ 1.6\\ 1.2\\ 9\\ 4.2\\ 2\\ 3.1\\ 1.4\\ 2.6\\ 3.1\\ 1.4\\ 2.5\\ 1.6\\ 3.0\\ 2.8\\ 7\\ 5.0\\ 1.6\\ 5.7\\ 1.6\\ 1.6\\ 1.6\\ 1.6\\ 1.6\\ 1.6\\ 1.6\\ 1.6$	$\begin{array}{c} 3.7 \\ 5.85 \\ 4.57 \\ 3.29 \\ 4.50 \\ 9.450 \\ 4.80 \\ 4.407 \\ 3.49 \\ 4.13 \\ 3.49 \\ 4.14 \\ 3.43 \\ 7.50 \\ 6.00 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5.50 \\ 5$	$\begin{array}{c} 3.1\\ 2.9\\ 4.6\\ 6.0\\ 3.4\\ 3.29\\ 3.0\\ 2.9\\ 0\\ 4.6\\ 3.3\\ 0\\ 2.3\\ 0\\ 3.5\\ 1.2\\ 5.5\\ 4.6\\ 5.5\\ 4.6\\ 5.5\\ 4.6\end{array}$	$\begin{array}{c} 3.1\\ 2.9\\ 0\\ 2.265\\ 2.25\\ 2.25\\ 2.25\\ 2.25\\ 2.25\\ 2.25\\ 2.20\\ 1.9\\ 9\\ 1.79\\ 1.8\\ 7\\ 1.79\\ 1.67\\ 1.67\\ \end{array}$	$\begin{array}{c} 1.560\\ 2.221\\ 3.450\\ 4.533\\ 4.522\\ 2.334\\ 4.533\\ 4.772\\ 8.84\\ 3.33\\ 4.432\\ 4.4366\\ 6.736\\ 2.22\\ 4.2\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 2.24\\ 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77 77 6 6 6 6 3.0 5 1.1 2 2 1.1 2 9.9 8 8 77 77 76 6 6 6 6 8 1.1 2 2 9 9 8 8 77 77 76 6 6 6 8 9 9 8 8 77 77 76 6 6 8 8 9 8 8 8 77 77 76 6 6 8 8 8 8 8 8 8 9 8 8 8 9 8 8 8 77 77 76 6 6 8 8 8 8 8 8 8 8 8 8	$\begin{array}{c} 0.77\\ .77\\ .77\\ .77\\ .82\\ 2.00\\ 1.30\\ 1.0\\ 1.11\\ 1.4\\ 1.20\\ .99\\ .87\\ .77\\ .77\\ .73\\ .90\end{array}$	$1.227 \\ 1.2732.4864 \\ 1.43227.1.00 \\ 1.44322.1.11 \\ 1.111 \\ 1.001.123 \\ 1.331.1.11 \\ 1.101.1.00 \\ 1.1234 \\ 1.421 \\ 1.421 \\ 1.421 \\ 1.421 \\ 1.421 \\ 1.421 \\ 1.421 \\ 1.421 \\ 1.421 \\ 1.421 \\ 1.421 \\ 1.421 \\ 1.421 \\ 1.421 \\ 1.421 \\ 1.421 \\ 1.421 \\ 1.421 \\ 1.421 \\ 1.421 \\ 1.421 \\ 1.421 \\ 1.421 \\ 1.421 \\ 1.421 \\ 1.421 \\ 1.421 \\ 1.421 \\ 1.421 \\ 1.421 \\ 1.421 \\ 1.421 \\ 1.421 \\ 1.421 \\ 1.421 \\ 1.421 \\ 1.421 \\ 1.421 \\ 1.421 \\ 1.421 \\ 1.421 \\ 1.421 \\ 1.421 \\ 1.421 \\ 1.421 \\ 1.421 \\ 1.421 \\ 1.421 \\ 1.421 \\ 1.421 \\ 1.421 \\ 1.421 \\ 1.421 \\ 1.421 \\ 1.421 \\ 1.421 \\ 1.421 \\ 1.421 \\ 1.421 \\ 1.421 \\ 1.421 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25 26 27 28 29 30 31	2.3 2.1 1.9 1.8 1.7 1.5 1.4	$ \begin{array}{r} 4.2 \\ 3.8 \\ 3.3 \\ 12.9 \\ \hline \end{array} $	$\begin{array}{r} 4.0 \\ 6.0 \\ 5.2 \\ 4.4 \\ 3.9 \\ 3.6 \\ 3.3 \end{array}$	$\begin{array}{r} 4.3 \\ 4.0 \\ 3.9 \\ 3.7 \\ 3.5 \\ 3.3 \end{array}$	2.0 2.0 2.1 1.7 1.6 1.5 1.5	$     \begin{array}{r}       4.8 \\       5.0 \\       5.3 \\       5.9 \\       5.7 \\       8.0 \\     \end{array} $	$     \begin{array}{r}       1.8 \\       1.6 \\       2.7 \\       3.8 \\       3.7 \\       2.7 \\       2.4 \\       \end{array} $	$2.4 \\ 1.5 \\ 1.4 \\ 1.5 \\ 1.2 \\ 1.2 \\ 1.0$	$ \begin{array}{c} 1.1 \\ 1.0 \\ .9 \\ .9 \\ .9 \\ .8 \\ \end{array} $	3.8 2.3 1.8 1.7 1.5 1.4 1.3	$   \begin{array}{r}     1.3 \\     10.0 \\     7.0 \\     4.0 \\     2.9 \\     2.3   \end{array} $	3.6 2.9 2.6 2.4 2.6 2.6 3.9

#### TOCCOA RIVER NEAR BLUERIDGE, GEORGIA.

This station, which was established by B. M. Hall November 25, 1898, is at the Morganton bridge, about 4 miles east of the town of Blueridge. It is described in Water-Supply Paper No. 36, page 171. Records of measurements for 1899 will be found in the Twenty-first Annual Report, Part IV, page 166. During 1900 the following measurements were made by B. M. Hall and his assistants.

March 23: Gage height, 3.36 feet; discharge, 967 second-feet. May 18: Gage height, 2.90 feet; discharge, 679 second-feet. November 28: Gage height, 2.95 feet; discharge, 626 second-feet. July 19: Gage height, 2.90 feet; discharge, 680 second-feet. December 17: Gage height, 2.65 feet; discharge, 419 second-feet.

Daily gage height, in feet, of Toccoa River near Blueridge, Georgia, for 1900.

Day.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
Day.	Mar.	$\begin{array}{c} \text{Apr.}\\ \hline \\ 3.1\\ 3.1\\ 3.0\\ 3.0\\ 3.0\\ 3.0\\ 3.0\\ 3.0\\ 3.0\\ 3.0$	May. 3.6 3.5 3.5 3.5 3.5 3.5 3.5 3.5 3.5	June.	July. 4 3 4 3 4 2 4 1 3 6 3 5 3 5 3 5 3 4 4 3 3 4 3 6 3 5 3 5 3 5 3 5 3 5 3 5 3 5 3 5	Aug. 3.6 3.5 4 3.4 4 3.4 4 3.4 4 3.4 4 3.3 3.3 3.3 3	Sept. 2.6 2.6 2.6 2.6 2.6 2.6 2.6 2.6 2.6 2.	Oct. 2552256 22552256 2266226 2266226 2266226 2266226 2268229 22882229 22882226 2266226 2266226 2266226 2266226 22666226 2266226 2266226 2266226 2266226 226526 226526 226526 226526 226526 226526 226526 226526 226526 226526 226526 226526 226526 226526 226526 226526 226526 226526 226526 226526 226526 226526 226526 226526 226526 226526 226526 226526 226526 226526 226526 226526 226526 226526 226526 226526 226526 226526 226526 226526 226526 226526 226526 226526 226526 226526 226526 226526 226526 226526 226526 22666226 226526 226526 22666226 226526 22666226 226526 22666226 22666226 22666226 22666226 22666226 22666226 22666226 22666226 22666226 22666226 22666226 22666226 22666226 22666226 22666226 22666226 22666226 22666226 22666226 22666226 22666226 22666226 22666226 22666226 22666226 22666226 22666226 22666226 22666226 22666226 22666226 22666226 22666226 22666226 22666226 22666226 22666226 22666226 2266626 2266626 2266626 226666226 226666226 226666226 226666226 226666226 226666626 226666626 22666666	Nov. 3.4 3.4 3.4 3.4 3.4 3.3 3.2 3.1 3.1 3.1 3.1 3.0 3.0 3.0 3.0	Dec. 2.6 3.0 3.6 3.5 5.5 3.5 3.4 3.3 3.3 3.3 3.2 3.2 3.0 2.8 2.8 2.8 2.8 2.8 2.8 2.8 2.8
20 22 22 23 24 25 25 26 27 27 28 29 29 29 30 31 31	33.55 G 15 15 15 15 15 15 15 15 15 15 15 15 15	6 : ::::::::::::::::::::::::::::::::::		5.0 5.0 4.5 4.3	$\begin{array}{c} 3.2 \\ 3.1 \\ 1.6 \\ 3.3.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 4.0 \\ 3.5.5 \\ 4.0 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3.5.5 \\ 3$	4.000008887+7-0 2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.	00088000000000000000000000000000000000	$\begin{array}{c} 2.69\\ 2.69\\ 8.60\\ 5.4\\ 3.66\\ 3.66\\ 3.66\\ 3.5\\ 3.\\ 3.\\ 3.\\ 3.\\ 3.\\ \end{array}$	00087777766666 33222222222222222222222222222	2:47 2:66 2:66 2:66 2:60 2:60 3:00 3:00 3:00 3:8 2:8

a No record May 20 to June 26, inclusive.

#### TENNESSEE RIVER AT KNOXVILLE, TENNESSEE.

This station was originally established by the United States Weather Bureau at the old county highway bridge, which has been torn down and replaced by a new bridge. Instead of placing the gage at the new bridge, it was decided to move it down the river, in order to get below some shoals and wing dams which have been put in for boating. A temporary gage was put in at the Knoxville and Augusta Railroad bridge, a half mile below the highway bridge, and was used during the greater part of the year 1899. In the latter part of that year a new permanent gage was established, and readings from it began November 1, 1899. The new gage is located on the right bank of the river, just below the mouth of the West Knoxville Bayou and about 1,000 feet below the temporary gage at the Knoxville and Augusta Railroad bridge. The gage, which is graduated to feet and tenths, is in two sections; the first, a sloping section made of a 2-inch by 4-inch pine timber spiked on top of an 8-inch by 8-inch oak sill well bolted to piles and embedded in crushed stone, reading from -2 feet to 12 feet; the second, a vertical section of standard Weather Bureau pattern, brass scale, screwed to one of the bents of the railroad trestle across the West Knoxville Bayou, about 50 feet from the bank of the river and from the sloping gage, reading from 12 feet to 36.5 feet. The gage is fastened to the upstream post of the bent facing away from the river. The zero of the gage is 804.3 feet above sea level. The bench mark is a cross in the stone on the east corner of the base to the rightbank pier of the Knoxville and Augusta Railroad bridge, and is 806.7 feet above sea level and 2.4 feet above the zero of the gage. The gage was located for the United States Weather Bureau by the United States Engineer Corps. Daily records are kept by the United States Weather Bureau and are furnished to the Geological Survey. Measurements are made at the Cherokee highway bridge 2 miles below the new gage. This bridge is a three-span iron structure and is about 80 feet above low water. The width of the river at low water is 550 feet. The section is a good one, but the current is rather sluggish at low During 1900 the following measurements were made by Max water. Hall:

April 25: Gage height, 4.35 feet; discharge, 17,219 second-feet. December 7: Gage height, 5.50 feet; discharge, 23,529 second-feet.

Daily gage height	, in feet, a	of Tennessee	River at Knox	ville, Tennessee,	for 1900.
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Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
				-	Ű		v	U				
		0.0	0.0	1.0								
1	0.7	$0.\frac{8}{7}$	3.9	4.2	2.7	1.2	3.8	2.7	1.2	0.6	1.1	3.0
3			11.1	3.5	2.4	11	2.8	14	1.0	.4	$1.0 \\ 1.1$	2.2
4	.2	1.0	9.1	3.4	2.4	1.1	2.8	1.2	.7	.ŝ	$\hat{1}.\hat{5}$	2.6
5	. 8	1.3	6.1	4.5	2.4	1.5	2.7	1.2	.5	.2	3.6	4.1
<u>6</u> • · · · · · · · · · · · · · · · · · ·	.8	1.6	5.0	4.1	2.3	2.4	2.5	1.1	.4	. 2	3.5	6.6
8	.9	1.9	4.0	0.0 3.2	2.2	2.0	2.0	1.0	.0	. (	$\frac{3.9}{2.1}$	0.9
9	1.0	3.0	9.5	3.0	2.0	2.2	1.7	.8	.3	.7	1.8	3.5
10	. 9	4.1	10.1	2.8	2.0	2.2	1.6	.7	.2	.7	1.5	3.0
11	1.1	4.2	7.9	2.7	2.1	1.9	1.4	. 6	.2	. 5	$\frac{1.3}{1.9}$	-2.7
13	4.6	6.9	0.4 5.5	2.8	21	1.0	1.0	6. 9	.1	. * 3	1.%	2.0
14	4.7	12.4	4.7	$\tilde{2.9}$	1.9	2.0	1.3	.6	.3	.2	1.0	1.9
15	4.3	12.7	4.2	2.7	1.8	2.0	1.4	.8	. 6	.2	-1.0	1.8
16	2.9	8.9	$\frac{4.0}{4.6}$	2.5	1.7	2.2	$\frac{1.3}{1.2}$	1.4	1.1	.3	. 9	1.7
18	2.0	5.6	4.0	4.0	1.0	4.0	$1.0 \\ 1.2$	1.0	0.0 3.6		.0	1.0
19	2.0	4.0	4.5	3.2	1.4	6.5	$\tilde{1}.\tilde{1}$	.7	2.2	.2	.8	$\hat{1}.\hat{3}$
20	2.6	3.3	6.0	4.7	1.4	5.1	1.0	. 6	1.4	.1	.7	1.3
21	3.1	2.9	11.9 12.9	$\frac{4.6}{5.7}$	1.4	$\frac{4.3}{2.2}$	.9	. 5	1.0	· 1	.8	1.3
23	$\frac{0.1}{2.9}$	3.2	9.4	6.4	1.4	0.0 2.7	$1.0 \\ 1.2$	.4	1.0		.0	2.5
24	2.5	5.0	6.7	$5.\hat{5}$	1.3	3.3	1.5	1.4	1.0	4.9	.8	2.5
25	2.0	5.0	5.5	4.7	1.3	3.6	1.5	1.5	1.0	9.4		2.3
26	2.1	4.9	5.7	$\frac{4.0}{2.0}$	1.8	4.4	$\frac{1.7}{5.6}$	$1.2 \\ 1.1$	1.0	5.8	5.6	2.2
28	1.8	4.8	6.9	3.6	1.8	4.2	5.0 6.0	1.1	1.0	4.0	9.0	1.9
29	1.5		5.8	3.2	1.5	3.4	4.8	. 9	.8	1.8	5.0	1.7
30	1.4		5.0	2.9	1.3	5.8	4.0	. 7	.7	1.4	3.6	1.7
31	1.1		4.5		1.2		3.5	. 9		1.3		1.8

#### TENNESSEE.

#### TENNESSEE RIVER AT CHATTANOOGA, TENNESSEE.

This station was established in 1879, at the foot of Lookout street, just below Chattanooga Island, by the Signal Corps of the United States Army; but since July 1, 1891, it has been in charge of the Weather Bureau. During the year 1900 a new gage was established. It is a vertical timber bolted to the south side of the third stone pier from the south end of the bridge. Gage heights are obtained from L. M. Prindell, United States Weather Bureau observer. Records of measurements made during 1899 will be found in the Twenty-first Annual Report, Part IV, page 168. During 1900 the following measurements were made by Max Hall and others:

March 13: Gage height, 11.25 feet; discharge, 66,012 second-feet. July 27: Gage height, 3.45 feet; discharge, 18,470 second-feet.

Daily gage height, in feet, of Tennessee River at Chattanooga, Tennessee, for 1900.

						~~~~~							
	Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1		3.05	9.95	8.05	T 85	6.20	9.85	8 85	6.20	9 10	2 00	2 00	8 70
-5		(a)	9.05	8 70	7 20	5 65	2.80	8 15	5.40	2 00	1 80	2 60	6 50
- 3		(a)	2 60	10 90	6.85	5 35	3.00	6.95	4.70	2.30	1.70	2 50	5 60
4		(a)	2.50	12.50	7.25	5.15	3.20	6.30	4.20	2.50	1.50	2.90	5.10
$\hat{5}$		(a)	2.90	12.75	8.05	4.95	3.20	5.80	3. 60	2.30	1.40	3.30	5.60
6		2.10	3.50	10.65	8.55	4.80	3.50	5.40	3.20	2.00	1.30	3.70	6.90
7		2.20	3.95	10.00	7.85	4.65	5.65	5.00	2.90	1.70	1.30	4.20	8.30
8		2.30	3.90	11.65	7.05	4.45	6.65	4.50	2.60	1.60	1.60	4.20	9.20
9		2.35	5.35	14.55	6.50	4.45	6.15	4.20	2.40	1.40	1.80	3.70	8.50
10		2.45	8.40	16.50	6.10	4.35	5.30	4.20	2.30	1.30	2.10	3.20	-7.00
11		3.35	9.40	16.15	6.50	4.30	5.00	4.30	-2.10	1.20	2.10	3.00	6.10
12		6.05	8.95	14.25	7.50	4.30	4.90	3.80	2.00	1.10	2.50	2.70	5.40
13		8.15	13.90	11.65	7.40	4.15	4.50	3.40	1.90	1.00	3.00	2.50	4.90
14		8.70	21.55	9.85	7.00	4.00	5.20	3.30	1.90	1.10	2.50	2.30	4.50
15	•••••••	8.45	24.00	8.65	6.00	3.85	5.30	3.30	2.10	1.80	1.90	2.20	4.30
16		7.80	21.40	8.00	6.30	3.75	5.25	3.30	2.20	3.10	1.80	2.10	4.20
17	• • • • • • • • • • • • • • • • • • • •	0.30	19.05	7.80	8.70	3.00	0.40 0.15	5.20	2.30	4.00	1.00 1.50	2.00	4.00
10		5.80	1.3.00	4.00	10.00	0.00 2.40	0.10	2.00	2 20	4.10	1.00 1.40	1.00	0.00
10	• • • • • • • • • • • • • • • • • • • •	9.50	2.20	9.55	9.40	2 40	0.00	2.00	2.00	4.00	1.40	1.00	0.40
20		9.40	7 10	11 60	11 70	3.95	8.00	2.50	1 90	3.00	$1.00 \\ 1.20$	2 10	3.00
39		8 85	7 70	14 95	12.00	3 15	7 65	2 50	1.80	3.00	1.20	2 90	4.00
23		7 95	8 50	17 40	11 35	3 05	6.40	2 50	1 70	2 60	1.40	2.30	4 20
24		7.20	8.55	16.45	10.70	3.00	6.25	2.80	1.80	2.40	2.20	2.80	4.70
25		6.15	8.55	12.65	9.75	3.15	7.15	3.00	1.90	2.70	4.10	3.20	5.20
26		5.50	9,50	11.15	8.50	3.20	7.60	3.10	2.50	2.70	7.00	7.80	5.40
27		5.00	9.30	10.90	7.80	3.35	8.05	3.30	3.10	2.60	7.50	13.90	5.20
28		4.65	8.45	10.70	7.45	3.60	8.20	4.60	2.70	2.40	6.00	15.60	4.60
29		4.20		10.20	7.05	3.60	8.60	. 8.00	2.50	2.30	4.90	15.60	4.30
30		3.90		9.35	6.60	3.35	8.70	8.20	2.30	2.20	3.70	13.20	4.20
31		. 3.55		8.50		3.05		7.30	2.20		3.40		-4.50
			1										

a Frozen.

[Continued in Water-Supply Paper No. 49, where will be found numerous miscellaneous measurements of streams in the southern Appalachian region.]

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Sixteenth Annual Report of the United States Geological Survey, 1894-95, Part II, Papers of an economic character, 1895; octavo, 598 pp.

Contains a paper on the public lands and their water supply, by F.H. Newell, illustrated by a large map showing the relative extent and location of the vacant public lands; also a report on the water resources of a portion of the Great Plains, by Robert Hay.

A geological reconnoissance of northwestern Wyoming, by George H. Eldridge, 1894; octavo, 72 pp. Bulletin No. 119 of the United States Geological Survey; price, 10 cents.

Contains a description of the geologic structure of portions of the Big Horn Range and Big Horn Basin, especially with reference to the coal fields, and remarks upon the water supply and agricultural possibilities.

Report of progress of the division of hydrography for the calendar years 1893 and 1894, by F. H. Newell, 1895; octavo, 176 pp. Bulletin No. 131 of the United States Geological Survey; price, 15 cents.

Contains results of stream measurements at various points, mainly within the arid region, and records of wells in western Nebraska, western Kansas, and eastern Colorado.

1896.

Seventeenth Annual Report of the United States Geological Survey, 1895-96, Part II, Economic geology and hydrography, 1896; octavo, 864 pp.

Contains papers on "The underground water of the Arkansas Valley in eastern Colorado," by G. K. Gilbert; "The water resources of Illinois," by Frank Leverett, and "Pre-liminary report on the artesian waters of a portion of the Dakotas," by N. H. Darton.

Artesian-well prospects in the Atlantic Coastal Plain region, by N. H. Darton, 1896; octavo, 230 pp., 19 plates. Bulletin No. 138 of the United States Geological Survey; price, 20 cents.

Gives a description of the geologic conditions of the coastal region from Long Island, N. Y., to Georgia, and contains data relating to many of the deep wells.

Report of progress of the division of hydrography for the calendar year 1895, by F. H. Newell, hydrographer in charge, 1896; octavo, 356 pp. Bulletin No. 140 of the United States Geological Survey; price, 25 cents.

Contains a description of the instruments and methods employed in measuring streams and the results of hydrographic investigations in various parts of the United States.

1897.

Eighteenth Annual Report of the United States Geological Survey, 1896–97, Part IV, Hydrography, 1897; octavo, 756 pp.

Contains a "Report of progress of stream measurements for the calendar year 1896," by Arthur P. Davis; "The water resources of Indiana and Ohio," by Frank Leverett; "New developments in well boring and irrigation in South Dakota," by N. H. Darton, and "Reser-voirs for irrigation," by J. D. Schuyler.

1899.

Nineteenth Annual Report of the United States Geological Survey, 1897–98, Part IV, Hydrography, 1899; octavo, 814 pp.

Contains a "Report of progress of stream measurements for the calendar year 1898," by F. H. Nøwell and others; "The rock waters of Ohio," by Edward Orton, and "A pre-liminary report on the goology and water resources of Nebraska west of the one hundred and third meridian," by N. H. Darton. Part II of the Nineteenth Annual contains a paper on "Principles and conditions of the movements of ground water," by F. H. King, and one on "Theoretical investigation of the motion of ground waters," by C. S. Slichter.

1900.

Twentieth Annual Report of the United States Geological Survey, 1898-99, Part IV, Hydrography, 1900; octavo, 660 pp.

Contains a "Report of progress of stream measurements for the calendar year 1898," by F. H. Newell, and "Hydrography of Nicaragua," by A. P. Davis.

1901.

Twenty-first Annual Report of the United States Geological Survey, 1899-1900, Part IV, Hydrography, 1900; octavo, 768 pp.

Contains a "Report of progress of stream measurements for the calendar year 1899," by F. H. Newell; "Preliminary description of the geology and water resources of the southern half of the Black Hills and adjoining regions in South Dakota and Wyoming," by N. H. Darton; and "The High Plains and their utilization," by W. D. Johnson.

Bulletins can be obtained only by prepayment of cost, as noted above. Money should be transmitted by postal money order or express order, payable to the Director of the United States Geological Survey. Postage stamps, checks, and drafts can not be accepted. Correspondence should be addressed to

The Director, U. S. Geol. Survey, Washington, D. C.

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WATER-SUPPLY AND IRRIGATION PAPERS.

- 1. Pumping water for irrigation, by Herbert M. Wilson, 1896.
- 2. Irrigation near Phœnix, Arizona, by Arthur P. Davis, 1897.
- 3. Sewage irrigation, by George W. Rafter, 1897.
- 4. A reconnoissance in southeastern Washington, by Israel C. Russell, 1897.
- 5. Irrigation practice on the Great Plains, by E. B. Cowgill, 1897.
- 6. Underground waters of southwestern Kansas, by Erasmus Haworth, 1897.
- 7. Seepage waters of northern Utah, by Samuel Fortier, 1897.
- 8. Windmills for irrigation, by E. C. Murphy, 1897.
- 9. Irrigation near Greeley, Colorado, by David Boyd, 1897.
- 10. Irrigation in Mesilla Valley, New Mexico, by F. C. Barker, 1898.
- 11. River heights for 1896, by Arthur P. Davis, 1897.
- 12. Underground waters of southeastern Nebraska, by N. H. Darton, 1898.
- 13. Irrigation systems in Texas, by W. F. Hutson, 1898.
- 14. New tests of pumps and water lifts used in irrigation, by O. P. Hood, 1898.
- 15, 16. Operations at river stations, 1897, Parts I, II, 1898.
- 17. Irrigation near Bakersfield, California, by C. E. Grunsky, 1898.
- 18. Irrigation near Fresno, California, by C. E. Grunsky, 1898.
- 19. Irrigation near Merced, California, by C. E. Grunsky, 1899.
- 20. Experiments with windmills, by Thomas O. Perry, 1899.
- 21. Wells of northern Indiana, by Frank Leverett, 1899.
- 22. Sewage irrigation, Part II, by George W. Rafter, 1899.
- 23. Water-right problems of Bighorn Mountains, by Elwood Mead, 1899.
- 24, 25. Water resources of the State of New York, Parts I, II, by G.W. Rafter, 1899.
- 26. Wells of southern Indiana (continuation of No. 21), by Frank Leverett, 1899.
- 27, 28. Operations at river stations, 1898, Parts I, II, 1899.
- 29. Wells and windmills in Nebraska, by Erwin Hinckley Barbour, 1899.
- 30. Water resources of the Lower Peninsula of Michigan, by Alfred C. Lane, 1899.
- 31. Lower Michigan mineral waters, by Alfred C. Lane, 1899.
- 32. Water resources of Puerto Rico, by H. M. Wilson, 1900.
- 33. Storage of water on Gila River, Arizona, by J. B. Lippincott, 1900.
- 34. Geology and water resources of southeastern S. Dak., by J. E. Todd, 1900.
- 35-39. Operations at river stations, 1899, Parts I-V, 1900.
- 40. The Austin dam, by Thomas U. Taylor, 1900.
- 41, 42. The windmill: its efficiency and use, Parts I, II, by E. C. Murphy, 1901.
- 43. Conveyance of water in irrigation canals, etc., by Samuel Fortier, 1901.
- 44. Profiles of rivers, by Henry Gannett, 1901.
- 45. Water storage on Cache Creek, California, by Albert E. Chandler, 1901.
- 46. Reconn. of Kern and Yuba rivers, Cal., by F. H. Olmsted and M. Manson, 1901. 47-52. Operations at river stations, 1900. Parts I-VI, 1901.
- Other papers are in various stages of preparation. Provision has been made for printing these by the following clause in the sundry civil act making appropriations for the year 1896–97:
- *Provided*, That hereafter the reports of the Geological Survey in relation to the gaging of streams and to the methods of utilizing the water resources may be printed in octavo form, not to exceed 100 pages in length and 5,000 copies in number; 1,000 copies of which shall be for the official use of the Geological Survey, 1,500 copies shall be delivered to the Senate, and 2,500 copies shall be delivered to the House of Representatives, for distribution. [Approved June 11, 1896; Stat. L., vol. 29, p. 453.]
- The endeavor is made to send these pamphlets to persons who have rendered assistance in their preparation through replies to schedules or who have furnished data. Requests made for a certain paper and stating a reason for asking for it are granted whenever practicable, but it is impossible to comply with general demands, such as to have all of the series sent.
 - Application for these papers should be made either to Members of Congress or to

THE DIRECTOR, UNITED STATES GEOLOGICAL SURVEY, WASHINGTON, D. C.

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DEPARTMENT OF THE INTERIOR

WATER-SUPPLY

AND

IRRIGATION PAPERS

OF THE

UNITED STATES GEOLOGICAL SURVEY

No. 49

OPERATIONS AT RIVER STATIONS, 1900 .- PAR

WASHINGTON GOVERNMENT PRINTING OFFICE 1901

IRRIGATION REPORTS.

The following list contains titles and brief descriptions of the principal reports relating to water supply and irrigation, prepared by the United States Geological Survey since 1890:

1890.

First Annual Report of the United States Irrigation Survey, 1890; octavo, 123 pp.

Printed as Part II, Irrigation, of the Tenth Annual Report of the United States Geological Survey, 1888-89. Contains a statement of the origin of the Irrigation Survey, a preliminary report on the organization and prosecution of the survey of the arid lands for purposes of irrigation, and report of work done during 1890.

1891.

Second Annual Report of the United States Irrigation Survey, 1891; octavo, 395 pp.

Published as Part II, Irrigation, of the Eleventh Annual Report of the United States Geological Survey, 1889-90. Contains a description of the hydrography of the arid region and of the engineering operations carried on by the Irrigation Survey during 1890; also the statement of the Director of the Survey to the House Committee on Irrigation, and other papers, including a bibliography of irrigation literature. Illustrated by 29 plates and 4 figures.

Third Annual Report of the United States Irrigation Survey, 1891; octavo, 576 pp.

Printed as Part II of the Twelfth Annual Report of the United States Geological Survey, 1890-91. Contains "Report upon the location and survey of reservoir sites during the fiscal year ended June 30, 1891," by A. H. Thompson; "Hydrography of the arid regions," by F. H. Newell; "Irrigation in India," by Herbert M. Wilson. Thustrated by 93 plates and 190 figures.

Bulletins of the Eleventh Census of the United States upon irrigation, prepared by

F. H. Newell: quarto. No. 35, Irrigation in Arizona; No. 60, Irrigation in New Mexico; No. 85, Irrigation in Utah; No. 107, Irrigation in Wyoming; No. 153, Irrigation in Montana; No. 157, Irrigation in Idaho; No. 163, Irrigation in Nevada; No. 178, Irrigation in Oregon; No. 193, Artesian wells for irrigation; No. 198, Irrigation in Washington.

1892.

Irrigation of western United States, by F. H. Newell; extra census bulletin No. 23, September 9, 1892; quarto, 22 pp.

Contains tabulations showing the total number, average size, etc., of irrigated holdings, the total area and average size of irrigated farms in the subhumid regions, the percentage of number of farms irrigated, character of crops, value of irrigated lands, the average cost of irrigation, the investment and profits, together with a résume of the water supply and a description of irrigation by artesian wells. Illustrated by colored maps showing the location and relative extent of the irrigated areas.

1893.

Thirteenth Annual Report of the United States Geological Survey, 1891-92, Part III, Irrigation, 1893; octavo, 486 pp.

Consists of three papers: "Water supply for irrigation," by F. H. Newell; "American irrigation engineering" and "Engineering results of the Irrigation Survey," by Herbert M. Wilson; "Construction of topographic maps and selection and survey of reservoir sites," by A. H. Thompson. Illustrated by 77 plates and 119 figures.

A geological reconnoissance in central Washington, by Israel Cook Russell, 1893; octavo, 108 pp., 15 plates. Bulletin No. 108 of the United States Geological Survey; price, 15 cents.

Contains a description of the examination of the geologic structure in and adjacent to the drainage basin of Yakima River and the great plains of the Columbia to the east of this area, with special reference to the occurrence of artesian waters.

1894.

Report on agriculture by irrigation in the western part of the United States at the Eleventh Census, 1890, by F. H. Newell, 1894; quarto, 283 pp.

Consists of a general description of the condition of irrigation in the United States, the area irrigated, cost of works, their value and profits: also describes the water supply, the value of water, of artesian wells, reservoirs, and other details; then takes up each State and Territory in order, giving a general description of the condition of agriculture by irri-gation, and discusses the physical conditions and local peculiarities in each county.

Fourteenth Annual Report of the United States Geological Survey, 1892-93, in two parts; Part II, Accompanying papers, 1894; octavo, 597 pp.

Contains papers on "Potable waters of the eastern United States," by W J McGee; "Natural mineral waters of the United States," by A. C. Peale; "Results of stream meas-urements," by F. H. Newell. Illustrated by maps and diagrams.

IRR 49

DEPARTMENT OF THE INTERIOR

WATER-SUPPLY

AND

IRRIGATION PAPERS

OF THE

UNITED STATES GEOLOGICAL SURVEY

No. 49



WASHINGTON GOVERNMENT PRINTING OFFICE 1901


UNITED STATES GEOLOGICAL SURVEY

CHARLES D. WALCOTT, DIRECTOR

OPERATIONS AT RIVER STATIONS, 1900

A REPORT OF THE

DIVISION OF HYDROGRAPHY

OF THE

UNITED STATES GEOLOGICAL SURVEY

PART III



WASHINGTON GOVERNMENT PRINTING OFFICE 1901 .

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OPERATIONS AT RIVER STATIONS, 1900. PART III.

MEASUREMENTS AT RIVER STATIONS.¹

MISCELLANEOUS MEASUREMENTS OF STREAMS IN SOUTHERN APPA-LACHIAN REGION.

A hydrographic investigation of the southern Appalachian region was made during the field season of 1900. A detailed report of the work will appear in a later publication. During the progress of the investigation a large number of measurements were made of various streams, as shown in the following tables. The tables are arranged in geographic order, commencing with the more northerly streams, which drain into the Atlantic Ocean, and ending with those which belong to the Gulf drainage.

Date.	Stream.	Locality.	Hydrographer.	Gage height.	Dis- charge.
1900. June 21 June 23 July 4	Yadkin Riverdo do do	Wilkesboro, N. Cdo do do	N. C. Curtis dodo	Feet. 26.73 26.14 26.83	Secft. 780.0 1,737.0 663.0
July 12 Aug. 6 Oct. 1 Nov 4	do	do do do	do do do do	$ \begin{array}{c} 27.05 \\ 27.20 \\ 27.20 \\ 26.22 \\ 26.22 \\ \end{array} $	$\begin{array}{r} 488.2 \\ 386.0 \\ 369.1 \\ 1.331.0 \end{array}$
June 20 July 14	do	Second ford below Patter- son's mill, North Carolina.	do	13.3 13.5	182.0 100.3
Aug. 7 Sept.26 June 20	do do Elk Creek	One-fourth mile above ford,	dodo	$ \begin{array}{r} 13.4 \\ 13.53 \\ 2.4 \end{array} $	$76.2 \\ 43.0 \\ 119.0$
July 13 Aug. 6 Sept.26	do do do		do do do	2.43 2.60 2.61	$\begin{array}{c} 61.0\\ 37.0\\ 30.0\end{array}$
June 21 July 13 Aug. 6	Stony Creek	Footbridge at Colberts, North Carolina. do	dodo	2.65 2.70	78.4 80.5 50.0
Sept. 26 June 21	Louis Fork of Yad- kin River.	Footbridge on Mount Pleas- ant road, North Carolina.	do do	2.87 3.10	31.10 127.0
Aug. 6 Sept. 26	do do do	do do do	do do do	3.23 3.30 3.33	99.0 69.0 63.0

¹Continued from Water-Supply Paper No. 48.

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Miscellaneous discharge measurements of Yadkin River, etc.-Continued.

Date.	Stream.	Locality.	Hydrographer.	Gage height.	Dis. charge,
1900. June 23 July 12 Aug. 4 Oct. 1 June 23	Reddie River do do 	North Wilkesboro, N. C do do Trestle of Greensboro and Wilkesboro division of	N. C. Curtis do	Feet. 24.73 25.15 25.25 21.93	$Secft. \\ 218.1 \\ 98.1 \\ 93.0 \\ 60.2 \\ 108.4$
July 3 Aug. 4 Sept.27 Nov. 2 June 25	do do do do Roaring River	Southern R. R., North Car- olinado do do do do Greensboro and Wilkesboro R. R. bridge, North Caro-		$\begin{array}{r} 22.25\\ 22.50\\ 22.42\\ 23.68\end{array}$	50.3 39.25 61.2 55.0 520.2
July 9 Aug. 4 Sept.27 Nov. 2 Sept.27 June 25	do do do do Big Bugaboo Creek. Big Elkin River	ina. do do do Ford of road from Roaring River to Elkin, N. C. Greensboro and Wilkesboro	do do do do do do do	$\begin{array}{c} 25.45\\ 25.75\\ 25.13\\ 24.27\\ 1.28\\ 24.53\end{array}$	$ \begin{array}{c} 161.4\\ 117.0\\ 109.0\\ 197.0\\ 30.0\\ 65.0 \end{array} $
July 9 Aug. 4 Sept.27 June26 July 10 Aug. 3 Sept.28 Nov. 1	do	R. R. bridge, North Caro- lina. do do do do do do do do do do	do do do do do do do	$\begin{array}{r} 25.95 \\ 26.22 \\ 21.63 \\ 24.00 \\ 24.25 \\ 24.25 \\ 24.25 \\ 29.26 \end{array}$	$\begin{array}{c} 29.0 \\ 24.0 \\ 27.0 \\ 393.1 \\ 139.2 \\ 119.0 \\ 160.0 \\ 216.0 \end{array}$
July 10 Aug. 3 Sept.28 Nov. 1 June 27 July 11 Aug. 2 Sept.29 Oct. 31	Fisher River	Greensboro and Wilkesboro R. R. trestle, North Caro- lina. do do do do do do do do do do do do do	do do do do do do do do do do do do do	$\begin{array}{c} 25.69\\ 20.93\\ 23.38\\ 23.60\\ 23.72\\ 23.70\\ 23.9\\ 26.0\\ 26.25\\ 26.46\\ 25.66\end{array}$	$\begin{array}{c} 172.0\\ 126.0\\ 119.0\\ 235.0\\ 801.0\\ 317.1\\ 265.44\\ 243.0\\ 307.0\\ \end{array}$

Miscellaneous discharge measurements of Catawba River and its tributaries.

Date.	Stream.	Locality.	Hydrographer.	Gage height.	Dis- charge.
1900. June 28 Aug. 20 Sept. 20 June 28 Aug. 20 Sept. 20 June 28	Catawba River do Mill Creek do Jarrett Creek	Oldfort, N. C	H. A. Pressey N. C. Curtis H. A. Pressey N. C. Curtis H. A. Pressey	Feet. 10.10 12.70 12.78 3.85 6.73	$\begin{array}{c} Sec. \textit{-ft.} \\ 53.0 \\ 11.0 \\ 12.0 \\ 85.0 \\ 27.0 \\ 13.0 \\ 17.0 \end{array}$
Do	Curtis Creek	Two hundred feet above ford of Oldfort road, North Car- olina.	N.C.Cuntic		82.11
June 28 Aug. 28	Crib Creek	Near ford of main road, North Carolina.	H. A. Pressey N. C. Curtis	4.9	10.50 28.03 10.0
June 28	Clear Creek	Two hundred feet above ford of main road, North Caro- lina.	H. A. Pressey		25.25
Aug. 28 June 14	do Buck Creek	One-eighth mile above mouth at main ford, North Carolina.	N. C. Curtis H. A. Pressey		12.0 51.91
Aug. 20 July 3	North Fork of Ca- tawba River.	First ford above mouth, North Carolina.	N. C. Curtis	5.35	41.4 240.2
Sept. 21	do	do	do	3.18	61.69

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Miscellaneous discharge measurements of Catawba River, etc.—Continued.

Date.	Stream.	Locality.	Hydrographer.	Gage height.	Dis- charge.
1900. June 15	Turkey Cove Creek.	Just above second ford, North	L. V. Branch	Feet. 5.75	Secft. 21.48
June 26	ob	Carolina.	do	5.50	164.8
June 14	Muddy Creek	Bridgewater, N. C	H. A. Pressey	5.80	161.9
June 16	do	do	L.V. Branch	4.1	618.0
July 10	do	do	do	6.0	119.2
Aug. 17	do	do	N. C. Curtis	6,43	98.6
Sept.21	Deddar Greek	Noon Puideomoton N. O	H A Duesser	0.01 11.9	101.1
June 14	Paddy Creek	do	L V Branch	5.4	203 67
July 10	0.0	do	do	11.55	11.5
Aug. 17	do	do	N.C.Curtis	12.35	7.0
June 21	Linville River	Linville, N. C.	H.A. Pressey	14.83	21.0
June 24	do	do	do	14.23	90,22
June 14	Cane Creek	Lowest ford of main Morgan-	do	5.72	18.58
June 18	ob	do	L. V. Branch	5.85	28.45
Aug. 17	do	do	N.C. Curtis	6.3	7.2
June 14	Silver Creek	Near Morganton, N. C	L. V. Branch	6.84	124.0
Aug. 10	do	do	N.C. Curtis	8.30	48.4
Sept.24	do	do	do	8.20	56.0
June 13	Upper Creek	One-fourth mile above mouth, North Carolina.	E. W. Myers	2.2	182.4
July 6	do	do	L.V.Branch	2.3	50.0
Aug. 8	do	do	N.C. Curtis		85.05
Sept. 24	do	Ford at Hondoncon's mill	H A Proseou	19.0	20.49
o uneo		North Carolina.	11. A. I Tessey	1	AU. 4A
Do	do	Upper Creek Falls, North	do		27.0
Do	Steel Creek	Footbridge 100 yards above	do	3,20	100.21
Sept. 25	Johns River	Collettsville N C	N C Curtis	4 77	40.0
Nov. 6	do	do	do	4.47	135.0
Sept.25	Mulberry Creek	At mouth, North Carolina	do	7.85	17.0
Nov. 6	do	do	do	7.95	39.0
Do	Wilson Creek	do	do	0. 75	208.0
June 13	Lower Creek	Two miles above mouth, North Carolina.	E. W. Myers	14.58	209.0
July 6	`do	do	L. V. Branch		132.0
Aug. 8	do	do	N.C. Curtis		69.0
Sept.24	do	do	do	15.38	56.0

Miscellaneous discharge measurements of Broad River (of the Carolinas) and its tributaries.

Date.	Stream.	Locality.	Hydrographer.	Gage height.	Dis- charge.
1900. Aug. 28	Broad River	Ford 1 mile above mouth of Second Broad River, North Carolina	H. A. Pressey	Feet. 5.95	Secft. 649.0
Aug. 25	do	McClure's bridge, North Car-	N.C.Curtis	23.43	220, 0
Oet. 18 Aug. 22	do do	Near mouth of Buffalo Creek, North Carolina.	do do	$22.67 \\ 15.2$	$\begin{array}{c} 434.0 \\ 57.1 \end{array}$
Oet 8 Aug. 21	do do	do Bridge at Batcave post-office,	do do	14.59	$\substack{145.4\\50.1}$
Do	do	N. C. do	do	10.15	48.0
Aug. 21 Do	Hickory Nut Creek Reedy Patch Creek	At mouth, North Carolina do	do do		15.2 13.0
Aug. 22	Buffalo Creek	Fifteen yards below main ford. North Carolina	do	4.10	17.0
Do	Cove Creek	Bridge at Rutherfordton road, North Carolina	do	18.65	69,3
Oct. 6 Aug. 25	do Mountain Creek	Near mouth. North Carolina	do	$18.16 \\ 6.83$	86.0 55.3
Oct. 8 Aug. 25	do Maple Creek	do do	do do	$ \begin{array}{c} 6.48 \\ 7.70 \end{array} $	70.2 8.4

Date.	Stream.	Locality.	Hydrographer.	Gage height.	Dis- charge.
1900. Aug. 25 Oct. 8 Sont 3	Green River	Cox's bridge, North Carolina do	N. C. Curtis	Feet. 22.9 22.6 17.7	Secft. 299.0 255.4 74.1
Do Aug. 31	Cove Creek White Oak Creek	road, North Carolina. Near mouth, North Carolina . One-half mile above mouth,	do do	5.40 4.65	19.2 64.0
Aug. 23 Oct. 5	Second Broad River.	North Carolina. One and one-half miles east of Forest City, N. C. do	do do	20.8 20.32	153.3 188.3
Aug. 24	do	Bridge on Rutherfordton- Morganton road, North Carolina.	do	7.35	55.0
Oct. 4 Aug. 24	Cane Creek	One mile above mouth, North Carolina.	do	$7.00 \\ 5.43$	64.0 17.0
Aug. 23 Do Aug. 24	Cathey Creek Hollins Creek Robersons Creek	At mouth, North Carolina do do	do do do	3.35 5.8	42.0 14.3 24.0
Aug. 23 Aug. 30 Oct. 10	Puzzle Creek First Broad River do	Near mouth, North Carolina . do	do do do	$ \begin{array}{c c} 6.70 \\ 17.7 \\ 16.2 \end{array} $	$ \begin{array}{r} 10.0 \\ 285.3 \\ 266.4 \end{array} $

Miscellaneous discharge measurements of Broad River, etc.-Continued.

Miscellancous discharge measurements of South Saluda Creek and its tributaries.

Date.	Stream.	Locality.	Hydrographer.	Gage height.	Dis- charge.
1900. Sept. 7	South Saluda Creek.	Freeman Bridge, below mouth of Middle Saluda Creek, North Carolina.	N. C. Curtis	Feet. 14.1	Secft. 223.0
Oct. 14	do	do	do	14.1	171.0
Sept. 7	do	Two miles above mouth of Middle Saluda Creek, North Carolina.	do	6.0	188.0
Oct. 14	do	do	do	6.0	134.0
Sept. 7	Middle Saluda Creek	One mile above mouth, North Carolina.	do	11.75	68.0
Oct. 13	do	do	do		55.0
Sept. 7	North Saluda Creek.	Iron bridge at Marietta, N.C	do	14.7	58.2
Oct. 13	do	do	do	14.17	80.0
Sept. 6	do	Bridge on Lima-Cleveland	do	12.9	56.1
Do	do	Mills road, North Carolina. 'Twomiles below Humphrey's store, North Carolina.	do	14.2	26.1
Do	Fall Creek	Bridge on road to Lima, N. C	do		a 15.0

a Estimated.

Miscellaneous discharge measurements of Tugaloo River tributaries.

Date.	Stream.	Locality.	Hydrographer.	Dis- charge.
1900. Dec. 21 Do Dec. 22 Do Do Dec. 23 Dec. 24 Do	South Prong of Pan- ther Creek. Tiger Creek Scott Creek Timpson Creek Tallulah River Stekoa Creek Chattooga River	Near Turnerville, Gado do do Six miles south of Tallulah Falls, Ga Clayton, Ga Five miles from Clayton, Ga Burton, Ga One mile east of Clayton, Ga Rogers Ford, Georgia	J. C. Conn do do do do do do do do do do	$\begin{array}{c} Secft.\\ 8.8\\ 33.5\\ 18.2\\ 11.8\\ 9.0\\ 12.2\\ 263.1\\ 9.9\\ 273.5\end{array}$

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Miscellaneous discharge measurements of Broad River (of Georgia) and its tributaries.

and the second s
rapher. Dis- charge.
Secft.
n 29.4
9.1
7.8
2.3
8.3
6.5
82.0
26.5
28.5
word

Miscellaneous discharge measurements of Savannah River tributaries.

Date.	Stream.	Locality.	Hydrographer.	Gage height.	Dis- charge.
1900. June 30 May 2 Oct. 18	Hollow Creek South Broad River Broad River	Kathwood, S. C Near Carlton, Ga Baker's ferry, about 25 miles below Carlton, Ga.	B. M. Hall Max Hall do	Feet. 3.20 2.20	Secft. 123.0 200.0 949.0

Miscellaneous discharge measurements of Oconee River and its tributaries.

Date.	Stream.	Locality.	Hydrographer.	Gage height.	Dis- charge.
1900. Aug. 27 Dec. 27 Dec. 28 Dec. 18 Dec. 19 Do Do Do Do Do Do Do Do	Oconce Riverdo do Appalachee River Cedar Creek Walnut River Middle Oconee River Murricane Creek North Oconee River do Hurricane Creek Middle Oconee River	Carey, Ga	W. E. Hall Max Hall do J. C. Conn do	Feet. 2.37 3.00 3.44	$\begin{array}{c} Sec. \textit{-ft.}\\ 1, 199.0\\ 1, 566.0\\ 2, 349.0\\ 11.4\\ 27.3\\ 66.8\\ 70.3\\ 6.5\\ 72.8\\ 103.8\\ 3.2\\ 61.4 \end{array}$

Miscellaneous discharge measurements of Ocmulgee River and its tributaries.

Date.	Stream.	Locality.	Hydrographer.	Dis- charge.
1900. Oct. 10 Dec. 18 Do Do Do Dec. 28 Do Do	Yellow River Stone Mountain Creek Big Creek Shoal Creek Alcovy River Shoal Creek Yellow River	Near Stone Mountain, Ga Stone Mountain. Ga Snellville, Ga Tripp, Ga Bramlett Shoals, Georgia do do do Annistown, Ga	Max Hall do do do do do do do do do	$Secft. \\112.0 \\18.1 \\2.0 \\3.9 \\9.3 \\33.7 \\34.5 \\8.5 \\151.7 \\$

Miscellaneous discharge measurements of Chattahoochee River and its tributaries.

Date.	Stream.	Locality.	Hydrographer.	Dis- charge.
Date. 1900. Aug. 20 Do	Stream. Cane Creek	Lecality. Near Dahlonega, Ga do do do do do Five miles above Dahlonega, Ga Five miles north of Dahlonega, Ga Five miles north of Dahlonega, Ga Near Louisville, Ga One mile above mouth, Georgia Near mouth, Georgia do Above mining ditch. Georgia Below Turner Creek, Georgia Six miles above mouth, Georgia Wear Pleasant Retreat, Ga At mouth, Georgia Near Pleasant Retreat, Ga Mear Pleasant Retreat, Ga Mear Pleasant Retreat, Ga Mear Pleasant Retreat, Ga Mear Menesey, Ga Near Menesey, Ga At mouth, Georgia Near Menesey, Ga	Hydrographer. W. E. Hall and H.G. Stokes. do do	$\begin{array}{c} \text{charge.}\\ \hline \\ Secft.\\ 28.6\\ 66.0\\ 287.0\\ 1.8\\ 30.4\\ 22.7\\ 13.3\\ 5.0\\ 9.0\\ 8.0\\ 0\\ 5.0\\ 220.0\\ 23.0\\ 69.0\\ 23.0\\ 69.0\\ 23.0\\ 69.0\\ 23.0\\ 69.0\\ 23.0\\ 69.0\\ 23.0\\ 69.0\\ 23.0\\ 69.0\\ 23.0\\ 69.0\\ 23.0\\ 69.0\\ 23.0\\ 69.0\\ 23.0\\ 69.0\\ 23.0\\ 69.0\\ 23.0\\ 69.0\\ 23.0\\ 69.0\\ 23.0\\ 69.0\\ 23.0\\ 69.0\\ 23.0\\ 69.0\\ 80.5\\ 69.0\\ 80.5\\ 89.$
Do Do Aug. 24 Dec. 21 Do	Soque River Flat Shoals Creek Little River Creek Glades Creek Hazel Creek	Porter Mills, Georgia Johnson's mill, near West Point, Ga. Near Land, Georgia Five miles northeast of Demorest, Ga. Demorest, Ga	Max Hall W. E. Hall and H. G. Stokes. J. C. Conn do	$\begin{array}{c} 212.0 \\ 113.0 \\ 12.3 \\ 62.9 \\ 92.7 \end{array}$

Miscellaneous discharge measurements of Etowah River and its tributaries.

Date.	Stream.	Locality.	Hydrographer.	Dis- charge.
1900. Aug. 14	Little River	Arnold's mill, Georgia	W. E. Hall and H.G. Stokes	Secft. 56.3
Do	Smithwick Creek	Between Arnold's mill, Georgia, and	do	8.0
Do	Buzzard Flopper	do	do	8.0
Do	Board Tree Creek	do	do	8.0
Aug. 15	Etowah River	Near Hightower, Ga.	do	664.0
Do	Yellow Creek	Near mouth, Georgia	do	13.0 45.7
Aug. 16	Amicalola River Spriggs Creek	One mile below Summerour place,	do do	$241.0 \\ 21.3$
Do	Little Amicalola	Georgia. Below Amicalola Falls, Georgia	do	4.3
. Do	Creek. Big Amicalola Creek	Near Afton post-office, Ga	do	83.0
Aug. 17 Do	Spriggs Creek Carder Creek	Near Juno post office, Ga Near mouth, Georgia	do do	27.7 16.2
Do Do	Parks Creek Pigeon Creek	Near Dawsonville, Ga	do	16.0 7.6
Do Do	Shoal Creek Etowah River	do Near Auraria, Ga	do [do	$ \begin{array}{r} 34.6 \\ 257.0 \end{array} $
Do	West Amicalola Creek.	Langston Ford, Georgia	B. M. Hall	15.9
Do Aug. 18	Crane Creek	Below Amicalola Falls, Georgia Near Emma, Ga	do do	6.5 9.0
Do Do	Spriggs Creek	At Spriggs Ford, Georgia Near Parks place, Georgia	do do	14.0 7.3
Do	Mill Creek	Near mouth, Georgia	W. E. Hall and H. G. Stokes.	34.0
Do Do	Nimblewill Creek Etowah River	One mile above mouth, Georgia Below mouth of Nimblewill Creek.	do	40.6 132.0
Aug. 21	Montgomery Creek	Georgia. Near Banda, Ga		10.4
Sept.25	Etowah River	Near Cartersville, Ga	Max Hall	a1,235.0 16.0
Do	Pumpkin Vine Creek	Alice Ga	do O P Hall	60.5
101.10	10 m a Crock	11100.00	0.1.1	0.1

a Gage beight, 2 feet.

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Miscellaneous discharge measurements of Coosawattee River and its tributaries.

Date.	Stream.	Locality.	Hydrographer.	Dis- charge.
1900.				Secft.
Ang. 13	Sugar Creek	Near Ramsey, Ga	O. P. Hall	4.0
Aug. 17	Clontz Creek	Southern's ford, Georgia	B. M. Hall	17.8
Oct. 18	Talking Rock Creek.	Near Carters, Ga	0. P. Hall	91.0
Do	Harris Creek	Goble, Ga	do	3.4
Do	Worley Creek	At mouth, Georgia	do	6.5
Do	Crawfords Creek	do	do	5.0
Oct. 19	Tails Creek	do	do	27.0
Do	Flat Creek	do	do	19.0
Oct. 20	Cartecay River	Ellijay, Ga	do	165.0
Do	Ellijay River		do	129.0
Do	Cox Creek	do	do	2.2
Do	Mill Creek	Near Ellijay, Ga	do	3.0
Do	Clonegar Creek	Five miles above Ellijay, Ga	do	3. U
Do	Clear Creek	One mile above mouth, Georgia	do	1.0
Do	Turkey Creek	One mile above mouth of Clear Creek,	ao	12.9
0.4 00	Lisla Land Churche	Georgia.		10.0
Oct. 22	Anderson Creek	Cartecay, Ga		10.0
Doll. At	Tialrapatler Piver	One mile above mouth, Georgia	do	101.0
10	rickanetiey river	Chealt Coordia	····· uo ·····	101.0
Do	Pumpkin Crook	Voer Tiekenotler Ge	do	20 8
D0	Downing Creek	One and one half miles above forks	do	92.6
D0	Downing Greek	Georgia		10.0
Do	Pawlston Creek	Near month Georgia	do	97 5
Do	Branch of Carteeav	Entering Carteesy River 9 miles	do	1 6
D0	River.	above Ellijav Ga		1.0
Do	Scrongetown Creek	Near mouth 7 miles above Ellijay Ga	do	57
Oct. 25	Owltown Creek	At mouth 3 miles above Ellijay. Ga	do	15.0
Do	Big Turnintown	Above month of Little Turnintown	do	17.4
20111	Creek.	Creek, Georgia.		
Do	Little Turniptown	One mile above month. Georgia	do	1.9
	Creek.			
Do	White Path Creek	At railroad crossing, Georgia	do	5.3
Do	Branch of Briar	Whitepath, Ga	do	.8
	Creek.			
Do	Briai Creek	One and one-half miles north of	do	3.0
		Whitepath, Ga.		
Do	Rock Creek	One mile above mouth, Georgia	do	32.5
Do	Cherry Log Creek	Near mouth, Georgia	do	21.9
Oct. 26	Boardtown Creek	do	do	28.1
Do	Parks Creek	At Boardtown road, Georgia	do	2.4
Do	Branch of Kells	Near mouth, Georgia	do	1.5
D	Creek.	All and the Change of	1	10.0
Do	Relis Creek	Above mouth, Georgia	do	10.6
Do	Branch of Ellijay	Near mouth, Georgia	ao	3.0
De	Kiver.	At huiden 1: wiles shows Ellider Co.	J.,	1~~ *
0.1	Contector Diver	At orluge 1/ miles above Emijay, Ga L		110.1
Dott. 4	Mountaintown	Above forly of Buteliff Ge	do	~00. 2 9~ 9
D0	Crook	Above fork at natchin, Ga		01.0
Do	Middle Prong of	Near month Georgia	do	17.0
10	Mountaintewn	rour mouth, coorganismission		11.0
	Creek.			
Do	West Prong of	Above mouth of Middle Prong	do .	23.2
	Mountaintown	Georgia.		NO. 14
	Creek.	-0		

Miscellaneous discharge measurements of Conasauga River and its tributaries.

Date.	Stream.	Locality.	Hydrographer.	Dis- charge.
1900. May 15 Aug. 13 Sept. 7 Ang. 13 Sept. 6 Ang. 13 Aug. 14 Do Sept. 6 Do Aug. 14 Sept. 6 Aug. 14 Sept. 5 Aug. 15	Conasauga River Rock Creek Holy Creek Mill Creek. Sumach Creek. do do Conasauga River Jacks River do Sheets Creek	Near Resaca, Ga Ramsey, Ga do Near Fort Mountain, Georgia Dunn, Ga North Prong at Long Bridge, Georgia Sonth Prong at Long Bridge, Georgia do North Prong at Long Bridge, Georgia Alaculsy, Ga do Near Alaculsy, Ga do	0. P. Hall do	$\begin{array}{c} Secft.\\ 420.0\\ 7.4\\ 4.2\\ 13.8\\ 13.5\\ 3.0\\ 3.2\\ 2.6\\ 4.1\\ 3.4\\ 16.2\\ 10.7\\ 30.6\\ 24.8\\ 2.0\\ \end{array}$

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Miscellaneous discharge measurements of Coosa River tributaries.

Date.	Stream.	Locality.	Hydrographer.	Dis- charge.
1900. Aug. 15 Aug. 16 Aug. 17	Talladega Creek Tallesschatchee Creek Hatchett Creek	Kymulga, Ala Childersburg, Ala Goodwater, Ala	J. R. Hall do do do	Secft. 107.0 102.0 84.0

Miscellaneous discharge measurements of Tallapoosa River and its tributaries.

Date.	Stream.	Locality.	Hydrographer.	Dis- charge.
1900. Apr. 7 Aug. 2 Aug. 3 Aug. 30 Aug. 30 Nov. 1 Dec. 12 Do	Tallapoosa River Longahatchee Creek Blue Creek Elkhatchee Creek Timber Cut Creek Tallapoosa Creek Chattasatkee Creek Sandy Creek	Muscadine, Ala Meader's bridge, Alabama Susauna, Ala Islaud Home, Ala Welche's ferry, Alabama Cherokee Bluff, Alabama Dadeville, Ala Near Dadeville, Ala	J. C. Conn J. R. Hall do do do do do do	$\begin{array}{c} Sec. \ ft. \\ 475.0 \\ 125.0 \\ 34.0 \\ 40.0 \\ 18.6 \\ 3,650.0 \\ 35.0 \\ 145.0 \end{array}$

Miscellaneous discharge measurements of New River and its tributaries.

Date.	Stream.	Locality.	Hydrographer.	Gage height.	Dis- charge.
1900.			N 0 0 11	Feet.	Sec. ft.
July 18	South Fork of New River.	Riverside, N. C.	N. C. Curtis	11.85	165.0
Oct. 25 July 23	Elannery Fork	Ford of Boone-Blowing Bock	do	11.00 6.35	741.1 10.4
Ort Pi	de	road, North Carolina.	đo	5.05	107 0
July 23	Middle Fork	Ford of Boone - Aho road,	do	5.70	24.4
Oct. 24	do	North Carolina. do	do		234.0
July 23	East Fork	do	do	5.70	10.4
July 18	Meat Camp Creek	One-fourth mile below Mor-	do	9.00	35.3
Oct. 25	do	etz, N. C. do	do	8.65	89.0
July 24	Elk Creek	Elk crossroads, North Caro- lina.	do	8.00	10.0
July 18	Old Field Creek	One-eighth mile a hove mouth	do	6.1	19.4
July at		North Carolina		2.00	20. T
July 19 July 27	Mulberry Creek	Near mouth, North Carolina	do	5.1	109.0
Do	Prather Creek	One and one-half miles below Scottville, N. C.	do	8.6	25.0
July 21	North Fork of New Biver	One mile below Creston, N. C.	do	6.7	49.3
Oct. 26	do	do	do	6.0	194.0
July 20		N. C., on road to Solitude,		N. 00	0/4. N
Do	Three Top Creek	N. C. Creston, N. C.	do	6.75	130.0
July 21 July 20	Big Laurel Creek	One hundred vards above	do	$7.25 \\ 6.40$	$ 37.0 \\ 26.2 $
Oct 28	do	mouth, North Carolina.	do	6.30	80.4
July 20	Buffalo Creek	One-eighth mile above mouth,	do	5.43	44.0
Oct. 26	do	North Carolina.	do		67.0
July 25	Horse Creek	One-fourth mile above mouth, North Carolina.	do	6.6	34.3
Oct. 27 July 25	Helton Creek	Below Peasley's mill North	do	6.05 4.28	$140 0 \\ 30.0$
Oct 9"	do	Carolina.	do	21110	105.0
July 28	Wilson Creek	Two miles above mouth, Vir-	do	6.3	35.1
Oct. 28	do	ginia. do	do	6.1	78.0

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Miscellaneous discharge measurements of New River, etc.—Continued.

Date.	Stream.	Locality.	Hydrographer.	Gage height.	Dis- charge.
1900, July 29 Oct. 28 July 31 Oct. 29 July 31 Oct. 29 July 30	Fox Creekdo Peach Bottom Creek do Little River do Elk Creek	One-fourth mile above mouth, Virginia. -do Two bundred yards above mouth, Virginia. -do Ford of Independence-Old- town road, Virginia. -do Two hundred yards above mouth, Virginia.	N. C. Curtis do do do do do do do	Feet. 4.9 9.1 4.0	Secft. 85.0 144.0 21.4 36.0 199.0 318.2 57.03

Miscellaneous discharge measurements of French Broad River and its tributaries.

Date.	Stream.	Locality.	Hydrographer.	Gage height.	Dis- charge.
1900. Sept. 7	French Broad River.	One half mile above Hot	L. V. Branch	Feet. 19.35	Secft. 938.0
Sept. 12 Oct 29	do	Springs, N. C. Alexander, N. C	E. W. Myers	17.15 16.27	840.0 2.058.0
Sept. 18	do	Fanning Bridge, North Caro- lina.	N. C. Curtis	16.22	1.161.0
Oct. 17 Sept.17 Sept.13	do do	Penrose, N. C	do do do	$ \begin{array}{r} 16.95 \\ 19.8 \\ 13.8 \end{array} $	614.0 1,160.0 266.5
Oct. 15 Sept. 14	do do	Eastatoe Bridge, North Caro-	do do do	$13.9 \\ 12.4$	206.5 113.0
Oct. 15 Sout 11	do	lina. do	do	11.21	102.4
Sept. 14	French Broad River.	mouth of West Fork, North Carolina.			100.0
Oct. 15 Sept. 16	do do	do Bridge on Brevard-Webster	do do	$ \begin{array}{r} 13.2 \\ 14.98 \end{array} $	$51.8 \\ 107.48$
Do	do	Ford on road between Tuck- er and Shoal creeks, North	do	7.3	75.0
Sept.14	West Fork of French Broad River	Near mouth, North Carolina	do	2.20	149.0
Oct. 15 Sept. 14	do Middle Fork of French Broad	Bridge 20 yards above ford, North Carolina	do do	5.25	$\begin{array}{c} 62.0 \\ 77.0 \end{array}$
Do	River. South Fork of French Broad	Footbridge at ford of main road, North Carolina.	do	10.3	71.0
Oct. 15	East Fork of French Broad River	Near mouth, North Carolina.	do	10.2	46.0
Sept.16	Tucker Creek	Two hundred yards above mouth, North Carolina.	do	4.61	28.0
Sept. 13	Cathey Creek	Ford of Brevard Jeptha road, North Carolina.	do	6.7	30.2
Sept. 17	King Creek	Brevard road, North Caro- lina.	do	4.71	15.46
Oct. 16 Sept. 17	Little River	Three fourths mile above	do	16.75 13.66	70.20 182.8
Oct. 16 Sept. 17 Do	do Boyiston Creek Mills River	Near mouth, North Carolina Near mouth, North Carolina Bridge on Old Haywood road,	do do do do	$14.35 \\ 5.35 \\ 13.11$	$69.2 \\ 28.67 \\ 211.64$
Oct. 17 Sept. 18 Do	do Mud Creek Caney Creek	North Carolina. do Near mouth, North Carolina. Bridge on Westfall's place,	do do do	$ \begin{array}{r} 13.4 \\ 5.11 \\ 10.1 \end{array} $	$94.0 \\ 108.0 \\ 60.0$
Do	Avery Creek	North Carolina. Bridge on road from Mills	do	6. 56	11.31
Sept. 19 Oct. 17	Hominy Creek	Asheville, N. C.	do	15.1	80.0
Sept. 19	Swannanoa River	Biltmore, N.C	do	2.91	76.33

Miscellaneous discharge measurements of French Broad River, etc.-Continued.

Date.	Stream.	Locality.	Hydrographer.	Gage height.	Dis- charge.
1900.				Feet	Sec .ft
Sept.20	North Fork of Swan-	Three miles above Swanna-	N. C. Curtis	16.07	21.45
Do	Flat Creek	Two miles below Black Moun-	do	4.05	22.83
Sept.12	Beaver Dam Creek	Fifty yards above mouth,	E. W. Myers	5.09	1.46
Oct 30	do	North Carolina.	L V Brouch	5.09	4.10
Sept. 16	Lees Creek	Olivette, N.C.	E. W. Myers	11.15	3.95
Oct. 30	do	do	L. V. Branch	10.95	2 29
Sept. 12 Sout 16	Newfound Creek	At mouth, North Carolina	E. W. Myers	17.75	9.41
Sept. 10		mouth. North Carolina.	00	10.19	01.10
Oct. 30	do	do	L. V. Branch	10.44	20.23
Sept. 12	Reams Creek	At mouth, North Carolina	E. W. Myers	12.1	4.89
Sent. 11	Flat Creek	do	E W Myers	18.05	5.33
Oct. 29	do	do	L. V. Branch	17.43	5.0
Sept. 12	San iy Mush Creek.	Bailey, N. C	E.W. Myers	9.73	21.72
Sept. 17 Oct 30		do	L V Branch	9.43	55.23
Sept. 16	Turkey Creek	Blackwell Springs, N. C	E. W. Myers	7.97	35.24
Oct. 30	do	do	L.V. Branch	8.32	16.24
Sept. 17	Big Ivy River	of Bull Creek, North Caro-	E. W. Myers	2.55	47.59
0.4.00		lina.	T TT D	0.00	(1.80
Sent 8	Little Pine Creek	One hundred varde shove	L. V. Branch	5.12	41.72
Sept. o	Little I me Creek	mouth, North Carolina.		0.01	0.00
Oct. 31	do	do	do	5.76	6.0
Sept. 8	Pawpaw Creek	One mile above mouth, North Carolina	do	4.6	0.35
Sept. 10	Walnut Creek	At mouth, North Carolina	do	23.24	1.36
Oct. 31	do	do	do	2.35	2.24
Sept. 8	Big Pine Creek	One hundred yards above mouth, North Carolina.	do	6.07	4.85
Oct. 31	do	do	do	6.01	4.45
Sept. 8	Laurel Creek	Two hundred yards above	do	16.13	49.0
Sept. 18	do	do	E. W. Myers	15.77	55.0
Sept. 7	Spring Creek	Near Hot Springs, N. C.	L.V. Branch	2.00	15.0
Nov. 1	do	do	do	2.07	16.0
Fept. 4	Shutin Creek		uo	2.01	0.40

Miscellaneous discharge measurements of Nolichucky River and its tributaries.

Date.	Stream.	Locality.	Hydrographer.	Gage height.	Dis- charge.
1900. Aug. 23 Sept. 4 Aug. 24 Oct. 17	Nolichucky River	Erwin, Tenn do do do	L. V. Branch do do do	$Feet. \\ 20.67 \\ 21.53 \\ 15.89 \\ 16.12$	Sec. ft. 770.0 411.0 381.0 301.0
July 2 Aug. 26 Oct. 21 Oct. 25 Aug. 27	North Toe River do do do do do	Sprucepine, N. C do do do Plumtree, N. C	H. A. Pressey L. V. Branch do do do do	$ \begin{array}{r} 18.20 \\ 18.37 \\ 17.15 \\ 7.55 \end{array} $	$\begin{array}{c} 323.0 \\ 105.0 \\ 78.0 \\ 570.0 \\ 79.0 \end{array}$
Do Do Do	Kentucky Fork of North Toe River. White Oak Creek	At ford of Linville-Cranberry road, North Carolina. At mouth, North Carolina	do do	3.6 2.85 2.26	18.0 9.7 3.36
Aug. 28 Oct. 24 Aug. 27 Do	Horse Creekdo Squirrel Creek Roaring Creek	do One-fourth mile above mouth, North Carolina. At mouth, North Carolina.	E. Graves L. V. Branch do	5.55 5.15 3.12 7.89	$ \begin{array}{r} 9.03 \\ 40.53 \\ 11.2 \\ 15.57 \end{array} $
Do Do Aug. 26	Plum Tree Creek Henson Creek Threemile Creek	Plumtree, N. C At mouth, North Carolina Near old post-office at Elsie, N.C.	do do do	2.99 6.94 5.38	8.09 4.8 2.63
Aug. 25 Oct. 21 Aug. 26	Beaver Creekdo Grassy Creek	Near Sprucepine, N. C do Sprucepine, N. C	do do do do	$ \begin{array}{r} 5.30 \\ 4.50 \\ 4.29 \\ 5.21 \\ \end{array} $	3, 57 3, 29 3, 08 6, 09

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Miscellaneous discharge measurements of Nolichucky River, etc.—Continued.

Date.	Stream.	Locality.	Hydrographer.	Gage height.	Dis- charge.
1900.				Feet.	Secft.
Oct. 20	Grassy Creek	Sprucepine, N. C	L.V. Branch	5.13	9.15
Aug. 26	Bear Creek	Flatrock, N. C	do	3.76	4.67
Oct. 20	do	do	do	3.70	3.73
Aug. 25	Snow Creek	Wing, N.C.		3.03	2.0
Do	Crabtree Creek	Ford of Burnsville-Spruce-	do	7.97	15.2
Oat 20	da	pine road, North Carolina.	do	7 01	14.55
Aug. 25	Brush Creek	Lower ford of Burnsville- Sprucepine road, North	do	1.39	4.37
		Carolina.			
Oct. 20 Aug. 24	Cane Creek	One-half mile above mouth,	do	$1.51 \\ 9.20$	11.78
2 1 10	2	North Carolina.	3.	0.90	0.00
Oct. 19		At month North Concline		9.20	9.92
Sept. a	Pigeon Creek	At mouth, North Carolina	do	5.60	1.00
Sent 3	Jack Creek	do	do	6.09	8 71
Oct. 19	do	do		6.10	6.83
Aug. 24	Big Rock Creek	Ford of Huntdale-Bakersville	do	2.42	51.3
Oct 19	do	road, North Carolina.	do	2 64	21.5
Aug 24	Pigeon Roost Creek	At mouth, North Carolina	do	7.39	14.5
Oct. 19	do	do	do	7.47	4.12
Aug. 23	Hollow Poplar Creek	Ford of Erwin-Bakersville road, North Carolina.	do	8.15	5.98
Oct. 16	do	do	do	8.26	2.61
Aug. 23	South Indian Creek.	Near Erwin, Tenn	do	5.38	52.3
Sept. 4	do	do	do	5.49	33.2
Sept.19	do	do	E. W. Myers	5.40	53.0
Aug. 23	Martin Creek	do	L. V. Branch	1.59	7.55
Sept. 4	do		do	1.68	6.45
Aug. 22	North Indian Creek.	Erwin, Ienn		0.90	01.0
Sept. 4	do	do	F W Myong	4.18	20.7
Oct 16	do	do	L V Branch	4.05	26 13
Ang 22	do	Unicoi Tenn	do	4.58	37.9
Do	Rock Creek	One hundred vards above	do	3.69	6.37
July 1	South Toe River	mouth, Tennessee.	'H A Pressev		220.8
oury r		road, North Carolina.			14/4010
Aug. 25	do	do	L. V. Branch	8.08	79.8
Aug. 30	do	do	do	7.98	86.23
Oct. 21		One will above month of		1.23	282.9
Aug. 51		Three Fork Creek, North Carolina.		4.04	20.0
Oct. 26	do	do	do	3.30	101.0
Aug. 31	Three Fork Creek	One-fourth mile above mouth,	do	1.49	9.49
Do	Rock Creek	Ford of Micaville-Marion	do	1.96	6.92
Oat 22	do	do	do	1 60	90 00
Ang 21	Middle Creek	do	do	1.0.2	2 70
Oct 26	do	do	do	3 61	0.10
Aug. 31	Colbert Creek	do	do	3.87	2.51
Oct. 26	do	do	do	3.50	7.24
Aug. 30	Locust Creek	At mouth, North Carolina	do	1.98	3.83
Oct. 26	do	do	do	1.87	7.96
Aug. 30	Whiteoak Creek	do	do	4.66	4.40
Oct. 26	do	Fond of Migg-ill Marti	do	4.28	19.86
Aug. 30	Brown Creek	road, North Carolina.		3.0%	4.94
Oct. 20	Tittle Grabber	do	do	2.85	9.43
Aug.30	Creek.	caville-Sprucepine road,	do	4.28	17.94
Oct. 27	ob	do	do	4.23	21.67
Aug. 30	Cane Branch	Ford of Micaville-Marion	do	3.92	2.98
Oct 28	do	do	do	3.79	8 56
Aug. 24	Caney River	Huntdale, N. C.	do	3 69	89.9
Sept. 3	do	do	do	3.82	62.77
Oct. 17	do	do	do	3.83	58.3
Sept. 1	do	Near Big Tom Wilson's,	do	1.33	17.15
0.1.1.		North Carolina.			
Oct. 18	do	do	do	1.34	13.9
Sept. 1	Elk Fork Creek	do	do	1.24	4.78
Oct. 18	Cattail Branch	Noon Punnorille M. C	do	1.28	1.49
Oct 18	do	do	do	9 61	1 60
500. 10					4.03

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Miscellaneous discharge measurements of Nolichucky River, etc.—Continued.

Date.	Stream.	Locality.	Hydrographer.	Gage height.	Dis- charge.
1900. Sept. 1 Oct. 18 Sept. 2 Oct. 18 Sept. 2 Oct. 18 Sept. 2 Do Oct. 17 Sept. 2 Oct. 17 Sept. 2 Oct. 17 Sept. 2 Oct. 17	Bowlen Creekdo Price Creekdo Bald Creekdo Elk Shoal Creek Bald Mountain Creek. do Little Bald Moun- tain Creez. do Big Creek	Near Burnsville, N.C do do do do do At mouth, North Carolina Carolina do At mouth, North Carolina do At mouth, North Carolina do do do	L. V. Branch do do do do do do do do do do	$Feet. \\ 5.03 \\ 4.97 \\ 2.48 \\ 2.53 \\ 4.56 \\ 1.63 \\ 3.43 \\ 3.55 \\ 4.91 \\ 4.90 \\ 2.83 \\ 2.89 \\ 1.62 \\ 1.62 \\ 1.63 \\$	

Miscellaneous discharge measurements of South Fork of Holston River and its tributaries.

Date.	Stream.	Locality.	Stream. Locality. Hydrographer.		Dis- charge.
1900.		Del an anti a Milli Davis	I W Doorah	Feet.	Secft.
July 23	ston River.	Virginia.	L. v. Branch	3.00	228.0
Oct. 3	do	do	E. W. Myers	3.21	199.0
July 28		Virginia.		≈.00	052.0
Oct. 3	ðo	A have month of Launal Fork	do	3.39	149.0
July 20	uo	Virginia.		1.01	101.0
Oct. 3	do	Byo Volloy, Virginia	do	8.06	48.0 20.0
Oct. 1	do	do	do	0.00	5.0
July 27	Jim Scot Branch	At mouth, Virginia	do		4.12
July 27	Pomer Creek	do	do	2.1	39.0
Oct. 1	do	do	do	2.29	5.0
July AI	Hogtrough Creek	ginia.		. 01	5.0
Oct. 2	do	do	do	5 70	1.0
Oct. 2	do	do		5.94	2.0
July 27	Grose Creek	do	L.V. Branch	3.88	2.0
July 27	Mill Creek	One mile above mouth, Vir-	do	4.32	18.0
Oct 0	đe	ginia.	E W Muona	4 12	19 09
July 28	Rush Creek	Ford 100 yards above mouth,	L. V. Branch	3.63	4.20
Dat 9	do	Virginia.	F W Myone		2.0
July 28	Laurel Fork of Hol-	One-half mile below Damas-	L.V. Branch	3.56	351.0
Oat 2	ston River.	cus, Va.	F W Muore	4 61	88.14
July 29	do	Near Laurel bloomery, Ten-	do	5.12	61.0
Do	do	nessee.	do	2.06	93.0
D0		bloomery, Tennessee.		2.00	
Do	Atcheson Creek	Near head of Laurel, Tenn	do	$1.82 \\ 5.47$	4.32
Oct. 2	do	do	do	5.72	34.3
July 28	Beaver Dam Creek.	Damascus, Va	do	11.36	189.0
July 23	Fifteenmile Creek	At mouth Virginia	L. V. Branch	4.45	7.37
Sept.27	do	do	E. W. Myers	4.23	10.46
July 21 Sopt 27	Denton Valley Creek	do	E. W. Branch	5.73	6.0
July 21	Wolf Creek	Lower ford of main road up	do	2.35	7.0
Inla 92	do	the river, Virginia.	L V Branch	2.36	7.0
Sept.27	do	do	E. W. Myers	2.21	12.24
July 21	Spring Creek	One mile above mouth, Vir-	L.V. Branch	. 90	13.0
Sept.27	do	ginia. do	E. W. Myers		10.0

a Almost dry.

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Miscellaneous discharge measurements of South Fork of Holston River, etc.—Cont'd.

Date.	Stream.	Locality.	Hydrographer.	Gage height.	Dis- charge.
1900. July 21	Jacobs Creek	At mouth, Tennessee	L. V. Branch	<i>Feet.</i> 9.1	Secft. 2.07
Sept.27	do	do	E. W. Myers		2.0
July 21	Sharp Creek	do	do	5.36	1.16
Sept.26	Fishdom ('moolr	do	do	0.00	1.19
Sopt 26	do	do	L V Branch	5 26	2.47
July 20	Jonah Creek	do	do	11.06	4.0
Sept.25	do	do	E. W. Myers	11.42	4.0
July 20	Riddle Creek	do	do	12.19	2.0
Sept.25	do	do	do	11.13	3.0
Do	Thomas Creek	Below railroad bridge, Ten-	do		2.46
Ter 1 00	Simbing Chools	nessee.	đo	4 02	11.0
July 29	Sinking Creek	do	do	4.00	11.0
July 20	do	One half mile above Paper-	L V Branch	3 6	3 48
oury wo		ville. Tenn.	1. The Distance in the second se	0.0	0. 10
Sept.25	Hatcher Creek	One-half mile above mouth,	E. W. Myers	5.92	0.34
	· · · · · · · · · · · · · · · · · · ·	Tennessee.			
July 24	Middle Holston	Five miles above mouth, Vir-	do	5.96	172.0
Class 4 80		ginia.	de	0.91	100.0
Sept. 28	Middle Feels of Hols	Sovermile ford Virginia	I V Propoh	12 00	71.92
July 20	ton River	Sevenimie foru, virginia	L. V. Dranch	10,00	11.40
Do	do	Above mouth of Bear Creek.		6.23	18.0
20		Virginia.		0	
Oct. 1	do	do	do	7.69	11.0
July 25	Bear Creek	At mouth, Virginia	do	6.99	2.01
Oct. 1	do	do	E. W. Myers	6.90	3.0
July 25	Staleys Creek	Marion, Va	L. V. Branch	9.26	14.32
Do	Hungry Mother	Ford of main road from Ma-	ao	1.18	2.40
Oat 1	do	do	E W Myors	1.17	9.26
July 25	Byars Creek	At mouth. Virginia	L V. Branch	1.52	4.0
Sept. 29	do	do	E. W. Myers	1.58	2.24
July 25	Walker Creek	Fifty yards above mouth,	do	4.90	3.0
v		Virginia.			
Sept.29	do	do	do	4.89	9.0
July 23	Huttons Branch	At mouth, Virginia	L. V. Branch	4.45	5.0
Sept. 29	Halla Crook	do	do myers	4.40	5.0 17 26
Do	Codar Creek	do	do	1.10	3 49
July 24	Hogthief Creek	One-half mile above mouth.	L. V. Branch	5.0	5.0
	and the second second	Virginia.		510	010
Sept.29	do	do	E. W. Myers		5.0

Miscellaneous discharge measurements of Watauga River and its tributaries.

Date.	Stream.	Locality.	Hydrographer.	Gage height.	Dis- charge.
1900. July 16 Aug. 2 Aug. 16 Oct. 5 Dec. 28 Dec. 31 July 16 Aug. 10 Oct. 7 Aug. 11 Oct. 7 Aug. 10	Watauga River do do do do do do do do do do do do do	Elizabethton, Tenn do do do do do watauga Falls, N.C. do One mile above Shull's mill, North Carolina. do Shull's mill, North Carolina.	E. W. Myers do do E. W. Myers L. V. Branch Ernest Graves N. C. Curtis L. V. Branch E. W. Myers L. V. Branch E. W. Myers L. V. Branch	$\begin{array}{c} Feet.\\ 15.87\\ 15.77\\ 16.03\\ 16.03\\ 15.27\\ 15.68\\ 15.22\\ \hline \\ 6.62\\ 6.52\\ 4.05\\ \hline \\ 3.78\\ 2.3\\ \end{array}$	$\begin{array}{c} secft,\\ 450.0\\ 593.0\\ 403.0\\ 993.0\\ 533.0\\ 993.0\\ 533.0\\ 973.0\\ 79.0\\ 533.0\\ 60.0\\ 19.0\\ 23.0\\ 12.0\\ \end{array}$
Oct. 7 Aug. 11 Aug. 10 Oct. 7 Aug. 10 Oct. 7 Aug. 10 Oct. 7	tauga River. do Moody Mill Creek Laurel Creek (up- per). do Dutch Creek Core Creek do	do At mouth, North Carolina do do Valle Cruces, N. C. do At mouth, North Carolina do	E. W. Myers L. V. Branch do E. W. Myers L. V. Branch E. W. Myers L. V. Branch E. W. Myers	$2.11 \\ 3.2 \\ 2.62 \\ 2.87 \\ 7.42 \\ 7.37 \\ 5.24 \\ 5.15 \\ $	$ \begin{array}{c} 13.0 \\ 4.0 \\ 10.0 \\ \hline 6.0 \\ 11.0 \\ 6.0 \\ 12.0 \\ 14.0 \\ \end{array} $

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Miscellaneous discharge measurements of Watauga River, etc.—Continued.

Date.	Stream.	Locality.	Hydrographer.	Gage height.	Dis- charge.
1900. Aug. 12	Cove Creek	Above mouth of Brushy Fork, North Carolina	L. V. Branch	Feet. 4.31	Secft. 23.0
Do	Brushy Fork of Cove Creek.	At mouth, North Carolina	do	2.06	5.19
Do Oct. 18	Rockhouse Creek	do	E. W. Myers	2.17	$16.3 \\ 0.8$
Aug. 10 Oct 7	Laurel Creek (lower)	do	L.V. Branch E. W. Myers	10.62	4.0
Aug. 9	Beaver Dam Creek.	Near Leander, N. C.	L. V. Branch	5.59	7.0
Aug. 9	Beech Creek	Above mouth of Fogey Creek, North Carolina.	L. V. Branch	5.6	8.0 7.3
Aug. 9	Fogey Creek	At mouth, North Carolina	L. V. Branch	5.7 2.94	1.4
Oct. 6 Aug. 9	Big Dry Run	One-eighth mile above mouth,	E. W. Myers L. V. Branch	$3.02 \\ 1.55$	$2.4 \\ 0.85$
Aug. 6	Elk Creek	North Carolina. One-half mile below mouth	do	7.21	64.0
Aug. 11	South Fork of Elk	At Banners Elk, North Caro- lina	do <mark></mark>	11.96	9.38
Oct. 8 Aug. 12	North Fork of Elk	do do	E. W. Myers L. V. Branch	$\begin{array}{c} 11.82\\ 5.61 \end{array}$	$\begin{array}{c} 8.48 \\ 7.0 \end{array}$
Oct. 8 Aug. 4	Creek. Cranberry Creek	do Cranberry, N. C.	E. W. Myers L. V. Branch	$5.64 \\ 6.95$	4.0 5.09
Do Aug. 6	Little Elk Creek	At mouth, North Carolina	do do	$6.03 \\ 1.2$	5.05 6.0
Do	Dark Ridge Creek.	One-half mile above mouth, Tennessee.	do	4.65	3.0
July 30	do	Above mouth of Mill Creek, Tennessee.	E. W. Myers	0. 7 4. 85	60.3 5.9
Do July 29	Forge Creek	Near mouth, Tennessee At Shoun crossroads, Ten-	do	4.53	7.0 29.2
Ang 13	do	nessee.	o. *	3.82	6.0
July 30	Mill Creek	At mouth, Tennessee	E. W. Myers	$9.48 \\ 5.23$	13.0
Aug. 13	do	do	L. V. Branch	5.49	26.2
Oct. 9 Aug.13	do do	Ivyspring post-office, Ten-	L. V. Branch	5. 46 5. 94	28.38
Aug. 3	Stony Creek	One-half mile above mouth, Tennessee.	do	6.95	44.0
Oct. 5 Dec. 31	do	do	E. W. Myers Ernest Graves	$7.59 \\ 4.60$	$ 16.0 \\ 48.0 $
Aug. 2	Doe.River	Above Elizabethton, Tenn	L. V. Branch	5.94 6.20	143.4 106.0
Oct. 5	do	do	E. W. Myers	6.23	82.0
Dec. 31 Aug. 3	do	Near Allentown, Tenn	L. V. Branch	5.23 5.56	304.0 72.0
Aug. 18	do	do	E W Myore	5.81	50.0
Aug. 3	do	Two miles below Roan Moun- tain, Tennessee.	L. V. Branch	8,46	41.3
Do Do	Wilson Creek	At mouth, Tennessee One mile above mouth, Ten-	do	$2.35 \\ 3.67$	$\begin{array}{c} 14.0 \\ 5.0 \end{array}$
Do Oct. 5	Little Doe River do	Allentown, Tenn	E. W. Myers	$\begin{array}{c} 4.42\\ 4.78\end{array}$	$\begin{array}{c} 35.0\\17.0\end{array}$
Dec. 29 Aug. 3	Laurel Fork of Doe River.	do do	L. V. Branch	$4.30 \\ 5.19$	$ 28.3 \\ 30.0 $
Aug. 17 Oct. 5	do do	do do	E. W. Myers	5.50 5.67	15.0 9.0
Aug. 2	Gap Creek	At mouth, Tennessee	L. V. Branch	4.00	7.0
Oct. 4 Aug. 2	Buffalo Creek	do	E. W. Myers L. V. Branch.	$4.12 \\ 5.85$	$\frac{3.0}{20.0}$
Oct. 4	do	do	E. W. Myers	5.92	10.0
Aug. 3	Sinking Oreek	Elizabethton road, Tennes- see.	L. v. branch	ə. 13	5.0
July 19	Brush Creek	Near Carter, Tenn	L. V. Branch	3.75 6.77	$\frac{4.0}{10.03}$
Aug. 16 Sept. 24	do	do	E. W. Myers	$6.82 \\ 6.94$	$9.47 \\ 5.14$
				5.01	0.11

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Miscellaneous	discharge	measurements of Hiwassee	tributaries River.	of	Tennessee	River	above

Date.	Stream.	Locality.	Hydrographer.	Dis- charge.
1900.				Secft.
Aug. 20	Tellico River	Tellico Plains, Tenn	O. P. Hall	82.0
Ďo	Cane Creek	Belltown, Tenn	do	2.0
Do	Ball Play Creek	Tariffville, Tenn	do	2.2
Do	Citico Creek	Lillian, Tenn	do	17.2
Sept. 1	do	do	do	15.8
Aug. 20	Mulberry Creek	Ipe, Tenn.	do	5.5
Aug. 21	Little Tennessee River.	Chilhowee, Tenn	do	1,751.0
Sept. 1	do	do	do	2, 115.0
Aug. 21	Abrams Creek	do	do	40.2
Aug. 31	do	do	do	35.2
Aug. 22	Hesse Creek	Millers, Tenn	do	4.8
Aug. 23	Big Spring Creek	Tuckaleechee Cove, Tenn	do	4.3
Do	Near Prong of Little	do	do	29.5
Do	Main Prong of Lit-	do	do	92.6
Aug. 30		do		112.5
Aug. 24	Walden Creek	Henderson Springs, Tenn	do	26.1
Aug. 30		do	do	6.2
Aug. 24	Little Cove Creek	do.	do	2.5
Ďo	West Fork of Little	do	do	95.2
	Pigeon River.			
Aug. 25	ðo	Sevierville, Tenn	do	88.0
Aug. 29	do	do	do	51.5
Aug. 25	East Fork of Little Pigeon River.	do	do	178.4
Do	Middle Creek	do	do	1.0
Do	Bird Creek	Bird Creek, Tenn	do	3.0
Aug. 29	do	do	do	1.5
Aug. 25	Middle Fork of Lit-	Richison, Tenn	do	126.8
	tle Pigeon River.			1
Aug. 28	do	do	do	68.9
Aug. 27	East Fork of Little	East Fork, Tenn	do	10.3
Aug. 28	do	0b	ob	9.1
Ang. 27	Cosby Creek	Cosby, Tenn	do	23 5
Aug. 28	do	Bison, Tenn	do	27 4
Aug. 27	Big Pigeon River	do	do	453.8

Miscellaneous discharge measurements of Hiwassee River and its tributaries.

Date.	Stream.	Locality.	Hydrographer.	Gage height.	Dis- charge.
1900				Feet	Sec .ft
July 26	Choestoe Creek	Choestoe, Ga	W. E. Hall and		17.3
			H. G. Stokes.		
Do	Nottely River	do	do		46.8
July 27	Level Land Creek	do	do		29.5
Do	Stink Creek	Caldwell, Ga.			22.8
Do	Town Creek				55.6
Do	Arququan Creek		do		18.8
Do	Wolf Creek	Ploingrillo Co	do		20.0
July 20	Coore Crook	Coore Crook Georgia	do		29.0 00.e
Do	Nottoly River	Blairevilla Ga	do	1 60	505.1
July 20	Young Cone Creek	Near month Georgia	ob	1.00	81.2
Do	Ivy Log Creek	Ivy Log Ga	do		32.7
Do	Camp Creek	Camp Creek, Georgia	do		13 7
July 31	Nottely River	Thompson's bridge, Georgia	do	1.40	462.0
Do	Moccasin Creek	Ivy Log. Ga	do		12.8
Do	Rapier Creek	Ranger, N. C	do		22.0
Do	Nottely River		do	1.40	500.4
Aug. 1	Brasstown Creek	Brasstown, Ga.	do		94.4
Aug. 2	Long Bullet Creek	Twine, N. C	do		11.9
Do	Hog Creek	Hiwassee, Ga	do		15.0
Do	Bell Creek	do	do		20.6
Do	Hiwassee River	do	do		337.8
Aug. 3	Scataway Creek	Visage, Ga	do		3.2
Do	Hightower Creek	Osborn, Ga	do		73.0
Do.!	Fodder Creek	Hiwassee, Ga	do		19.0
Do	Owl Creek	do	do		12.3
Do	Mill Creek		do		22.3
Aug. 4	Centers Creek	mountain Scene, Ga			23.9
Do	High Shoals Creek				18.5

Miscellaneous discharge measurements of Hiwassee River, etc.-Continued.

Date.	Stream	Locality.	Hydrographer.	Dis- charge.
1900. Aug. 17 Sept. 4 Aug. 17 Do Sept. 4 Aug. 18 Do Sept. 3	Lost Cree': do Ellis Creek Joring Creek do Childers Creek Spring Creek Conasauga Creek do	Near Reliance, Tenn do do At mouth, Tennessee do Near Reliance, Tenn Springtown, Tenn Mecca, Tenn Near Jalapa, Tenn	O. P. Hall do do do do do do do do do	$\begin{array}{c} Sec.\text{-ft.} \\ 7.7 \\ 6.5 \\ 2.0 \\ 6.8 \\ 4.3 \\ 6.8 \\ 4.0 \\ 25.0 \\ 20.2 \end{array}$

Miscellaneous discharge measurements of Toccoa (Okoee)^a River and its tributaries.

Date.	Stream.	Locality.	Hydrographer.	Dis- charge.
1900. July 19 Do Do July 20 Do July 23 Do July 23 Do July 24 Do Do Do Do	Weavers Creek Starr Creek German Creek Persimmon Creek Toccoa River Nontootly Creek. Big Creek Skeinah Creek Coopers Creek Toccoa River Suches Creek Suches Creek Toccoa River	GEORGIA. Near Blueridge	W. E. Hall and H. G. Stokes. do do do do do do do do do do do do do	$\begin{array}{c} secft.\\ 10.0\\ 13.6\\ 13.0\\ 26.0\\ 8.0\\ 384.2\\ 126.0\\ 52.0\\ 15.6\\ 46.0\\ 102.0\\ 102.0\\ 27.0\\ 22.0\\ 19.6\\ \end{array}$
Aug. 15 Do Aug. 16 Do Sept. 4 Sept. 5	Sylco Creek Greasy Creek Okoee (Toccoa) River. Bakers Creek Greasy Creek Okoee (Toccoa) River.	TENNESSEE. At mouth do Parksville do Above mouth of Rock Creek. Parksville.	O. P. Hall do do do do do do do	3.8 11.3 734.0 4.0 5.1 667.0

a After entering Tennessee the Toccoa is known as Okoee River.

OLENTANGY RIVER AT COLUMBUS, OHIO.

This station was established November 22, 1898, at the Fifth avenue bridge, Columbus. It is described in Water-Supply Paper No. 36, page 175. The observations of river heights are made under the general direction of Prof. C. N. Brown, of the Ohio State University. Records of measurements for 1899 will be found in the Twenty-first Annual Report, Part IV, page 169. A number of measurements made in the latter part of 1899 were not published in the foregoing reports, and they, together with a measurement made on March 8, 1900, are given in the following list:

October 13, 1899: Gage height, 1 foot; discharge, 7 second-feet. October 13, 1899: Gage height, 1 foot; discharge, 7 second-feet. Octoben 14, 1899: Gage height, 1 foot; discharge, 7 second-feet.

OHIO.

October 20, 1899: Gage height, 1 foot; discharge, 7 second-feet. November 17, 1899: Gage height, 1.20 feet; discharge, 44 second-feet. December 2, 1899: Gage height, 1.10 feet; discharge, 15 second-feet. March 8, 1900: Gage height, 5.42 feet; discharge, 5,039 second-feet.

Daily gage height, in feet, of Olentangy River at Columbus, Ohio, for 1900.

have been as a second s												
Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1	1.80	1.80	2.90	2.25	1.40	1.50	1.10	1.35	1.60	1.00	1.00	1.70
2	1.80	1.80	2.80	2.60	1.40	1.90	1.10	1.20	1.60	1.00	1.00	1.50
ð	1.80	1.80	2.80	2.15	$1.40 \\ 1.40$	1.90 1.90	1 10	1 10	1.40	1.00	1.00	$1.00 \\ 1.25$
5	1.80	1.80	2.90	1.90	1.40	1.60	1.10	1.10	1.20	1.00	1.00	1.20
6	1.80	1.80	5.55	1.75	1.30	1.40	1.10	1.10	1.10	1 00	1.00	1.20
7	1.80 1.80	1.70	6.90	1.60 1.30	1.30	1.35	1.10 1.10	1.10	1.00	1.00 1.00	1.00	1.20 1.20
9	1.80	3.85	3.65	1.30	1.25	1.20	1.10	1.10 1.10	$1.00 \\ 1.00$	1.00	1.00	1.30
10	1.80	3.10	3.15	1.35	1.20	1.20	1.10	1.10	1.00	1.00	1.00	1.30
11	1.80	2.15	2.80	1.40	1.20	1.20	1.10	1.10	1.00	1.00	1.00	1.30
12	2.35	1.80	2.60	140 150	1.20	1.20 1.20	1.10	$1.10 \\ 1.00$	1.00	1.00 1.00	1.00	1.30 1.36
14	2.50	3.90	1.95	1.50	1.20	1.20	1.10	1.00	1.60	1.00	1.00	1.60
15	2.25	3,00	1.75	1.50	1.20	1.20	1.19	1.00	1.00	1.00	1.00	1.60
16	2.50	1.90	1.60	1.50	1.20	1.45	1.10	1.00	1.00	1.00 1.00	1.00	1.60
16 18	2.55	1.80	$1.00 \\ 1.60$	2 20	1.20	$1.00 \\ 1.35$	1.10	1.00	1.00	1 00	1.00	1.00 1.55
19	2.20	1.80	1.60	2.90	1.20	1.20	1.30	1.00	1.00	1.00	1.00	1.30
20	3.40	1.80	1.60	2.30	1.20	1.10	1.25	1.35	1.00	1.00	1.00	1.30
21	$\frac{4.00}{2.20}$	1.80	1.60 1.60	1.90	1.20 1.20	1.10 1.10	1.10	1.20	1.00	1.00 1.00	1.400	1.30 1.90
23	2.40	3.20	1.60	3, 65	1.20	1.10	1.00	1.20	1.00	1.10	1.10	1.20
24	1.95	2.55	1.60	3.05	1.20	1.20	1.00	2.15	1.00	1.05	1.20	1.20
25	1.80	1.80	1.60	2.60	1.20	1.20	1.05	1.80	1.00	1.00	1.80	1.20
20	$1.80 \\ 1.80$	1.80	1.00	2.05	1.20	$\frac{1.20}{1.20}$	1.30 1.40	2.00	1.00 1.00	1.00	2.50	1.20 1.20
28	1.80	2.50	1.60	1.50	1.20	1.30	1.90	3.20	1.00	1.00	2.20	1.20
29	1.80		1.60	1.40	1.20	1.30	1.80	3.00	1.10	1.00	1.80	1.20
30	1.80		1.60	1.40	1.30	1.25	1.70	2.20	1.00	1.00 1.00	1.70	1.20
	1.80		1.40		1.99		1.00	1.69		1.00		1.20

SCIOTO RIVER AT COLUMBUS, OHIO.

This station was established November 22, 1898, at the Grandview avenue bridge, Columbus. It is described in Water-Supply Paper No. 36, page 176. The observations are made under the general direction of Prof. C. N. Brown, of the Ohio State University. Measurements for the year 1899 will be found in the Twenty-first Annual Report, Part IV, page 170. A number of measurements made in the latter part of 1899 were not published in the foregoing reports, and they, together with the measurements made in 1900, are given in the following table:

Discharge measurements of Scioto River at Columbus, Ohio.

Date.	Gage height.	Discharge.	Date.	Gage height.	Discharge.
Oct. 13, 1899 Oct. 14, 1899 Oct. 20, 1899 Nov. 17, 1899 Nov. 30, 1899	Feet. 9.10 9.10 9.20 9.30 9.30	Secft. 14 13 14 33 37	Dec. 2, 1899 Jan. 18, 1900 Feb. 15, 1900 Mar. 7, 1900	Feet. 9.40 11.90 12.90 17.37	Secft. 43 1,328 2,391 8,581

Daily gage height, in feet, of Scioto River at Columbus, Ohio, for 1900.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oet.	Nov.	Dec.
1	9.75	10.45	12.55	12.15	10.20	9.60	9.40	9.90	9.45	9.25	9.15	10.60
2	9.70	10.40	13.00	12.70	10.15	9.60	9.40	9.60	9.30	9.20	9.15	10.35
3	9.65	10.35	12.60	12.90	10.10	9.70	9.30	9.45	9.30	9.20	9.10	10.15
*	9.00	10.30	12.00	11 85	10.00	9.90	9.00	9.30	9.20	9.00	9.20	10.05
9 ß	9.00	10.30	16 65	11.00	0.00	9.90	9.20	9.29	9.20	9.20	9.10	9,95
7	9.50	10.35	17 50	11 10	9.90	9.95	9.20	9.20	9 20	9.00	9.20	9.80
8	9.55	11 50	16 05	10.85	9.90	9.90	9 20	9.10	9.15	9.00	9.20	9.80
9	9.60	14.00	15.80	10.65	9.90	9.80	9.20	9.15	9.10	9.20	9.05	9.85
30	9.60	13.25	15.15	10.50	9.80	10.20	9.10	9.25	9.10	9.20	9.10	9.90
11	9.70	12.75	14.40	10.40	9.90	10.45	9.10	9.10	9.00	9.20	9.10	9.75
12	9.75	12.15	13.60	10.40	9.90	10.30	9.10	9.00	9.00	9.40	9.10	9.65
13	11.30	13.55	12.95	10.60	9.90	10.05	9.10	9.00	8.95	9.65	9.15	9.65
14	11.40	13.75	12.30	10.95	9.80	9.75	9.15	8.90	8.90	9.50	9.20	9.45
15	11.35	12.95	11.80	10.90	9.70	9.55	9.10	9.00	8.95	9.35	9.20	9.40
10	11.45	12.50	11.40	10.80	9.70	9.45	9.10	9.25	9.00	9.30	9.20	9.40
11	12.15	11.45	10.90	10.75	9.10	9.45	9.20	9.15	9.00	9.20	9.20	9.40
10	11.90	10.90	10.90	19.65	9.10	9.00	9.10	9.00	9.20	9.20	9.20	9.40
20	13 25	10.85	11.00	12.00	9.00	9.00	9.05	0.50	8.00	9.10	0.25	0.35
91	15.00	10.00	11.19 11.10	11 65	9.00	0.40	0.30	9.00	8 80	8 10	9.30	9.30
22	14 20	11 90	10.85	12.50	0.60	9 40	0.20	9.50	8.80	9 10	9.30	9.35
23	13.55	12.65	10.70	12.15	9.60	9.30	9.10	9.30	8.70	9.20	9,80	9,40
24	13.15	13.05	10.60	11.90	9.55	9.00	10.15	9.80	8.75	9.20	10.15	9.40
25	12.35	12.30	10.60	11.60	9.50	9.00	9.40	10.05	8.85	9.20	10.65	9.40
26	11.70	12.85	10.80	11.15	9.50	9.05	9.15	10.30	8.90	9.15	11.70	9.35
27	11.10	12.95	10.80	10.80	9.50	9.10	9.05	10.25	8.90	9.00	11.55	9.30
28	10.70	12.65	10.75	10.55	9.50	9.25	9.10	10.05	8.90	9.05	11.50	9.30
29	10.65		10.80	10.45	9.50	9.50	9.10	9.95	9.05	9.05	11.40	9.35
30	10.50		10.90	10.35	9.50	9.35	10.40	9.80	9.30	9.00	11.10	9.35
31	10.85		10.80		9.50		9.90	9.10		9.10		9.35
						-						

MAUMEE RIVER NEAR WATERVILLE, OHIO.

This station was established on November 19, 1898, by H. A. Pressey and B. H. Flynn. It is located at the highway bridge near Waterville, the gagings being made on the downstream side. It is described in Water-Supply Paper No. 36, pages 178 and 179, where will also be found the results of the discharge measurements made during 1899. During 1900 the following measurements were made by B. H. Flynn:

July 26: Gage height, 3.30 feet; discharge, 2,143 second-feet.

November 24: Gage height, 4.85 feet; discharge, 6,784 second-feet.

Daily gage height, in feet, of Maumee River near Waterville, Ohio, for 1900.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1	4.00	3.70	3.60	5.40	3, 55	3, 80	2.70	3.30	2,45	2.10	2.20	4.35
2	4.25	3.60	3.50	5.40	3.30	4.05	2.60	3.25	2.50	2.20	2.20	4.70
3	4.45	3.60	3.55	5.55	3.30	4.45	2.65	3.10	2.35	2.30	2.30	4.45
4	4.50	3.85	3.80	5.60	2.90	4.45	2.75	2.90	2.25	2.20	2.35	4.25
5	4.50	4.05	4.35	5.75	2.80	4.15	2.80	2.80	2.20	2.25	2.40	4.05
6	4.70	4.25	4.75	5.90	2.80	3.90	2.80	2.70	2.10	2.15	2.55	3.80
7	4.35	4.40	5.35	5.50	2.90	3.40	2.50	2.50	2.20	2.15	2.55	3.75
8	3.90	4.80	5.95	4.90	3.05	3.30	3.20	2.40	2.20	2.10	2.40	3.45
9	3.50	5.55	7.90	4.25	3.10	3.50	3.80	2.40	2.15	2.20	2.35	3.55
10	3.05	6.60	11.40	3.85	3.00	3.70	4.25	2.65	2.20	2.20	2.30	3.10
11	2.90	7.05	11.80	3.55	2.90	3.80	4.30	2.75	2.20	2.20	2.30	3.00
12	3.35	6.65	10.10	3.60	2.70	4.35	4.05	2.45	2.10	2.35	2.25	-3.00
13	-3.50	6.25	8.60	3.95	2.70	4.60	3.65	2.30	2.15	2.40	2.20	3.00
14	3.50	6.55	7.85	4.00	2.70	4.35	3.60	2.30	2.10	2.50	2.25	3.20
15	3.55	6.40	6.80	4.20	2.80	4.00	3.50	2.20	2.10	2.40	2.30	2.95
16	3.40	6.75	6.10	4.35	2.65	3.90	3.40	2.20	2.10	2.35	2.35	2.85
17	3.30	6.05	6.00	4.60	2.60	3.55	3.35	2.10	2.10	2.30	2.35	2.80
18	3.20	4.80	5.65	5.00	2.50	3.50	3.70	2.10	2.10	2.20	2.45	2.70
19	3.55	3.40	6.80	5.35	2.60	3.30	3.60	2.10	2.10	2.10	2.65	2.65
20	4.05	3.35	6.75	5.05	2.65	3.20	3.50	2.10	2.10	2.15	3.45	2.55
21	4.80	3.50	6.55	5.00	2.65	3.00	3.65	2.10	2.10	2.15	4.15	2.50
22	5.05	3.50	6.70	5.75	2.50	-3.00	3.80	2.25	2.10	2.10	4.80	2.50
23	5.30	3.60	6.70	6.10	2.55	3.35	3.75	2.65	2.10	2.20	5.25	2.50
24	5.00	3.85	6.85	6. (X)	2.50	3.85	3.36	3.00	2.10	2.20	5.35	2.50
25	5.20	4.05	6.65	5.70	2.50	4.50	3.10	3.20	2.10	2.20	5.40	2.35
26	5.10	4.45	6.40	5.25	2.45	4.55	3.30	3.30	2.10	2.20	5.30	2.40
20	4.65	4.10	6.30	4.85	2.40	4.15	3.15	3,15	2.10	2.20	5.25	2.70
28	4.35	3.85	5.90	4.20	2.45	3, 65	2.95	2.75	2.10	2.20	4.95	2.75
20	4.00		5.35	3.90	2.60	3.15	2.90	2.70	2.10	2.20	4.55	2.55
0U	3.60		5.00	3.80	3.10	2.15	2. 75	2.45	z.10	2.20	4.20	2.70
	3.60		5.25		3.70		3.15	2.40		2.20		2.70

OHIO.

SANDUSKY RIVER NEAR MEXICO, OHIO.

This station was established November 17, 1898, at the highway bridge near Mexico, about 40 miles above Fremont, Ohio. It was abandoned November 17, 1900. Only one measurement was made in 1899, when, at a gage height of 5.40 feet, the discharge was 1,386 secondfeet. During 1900 the following measurements were made by B. H. Flynn:

July 25: Gage height. 1.75 feet; discharge, 133 second-feet. November 22: Gage height, 1.80 feet; discharge, 225 second-feet.

Daily gage height, in feet, of Sandusky River near Mexico, Ohio, for 1900.

Day.	Jan.	Feb.	Mar	Apr.	May.	June.	July.	Aug.	Sept.	Oet.	Nov.
$\begin{array}{c} 1 \\ 2 \\ 2 \\ 3 \\ 4 \\ 5 \\ 6 \\ 7 \\ 8 \\ 8 \\ 9 \\ 10 \\ 12 \\ 10 \\ 12 \\ 13 \\ 14 \\ 15 \\ 16 \\ 17 \\ 18 \\ 19 \\ 20 \\ 21 \\ 22 \\ 23 \\ 24 \\ 24 \\ 23 \\ 23 \\ 24 \\ 25 \\ 26 \\ 27 \\ 27 \\ 28 \\ 27 \\ 28 \\ 29 \\ 30 \\ 31 \\ 31 \\ 31 \\ 31 \\ 31 \\ 31 \\ 31$	$\begin{array}{c} 1.55\\ 1.4\\ 1.2\\ 1.1\\ 1.1\\ 1.1\\ 1.1\\ 1.0\\ 0\\ 2.35\\ 4.20\\ 4.40\\ 4.8\\ 4.5\\ 5.22\\ 7.8\\ 1\\ 3.79\\ 7.8\\ 1\\ 3.8\\ 1\\ 2.6\\ 3\\ 2.0\\ 2.1\\ \end{array}$	$\begin{array}{c} 2.0\\ 1.9\\ 1.8\\ 2.7\\ 1.8\\ 9\\ 1.8\\ 2.7\\ 7.5\\ 3.5\\ 5.8\\ 3.5\\ 5.8\\ 3.2\\ 2.7\\ 4.4\\ 4.6\\ 2\\ 2.2\\ 4.4\\ 4.4\\ 4.9\\ 3.9\\ 7\\ 7.5\\ 3.5\\ 5.8\\ 1.4\\ 3.9\\ 7\\ 1.8\\ 2.2\\ 1.4\\ 1.0\\ 1.8\\ 1.0\\ 1.0\\ 1.0\\ 1.0\\ 1.0\\ 1.0\\ 1.0\\ 1.0$	$\begin{array}{c} 4.4\\ 4.6.6\\ 3.3\\ 3.8.6\\ 5.5.5\\ 5.8.5\\ 10.91\\ 1.4.5\\ 8.8.6\\ 1.8.8\\ 2.2.2\\ 3.2.2\\ 3.2.2\\ 3.2.2\\ 2.2.2\\ 3.2.2\\ 2.2.2\\ 3.2.2\\ 2.2.2\\$	$\begin{array}{c} 3.2 \\ 6.0 \\ 3.4 \\ 0.0 \\ 4.0 \\ 4.0 \\ 4.0 \\ 3.2 \\ 2.2 \\ 3.2 \\$	$\begin{array}{c} 1.9\\ 1.8\\ 1.8\\ 1.6\\ 1.6\\ 1.6\\ 1.6\\ 1.7\\ 1.6\\ 1.5\\ 1.4\\ 1.4\\ 1.4\\ 1.3\\ 1.2\\ 2\\ 1.1\\ 1.1\\ 1.4\\ 1.5\\ 6\\ 1.7\\ 1.6\\ 1.5\\ 1.6\\ 1.7\\ 1.6\\ 1.6\\ 1.7\\ 1.6\\ 1.7\\ 1.6\\ 1.6\\ 1.7\\ 1.6\\ 1.6\\ 1.7\\ 1.6\\ 1.6\\ 1.7\\ 1.6\\ 1.6\\ 1.7\\ 1.6\\ 1.6\\ 1.7\\ 1.6\\ 1.6\\ 1.6\\ 1.7\\ 1.6\\ 1.6\\ 1.6\\ 1.7\\ 1.6\\ 1.6\\ 1.6\\ 1.6\\ 1.6\\ 1.6\\ 1.6\\ 1.6$	$\begin{array}{c} 1.9\\ 2.1\\ 2.7\\ 2.4\\ 1.9\\ 0\\ 2.2\\ 1\\ 2.1\\ 1\\ 2.1\\ 1\\ 2.1\\ 1\\ 1.8\\ 1\\ 1.5\\ 1.5\\ 1.5\\ 1.5\\ 1.6\\ 1.6\\ 1.5\\ 1.6\\ 1.6\\ 1.6\\ 1.6\\ 1.6\\ 1.6\\ 1.7\\ 1.6\\ 1.6\\ 1.6\\ 1.6\\ 1.6\\ 1.7\\ 1.6\\ 1.6\\ 1.6\\ 1.6\\ 1.6\\ 1.6\\ 1.6\\ 1.6$	$\begin{array}{c} 1.6\\ 1.5\\ 1.4\\ 1.3\\ 1.2\\ 1.2\\ 1.2\\ 1.2\\ 1.2\\ 1.2\\ 1.2\\ 1.2$	$\begin{array}{c} 2.0\\ 1.9\\ 1.7\\ 1.6\\ 1.1\\ 1.1\\ 1.1\\ 1.0\\ 1.0\\ 1.0\\ 1.0\\ 1.0$	$\begin{array}{c} 1.7\\ 1.6\\ 1.5\\ 1.4\\ 1.3\\ 1.1\\ 1.2\\ 1.2\\ 1.2\\ 1.3\\ 1.4\\ 1.7\\ 1.5\\ 1.4\\ 1.3\\ 1.4\\ 1.3\\ 1.4\\ 1.3\\ 1.4\\ 1.0\\ 1.0\\ 1.0\\ 1.0\\ 1.0\\ 1.0\\ 1.0\\ 1.0$	$\begin{array}{c} 1.3\\ 1.4\\ 1.6\\ 1.5\\ 1.5\\ 2.2\\ 2.1\\ 1.9\\ 1.5\\ 1.5\\ 1.5\\ 1.5\\ 1.5\\ 1.5\\ 1.5\\ 1.5$	0.99 88 88 88 80 90 90 100 100 100 100 100 100 100 100

a Gage destroyed.

SANDUSKY RIVER AT FREMONT, OHIO.

This station, which was established November 18, 1898, by H. A. Pressey and B. H. Flynn, is at the bridge of the Lake Shore Railroad at Fremont. It is described in Water-Supply Paper No. 36, page 181. One measurement was made in 1899—gage height, 2.32 feet; discharge, 1,784 second-feet. The following measurements were made during 1900:

July 26: Gage height, 2.75 feet; discharge, 2,316 second-feet. November 23: Gage height, 1.60 feet; discharge, 463 second-feet. Daily gage height, in feet, of Sandusky River at Fremont, Ohio, for 1900.

		1										
Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1	0.95	0.65	1.95	1.20	0.60	1 50	0.85	1.40	1.00	1 10	1 00	1 75
2	. 95	. 65	2.70	1.70	. 50	1.60	. 85	1.30	. 95	1.20	1.05	1.70
3	. 95	. 60	2.75	1.70	. 40	1.65	. 85	1.20	. 95	1.10	. 90	1.60
4	, 90	. 65	2.85	1.60	. 40	1.70	. 80	1.10	1.00	1.05	. 80	• 1.35
5	. 90	. 65	2.90	1.60	. 40	1.60	. 75	. 90	1.50	1.10	. 85	1.30
6	. 90	. 75	4.65	1.50	. 30	1.50	. 65	. 80	1.65	1.20	. 80	1.35
3	. 90	. 10	0. 1 0 e 00	1.20 1.00	. 30 20	1.00	. 10	. 80	1.00	1.20 1.10	. 89	1.20
0	. 90	3.30	5.70	1.00	. 00	1.00	. 00	. 80	1.00	1.10	. 00	1 30
10	. 90	2.80	5.30	. 80	. 40	1.50	.95	. 85	1.70	1.15	. 90	1.25
11	.95	2.15	3, 55	. 80	.40	1.60	. 90	. 65	1.70	1.10	.85	1.20
12	1.05	1.45	2.35	1.35	. 30	1.50	. 75	. 60	1.65	1.05	. 85	1.15
13	1.40	3.30	1.65	1.50	. 30	1.40	. 75	. 75	1.65	1.05	. 75	1.10
14	1.95	3.35	1.55	1.40	. 30	1.50	. 65	. 75	1.70	. 90	. 80	1.05
15	$\frac{2.00}{2.15}$	$\frac{2.70}{1.95}$	1.80	1.30	. 30	1.40	. 50	. 80	1.65	. 85	- 75	1.00
10	$\frac{3.10}{2.15}$	1.00	1.40	1.20	. 40	1.20 1.20	. 00	. 10	1.70	. 00	. 10	1.10 1.20
18	2.05	1.10	1.20	2 15	. 30	1 20	60	1 10	1.70	1 00	. 00	1 15
19	1.75	.95	1.40	2.20	.20	1.20	. 55	1.05	1.65	. 85	. 80	1.10
20	2.00	. 85	1.30	1.80	. 20	1.10	. 40	1.15	1.75	. 80	1.10	1.00
21	3.20	. 85	1.10	1.60	. 20	1.10	. 40	2.75	1.80	, 90	1.50	-1.00
22	2.95	1.35	1.10	1.45	. 10	1.20	. 40	2.55	1.75	. 95	1.70	1.05
23	2.40	1.50	1.00	1.85	. 25	1.20	. 90	2.20	1.60	1.10	1.80	1.10
24	1, 80	1.50	. 90	1.90	1 10	1.10	1.00	2 75	1.40	1.00	2 10	1.00
96	1.35	1.70	. 90	1.45	1.10	1.10	2 35	3.05	1 10	1 10	2.30	1.05
27	1.25	1.65	. 90	1.05	1.30	. 90	1.75	2.80	1.00	1.05	2.60	1.15
28	. 85	1.80	1.10	. 90	1.40	. 95	1.70	2.00	1.10	1.00	2.20	1.10
29	. 70		1.10	. 70	1.40	. 90	1.50	1.50	1.00	. 90	2.00	1.00
30	. 70		1.00	. 70	1.40	. 80	1.50	1.45	1.00	. 85	1.90	1.00
31	. 70		1.00		1.40		1.50	1.00		1.00		. 90
								(

SENECA RIVER AT BALDWINSVILLE, NEW YORK.

Records of the stations on the New York streams which belong to the coast drainage will be found in Water-Supply Paper No. 47, pages 42 to 80. A number of the streams of that State on which stations have been established belong to the Great Lakes drainage, and following the geographic arrangement which has been determined upon for the publication of the records contained in these reports, the records for these stations are inserted on this and the following pages. The methods employed in the gaging of these streams is discussed on pages 37 to 41 of Water-Supply Paper No. 47, where will also be found a list of the gaging stations in New York State, a table of the currentmeter measurements made during 1900, a table of the drainage areas, and other interesting information.

The gaging station on Seneca River at Baldwinsville is described in Water-Supply Paper No. 36, page 183. This river drains the central lake region of New York. The outlets of Otisco, Skaneateles, and Owasco lakes are crossed by Erie Canal, and a portion of their flow is intercepted for water-supply purposes. Water from Lake Erie feeds the main canal as far as Port Byron. Some of this water is discharged into Seneca River, and thence is delivered into Lake Ontario.

The upper reaches of Seneca River are canalized, forming the Cayuga and Seneca canals, while dams on the lower portion admit of slackwater navigation, forming a part of Oswego Canal. During the summer but little water flows over the dam at Baldwinsville. In times of low water the mills are allowed to run a certain number of hours during the day, or until the supply accumulated in the pond above the dam is drawn down to a certain level. The water is diverted through three power canals, and is conducted to the water wheels by means of short lateral channels. The loss through leakage of wheel gates, flumes, and penstocks is considerable.

The following current-meter measurements were made at Baldwinsville:

June 11, 1900:	Second-feet.
Amos race	193.5
Oswego Canal	504.5
Main stream at railroad bridge 1	1,183.0
Total flow	1,881.0
South Side Canal	475.0
Oswego Canal	317.0
Amos race	127.0
Total flow	919.0

The Baldwinsville record shows a relatively low run-off for this stream. The 1900 record is withheld for the present, additional measurements to determine leakage, etc., being needed.

CHITTENANGO CREEK AT BRIDGEPORT, NEW YORK.

This station is described in Water-Supply Paper No. 36, page 184. A current-meter measurement was made at a highway bridge below the inflow of Butternut Creek, near Bridgeport, on June 16, 1900, and the total flow of Chittenango Creek at that point was found to be 95 second-feet. The stage of the stream, as shown by the record kept at Bridgeport, was uniform for several days. The mean flow, as computed from the gage readings, was 95 second-feet for June 15 and There is no opportunity to measure separately the discharge 16. through the turbines or the leakage of the dam at this station, and an allowance of 15 second-feet has been made for the leakage of the dam and the dike leading to the old sawmill. The sawmill, situated on the left side of the stream, runs very irregularly. The water wheels are old, and the penstocks leak considerably. On June 16 a current-meter measurement was made in the headrace leading to the sawmill. The water wheels were running, and the flow was found to be 14.4 second-feet.

The relatively low run-off from the watershed of Chittenango Creek, as shown in the accompanying tables, may be attributed to the diversion of a portion of the flow to supply the summit level of Erie Canal.

State dams are located on the main stream at Chittenango, and on its two tributaries, Limestone Creek and Butternut Creek. Cazenovia Lake, Erieville, De Ruyter, and Jamesville reservoirs impound storage, by which the flow is regulated to some extent. Water is also diverted from Tioghnioga River, entering the Orville feeder through Limestone Creek.

Additional information in regard to this creek will be found in Water-Supply Paper No. 47, pages 37 to 41, in a paper entitled "Methods employed in the gaging of New York streams during the year 1900."

Daily discharge, in second-feet, of Chittenango Creek at Bridgeport, New York, for 1898.

Day.	Sept.	Oct.	Nov.	Dec.	Day.	Sept.	Oct.	Nov.	Dec.
1		180	562	<u>427</u>	18	a 53	284	500	a 605
3		171	434	348	20	139	320	a 675	669
4	<i>(a)</i>	172	358	a385	21	117	269	728	793
5 6		$156 \\ -309$	$\frac{379}{a,385}$	$\frac{471}{414}$	22	$\frac{111}{115}$	463 a 465	623 593	1,155 1 293
Ĩ		235	331	404	24	135	487	569	1,401
8		$a \frac{204}{130}$	359 386	320 261	25	$\frac{a85}{142}$	472	$\frac{490}{442}$	a1,075 857
10		165	474	265	27	149	867	$a\overline{465}$	726
11	(a)	194	1,339 1,571	a 465	28	214	972	523	541
13		190	$a^{1,371}_{1,265}$	454	30	194	a565	413	630
14		181	921	442	31		519		630
16	82	a 335	694	450 472	Mean	129	344	612	597
17	116	299	615	619					

[Drainage area, 307 square miles.]

a Sunday.

Daily discharge, in second-feet, of Chittenango Creek at Bridgeport, New York, for 1899.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1	$\begin{array}{c} a 515 \\ 571 \\ 636 \\ 636 \\ 737 \\ 1, 067 \\ 1, 282 \\ a1, 133 \\ 724 \\ 486 \\ 238 \\ 497 \\ 3849 \\ 738 \\ a1, 280 \\ 1, 280 \\ 1, 280 \\ 1, 280 \\ 1, 280 \\ 1, 280 \\ 1, 280 \\ 3996 \\ 3392 \\ 3396 \\ 3398 \\ 3398 \\ 3322 \\ a385 \\ 348 \\ 335 \\ a488 \\ 568 \\ 348 \\ 358 \\ 348 \\ 358 \\ 348 \\ 358 \\ 348 \\ 35$	$\begin{array}{c} 520\\ 484\\ 485\\ a385\\ 336\\ 342\\ 385\\ 385\\ 385\\ 385\\ 385\\ 385\\ 385\\ 385$	$\begin{array}{c} 632\\ 473\\ 385\\ 520\\ a1,260\\ 1,331\\ 1,475\\ 1,069\\ 859\\ a565\\ 659\\ a565\\ a565\\ 1,066\\ 1,061\\ 970\\ 6655\\ 634\\ 526\\ a565\\ 736\\ 766\\ 962\\ 1,061\\ 1,345\\ 1,061\\ 1,345\\ 766\\ 962\\ 1,061\\ 1,345\\ 1,061\\ 1,345\\ 1,061\\ 1,075\\ 1,061\\$	$\begin{array}{c} & 837 \\ & 837 \\ & 795 \\ & 752 \\ & 861 \\ & 866 \\ & 864 \\ & 857 \\ & 1, 369 \\ & 1, 306 \\ & 1, 274 \\ & 1, 306 \\ & 1, 274 \\ & 1, 339 \\ & 1, 339 \\ & 1, 221 \\ & 1, 339 \\ & 861 \\ & 1, 339 \\ & 861 \\ & 1, 221 \\ & 861 \\ & 627 \\ & 527 \\ & 476 \\ & 331 \\ & 279 \\ & 359 \\ & 331 \\ & 279 \\ & 359 \\ & 331 \\ & 279 \\ & 350 \\ & 350 $	$\begin{array}{c} 447\\ 447\\ 357\\ 310\\ 172\\ 172\\ 157\\ a95\\ 172\\ 237\\ 172\\ 237\\ 172\\ 237\\ 172\\ 237\\ 172\\ 237\\ 172\\ 237\\ 172\\ 237\\ 195\\ 282\\ 281\\ 285\\ 252\\ 252\\ 252\\ 252\\ 252\\ 252\\ 252$	$\begin{array}{c} 426\\ 346\\ 234\\ a105\\ 184\\ a229\\ 229\\ 224\\ 192\\ 147\\ a70\\ 169\\ 192\\ 182\\ 109\\ 182\\ 109\\ 184\\ 192\\ a70\\ 152\\ 84\\ 92\\ 100\\ 124\\ 134\\ a70\\ 109\\ 84\\ 91\end{array}$	$\begin{array}{c} 116\\ a55\\ 97\\ 113\\ 132\\ 99\\ 99\\ 123\\ 132\\ 132\\ 132\\ 169\\ 262\\ 271\\ 169\\ 99\\ 99\\ 99\\ 99\\ 99\\ 99\\ 99\\ 101\\ 221\\ 169\\ 101\\ 221\\ 102\\ 102\\ 102\\ 102\\ 102\\ 102$	$\begin{array}{c} 84\\ 79\\ 169\\ 126\\ 134\\ a70\\ 125\\ 125\\ 125\\ 125\\ 125\\ 125\\ 125\\ 126\\ 125\\ 103\\ 87\\ 76\\ 6\\ 103\\ 87\\ 76\\ 6\\ 91\\ a25\\ 5\\ 120\\ 109\\ 96\\ \end{array}$	$\begin{array}{c} 81\\ 499\\ a455\\ 133\\ 81\\ 76\\ 96\\ 996\\ a151\\ 974\\ 996\\ 996\\ 996\\ 992\\ 225\\ 889\\ 996\\ 906\\ 88\\ 89\\ 996\\ 906\\ 117\\ 39\\ 84\\ 49\\ 49\\ 112\\ 916\\ 996\\ 976\\ 97$	$\begin{array}{c} a \ 75 \\ 90 \\ 91 \\ 990 \\ 800 \\ 841 \\ 895 \\ a \ 45 \\ 107 \\ 117 \\ 1101 \\ 101 \\ 101 \\ 101 \\ 101 \\ 101 \\ 101 \\ 300 \\ 388 \\ 457 \\ 415 \\ 600 \\ 688 \\ 433 \\ 85 \\ 457 \\ 415 \\ 600 \\ 688 \\ 433 \\ 577 \\ 485 \\ 425 \\ 600 \\ 688 \\ 433 \\ 577 \\ 600 \\ 688 \\ 433 \\ 577 \\ 600 \\ 688 \\ 433 \\ 577 \\ 600 \\ 688 \\ 435 \\ 577 \\ 600 \\ 688 \\ 435 \\ 577 \\ 600 \\ 688 \\ 485 \\ 688 \\ 485 \\ 688 \\ 485 \\ 688 \\ 485 \\ 688 \\ 485 \\ 688 \\ 485 \\ 688 \\ 485 \\ 688 \\ 485 \\ 688 \\ 485 \\ 688 \\ 485 \\ 688 \\ 485 \\ 688 \\ 485 \\ 688 \\ 485 \\ 688 \\ 485 \\ 688 \\ 488 \\ 688 \\ 485 \\ 688 \\ 6$	$\begin{array}{c} 60\\ 145\\ 145\\ 145\\ 160\\ a165\\ 228\\ 128\\ 128\\ 128\\ 128\\ 128\\ 128\\ 128$	$\begin{array}{c} 1133\\127\\a143\\159\\149\\151\\166\\a169\\185\\a18\\211\\2326\\395\\344\\a355\\395\\344\\a355\\395\\334\\466\\a355\\395\\334\\466\\133\\229\\334\\210\\229\\233\\261\\139\\223\\34\\261\\229\\244\\244\\244\\244\\244\\244\\244\\244\\244$
Mean	637	551	1,360 893	921	229	161	141	96	76	65	95	281

				2.								
Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1	161	467	774	a 1,230	266	106	a 38	107	91	67	108	a608
2	247	581	671	1,394	268	80	91	108	a53	108	100	355
3	242	581	605	1,447	245	a70	- 99	68	75	67	82	356
£	263	a595	a 595	1,447	245	134	33	80	79	75	a 34	288
5	318	580	792	1,342	237	125	82	a 38	55	75	67	865
6	379	507	776	1,327	a215	132	153	103	67	91	70	1,330
1	a215	002	892	1,318	295	117	132	40	55	a 38	13	1,100
8	3/1	1,437	591	$a_{1,365}$	287	105	a 130	40	- 33	100	105	a1,035
9	292	1 909	285	$1, \pm 0.0$ 1, 955	295	105	100	+9	a 33	103	130	090
10	301	1,010	011	1,200	- 241) 9/2/2	116	20	40	60	114		220
11	202	21,115	162	1,014	407	108	62	00	72	110	102	252
19	. 373	1 187	441	600	a 165	67	66	38	37	79	105	480
11	a 275	1,200	383	675	247	ae	a 80	120	57	a 12	106	456
15	373	1,100	367	a 595	259	95	42	89	65	98	98	a 452
16	422	1, 188	383	544	283	95	96	92	a 15	94	106	425
17	504	985	375	667	268	a 70	160	83	70	89	105	497
18	599	a 275	a355	620	280	117	136	96	62	63	a 45	538
19	971	187	603	1,703	237	73	101	a53	53	77	153	421
20	1,540	189	589	801	a215	107	136	63	111	57	169	423
21	a1,485	242	603	880	222	92	134	83	70	a 42	136	431
22	1,445	987	788	a785	166	69	a 105	66	117	86	139	a 358
23	1,195	992	782	860	171	78	129	124	a 53	58	111	378
24	1,074	1,005	1,003	770	136	a 43	100	- 11	79	100	113	844
25	422	a 790	a1,115	577	118	116	101	92	62	96	a 45	1,231
26	429	706	788	436	98	81	252	a 38	84	94	1,255	452
21	761	591	707	300	a 40	13	172	10	99	75	1,953	606
28	a 190	591	982	268	150	100	117	95	117	a 33	1,835	618
29	022		1,090	a 215 270	92	155	a 105	86	108	70	1,272	a 113
90	312		1,221 1.251	370	117	11	124	40	(1 33	90	1,105	215
	012		1,551		90		199	00		66		941
Mean	561	725	697	911	207	93	110	73	68	81	327	562

Daily discharge, in second-feet, of Chittenango Creek at Bridgeport, New York, for 1900.

a Sunday.

ONEIDA CREEK AT KENWOOD, NEW YORK.

A description of this station, which is located at the silk-mill dam in Kenwood, will be found in Water-Supply Paper No. 36, page 186. There is no leakage of the dam, and only a slight leakage of the flume and head gates, which has been taken at 2 second-feet. The flow over a wasteway near the mill is computed by means of Francis's formula. A second spillway in the canal bank near the dam has a broad, irregular crest, over which water sometimes flows. A discharge curve for this spillway has been prepared, using coefficients from the Cornell experiments for dam with a broad, flat crest.¹

Current-meter measurements were made to check the calculated flow at Kenwood, with the following results:

June 1, 1900:	Second	d-feet.
Total flow at Oneida Castle	-	36.6
Flow over dam, crest gage reading 0.15 foot	. 19	
Flow through turbine, 11.75 feet head, one-third gate	. 15	
Flow over wasteway near mill	. 1	
Assumed leakage	2	
Total flow (computed) September 17, 1900:	-	37.0
Total flow measured in headrace	-	20.0
Flow through turbine, one-third gate	. 15	
Assumed leakage	. 2	
Total flow (computed)	-	17.0

¹See Proc. Am. Soc. C. E., March, 1900, p. 282.

At Oneida is a State dam diverting water for the supply of the summit level of Erie Canal. No measurements of diversion to the feeder have been made. Practically the entire flow of Oneida Creek, less leakage of the dam, is taken for this purpose during the low-water season.

Additional information in regard to this creek will be found in Water-Supply Paper No. 47, pages 37 to 41, in a paper entitled "Methods employed in the gaging of New York streams during the year 1900."

Daily discharge, in second-feet, of Oneida Creek at Kenwood, New York, for 1898. [Drainage area, 59 square miles.]

$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	Day.	Oct. (a) 112 58 60 58 a 45 23 23 23 23 23 25 1 110 a 100 102	Nov. 900 72 700 65 600 588 511 2055 2714 172 a 1400 119 1233 1066	$\begin{array}{c c} \hline Dec. \\ \hline \\ $	Day. 18	Oct. 75 75 75 70 1100 a 100 120 180 180 180 180 100 100 80 100 80 100 80 100 80 100 80 80 80 80 80 80 80 80 80	$\begin{array}{c} \text{Nov.} \\ \hline 102\\ 115\\ a \ 121\\ 123\\ 109\\ 123\\ 100\\ 86\\ 66\\ 93\\ a \ 77\\ 61\\ 76\\ 64\\ \hline \\ 105\\ \end{array}$	Dec.
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a Sunday.

Daily discharge, in second-feet, of Oneida Creek at Kenwood, New York, for 1899.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Oet.	Nov.	Dec.
1	a 76	50 65	115	122	71 e0	46	18	a 15	144	23
3	108	80	115	$\frac{115}{116}$	60	36	20	21		a25
4	$210 \\ 300$	72	112	96 122	$59 \\ 54$	a 35 31	$\frac{20}{30}$	21 21	66	27
6	160	50	22	131	55	31	34	21	44	29
8	$a \frac{143}{114}$	50 50	$\frac{202}{168}$	$\frac{166}{334}$	$a 48 \\ 53$	$\frac{31}{24}$	21 41	$a\frac{24}{18}$	$\frac{40}{26}$	25
9	95 80	35	128	$a \frac{260}{214}$	53	24	$a_{\frac{40}{51}}$	24	26	41
11	138	100	90	196	54 54	a 25	26	21	26	97
12	$\frac{180}{205}$	$a74 \\ 56$	$a 149 \\ 235$	496 416	59 59	$\frac{26}{26}$	24 24	24 24	$\frac{a 27}{28}$	70 70
14	273	37	157	406	$a\frac{48}{52}$	26	24	24	26	91
16	183	42	140	$a^{341}{260}$	60 60	41	$a \overset{21}{20}$	25 a 19	26	
17 18	$135 \\ 101$	39 41	144 133	196 166		$\frac{36}{a,30}$	31 28	25 25	$\frac{26}{22}$	a 30 30
19	75 65	a 40	a 157	166	66	26	26	24	a 25	97
20	67	160	$135 \\ 135$	136	a^{91}_{80}	$^{51}_{26}$	20	25	24	92
223	$a57 \\ 55$	365 232	157 254	$a \frac{110}{102}$	82 63	$\frac{26}{31}$	a^{25}_{a25}	a_{25}^{25}	26 24	80 68
24	75	147	183	96 01	54	31	26	25	26	a 55
26	60	a 161	a 170	110	43	$31 \\ 31$	21	25	a^{25}_{25}	35
27	55 42	$\frac{232}{122}$	$157 \\ 123$	$110 \\ 91$	a^{43}_{71}	$\frac{31}{24}$	$\frac{20}{21}$	24 25	$\frac{26}{26}$	39 27
29	a 43		230	86	$108 \\ 76$	24 21	18	(1 26 20	$\frac{26}{26}$	34 97
31	75		$165 \\ 165$		59		21	31		a 34
. Mean	117	93	157	183	62	30	25	23	33	60

a Sunday. NOTE.—No record for August and September.

	Day.	Jan.	Mar.	Apr.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
-12345678901123456789011232234256789011234567890112345678900122234256789001222234256789000000000000000000000000000000000000		$\begin{array}{c} & & & \\$	$\begin{array}{c c} & & & & \\ & & & & \\ & & & & \\ & & & & $	$\begin{array}{c} (a) \\ 290 \\ 208 \\ 154 \\ 149 \\ 313 \\ 382 \\ (a) \\ 220 \\ 220 \\ 220 \\ 200 \\ 195 \\ 212 \\ 201 \\ 201 \\ 201 \\ 201 \\ 204 \\ (a) \\ 224 \\ 177 \\ (a) \\ 224 \\ 177 \\ (a) \\ 234 \\ 160 \\ 134 \\ 160 \\ 134 \\ 102 \\ 85 \\ 88 \end{array}$	$ \begin{array}{c} 19 \\ 18 \\ (a) \\ 23 \\ 20 \\ 17 \\ 23 \\ 452 \\ (a) \\ 30 \\ 23 \\ 152 \\ (a) \\ 30 \\ 23 \\ 17 \\ 17 \\ 17 \\ 17 \\ 17 \\ 17 \\ 17 \\ 1$	$ \begin{array}{c} (a) \\ (a) \\ 325 \\ (a) $	$\begin{array}{c} & & \\$	$\begin{array}{c} 15\\ (a)\\ 15\\ 15\\ 15\\ 15\\ 15\\ 16\\ 19\\ 14\\ (a)\\ 15\\ 15\\ 15\\ 15\\ 15\\ 15\\ 15\\ 15\\ 15\\ 15$	$\begin{array}{c} 17\\ 17\\ 17\\ 14\\ 14\\ 17\\ 17\\ 14\\ 14\\ 17\\ 17\\ 16\\ 35\\ 18\\ 8\\ 17\\ 17\\ 19\\ 9\\ a\\ 13\\ 25\\ 23\\ 25\\ 19\\ 9\\ 19\\ 19\\ 19\\ 19\\ 19\\ 19\\ 19\\ 19\\$	$\begin{array}{c} 266\\ 266\\ 16\\ 16\\ 16\\ 16\\ 16\\ 16\\ 16\\ 16\\ 23\\ 33\\ 33\\ 25\\ 222\\ 222\\ 22\\ 23\\ 50\\ 50\\ 50\\ 46\\ 43\\ 353\\ 25\\ 25\\ 23\\ 23\\ 23\\ 25\\ 25\\ 23\\ 23\\ 25\\ 25\\ 25\\ 25\\ 25\\ 25\\ 25\\ 25\\ 25\\ 25$	$\begin{array}{c} 711\\ a\ 63\\ 55\\ 126\\ 193\\ 160\\ 138\\ a\ 149\\ 160\\ 138\\ a\ 169\\ 108\\ 108\\ 108\\ 88\\ a\ 128\\ 108\\ 108\\ 88\\ a\ 128\\ 158\\ 160\\ 138\\ 168\\ 138\\ 168\\ 138\\ 168\\ 138\\ 168\\ 168\\ 168\\ 118\\ 108\\ 118\\ 108\\ 118\\ 108\\ 118\\ 108\\ 10$
29 30 31		46 45 47	$ \begin{array}{r} 128 \\ 128 \\ 118 \end{array} $	(a) 61	19 26	$(a) \\ 31 \\ 28$	$28 \\ 20 \\ 19$	$a \frac{15}{11} \\ 17$	$ \begin{array}{c} 19 \\ 19 \\ 23 \end{array} $	225 168	96 a 97 98
	Mean	92	148	198	21	38	19	16	19	91	127

Daily discharge, in second-feet, of Oneida Creek at Kenwood, New York, for 1900.

WEST BRANCH OF FISH CREEK AT MCCONNELLSVILLE, NEW YORK.

This station is described in Water-Supply Paper No. 36, page 186. During the summer the flashboards are on the dam, and Francis's formula is used in computing the flow. At other times a discharge curve derived from Cornell experiments is used. Three water wheels are in use. Two are 54-inch wheels built by the Camden Water Wheel Works, and are usually run ten hours a day, at a nearly constant gate opening.

Current-meter measurements of the discharge of one of these wheels under light and heavy load gave the following results:

June 2, 1900, discharge, 43.2 second-feet. September 6, 1900, discharge, 51.8 second-feet.

Ten dams located on this stream furnish power to 17 mills.

Additional information in regard to this creek will be found in Water-Supply Paper No. 47, pages 37 to 41, in a paper entitled "Methods employed in the gaging of New York streams during the year 1900."

a Sunday. NOTE.—No record for February and May.

Daily discharge, in second-feet, of West Branch of Fish Creek at McConnellsville, New York, for 1898.

[Drainage area, 187 square miles.]

Day.	Sept.	Oct.	Nov.	Dec.	• Day.	Sept.	Oct.	Nov.	Dec.
1	 100 90 96 47	$\begin{array}{c} 137\\ a50\\ 111\\ 121\\ 130\\ 137\\ 131\\ 122\\ a65\\ 102\\ 81\\ 87\\ 124\\ 134\\ 134\\ 597\\ a360\\ \end{array}$	$\begin{array}{c} 365\\ 319\\ 292\\ 155\\ a120\\ 146\\ 138\\ 135\\ 557\\ 1,562\\ 997\\ a700\\ 734\\ 434\\ 514\\ \end{array}$	$\begin{array}{c} 237\\ 245\\ 217\\ 182\\ 195\\ 182\\ 196\\ 182\\ 199\\ 180\\ a140\\ 199\\ 186\\ 212\\ 212\\ 157\end{array}$	18	a 50 98 81 55 55 332 a 360 197 231 181 181 147 	$\begin{array}{r} 346\\ 227\\ 190\\ 172\\ 467\\ a700\\ 750\\ 624\\ 434\\ 1,097\\ 871\\ 686\\ a440\\ 464\\ \hline 333\\ \end{array}$	$\begin{array}{c} 365\\ 365\\ 365\\ a 370\\ 371\\ 220\\ 216\\ 300\\ 329\\ a 255\\ 299\\ 251\\ 172\\ 384\\ \end{array}$	$\begin{array}{c} a 120 \\ 187 \\ 157 \\ 190 \\ 287 \\ 317 \\ 468 \\ a 390 \\ 285 \\ 285 \\ 225 \\ 170 \\ 120 \\ 120 \\ 210 \end{array}$
17	47	562	365	147	110011	101	000		210

a Sunday.

Daily discharge, in second-feet. of West Branch of Fish Creek at McConnellsville, . New York, for 1899.

Day.	Jan.	Feb.	Mar.	Apr.	May.	Day.	Jan.	Feb.	Mar.	Apr.	May.
1	$\begin{array}{c} a \ 120 \\ 126 \\ 194 \\ 261 \\ 391 \\ 396 \\ 396 \\ 395 \\ 422 \\ 502 \\ 502 \\ 5873 \\ 873 \\ 873 \\ a \ 795 \\ 785 \end{array}$	$\begin{array}{c} 228\\ 183\\ 183\\ 172\\ a\ 120\\ 212\\ 156\\ 156\\ 147\\ 136\\ 117\\ a\ 80\\ 99\\ 132\\ 94\\ 131\\ 148\end{array}$	$\begin{array}{r} 402\\ 402\\ 438\\ 595\\ a\ 700\\ 856\\ 583\\ 546\\ a\ 700\\ 1,178\\ 1,178\\ 1,178\\ 1,178\\ 792\\ 752\end{array}$	$\begin{array}{c} 586\\ a\ 520\\ 601\\ 601\\ 601\\ 591\\ 689\\ 1,557\\ a2,110\\ 1,690\\ 1,724\\ 2,055\\ 2,440\\ 2,920\\ 3,040\\ a2,410\\ 1,724\\ 1,790\\ 2,920\\ 3,040\\ a2,410\\ 1,790\\ 2,920\\ 3,040\\ a3,040\\ 3,$	$\begin{array}{c} 273\\ 313\\ 243\\ 184\\ 184\\ 184\\ a\ 120\\ 183\\ 154\\ 154\\ 183\\ 243\\ 194\\ a\ 120\\ 189\\ 189\\ 189\\ 189\end{array}$	13 19 20 21 22 23 24 25 26 27 28 29 30 31 Mean	$\begin{array}{c} 615\\ 615\\ 530\\ 495\\ a \ 360\\ 314\\ 425\\ 350\\ 325\\ 338\\ a \ 225\\ 278\\ 278\\ 278\\ 278\\ 278\\ 435\\ \end{array}$	a 153 a 120 183 198 258 338 438 438 438 403 403 403 206	$\begin{array}{r} 567\\ a\ 485\\ 505\\ 433\\ 442\\ 443\\ 442\\ 442\\ 442\\ a\ 360\\ 552\\ 599\\ 599\\ 599\\ 599\\ 599\\ 599\\ 648\\ \end{array}$	$1, 644 \\ 1, 434 \\ 1, 174 \\ 1, 085 \\ 1, 045 \\ a 940 \\ 664 \\ 564 \\ 470 \\ 366 \\ 366 \\ 366 \\ 366 \\ a 220 \\ \hline \\ 1, 206 \\ 1, 206 \\ \hline$	$\begin{array}{c} 189\\ 374\\ 374\\ 374\\ 374\\ a 255\\ 303\\ 244\\ 194\\ 189\\ 189\\ 174\\ 134\\ a 50\\ 7000\\ 455\\ 483\\ \hline 239\\ \end{array}$

a Sunday.

NEW YORK.

Day.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1	278	96	a 52	60	48	69	157	16(
2	255	78	78	60	$a\overline{10}$	54	144	117
3	232	a 28	78	60	20	49	133	144
4	243	70	52	58	50	65	93	12:
5	243	58	52	$\alpha 10$	50	65	132	257
6	a205	70	96	50	60	64	104	203
7	225	70	80	50	60	a34	143	169
8	165	88	a 52	50	28	39	217	150
9	185	90	78	50	a10	39	180	117
.0	185	a52	78	58	50	59	163	118
1	185	78	78	50	50	55	110	13
<i>i</i>)	172	70	70	a 30	60	54	107	127
3	a105	60	70	56	60	64	107	12
4	148	68	60	168	60	a36	132	13
5	140	78	a10	98	58	71	112	91
.6	135	86	60	61	a10	76	101	8
7	125	a52	60	64	* 60	76	86	12
8	120	72	70	48	60	46	78	11:
9	106	58	60	a 19	55	86	144	9
0	a75	78	60	30	55	71	207	- 58
21	104	70	60	50	196	$\alpha 60$	224	5(
h)	104	70	a10	50	239	106	239	28
3	96	68	60	60	a 128	116	$2^{j}6$	3.
4	96	a28	50	55	87	218	231	3.
5	86	70	64		87	148	196	3.
6	86	70	60	a 19	66	134	- 330	3.
7	a38	70	76	60	66	140	355	5.
8	82	70	26	134	66	a 128	223	5.
9	71	70	a 36	76	50	150	187	3.
0	52	68	60	50	a58	150	179	31
	88		60	50		206		58
Mean	143	68	60	57	65	88	168	. 99

Daily discharge, in second-feet, of West Branch of Fish Creek at McConnellsville, New York, for 1900.

a Sunday.

OSWEGO RIVER ABOVE MINETTO, NEW YORK.

Oswego River is formed by the junction of Oneida and Seneca rivers at Three River Point. It has extensive natural storage in Oneida Lake, which covers an area of 80 square miles, and in the Finger Lakes of central New York, which it drains. Certain tributary lakes serve also as reservoirs for the water supply of the middle division of Erie Canal, and a portion of the flow is diverted for this purpose.

Oswego River has been canalized by the construction of dams, affording slack-water navigation on a part of the stream. In all there are 7 dams on the river. Surplus water at the State dams supplies power to numerous mills situated on the adjacent banks. Lateral canals and locks carry boats around the dams and connect with backwater from the next succeeding dam in each instance.

In establishing a gaging station it was impossible to measure the entire stream in a single channel, since, in order to avoid slack water from dams, it was necessary to select a site where the river is paralleled by the canal. A cable station was established September 14, 1900, 3 miles above Minetto, and below the State dam at Battle Island. A gage board was placed one-fourth mile upstream from the cable. A

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weight gage is used, being suspended from a framework projecting over the water beyond the low-water margin. The position of the weight when the gage reads zero has been determined with reference to a fixed bench mark. The gage is so arranged that the readings are reversed, thus, 8.00 would be extreme low water, and when the water rises the readings are less. Morning and evening readings are taken, usually twelve hours apart, and the average of the two readings is given in the table.

A current-meter measurement was made at the cable station on September 15. The mean gage height during the measurement was 5.4 feet, and the discharge 1,677 second-feet. This does not include the diversion through Oswego Canal. The lowest water on this stream usually occurs Sundays, due to the stopping of water wheels and the consequent refilling of ponds.

In this connection reference may be made to the gaging record which was maintained by the United States Board of Engineers on Deep Waterways on Oswego River at the Oswego Falls dam from November, 1898, to May, 1899, inclusive. A description of this station will be found in Water-Supply Paper No. 36, page 188.

The drainage areas tributary to Oswego River at the different gaging stations are as follows:

Drainage areas of Oswego River.

	oqu	are mne
At mouth		5,002
At high dam near Oswego		5,000
At cable station		4,990
At Fulton		4,916

Additional information in regard to this river will be found in Water-Supply Paper No. 47, pages 37 to 41, in a paper entitled "Methods employed in the gaging of New York streams during the year 1900."

Daily gage height, in feet, of Oswego River above Minetto, New York, for 1900.

Day.	Sept.	Oct.	Nov.	Dec.	Day.	Sept.	Oct.	Nov.	Dec.
1 2 3 4 5 6 7 9 10 12 13 14 15 16	5. 72 5. 70 6. 50	$\begin{array}{c} 5.65\\ 5.65\\ 5.58\\ 5.55\\ 5.55\\ 5.55\\ 5.55\\ 5.55\\ 5.55\\ 5.30\\ 5.55\\ 5.30\\ 5.55\\ 5.30\\ 5.55\\ 5.30\\ 5.55\\ 5.30\\ 5.52\\ 0.552\\ 5.30\end{array}$	$\begin{array}{c} 4.90\\ 4.90\\ 5.75\\ 5.75\\ 5.00\\ 4.75\\ 4.66\\ 4.70\\ 4.80\\ 4.90\\ 5.50\\ 4.50\\ 4.60\\ 4.55\\ 4.55\\ 4.55\\ 4.55\end{array}$	$\begin{array}{c} 0.70\\ .85\\ .50\\ c.65\\ c.1.50\\ c.1.50\\ c.1.50\\ c.1.35\\ c.1.10\\ c.1.35\\ c.85\\ c.85\\ c.85\\ c.85\\ c.30\\ c.30\\ c.30\\ \end{array}$	17. 18. 19. 20. 21. 22. 23. 24. 25. 26. 27. 28. 29. 30. 31.	$\begin{array}{c} 6.20\\ 5.65\\ 5.82\\ 5.52\\ 5.55\\ 5.28\\ 5.60\\ 6.10\\ 5.82\\ 5.60\\ 5.72\\ 5.72\\ 5.70\\ 5.75\\ \end{array}$	$\begin{array}{c} 5.08\\ 5.15\\ 5.18\\ 4.70\\ 6.15\\ 5.485\\ 5.55\\ 5.55\\ 5.55\\ 5.50\\ 5.50\\ 6.45\\ 5.05\\ 4.95\\ 4.80\end{array}$	$\begin{array}{c} 4.55\\ 5.70\\ 4.75\\ 4.25\\ (a)\\ (a)\\ (a)\\ (a)\\ (a)\\ (b)\\ b3.05\\ 2.25\\ 1.60\\ 1.15\\ .60\\ \end{array}$	$\begin{array}{c} c \ 0.\ 35\\ c \ .\ 70\\ c \ .\ 50\\ c \ .\ 45\\ c \ .\ 45\\ c \ .\ 35\\ c \ .\ 40\\ c \ .\ 15\\ c \ .\ 25\\ .\ 10\\ .\ 40\\ .\ 55\\ .\ 80\\ \end{array}$

a No record.

b New weight gage.

c Used board gage.

NEW YORK.

OSWEGO RIVER AT HIGH DAM NEAR OSWEGO, NEW YORK.

A description of this station, with tables of daily gage heights, will be found in Water-Supply Paper No. 36, page 189. The dam is of masonry, with a crest 365.5 feet long. Flashboards are maintained on the dam during the greater part of the year. When flashboards are on, the flow over the dam has been computed by means of Francis's formula, with a constant coefficient of 3.33. In estimating the flow over the dam when flashboards are removed a discharge curve has been prepared, using coefficients in the weir formula derived from Cornell University experiment No. 3,¹ and taking into consideration irregularities in the profile of the crest.

A headrace at the left end of the dam diverts water to supply power to an electric-light plant and to the waterworks pumping station. There are 8 water wheels in use. A regular record of the run of the water wheels has not been kept, and the diversion for this purpose has been estimated from current-meter measurements in the headrace.

• Date.	Working head on wheels.	Meas- ured dis- charge.
June 12	Feet. 13	Secfeet.
September 15	14	59%

Power diversions at high dam near Oswego.

Three pairs of water wheels, which were in operation when the foregoing measurements were made, are run twenty-four hours a day. Taking the average of the foregoing measurements and adding 105 second-feet for the additional pair of wheels, the diversion for water power has been estimated at 450 second-feet, as a round figure.

The flow from an auxiliary spillway in the end of the headrace has been calculated from the weir formula, using coefficients derived by Bazin for a dam having a similar crest section.

Some uncertainty attaches to the record at this station during the spring months, owing to the carrying away of the flashboards by high water at dates not definitely ascertained.

In the accompanying tables of monthly and daily mean flow no allowance has been made for diversion to Oswego Canal.

Additional information will be found in Water-Supply Paper No. 47, pages 37 to 41, in a paper entitled "Methods employed in the gaging of New York streams during the year 1900."

¹ See Proc. Am. Soc. C. E., March, 1900, p. 274.

Day.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1	12,150		4,500	1,470	a 3,300	1,760	1,200	1,020	3,000
2	11,550	a7,750	4,620	2,650	3,300		1,150	1,260	3,000
3	10,950	7,550	4,620	2,480		1,760	(<i>a</i>)	1,430	-3,220
4	(a)	7,250	4,620	(a)	3,300	1,670	850	1,430	2,950
ð	10,950	7,220		2,480	3,050	(a)	1,050	1,320	a3,850
6	10,950	6,900	a 4, 520	2,400		1,000	1,100	1,430	
7	10,950	6,800	4,520	2,150	2,810	1,760	1,100	(a)	3,620
8	10,750		4,400	1,700	(a)	1,670	910	1,370	3,620
9	11,000	a 0,000	4,400	1,820	2,100	1.840	9,20	1,450 1,570	4,400
10	a11 550	6,400	4,400	1,700	2,000	1,070	(a)	1,370 1,420	4,000
11	11,550	$0, \pm 00$	4,400	9 200	2,000	(1)	1,050	1,400 1,420	4,000
1.%	11,550	6 975	a.1. 100	1 670	2 330	1 100	1,050	1,400 1,220	(0)
10	10,950	6 150	4 170	1.480	2,450	1,200	1 220	a 1 320	4,000
15	10,950	0,100	4 170	1.670	(a)	1,150	1 100		5,500
16	10,750	a.6.275	4 150	1.830	2 150	1,200	1,150	1 630	5 400
17	10,100	6 275	3,900	1,830	2 500	1 020	(a)	1,750	5 500
18	a10.200	6.275	3,770	(a)	2,500	970	750	1,850	5,500
19	9,800	5,900	0,	1.980	2.330	(<i>a</i>)	1,100	$\hat{2},020$	(a)
20	9,550	5,650	a 3,610	1.900	2,330	850	1,300	2.020	5.500
21	9,350	5,650	3,070	1,980	2,250	880		(a)	5,100
<u>,,,</u>	9,250		3,070	1,830	(a)	920	1,220	2,120	4,780
23	9,100	a5,520	2,870	1,900	2,000	920	1,220	1,850	4,780
24	8,900	5,250	2,870	1,670	1,900	920	(a)	2,120	3,630
25	a 8,100	5,520	2,670	(<i>a</i>)	1,900	1,100	1,150	2,120	-3,200
26	8,100	5,250		2,480	1,850	(a)	1,100	2,120	(a)
27	8,100	5,150	a2,870	2,660	1,850	1,020	1,050	2,870	3,850
28	8,100	5,150	2,550	2,660	1,850	1,350	1,100	(a)	3,420
29	8,060		2,970	3,500	(a)	970	1,020	3,650	• 2,900
30	[-7,500]	a5,500	2,720	3,170	1,760	1,050	1,020	3,650	3,620
31		5,500		3,240	2,160		(a)		3,430
Mean	10,048	6,166	3,801	2,174	2,370	1,244	1,076	1,821	4,168

Daily discharge, in second-feet, of Oswego River at high dam near Oswego, New York, for 1897.

a Sunday.

Daily discharge, in second-feet, of Oswego River at high dam near Oswego, New York, for 1898.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1	2,600 (a)	$5,520 \\ 5,520$	$10,350 \\ 10,200$	9,400 9,250	(a) 8,250	6,430	$2,780 \\ 2,780$	780 780	$1,480 \\ 1,480$	a1,470	$3,250 \\ 3,250$	3, 900 3, 900
3	$ \begin{array}{r} 3,000 \\ 2,600 \\ 3,320 \\ 3,000 \end{array} $	$5,520 \\ 5,000 \\ 5,000$	9,900 9,600 9,250	(a) 8,750 8,620	8,080 8,850 8,900	6,540 5,630 $\alpha 5,630$ $\alpha 5,630$	(a)	$780 \\ 1,200 \\ 950 \\ 0.50$	$1,400 \\ a950 \\ 1,330 \\ 1,200$	$1,470 \\ 1,400$	3,250 3,250	$a_{4,700} \\ 3,900 \\ 3,900$
8 9	3,430 3,220 (a)	(a) 5,520 5,000 5,100	(<i>a</i>) 8,820 8,960 8,960	8,080 7,800 7,500	$ \begin{array}{c} 8,900 \\ 9,120 \\ (a) \\ 9,120 \end{array} $	5,630 5,630 4,880 4,880	1,480	$a850 \\ 1,070 \\ 850$	1,260 1,260 1,770 1,770	1,330	$\begin{array}{c} a_{5}, 050 \\ 3, 220 \\ 3, 050 \\ 3, 250 \end{array}$	$ \begin{array}{r} 3, 400 \\ 3, 900 \\ 3, 350 \\ 3, 150 \end{array} $
$\begin{array}{c} 10\\ 10\\ 11\\ 12\\ \end{array}$	2,820 2,820 3,220	5,100 5,100 5,100 6,550	8,960 9,100 9,400	(a) 7,370 6,950	8,960 8,670	$ \begin{array}{r} 4,650 \\ 4,650 \\ a4,650 \end{array} $	$a1,200 \\ 1,200 \\ 1,330$	850 770 680	1,770 a1,480 1,630	1,260 1,200 1,200	4,800 4,900	a3,260 3,260
$ \begin{array}{c} 13 \\ 14 \\ 15 \\ 1e \end{array} $	4,770 5,100 5,500	(a) 5,400 5,100	(a) 10,200 10,350 10,250		${}^{8,370}_{a8,370}_{a8,280}$	$ \begin{array}{r} 4,400 \\ 4,170 \\ 4,100 \end{array} $	$1,950 \\ 1,950$	$ \begin{array}{c} 630 \\ a900 \\ 680 \\ 850 \end{array} $	1,770 1,480 1,330 1,220	860	a5,800 5,800 5,530	2,300 2,100 2,470 2,50
10 17 18 19	$\begin{array}{c} (a) \\ 6,280 \\ 5,400 \\ 5,400 \end{array}$	4,000 6,750 7,080 7,080	10,350 10,550 10,350 10,350	(a) 6,080 5,900	7,370	$3,770 \\ 3,770 \\ a3,500$	(a)	850 850 850	1,350 1,760 a1,200 1,200	$ \begin{array}{c} 1,770 \\ 1,630 \\ 1,770 \\ 1.770 \\ \end{array} $	5,200 5,200 5,050	$a_{2,850}$ $a_{2,650}$
20 21 22 22	$5,400 \\ 6,150 \\ 6,400$	(a) 7,350 7,350 7,350	(a) 10,350 10,550	6,700 6,000 5,900	(a)	3,500 3,500 3,300 2,200			1,200 1,200 1,200 1,200	1,950 1,950	a5,050 5,050 5,300	2,850 3,900 4,580
23 24 25 26	(a) 7,880 7,880 5,950	$ \begin{array}{r} 7,750 \\ 8.150 \\ 8,150 \\ 8.150 \end{array} $	10,550 10,350 10,350 10,200	$ \begin{array}{c} 5,900 \\ (a) \\ 8,080 \\ 8,500 \end{array} $	6,850	3,300 3,170	(a)	850 760 830 1 480	1,200 1,330 a1,400 930	a2,460 2,850 2,850 2,920	$ \begin{array}{r} 4,900 \\ 4,770 \\ 4,770 \end{array} $	5,650 a 5,800 5,800
27 28 29	$\begin{array}{c} 7,600\\ 6,550\\ 6,550\end{array}$	(<i>a</i>) 7,880	(a) 9,880 9,880		(<i>a</i>)	2,970 2,850		$ \begin{array}{c} 1,320 \\ a1,320 \\ 1,320 \\ 1,320 \end{array} $	$ \begin{array}{r} 1,330 \\ 1,200 \\ 1,330 \end{array} $	$\begin{array}{c} 3,050 \\ 3,360 \\ 3,250 \end{array}$	$a4,580 \\ 4,580 \\ 4,350$	5,650 4,770 5,300
30 31	(a) 4,550 4,902		9,750 9,750	8,850	6,550	2,780	(a)	1,130 1,130 	1,400	(a) 3,250	4,350	5,300
mean	4,890	0,238	9,898	1,518	5, 161	- 8, 331	1,854	925	1, 517	2,018	4,452	5,899

a Sunday.

NEW YORK.

Day.	Jan.	Feb.	Mar.	Ap r .	May.	June.	July.	Aug.	Sept.	Oet.	Nov.	Dec.
1	a4,450	2,750	3,670	6,300	9,600	5,370	1.000	580	670	a540	1,100	650
·····	4,020	2,310	3,900	(a) e ==0	9,600	5, 510	$a_{1,000}$	050	a150	060	1,100 1,250	090
ð	4,400	4,100	4,120	6,550	9,000	a1 400	1 000	650	580	580	1,000	080
5	0,110	a2 370	a5 050	6,550	8 650	4 400	1,000	0.00	540	580	a1 350	780
6	5.580	2.370	850	6, 550	0,000	3,950	780	a650	510	580	1.500	980
7	4.700	2,300	5,300	6,300	a6,950	1.230	650	650	650		1,350	900
8	a4,100	1,070	4,800		8,080	1,000		545	540	(a)	930	980
9	3,250	530	4,580	a8,530	7,520	780	a1,000	650		540	1,350	
10	3,050	630	4,580	8,250	6,960		900	580	a2,670	540	980	a1,360
11	3,250			8,530	6,960	a900	1,000	650	510	540		1,100
12	3,250	a630	a5,050	8,800		900	780		450	540	a1,350	1,980
13	3,900	1,630	5,050	8,800	0.170	1 720	780	a380	520	480	1 100	1,100
14		1,950	4,800	8,550	ab, 150	1,800	690	540	630	510	1,100	1,500 1,500
10	α 3, 330	2,510	4,900	a0 590	0,100	1,800	~000	080 650	450	(<i>a</i>) 510	980	1.900
10	5,000	2,000	3,030	ao, 550	6 420	1,000	720	650	(a)	450	980	a2 500
18	5 280	2, 10	4, 500	8,530	6 490	a1 800	650	450	(u)	580	900	2 500
19	5,170	a2. 470	a4 580	8 250	6 150	1 650	650	100	480	460	a1 100	2,700
20	5 280	2 750	4 580	8,530	0,100	1,650	650	a450	540	540	980	2,500
21		2.850	4,700	7.670	a6.150	1,500	580	540	450	010	1.100	2,700
22	a4.780	3.260	.,	.,	6,150	1.500		650	480	a650	980	2,500
23	4.780	3.260	5,050	a7.550	6,150	1,230	$\alpha 650$	580		650	980	
24	4,580	3,260	4,900	7,200	6,150		650	540	a450	650		a2,500
25	5,050			6,820	5,630	a1,500	580	580	540	580		2,500
26	5,180	a3,910	a5,650	6,820	5,400	1,800		580	540	540	(a)	1,500
27	2,300	3,800	5,650	6,680		1,500	650	a540	540	650	980	1,500
28	3,050	3,800	5,550	6,820	a5,400		580	540	540		980	1,120
29	a2,300	•••••	6,550		5,400	780		990	540	a900	980	1 780
30	2,650		6,830	a9,900	5,400	720	a580	800		650	780	1,820
	2,650		0,830		5,400		580	690		650		(a)
Mean	4,252	2,475	4,874	7,684	6,754	2,002	748	612	615	585	1,095	1,612

Daily discharge, in second-feet, of Oswego River at high dam near Oswego, New York, for 1899.

a Şunday.

Daily discharge, in second-feet, of Oswego River at high dam near Oswego. New York, for 1900.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1	$1,820 \\ 1,360$	2,880 2,880	$4,140 \\ 1,970$	$a11,600 \\ 12,250$	$11,480 \\ 11,150$	4.880 4,880	$a_{2,000} \\ 1,840$	650 720	a650	720 780	$1,220 \\ 1,220$	a7,450
3	1,360	ad 800	3,930	12,250 12,250	10,550	a4,650	1,060	980	650	780	980	6,950
5	1,500	3.700	4.600	12,200 12,600	9,600	$\frac{4}{3}, \frac{150}{980}$	2.150	a780	650	780	1.220	8,530
6		3,250	4,600	12,600	a8,980	3,980	3, 500	650	720		1,220	8,800
7	a1,820	3,700	4,800		8,980	3,980		650	720	a900	1,220	9,130
8	1,820	5,050	4,600	a17,550	9,900	4,180	a650	720		900	1,500	9,130
9	2,150	5,300	4,600	16,800	8,980	3,500	580	650	a720	900	1,220	a8,250
10	1,820			16,450	8,670	a3.300	460	650	650	900	1,650	8,530
11	1,820	a5, 550	a4, 140	16,040	8,670	3,300	580	650	650	900	(a)	7,700
12		1,900	4, 550	16,040	8,080	3,080	510	a650	580	980	<i>a</i> 1, 500	1,700
10	41.070	0. 520	4,140	10,040	(<i>a</i>)	3,080	910	090			1 500	6,200
15	1 070	6 200	4,000	a15 320	7 800	9,000	0780	080	990	220	1,500	0,400
16	1,810	6 850	4,000	14 940	7 250	A, 000	790	580	a650	780	1,500	a5 880
17	1,000	6,050	1,110	14 940	7 250	a3 500	780	650	580	780	1,000	4 850
18	2.720	$\alpha 6.050$	a3.930	14,600	6.950	2.880	780	0.00	580	980	a1.500	6 120
19	3.250		4.140	14.250		2,700	780	a650	580		1.500	5.880
20		5,050	4,140	14,600	a6, 420	2,700	780	720	780	780	1.650	5,880
21	a6,320	5,050	4,600		6,420	2,500		650	780	a780	1.820	5,880
	6,600	5,350	5,300	a14,250	5,900	2,320	a780	650		780	1,650	
23	6,320	4,600	5,550	13,850	6,420		720	580	a780	980	1,650	a6,660
24	5,800		6,600	13,850	5,900	a2,320	720	580	550	900		6,120
25	5,550	a1,970	a6,320	12,780	5,530	1,840	900		720	780	a2,880	-6,400
26	2,880	1,360	6,600	12,450	5,150	2,000	780	a720	780	900	5,050	6,400
A4		2,880	6,600	12,450	a5, 150	2,000	720	580	780		5,800	6,400
20	2 700	1,820	0,850	-19 100	-3,100	2,000	- 720	580		a900	5,800	6,120
20	3,700		6,010	11 700	4,880	2,000	0080	550		980	0,850	
31	3, 100		0,0.0	11,780	4,000	2,000	650	000	0120	980	0,850	40,880
							000	000		990		5,880
Mean	3,077	4,653	4,991	14,025	7,645	3,132	966	669	670	853	2,418	6,990

SALMON RIVER ABOVE PULASKI, NEW YORK.

A current-meter station was established on this stream September 5, 1900. It is located at a highway bridge 2 miles from the village of Pulaski. The stream bed is of gravel, the banks are bold, and the channel bottom is nearly flat. The gage board is attached to the center pier of the bridge, and readings are taken twice daily, at 6 a. m. and at 7 p. m. The mean of the two observations for each day is given in the table. A current-meter measurement made on September 4 showed a discharge of 103 second-feet. The mean gage reading during the measurement was 1.03 feet. There are 3 dams at Pulaski, furnishing power to 14 establishments. The total effective head obtained varies, with the stage of the stream, from 24 feet to 36 feet.

There is an undeveloped power, with a precipitous fall of 110 feet, at Salmon Falls. In November, 1898, a gaging station was established by the United States Board of Engineers on Deep Waterways 1 mile above these falls, but it was abandoned in June, 1899. A description of the station will be found in Water-Supply Paper No. 36, page 190. The drainage above the abandoned gaging station is 191 square miles, while that above the bridge station near Pulaski is 264 square miles.

Additional information regarding this river will be found in Water-Supply Paper No. 47, pages 37 to 41, in a paper entitled "Methods employed in the gaging of New York streams during the year 1900."

Daily gage height, in feet, of Salmon River above Pulaski, New York, for 1900.

Day.	Sept.	Oct.	Nov.	Dec.	Day.	Sept.	Oct.	Nov.	Dec.
1 2 3 4 5 6 7 8 9 10 11	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	$\begin{array}{c} 1.\ 60\\ 1.\ 50\\ 1.\ 35\\ 1.\ 25\\ 1.\ 20\\ 1.\ 05\\ 1.\ 10\\ 1.\ 35\\ 1.\ 85\\ 1.\ 80\\ 1.\ 60\\ \end{array}$	$\begin{array}{c} 1.\ 20\\ 1.\ 20\\ 1.\ 85\\ 1.\ 85\\ 1.\ 90\\ 1.\ 75\\ 2.\ 55\\ 2.\ 25\\ 1.\ 90 \end{array}$	$\begin{array}{c} 2.50\\ 2.30\\ 2.20\\ 2.50\\ 2.75\\ 2.45\\ 2.30\\ 2.15\\ 1.65\\ 1.50\\ 1.50\end{array}$	17	$\begin{array}{c} 1.00\\ 1.00\\ 1.00\\ 1.00\\ 2.15\\ 2.25\\ 1.75\\ 1.65\\ 1.55\\ 1.35\\ 1.25\\ \end{array}$	$\begin{array}{c} 1.40\\ 1.40\\ 1.35\\ 1.35\\ 1.30\\ 1.25\\ 1.45\\ 2.00\\ 1.95\\ 1.85\\ \end{array}$	$\begin{array}{c} 1.50\\ 1.70\\ 2.55\\ 4.20\\ 4.30\\ 3.65\\ 3.10\\ 2.45\\ 2.50\\ 3.50\\ 4.70\end{array}$	$\begin{array}{c}$
12 13 14 15 16	$ \begin{array}{r} .90 \\ .90 \\ .90 \\ .95 \\ 1.00 \end{array} $	$\begin{array}{c} 1.50 \\ 1.40 \\ 1.40 \\ 1.30 \\ 1.40 \end{array}$	$ \begin{array}{c} 1.90\\ 1.80\\ 1.80\\ 1.70\\ 1.50 \end{array} $	$\begin{array}{c} 1.30\\ 1.40\\ 1.40\\ 1.35\\ 1.30\end{array}$	28 29	1.25 1.25 1.45	$ \begin{array}{r} 1.85 \\ 1.70 \\ 1.75 \\ 1.75 \\ 1.75 \end{array} $	3. 75 3. 35 2. 55	$ \begin{array}{r} 2.20 \\ 2.10 \\ 2.20 \\ 2.30 \\ 2.30 \\ \end{array} $

MOOSE RIVER AT MOOSE RIVER, NEW YORK.

On June 5, 1900, a gaging station was established on this stream at Moose River, 4 miles below the McKeever railroad station. The section of the channel chosen to be spanned by a cableway has a width of 225 feet, with a nearly flat gravel bottom. A vertical gage board was attached to a pile driven out in the stream beyond the low-water margin and protected from ice and logs by a floating boom anchored upstream.

Moose River is characterized throughout its entire course by rifts
NEW YORK.

and rapids. Topographically the watershed is rocky, precipitous, and mostly timbered. The drainage area above the gaging station is 346 square miles. An area of 41 square miles in the headwaters is subject to regulation by storage, controlled by a State dam at Old Forge, at the foot of the Fulton Lakes. There are numerous undeveloped water powers on the stream, including two falls near Lyonsdale, where a head of 30 or more feet might be obtained, and another (Millers Falls) of nearly equal height below the town of Moose River. Water power is developed at 8 dams, a total fall of 225 feet being utilized, the aggregate capacity of the turbines installed being more than 7,000 horsepower.¹

No eurrent-meter measurements have thus far been made. Gage readings are taken twice daily, morning and evening, and the mean of the two readings for each day is given in the accompanying table.

Additional information in regard to this river will be found in Water-Supply Paper No. 47, pages 37 to 41, in a paper entitled "Methods employed in the gaging of New York streams during the year 1900."

Daily gage height, in feet, of Moose River at Moose River, New York, for 1900.

Day.	June.	July.	Aug.	Sept.	Oet.	Nov.	Day.	June.	July.	Aug.	Sept.	Oct.	Nov.
1		0.50	0.85	0.90	0.70	$1.15 \\ 1.20$	17	$0.92 \\ 65$	0.80	$1.20 \\ 1.00$	0.70	0.75	2.05 2.30
3		. 25	. 70	. 65	. 80	1.05	19	.60	.85	. 85	.60	. 65	1.70
5	2.00	. 30	. 50	. 60	. 60	. 95	20 21	. 80	. 80	. 60	. 80	. 75	6. 91 4. 45
6 7	$1.55 \\ 1.25$. 35 . 70	. 55 . 60	.55 .55	. 60 . 60	$1.10 \\ 1.10$	22 23	. 90	. 65 . 55	. 60 . 50	$1.20 \\ 1.55$	$.70 \\ .70$	4.10 3.70
8 9	$1.20 \\ 1.95$	$.85 \\ .75$. 55 . 55	. 60 . 65	. 65 . 60	$2.25 \\ 3.10$	24 25	$\begin{bmatrix} .70 \\ .80 \end{bmatrix}$. 60 . 85	$.45 \\ .55$	$1.30 \\ 1.05$	$1.30 \\ 2.00$	3.35 3.20
10	$1.55 \\ 1.40$. 70	$\frac{.60}{.70}$.70 .55	. 60	$2.50 \\ 1.75$	26 27	. 60	$\frac{3.05}{1.85}$	$.65 \\ 1.75$. 90	$1.65 \\ 1.30$	3.05 3.65
12	$1.20 \\ 1.08$. 90	. 65	. 55	$.55 \\ 45$	$1.15 \\ 95$	28	.30	$1.20 \\ 90$	$2.00 \\ 1.35$	$.85 \\ 70$	$1.30 \\ 1.25$	3.75 3.55
14	1.05	. 80	1.80 1.75	. 50	.45	.90	30 31	. 55	$.75 \\ .75 \\ .70$	1.40	. 80	1.25	3.20
16	1.05	1.70	1.25	.70	.85	1.75	04		. 10	. 90		1.00	

BEAVER RIVER, NEW YORK.

Beaver River rises in the western part of Hamilton County, crosses Herkimer County, and emerges from the Adirondacks at the town of Number Four, on the Lewis County line. The flow from the tributary watershed above Beaver, comprising an area of 153 square miles, or 47.5 per cent of the entire drainage area, is regulated by storage in the Beaver Flow or Stillwater, an artificial lake formed by a timber dam 16 feet high. In addition to the reservoir formed by the State dam at Beaver, there are within this region more than 50 natural lakes, including Red Horse Chain, so that a comparatively uniform flow is maintained throughout the summer season.

An examination of Beaver River with reference to facilities for gaging was made early in July, 1900. The almost continuous rapids in the upper reaches of the stream limit the desirable sites for gaging stations to the stream channel below Beaver Falls, 4 miles from its confluence with Black River at Castorland. Arrangements were made for the establishment of a cable station, but owing to the presence of log rafts in the stream during the greater portion of the summer the record has not yet been started.

From the State dam at Beaver to the town of Number Four, a distance of 10 miles, the stream consists of numerous bowlder rapids, alternating with short stretches of smooth water. Above Beaver Lake there is a high fall, forming a descent of 60 feet within a distance of 400 or 500 feet. From the foot of Beaver Lake to Belfort, a distance of 12 miles, the stream channel continues rocky and precipitous, although the adjacent watershed is sandy and for the most part covered with timber. Eagle Falls, 2 miles below Beaver Lake, consists of a series of cascades, aggregating a descent of 75 feet. There are a number of other undeveloped water powers in this vicinity.

Water power is developed at Beaver Falls, at Croghan, and at Belfort, aggregating 4,400 horsepower, at five dams, and utilizing a fall of 133 feet. There is also an abandoned power at Tisses Falls, below Belfort, where a total head of 60 feet could be obtained. Power is developed at Belfort, under a head of 50 feet, for the generation of electricity which is transmitted to adjacent towns, a distance of 16 miles.

Rainfall and other meteorological records have been kept since January, 1889, at Number Four, in the heart of the timber-covered portion of the watershed.

Additional information regarding this river will be found in Water-Supply Paper No. 47, pages 37 to 41, in a paper entitled "Methods employed in the gaging of New York streams during the year 1900."

BLACK RIVER AT HUNTINGTONVILLE DAM, NEAR WATERTOWN, NEW YORK.

A description of this station, including tables of daily gage heights, will be found in Water-Supply Paper No. 36, page 191. The entire flow of Black River at this point, aside from leakage and a slight diversion for the municipal water supply of Watertown, passes over the Huntingtonville dam. Two or more readings of the crest gage are taken daily, and the mean of the readings from midnight to midnight has been used in estimating the mean daily flow. In computing the flow over the dam, an allowance of 200 second-feet has been made for leakage through seams and crevices in the limestone rock underlying the dam. This amount has been arrived at from an estimate of the size of the orifices and the head on the same, when the water was drawn down in the summer of 1897.

There is no way to check direct the flow during high water immediately below the dam, but a current-meter measurement was made at Glenpark Bridge on June 6, 1900, which gave a total flow of 2,175 second-feet.

The mean daily flow for the years 1897, 1898, 1899, and 1900 is given

in the accompanying tables. It does not represent the total wateryielding capacity of the tributary drainage area, inasmuch as a portion of the flow from the headwaters is diverted to the Forestport feeder to supply Black River Canal. Storage reservoirs, to compensate waterpower users, are maintained by the State of New York on Beaver and Moose rivers, the principal tributaries of Black River. Owing to floodwater storage, diversion, and the effect of mills starting and stopping irregularly, the regimen of this stream is far from natural. Measurements of the amount of diversion of Black River below Forestport reservoir have been made by Mr. E. C. Murphy, for the New York State canal survey.

The highest water observed while the record has been kept was on the morning of April 21, 1900, the reading of the crest gage being 108.41 feet, and the corresponding flow 30,150 second-feet, equivalent to a flow of 16 second-feet per square mile of tributary drainage.

This stream is of great importance as a source of water power, having 22 dams in its lower stretch of 18 miles, furnishing, in round numbers, 60,000 horsepower to 80 mills along its banks, which employ an aggregate of 3,900 persons.

Additional information will be found in Water-Supply Paper No. 47, pages 37 to 41, in a paper entitled "Methods employed in the gaging of New York streams during the year 1900."

Day.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Oct.	Nov.	Dec.
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 20 21 22 23 24 25 26 27	1,460 2,610 1,850 3,420	$\begin{array}{c} 1,220\\ \hline 2,060\\ 2,855\\ a(3,230\\ 3,600\\ 5,650\\ 5,970\\ 6,602\\ c(5,260\\ 5,570\\ 5,130\\ 5,570\\ 8,550\\ 2,240\\ a(5,560\\ 5,130\\ 8,550\\ 2,240\\ a(5,560\\ 10,760\\ a(7,924\\ 5,60)\\ 10,760\\ $	$\begin{array}{c} 5,050\\ 5,170\\ 5,850\\ 8,020\\ 8,650\\ 9,590\\ 10,916\\ 11,540\\ a10,550\\ 7,120\\ 7,340\\ 8,750\\ 8,850\\ a9,290\\ 9,290\\ 9,290\\ 9,290\\ 9,290\\ 9,290\\ 9,290\\ 9,648\\ a9,144\\ 112,640\\ 12,640\\ 14,142\\ \end{array}$	$\begin{array}{c} 8,550\\ a,6,502\\ a,6,502\\ a,6,502\\ a,7,602\\ a,7,739\\ a,2,900\\ a,7,739\\ a,2,900\\ a,2,900$	$\begin{array}{c} 3,3625\\ 3,3625\\ 2,3328\\ 3,3528\\$	$\begin{array}{c} 978\\ 956\\ 1,066\\ a890\\ 782\\ 646\\ 1,066\\ 1,066\\ 710\\ 678\\ 746\\ a582\\ 836\\ 614\\ 1,110\\ 1,19\\ 836\\ 0,000\\ 728\\ 630\\ a480\\ 1,000\\ 934\\ 890\end{array}$		$1,044 \\ 1,220 \\ 2,455 \\ a854 \\ 1,176 \\ 1,110 \\ 956 \\ 854 \\ 854 \\ 856 \\ 756 \\ 756 \\ 756 \\ 752 \\ 854 \\ 854 \\ 752 \\ 854 \\ 854 \\ 752 \\ 854 \\$	$\begin{array}{c} 598\\872\\1,536\\2,3302\\2,356\\4,456\\2,2386\\2,376\\2$	$\begin{array}{c} 6,812\\ 5,850\\ 2,845\\ 2,845\\ 2,845\\ 2,845\\ 2,845\\ 2,845\\ 2,845\\ 2,850\\ 2,850\\ 2,7,428\\ 2,7,1220\\ 3,140\\ 2,850\\ 2,7,428\\ 2,7,1220\\ 3,195\\$
29 30 51		6,176 5,450 5,450	13,806 10,552	$4,020 \\ \alpha 3,775 \\ 3,600$	978 934	1,220 1,940 2,000	a1,254	$710 \\ 710 \\ a678 $	9,890 8,116	2,060 2,000 1,804
Mean	2,160	6,317	9,484	4,267	2,713	879	2,280	954	4,155	4,725

Daily discharge, in second-feet, of Black River at Huntingtonville dam, New York, for 1897.

a Sunday.

NOTE.-No record from September 1 to October 13, inclusive.

Daily discharge, in second-feet, of	Black	River	at	Huntingtonville	dam,	New	York,
	for	1898.					

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1	1,738 a2.270	2,770 2,930	2,300 2,610	7,340 6,646	$a^{4},411$ 3,362	2.770 2.362	1,436 1.316	$1,110 \\ 1,580$	1,244 1 220	1,556	3,095 2,706	2,548 2,455
3	1,940	2,835	2,300	a5,050	3,530	2,030	a872	1,132	1,110	1,088	2,610	2,455
4	2,000	2,610	2,300	3,950	3,705	1,804	800	1,292	a330	1,110	2,393	a2,240
ə	2,120	2,110	2,150	3,600	3,915	1 556	1,110 1.088	1,460	1,340 1 766	1,412 2 770	2,300	2,300
7	1.850	2,610	2,150	3,420	4,411	1,530 1.532	1,000	a1,000	1,700	3 420	3 095	1 940
8	1,580	2,610	2,210	3,362	a3, 420	1,340	1,022	1,580	2,060	2,865	2,930	1,804
9	a1,850	2,455	2,674	3,095	2,770	1,176	956	1,244	1,940	a1,910	2,930	1,658
10	1,804	2,300	3,420	a3,029	2,930	1,244	a728	1,110	1,804	1,940	2,930	1,684
11	1,804 1,766	3,195	0, 380	3,029	2,455 1 940	1,484 a1,902	1 000	1,110 1,176	$a_{1,460}$	1,684 1 264	8,404	$a_{1,532}$
13	3,029	a8.164	a18,200	2,642	3,600	1.340	1,000	1,340	1,202 1.292	1,004 1.292	a9.144	1,804 1,804
14	4,300	7,340	23,300	2,706	3,800	1,804	978	a1,268	956	1,606	8,750	1,850
15	4,665	6,470	27,900	2,930	a3,328	2,150	1,000	630	1,000	2,706	7,472	1,850
16	a4,448	5,450	23,700	2,900	2,642	2,030	1,000	1,244	890	a3,500	6,176	1,880
16	4,200	4,484	14,900	2 240	2,610 2 262	1,804 1,539	1 000	1,000	812	9 775	4,592	2,000
19	3,530	3,600	13,750	2.548	2,150	al. 154	1,436	956	800	2,996	3,860	1 940
20	3,420	a3, 362	a12,304	2,865	2,548	1,850	1,154	934	818	2,706	a2,963	2,090
21	4,300	3.775	12,804	3,775	2,865	2,150	1,220	$\alpha 956$	1,132	2,674	3,294	2,090
22	5,650	3,985	13,582	4,265	$ \alpha_2, 706 $	2,000	1,220	818	1,044	2,963	3,294	2,548
40 24	a5,050 6 176	3,913	13,034 11,980	0,200 06 386	2,424	1,804 1,658	1,220	1,110 2 150	1 460	5 480	3,029	4,230 5,810
25	5.970	3,230	9,390	7.252	2.770	1,000 1.340	1.292	$\tilde{2}, \tilde{6}10$	a2.738	4.592	2,800	a5,450
26	5,530	2,930	8,260	8,950	2,865	a1,220	2,000	3,095	2,865	4,055	2,548	5,130
27	4,739	a2,770	a6,900	10,140	3,775	1,066	1,710	3,130	2,770	5,570	a1,658	4,300
28	3,950	3,095	6,176	9,690	4,055	1,340	1,340	a2,706	2,393	6,680	2,030	3,420
29	a, 390 a2, 000		7 340	5 850	2 230	1,310 1 902	1,001 1 909	1 460	1 850	5,250	2,001	- 3,093 3 705
31	2,930		7,924		3,130		a1,508	1,658	1,000	3,950		4,813
Moon	3 402	3 808	0.800	4 654	9 174	1 690	1 198	1 (95	1 492	3 198	3 039	9 790
mean	0, 10.	0,000	9,009	1,004	0,114	1,005	1,140	1,455	1,400	0,100	0,000	~, 120

a Sunday.

Daily discharge, in second-feet, of Black River at Huntingtonville dam, New York, for 1899.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1	$\begin{array}{c} 4,230\\ 3,985\\ 3,396\\ 3,600\\ 10,396\\ 9,740\\ 8,750\\ a8,750\\ 5,810\\ 5,810\\ 5,810\\ 8,950\\ 5,810\\ 8,950\\ 5,810\\ 8,950\\ 5,810\\ 8,950\\ 8$	$\begin{array}{c} 1,940\\ 2,090\\ 2,030\\ 2,030\\ 2,000\\ 2,000\\ 2,000\\ 2,000\\ 2,000\\ 1,984\\ 1,850\\ a1,984\\ 2,240\\ 2,240\\ 2,240\\ 2,240\\ 2,240\\ \end{array}$	$\begin{array}{c} 3,565\\ 3,260\\ 3,230\\ 3,328\\ a3,880\\ 5,170\\ 5,530\\ 5,690\\ 4,592\\ 4,125\\ a5,090\\ 4,592\\ 4,125\\ 8,164\\ 8,020\\ 7,736\\ 6,900\\ \end{array}$	$\begin{array}{c} 4,125\\ a,3,915\\ 3,800\\ 3,565\\ 3,600\\ 3,985\\ 4,520\\ 6,900\\ a,8,116\\ 8,308\\ 8,956\\ 11,072\\ 12,136\\ 13,694\\ 313,806\\$	$\begin{array}{c} 18,000\\ 16,150\\ 14,800\\ 13,694\\ 12,080\\ 9,490\\ a7,516\\ 5,090\\ 4,125\\ 3,705\\ 3,362\\ 3,705\\ 3,880\\ a3,260\\ 2,930\\ 3,029\end{array}$	$\begin{array}{c} 3,095\\ 2,393\\ 2,240\\ a1,804\\ 1,658\\ 1,710\\ 1,658\\ 1,710\\ 1,532\\ a1,220\\ 1,532\\ a1,220\\ 1,532\\ a1,220\\ 1,340$	$\begin{matrix} 1,460\\ a1,022\\ 1,000\\ 956\\ 1,388\\ 1,436\\ 1,580\\ 1,460\\ a1,176\\ a1,176\\ a1,176\\ 1,880\\ 1,340\\ 2,150\\ 1,738\\ 1,532\\ 1,412\\ a1,022\\ 1,738\\ 1,532\\ 1,412\\ a1,022\\ 1,738\\ 1,532\\ 1,412\\ 1,738\\ 1,532\\ 1,412\\ 1,738\\ 1,532\\ 1,412\\ 1,738\\ 1,532\\ 1,412\\ 1,738\\ 1,532\\ 1,412\\ 1,738\\ 1,532\\ 1,412\\ 1,738\\ 1,532\\ 1,412\\ 1,738\\ 1,532\\ 1,412\\ 1,738\\ 1,532\\ 1,412\\ 1,738\\ 1,532\\ 1$	$\begin{array}{c} 956\\ 1,000\\ 1,110\\ 1,000\\ 854\\ a\ 678\\ 800\\ 890\\ 1,000\\ 854\\ 728\\ 678\\ a\ 710\\ 728\\ 678\\ a\ 710\\ 728\\ 1,044\\ 1\ 10\end{array}$	$\begin{array}{c} 978\\ 9,244\\ a\ 630\\ 1,110\\ 480\\ 1,000\\ 890\\ 1,022\\ 1,066\\ a1,022\\ 1,220\\ 678\\ 1,340\\ 630\\ 694\\ 1\ 176\\ 631\\ 1176\\ \end{array}$	$\begin{array}{c} a \ 956\\ 956\\ 1,460\\ 1,340\\ 1,176\\ 1,022\\ a \ 678\\ 1,044\\ 854\\ 956\\ 800\\ 818\\ 818\\ a \ 818\\ a \ 818\\ 694 \end{array}$	$\begin{array}{c} 2,240\\ 3,420\\ 4,055\\ 3,230\\ a2,900\\ 2,706\\ 2,393\\ 1,850\\ 1,452\\ 1,460\\ 1,412\\ a1,066\\ 1,436\\ 1,132\\ 1,220\\ 1,364\\ 1,132\\ 1,220\\ 1,364\\ 1,366\\ $	$\begin{array}{c} 1,176\\ 1,198\\ a1,412\\ 2,090\\ 2,060\\ 1,658\\ 1,460\\ 1,220\\ 1,198\\ a1,110\\ 1,658\\ a1,110\\ 1,658\\ 8,404\\ 8,404\\ 7,928\\ 5,650\end{array}$
10 17 17 18 20 20 21 22 23 24 25 24 25 26 27 28 29 30 31 Mean	$\begin{array}{c} 5, 810\\ 5, 810\\ 5, 450\\ 5, 450\\ 5, 250\\ 3, 095\\ 3, 740\\ 2, 3, 362\\ 3, 195\\ 2, 930\\ 2, 930\\ 2, 930\\ 2, 610\\ 2, 393\\ \mathbf{a}2, 000\\ 2, 300\\ 2, 120\\ 4, 712\\ \end{array}$	$\begin{array}{c} 2,150\\ 2,210\\ 1,984\\ a1,850\\ 2,000\\ 2,362\\ 2,963\\ 3,465\\ 3,420\\ a3,095\\ 3,420\\ a3,095\\ 3,420\\ 3,530\\ \hline \\ \hline \\ 2,326\\ \hline \\ 2,326\\ \end{array}$	$\begin{array}{c} 6,900\\ 6,680\\ 5,850\\ a5,250\\ 4,629\\ 4,665\\ 4,629\\ 4,665\\ 5,050\\ a4,776\\ 4,592\\ 4,230\\ 4,592\\ 4,230\\ 4,592\\ 4,230\\ 4,592\\ 5,051\\ \end{array}$	$\begin{array}{c} a13,806\\ 14,086\\ 14,086\\ 14,086\\ 14,700\\ 17,400\\ 20,900\\ 24,400\\ 24,950\\ 24,950\\ 24,950\\ 24,950\\ 24,950\\ 22,250\\ a20,350\\ \hline \\ \hline \\ 13,894\\ \end{array}$	$\begin{array}{c} 3,029\\ 3,095\\ 3,705\\ 3,705\\ 3,029\\ 3,775\\ 3,902\\ 3,775\\ 3,775\\ 3,775\\ 3,500\\ 2,900\\ 2,424\\ 2,485\\ a2,393\\ 2,362\\ 3,362\\ 3,362\\ 3,420\\ \hline 5,609 \end{array}$	$\begin{array}{c} 1,460\\ 1,460\\ a1,460\\ 1,658\\ 1,340\\ 1,220\\ 1,220\\ 1,220\\ 1,220\\ 1,220\\ 1,220\\ 1,220\\ 1,220\\ 1,232\\ 1,340\\ 1,176\\ 1,340\\ \hline \end{array}$	$\begin{array}{c} a1,022\\934\\934\\1,000\\01,292\\956\\956\\1,000\\a978\\1,220\\1,340\\1,132\\1,044\\1,088\\836\\a550\\458\\458\\1,205\\\end{array}$	$\begin{array}{c} 1,110\\ 1,066\\ 1,606\\ 1,000\\ a\ 710\\ 522\\ 1,000\\ 890\\ 854\\ 1,244\\ 1,110\\ a\ 854\\ 872\\ 890\\ 1,000\\ 956\\ \hline \end{array}$	$\begin{array}{c} 1,176\\ a\ 764\\ 1,220\\ 1,176\\ 710\\ 800\\ 1,066\\ 710\\ a\ 630\\ 1,198\\ 1,198\\ 1,198\\ 1,198\\ 1,198\\ 1,198\\ 1,532\\ \hline \end{array}$	$\begin{array}{c} 694\\ 1,000\\ 978\\ 1,044\\ 1,088\\ 854\\ a522\\ 1,000\\ 956\\ 1,066\\ 1,110\\ 1,110\\ 1,110\\ 1,110\\ 1,1066\\ 1,292\\ 1,940\\ \hline \end{array}$	$\begin{array}{c} 1,304\\ 1,460\\ 1,460\\ a1,066\\ 1,110\\ 1,244\\ 1,176\\ 1,066\\ 1,100\\ a782\\ 1,088\\ 1,110\\ a782\\ 1,088\\ 1,132\\ 1,066\\ 912\\ \hline \\ \hline \\ 1,652\\ \end{array}$	$\begin{array}{c} 3, 650\\ a2, 706\\ 3, 294\\ 4, 702\\ 5, 450\\ 6, 470\\ 6, 680\\ 5, 650\\ a4, 337\\ 4, 300\\ 2, 930\\ 2, 548\\ 2, 300\\ 2, 240\\ a1, 804\\ \hline \hline 3, 501\\ \end{array}$

a Sunday.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1	1,766	2,300	2,865	a 3, 800	11,280	2,000	a 978	1,340	1,240	780	1,610	9,900
2	1,710 1,710	2,300 2 240	2,610 2,579	4,265 5,370	11,020 10,812	1,710 2,000	978	1,110 1,220	1,200	1,440 1,200	1,535 1,440	8,000
4	1,710	$a^{2,060}_{2,060}$	a2,770	6,050	9,740	$a^{2}_{2},060$	854	1,000	(b)	960	1,120	5,650
5	1,710	2,060	2,770	7,384	9,000	2,200	1,000	a 854		1,120	1,370	5,700
6	1,710	2,150	2,930	7,560	a7,780	2,000 2,150	1,110	694		1,200	1,120 1 245	5,650
8	2 300	2,200	2,600	a12 192	6 050	2,130	a 764	1,154		1.010	1,4±0	4,900
9	2,362	4,850	2,930	10,760	5,650	2,579	1,268	690	(a)	960		4,180
	2,362	5,850	2,930	10,760	6,602	2,485	1,244	820		1,240		3,300
1	2,240	$a_{5,770}$	a2,674	10,240 10,244	7,560	$a_{2,610}^{a_{2,610}}$	1,340 1 969	780	760	980	2,990	3,460
2	2,150	6 344	2,950 2.674	9 490	a5 770	2,000 2,030	1,200 1,532	1,010	740	780	2 475	2 996
4	a1, 710	11,458	2,610	7,340	5,650	1,766	1,580	1,490	780	a 580	2,120	2,780
5	1,940	12,304	2,610	a 6, 386	5,250	1,580	a1, 198	1,730	740	820	2,250	3,080
l6	1,850	14,030	2.610	7,208	5,250	1,580	1,460	1,680	a 390	1 010	1,485	2,200
8	1,380 1,710	15, 470	2,010	10 604	5,000	a1,208 a1,154	1,220 1 268	1,000 1,240	1 1 1 20	1,010	1,480	2 25
9	1,940	9,590	2,610	20,100	5,250	1,460	1,340	a2, 120	1,100	1,050	3,900	2,595
20 0	2,930	7,924	2,610	27,050	a5,170	1,364	1,766	1,010	1,120	1,050	8,600	2,830
21	a5,930	5,770	2,610	30,000	4,930	1,044	1,580	1,240	980	a740	9,175	2,780
22	5,250	5,130 5,130	3,420	27 700	1 265	1,044	1,400 1,556	1,200	980 al 055	900	8,900	2,00
24	5,770	4,850	3,915	25,200	3,705	1,110	1.766	480	1.240	1,440	7.820	3.640
5	4,850	a 4,230	a3,600	23,300	3,161	a1,176	1,340	810	1,780	1,980	6,280	5,450
26	4,125	3,775	-3,600	21,750	[3, 420]	1,340	1,220	a 500	1,490	2,340	6,680	5,280
7	3,670	3,095	3,260	17,000	2 185	978	1,100 1,850	780	1,290 1,200	2,120	9,900	4,900
29	3, 195	1,000	3,260	a14.800	2,150	764	a1.316	1.780	915	1.860	13, 900	3.810
30	2,865		3,260	12,752	2,000	1,044	1,268	1,440	a 800	1,885	12,250	
31	2,548		3,465		1,904		1,176	1,240		1,935		
Mean	2,834	5,734	2,970	13,926	5,711	1,630	1,321	1,134	1,020	1,218	5,014	4,230

Daily discharge, in second-feet, of Black River at Huntingtonville dam, New York, for 1900.

a Sunday.

b Sluice gates open.

GRAND RIVER, MICHIGAN.¹

This is the largest stream in the State. Its drainage basin, which includes a total area of 5,572 square miles, is situated in the central portion of the lower peninsula, and drains into Lake Michigan. It lies in the southern border of the pine belt and is for the most part cleared. Occasional tracts of forest remain, however, as, for example, Slocum's Grove, in Muskegon County, which forms a part of the drainage basin of Crockery Creek, and contains between 4,000 and 5,000 acres of hard-wood and hemlock timber, now being lumbered. The basin is overlain with glacial drift deposits, including sand, clay, overwash, gravel, and till, with outcroppings of rock at rare intervals. A stratum of limestone, said to be 52 feet thick, appears in the east side of the bed of Grand River at Grand Rapids, 100 feet above the Pearl street bridge. It dips in a northeasterly direction, at a slope of 50 feet to the mile, and does not appear in the west side canal. The watershed receives an annual rainfall varying from 25 inches in the region of the headwaters to 30 or 35 inches near the mouth of the river. From the foot of the rapids formed by the limestone ledge at Grand Rapids to the mouth of the river at Lake Michigan the flow is

¹ Report of Robert E. Horton.

very sluggish; the fall in this portion is given below, from levels run by Mr. Fred Morley, United States assistant engineer.

Section.	Dis- tance.	Fall.
Grand Rapids to Grandville Grandville to Lamont Lamont to Grand Haven	Miles. 6.0 11.5 21.64	Feet. 2.85 2.92 0.43
Total	39.14	6.20

Fall of Grand River between Grand Rapids and its mouth.

In the upper half of this stretch of the river the immediate banks of the stream are high, sometimes forming natural levees at elevations greater than that of the adjacent flood plain. Mr. Morley states that below Lamont bayous and low swamps are common between the river banks and the foothills bordering the valley. The valley as a whole is narrow; gravel bluffs from 50 to 60 feet high occasionally stand close to the stream. The river below Grand Rapids has been adjudged navigable, and a project has been formed for its canalization, the plan being for a waterway, with a navigable depth of 10 feet, connecting the eity of Grand Rapids with Lake Michigan.

The drainage areas of the main stream and its tributaries at various points are given in the following table:

Drainage areas o	f Grand	River and	its tributaries.
------------------	---------	-----------	------------------

Stream.	Location.	Area.
		Sq. mi.
Grand River	Above Lansing	756
Red Cedar River	Above mouth	47:
Grand River	. Below mouth of Red Cedar River	1,229
Do	Above Portland	1,40
Lookingglass River	Above mouth	304
Grand River	Below mouth of Lookingglass River	1,710
Do	Above Lyons	1,748
Maple River	Above Maple Rapids	459
Do.	Above mouth	919
Grand River	Below mouth of Maple River	2,66
Do	At Ionia	2,818
Do	Above Lowell	2,91
Flat River	Atmouth	60:
Grand River	Below mouth of Flat River	3,578
Thornapple River	Above mouth	824
Grand Kiver	Above Grand Kapids water-power dam	4,58
Do	Above mouth	0,043

The watershed is comparatively flat. The total fall of the river from the extreme headwaters to the mouth, a distance of more than 200 miles, is about 350 feet.

Fall and slope of Grand River.

Tractin	Elevation	Approxin	nate fall.	Approximate dis- tance.		
Location.	mean tide.	To mouth of stream.	Between points.	From mouth.	Between points.	
Grand Haven Grand Rapids <i>a</i> Lowell Ionia Portland Lansing Jackson	$\begin{array}{c} Feet. \\ 581.3 \\ 587.5 \\ 635.0 \\ 640.0 \\ 710.0 \\ 825.0 \\ 915.0 \end{array}$	$\begin{array}{c} Feet. \\ 0.0 \\ 6.2 \\ 53.7 \\ 58.7 \\ 128.7 \\ 243.7 \\ 333.7 \end{array}$	$\begin{matrix} Feet. & 0.0 \\ 6.2 \\ 47.5 \\ 5.0 \\ 70.0 \\ 115.0 \\ 90.0 \end{matrix}$	$Miles. 0 \\ 39 \\ 67 \\ 83 \\ 106 \\ 138 \\ 192$	Miles. 0 28 16 23 32 54	

a Foot of rapids.

The northwestern and southeastern portions of the watershed are thickly interspersed with small lakes. A considerable number of these have no surface outlets, and their drainage basins do not contribute to the run-off of the river except through ground water.

The water of Grand River is hard. Samples collected on June 20, 1899, showed the following analyses:¹

Analyses of water from Grand River and tributary streams, in parts per million.

Stream.	Location.	Total residue.	Chlo- rine.	Free ammo- nia.	Albu- minoid ammo- nia.	Tempo- rary hard ness.
Grand River Thornapple River Muskegon River Bailey Creek (spring fed)	Grand Rapids pumping station. At Cascade Above Big Rapids	$281.6 \\ 280.0 \\ 184.0 \\ 245.6$	4.0 4.3 1.9 1.7	$\begin{array}{c} 0.112\\ .094\\ .052\\ .006\end{array}$	$\begin{array}{c} 0.320 \\ .208 \\ .344 \\ .096 \end{array}$	240 250 170 225

Grand River serves as a source of water supply to the city of Grand Rapids. The average daily consumption of that city for the year 1899-1900 was 13,693,499 gallons a day, equivalent to a flow of 21.3 second-feet. The population in 1900 was 87,565.²

In connection with proposed improvements for navigation, gaging stations have been established at various points on Grand River below Grand Rapids. All gages are set with their zeros at the Lake Michigan datum, 581.28 feet above mean tide of the New York harbor deepsea levels. Since 1890 observations have been taken at different stages of the stream, notably during high water, with a view to determining its slope. Cross sections have also been made, and these data will, when completed, form a basis for computing the flow of the river by means of Kutter's formula.

¹ Report of Consulting Engineers to Pure Water Commissioners of the City of Grand Rapids Michigan, 1899. ² Report of Board of Public Works, Grand Rapids, 1900.

The results of the gage readings for the year 1891, referred to the Lake Michigan datum, are given in the following table:

	Me	Mean gage heights.				Highest observed.				Lowest observed.			
Month.	Grand Rapids.	Grandville.	Lamont.	Grand Haven.	Grand Rapids.	Grandville.	Lamont.	Grand Haven.	Grand Rapids.	Grandville.	Lamont.	Grand Haven.	
1891. January February March April May June June July August September	$\begin{array}{c} 8.16\\ 8.95\\ 11.91\\ 11.45\\ 6.93\\ 6.45\\ 5.77\\ 5.33\\ 5.60\\ \end{array}$	$\begin{array}{c} 4.93 \\ 5.90 \\ 9.48 \\ 8.52 \\ 3.62 \\ 2.99 \\ 2.51 \\ 2.12 \\ 2.51 \end{array}$	$\begin{array}{c} 1.81\\ 2.72\\ 5.35\\ 4.65\\ .92\\ .66\\ .37\\ .09\\ .26\end{array}$	$\begin{array}{r} -0.70 \\93 \\79 \\47 \\35 \\63 \\41 \\32 \end{array}$	$\begin{array}{c} 9.74\\ 13.64\\ 16.64\\ 14.49\\ 8.19\\ 6.99\\ 6.49\\ 6.34\\ 5.14\end{array}$	$\begin{array}{c} 6.38\\ 10.68\\ 14.08\\ 11.48\\ 5.08\\ 3.78\\ 3.18\\ 3.08\\ 3.08\\ 3.08\end{array}$	$\begin{array}{c} 2.37\\ 6.67\\ 8.87\\ 6.87\\ 2.17\\ 1.07\\ .77\\ .87\\ .77\end{array}$	$\begin{array}{r} +0.42 \\13 \\29 \\ + .17 \\ + .17 \\ + .72 \\ + .02 \\ + .02 \end{array}$	$\begin{array}{c} 7.\ 19\\ 7.\ 04\\ 8.\ 99\\ 8.\ 29\\ 6.\ 24\\ 5.\ 74\\ 5.\ 16\\ 4.\ 92\\ 5.\ 12 \end{array}$	$\begin{array}{r} 4.08\\ 4.28\\ 6.18\\ 5.18\\ 2.78\\ 2.38\\ 2.08\\ 1.78\\ 1.73\end{array}$	$\begin{array}{c} 1.27\\ 1.37\\ 2.77\\ 2.77\\ 3.77\\ .37\\ .37\\13\\23\end{array}$	$\begin{array}{c} -1.28 \\ -1.68 \\ -1.53 \\ -1.08 \\90 \\90 \\91 \\72 \\ -1.29 \end{array}$	

Gage heights, in feet, of Grand River at various points.

Float measurements of the flow of Grand River were made by Mr. Morley during the low-water period of 1891, as follows:¹ July 21, 5.52 miles below Grand Rapids; August 18, 16.68 miles below Grand Rapids. Rod floats were run across the stream at intervals of 10 feet, and were timed while passing downstream a distance of 100 feet. From these measurements the minimum flow of 1891 was estimated at 981.5 second-feet, the corresponding stage on the Grand Rapids gage being 5.67 feet.

In addition to the foregoing, Mr. Morley calculated the flow at various stages, from measured slopes and sections, by means of Kutter's formula, with the following results:

Gage height on Grand Rapids gage.	Corre- sponding gage height at discharge section.	Area of cross sec- tion. (A)	Wetted perim- eter. (P)	$\begin{array}{l} \text{Hydraulic} \\ \text{radius}\\ \frac{\text{A}}{\text{P}}=\text{R}. \end{array}$	Slope.	Coefficient of rough- ness.	Mean ve- locity.	Dis- charge.
$Feet. \\ 5.67 \\ 7.32 \\ 10.32 \\ 14.32$	$Feet. \\ 2.57 \\ 4.24 \\ 7.62 \\ 11.54$	Square feet. 1,205.5 1,765.4 2,961.9 4,365.4	<i>Lineal</i> <i>feet.</i> 330.0 345.5 367.5 392.0	$3.653 \\ 5.109 \\ 8.059 \\ 11.136$	Feet per foot. 0.000035 .0000466 .0000559 .000087	0, 026 . 026 . 026 . 026 . 026	Feet per second. 0.8142 1.2187 1.8614 2.8363	$\begin{array}{c} Second-\\feet.\\981.5\\2,151.0\\5,514.0\\12,382.0\end{array}$

Calculated flow of Grand River near Grand Rapids.

A nearly continuous record of the stage of Grand River at the Chicago and West Michigan Railroad bridge, 1 mile below the dam in Grand Rapids, has been kept since May 26, 1897. A copy of this record has been furnished by George W. Bunker, United States assistant

¹Report on Survey of Grand River below Grand Rapids, War Department, 1892.

engineer. The daily gage heights, referred to the Lake Michigan datum, are given in the following tables:

Daily gage height, in feet, of Grand River at Grand Rapids, Michigan, for 1897.

Day.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1		$7.5 \\ 6.8$	6.5 6.5	6.9	$6.2 \\ 6.4$	5.9	6.3 5.9	6.4 6.4
3 4		$7.2 \\ 7.1$	6.5	$\begin{array}{c} 6.9\\ 6.7\end{array}$	$\begin{array}{c} 6.6\\ 6.4 \end{array}$	$\begin{array}{c} 6.0\\ 6.0\end{array}$	$5.8 \\ 5.9$	$6.4 \\ 6.4$
5 6 7	·····	7.0	6.3 6.3		6.1	$\begin{array}{c} 6.0\\ 5.9\\ 5.8\end{array}$	5.9 6.0	6.8 6.8
8		$6.8 \\ 7.0$	$6.3 \\ 5.4$	6.8	$6.3 \\ 6.4$	$5.0 \\ 5.9 \\ 5.8$	6.1	7.0 7.0 7.0
10 11 19		7.0 6.9 6.8	5.4 6.3		$\begin{array}{c} 6.4 \\ 6.2 \end{array}$	5.9 6.0		$7.0 \\ 7.6$
13 14		6.6	$6.5 \\ 6.8$	$\begin{array}{c} 6.6\\ 6.4 \end{array}$	$\begin{array}{c} 6.1\\ 6.2 \end{array}$	$\begin{array}{c} 6.1\\ 6.3\end{array}$	6.7	$\begin{array}{c} 8.1\\ 8.2\end{array}$
15 16 17			${f 7.3}{f 7.2}{f 7.0}$	6.4 6.4	6.2 5.9	$\begin{array}{c} 6.4 \\ 6.3 \end{array}$		8.2 8.1 8.0
18 19		$ \begin{array}{c} 7.0 \\ 6.9 \end{array} $	6.7		6.1	$\begin{array}{c} 6.1 \\ 6.1 \end{array}$	6.9 6.6	7.0
20 21 99	•••••	6.9 6.9	6.6 6.5 6.5	$\begin{array}{c} 6.3\\ 6.3\end{array}$	$6.2 \\ 6.2 \\ 6.1$	$5.9 \\ 6.1 \\ 6.2$	6.6	$7.2 \\ 7.2 \\ 7.5$
23 24			$6.5 \\ 6.6$	$\begin{array}{c} 6.2\\ 6.2\end{array}$	6.1 6.1	6.2	6.6 6.6	
25 26 27	8.2		6.5	6.3 6.3	6.0	6.0 6.0 5.9	6.7	8.4
28 29	$\frac{8.0}{7.9}$	$\begin{array}{c} 6.6\\ 6.5\end{array}$	6.5 6.9	6.4	6.9 6.0	5.7 5.8	6. 7	8.4 8.4
30 31		6.5	$7.3 \\ 7.2$	$\begin{array}{c} 6.6 \\ 6.1 \end{array}$	6.0	$\begin{array}{c} 6.1 \\ 6.1 \end{array}$	6.5	8.0 8.0

Daily gage height, in feet, of Grand River at Grand Rapids, Michigan, for 1898.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27	$\begin{array}{c} 7.9\\ 7.9\\ 7.1\\ 4\\ 4\\ 7.4\\ 4\\ 66.9\\ 7.7\\ 8.0\\ 0\\ 8.8\\ 8.8\\ 7.7\\ 7.9\\ 9\\ 8.9\\ 0\\ 2\\ 2\\ 9.4\\ 10\\ 0\\ 2\\ 9.2\\ 10\\ 0\\ 2\\ 9\\ 10\\ 0\\ 2\\ 9\\ 10\\ 0\\ 2\\ 10\\ 0\\ 1\\ 0\\ 1\\ 0\\ 1\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\$	$\begin{array}{c} 9.8\\ 9.7\\ 9.2\\ 9.3\\ 9.1\\ 9.9\\ 9.8\\ 9.1\\ 9.8\\ 11.7\\ 12.5\\ 12.8\\ 13.0\\ 13.1\\ 12.9\\ 12.9\\ 12.9\\ 13.1\\ 13.1\\ 13.1\\ 13.1\\ 13.1\\ \end{array}$	$\begin{array}{c} 12.2\\ 11.9\\ 11.4\\ 9.2\\ 9.6\\ 10.2\\ 9.6\\ 13.5\\ 15.7\\ 19.5\\ 19.7\\ 19.6\\ 18.1\\ 19.6\\ 18.1\\ 17.0\\ 16.7\\ 16.6\\ 16.4\\ 15.8\\ 13.2\\ \end{array}$	$\begin{array}{c} 14.1\\ 13.9\\ 12.4\\ 11.6\\ 11.2\\ 10.7\\ 10.3\\ 10.0\\ 9.5\\ \hline 9.0\\ 8.8\\ 8.4\\ 8.4\\ 8.2\\ 8.2\\ 8.4\\ 8.5\\ 8.7\\ \hline 8.8\\ 8.7\\ 8.8\\ 8.7\\ \hline 8.8\\ 8.8\\ 8.7\\ \hline 8.8\\ 8.8\\ 8.7\\ \hline 8.8\\ 8.8\\ 8.8\\ 8.8\\ 8.8\\ 8.8\\ 8.8\\ 8$	8.1 8.1 8.1 8.1 8.1 8.1 8.1 8.1 8.1 8.1	$\begin{array}{c} 6.8\\ 6.4\\ 6.9\\ 6.1\\ \hline \\ 6.2\\ 6.4\\ 6.5\\ 6.6\\ 6.6\\ 6.6\\ 6.8\\ \hline \\ 7.2\\ 7.0\\ 6.9\\ 6.5\\ 6.4\\ 6.5\\ 6.4\\ 6.5\\ 7.2\\ 7.4\\ \hline \end{array}$	$\begin{array}{c} 6.9\\ 7.0\\ \hline \\ 6.6\\ 6.6\\ 6.7\\ 6.5\\ 6.5\\ 6.5\\ 6.5\\ 6.4\\ 6.3\\ 6.4\\ 6.3\\ \hline \\ 6.4\\ 6.4\\ 6.4\\ 6.4\\ 6.4\\ \hline \\ 6.4\\ 6.4\\ \hline \\ 6.4\\ 6.2\\ \hline \end{array}$	6.4 6.4 6.4 6.5 6.65 6.55 6.88 6.87 6.88 6.87 6.88 6.87 6.88 6.87 6.88 6.87 9.12 7.70 7.00 7.08 6.88 6.88	$\begin{array}{c} 6.6\\ 6.7\\ 6.6\\ 6.6\\ 6.6\\ 6.6\\ 6.6\\ 6.5\\ 6.2\\ 6.2\\ 6.2\\ 6.4\\ 6.2\\ 6.8\\ 6.8\\ 6.8\\ 6.8\\ 6.5\\ 6.5\\ 6.5\\ 6.5\\ 6.8\\ 7.2\\ 7.6\\ 7.6\\ \end{array}$	6.8 6.9 6.7 6.3 6.35 6.76 6.43 6.55 6.64 6.55 6.79 6.98 7.36 7.56 7.56	1443 1443 1493 1495 1493 1495 1495 1495 1495 1495 1495 1495 1495	
28 29 30 31	9.6 9.6 9.4	12.4	$\begin{array}{c} 14.2 \\ 13.9 \\ 14.0 \\ 14.2 \end{array}$	8.6 8.5 8.3	7.3 	7.3 7.0 7.0	$\begin{array}{c} 6.2\\ 6.2\\ \end{array}$		7.2 6.8 6.8	7.6 7.7 7.6	7.8 7.9 7.9 7.9	9.9 9.6 9.2 10.0

Daily gage height, in feet, of Grand River at Grand Rapids, Michigan, for 1899.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oet.	Nov.	Dec.
1 2 3 4 5 6 7 7 8	10.0 9.3 10.2 10.3 13.0	9.9 9.8 9.4 9.4 9.0 8.9	$ \begin{array}{c} 14.1\\ 14.3\\ 14.7\\ 15.3\\ 14.9\\ 14.6\\ 14.2$	$ \begin{array}{r} 10.0\\ 9.9\\ 10.4\\ 11.4\\ 13.1\\ 14.0\\ 14.6 \end{array} $	9.39.49.59.49.79.68.7	8.6 8.4 8.3 7.9 7.6 7.6 7.4	6.0 6.2 7.0 6.7 6.8	6.9 6.8 6.5 6.8 6.9 6.6	$ \begin{array}{c} 6.4\\ 6.4\\ 6.4\\ 6.5\\ 6.6\\ 6.7\\ \end{array} $	7.2 6.7 6.7 6.7 6.7 6.7	$\begin{array}{c} 6.6\\ 7.0\\ 7.0\\ 7.0\\ 6.8\\ 7.1\\ 7.0\\ 6.9\\ 9.9\\ \end{array}$	$ \begin{array}{r} 6.7\\ 6.7\\ 6.5\\ 6.3\\ 6.3\\ 6.3 \end{array} $
9 10 11 12 13 14 15 16 17	$ \begin{array}{c} 12.6 \\ 12.0 \\ 12.8 \\ 11.2 \\ 11.2 \\ 11.4 \\ \hline 12.3 \\ 12.4 \end{array} $	8.1 8.1 8.1 8.4 8.4	$ \begin{array}{c} 13.0\\ 11.9\\ 11.4\\ \hline 12.5\\ 12.8\\ 13.1\\ 13.3\\ 13.9\\ \end{array} $	$\begin{array}{c} 16.0\\ 16.3\\ 16.5\\ 16.5\\ 16.4\\ 16.2\\ 15.7\\ 14.9 \end{array}$	8.5 8.3 8.2 8.2 8.2 7.6 7.6 7.6	7.4 7.4 6.8	6.6 6.9 6.9	$ \begin{array}{c} 6.6\\ 6.5\\ 6.4\\ 6.5\\ 6.4\\ 6.5\\ 6.5\\ 6.5\\ 6.5\\ 6.5\\ \end{array} $	$\begin{array}{c} 6.7\\ 6.6\\ 6.7\\ 6.5\\ 6.5\\ 6.6\\ 6.5\end{array}$	$ \begin{array}{c} 6.6\\ 6.4\\ 6.7\\ 6.6\\ 6.5\\ 6.6\\ 6.9\\ 6.8 \end{array} $	$ \begin{array}{r} 6.8\\ 6.8\\ 7.0\\ \hline 6.9\\ 7.0\\ 7.0\\ 7.2\\ 6.8\\ \end{array} $	6.8 7.6 7.5 7.5 7.6
18 19 20 21 22 23 24	$ \begin{array}{r} 12.4\\ 12.3\\ 12.0\\ 11.8\\ 10.6\\ 10.3\\ \end{array} $	8.1 9.1 9.4 9.4 9.4	$\begin{array}{c} 13.3 \\ 12.2 \\ 12.3 \\ 12.3 \\ 12.1 \\ 11.3 \end{array}$	$ \begin{array}{r} 14.2\\ 13.4\\ 12.3\\ 11.8\\ 11.1\\ 10.4 \end{array} $	7. 7 7. 7 7. 7 7. 6 7. 4 7. 2	6.5	6.9 6.9 6.6 6.6 6.8	6.4 6.4 6.4 6.4	$\begin{array}{c} 6.7 \\ 6.9 \\ 6.9 \\ 6.7 \\ 6.9 \\ 6.7 \\ 6.9 \end{array}$	6.9 7.0 6.8 6.8 6.9 6.9 6.6	$\begin{array}{c} 7.2 \\ 7.0 \\ 7.0 \\ 7.0 \\ 6.9 \\ 6.6 \\ 6.6 \\ 6.6 \end{array}$	7.4 7.2 7.3 7.2 7.0
25 26 27 27 28 29 30 31	$ \begin{array}{r} 9.9 \\ 10.6 \\ 10.0 \\ \hline 9.8 \\ 9.9 \\ \end{array} $	9.3 13.7 14.0	$ \begin{array}{c} 11.0\\ 10.5\\ 10.8\\ 10.8\\ 10.2\\ \end{array} $	10. 0 9. 9 9. 7 9. 4		$6.1 \\ 6.2 $	$\begin{array}{c} 6.7 \\ 7.0 \\ 7.1 \\ 7.0 \\ 6.9 \\ \hline 7.1 \end{array}$	$ \begin{array}{r} 6.6 \\ 6.6 \\ 6.3 \\ 6.3 \\ 6.4 \\ 6.4 \end{array} $	7.4 7.6 7.3 7.3 7.1	6.5 6.8 7.2 7.0	6.8 6.6 6.4	7.5 7.4 7.6 7.6 7.6

Daily gage height, in feet, of Grand River at Grand Rapids, Michigan, for 1900

Da	ay.	Jan.	Feb.	Mar.	Apr.	Day.	Jan.	Feb.	Mar.	Apr.
1			11.6 14.1 13.9 13.4 12.8 12.7 12.8 12.8	$\begin{array}{c} 8.3\\ 8.31\\ 7.99\\ 7.99\\ 7.99\\ 8.11\\ 7.8.11\\ 8.90\\ 8.822\\ 8.8$	$\begin{array}{c} 16.8\\ 16.7\\ 16.5\\ 16.3\\ 16.1\\ 15.7\\ 15.1\\ 13.5\\ 12.7\\ 11.8\\ 11.2\\ 10.6\\ 10.3\\ \hline 10.0\\ \end{array}$	17 18 19 20 21 22 23 24 25 26 27 28 29 30 30 31	7.9 7.9 7.7 7.4 7.0 6.7 7.0 8.7 8.7 8.5	$\begin{array}{c} 12.3\\ 11.5\\ 11.0\\ 10.6\\ 10.2\\ \hline 9.7\\ 9.3\\ 9.0\\ 8.5\\ 8.3\\ \hline \\ \hline \\ 8.5\\ 8.3\\ \hline \\ \hline \end{array}$	$\begin{array}{c} 8.9\\ 8.77\\ 8.77\\ 8.77\\ 8.87\\ 8.8\\ 9.8\\ 11.4\\ 12.28\\ 13.5\\ 15.4\\ 16.7\\ 17.0\\ 17.0\\ 17.0\\ \end{array}$	9.8

In 1899 the following measurements of the volume of flow of the stream were made under Mr. Bunker's direction. The measurements were made by means of rod floats spaced at intervals of 20 feet across the channel, and timed through a distance of 100 feet.

Date.	Location of section.	Eleva- tion of water surface, Lake Michigan datum.	Corre- sponding stage at Grand Rapids gage.	Mean area of section.	Mean velocity per second.	Dis- charge.
1899. Apr. 13 Apr. 23 June 19 June 29 Aug. 31 June 16 June 29 Sept. 8 Apr. 19 June 28 June 30	Brick Housedo do do do Lamont do do Grand Rapidsdo do do	$Feet. \\ 14.514 \\ 8.968 \\ 4.048 \\ 3.480 \\ 3.301 \\ 1.077 \\ .487 \\ \hline 13.334 \\ 6.142 \\ 6.168 \\ \hline$	$\begin{array}{c} \hline Feet. \\ 16.49 \\ 11.09 \\ a \ 6.39 \\ 6.17 \\ 6.44 \\ a \ 7.09 \\ 6.17 \\ 6.69 \\ 13.39 \\ 6.14 \\ 6.17 \end{array}$	$\begin{array}{c} Sq. \ ft. \\ 6, 131.6 \\ 3, 337.6 \\ 1, 437.6 \\ 1, 437.6 \\ 1, 177.0 \\ 751.2 \\ 1, 699.1 \\ 1, 402.2 \\ 1, 214.2 \\ 1, 214.2 \\ 4, 091.4 \\ 784.3 \\ 619.5 \end{array}$	$\begin{matrix} Feet. \\ 3.061 \\ 2.237 \\ 1.377 \\ 1.1877 \\ 1.210 \\ 1.206 \\ .957 \\ .749 \\ 2.554 \\ 1.903 \\ 1.756 \end{matrix}$	$\begin{array}{c} Sec.\text{-feet},\\ 18,770\\7,465\\1,986\\1,397\\909\\2,048\\1,342\\910\\10,571\\1,492\\1,098\end{array}$

Discharge measurements of Grand River.

a Approximate; interpolated.

The relation between the various sections is shown in the following table:

Table showing relation between sections on Grand River where discharge measurements were made.

Location.	Distance below Grand Rapids.	Drainage area.	Propor- tional drainage area at Grand Rapids.
Brick House Lamont C. & W. M. R. R. bridge, Grand Rapids	Miles, 4.0 16.5 0.0	$\begin{array}{c} Sq. \ miles. \\ 4,961 \\ 5,179 \\ 4,900 \end{array}$	Per cent. 98.7 94.6 100.0

A gaging was made at Grand Rapids on July 13, 1898, by W. M. Mills, C. E., from which the flow was estimated at 1,000 second-feet. The results of all gagings thus far made are summarized in the following table, the results of measurements made below Grand Rapids having been reduced to equivalent flow at the Chicago and West Michigan Railroad bridge:

 Table showing discharge of Grand River at Chicago and West Michigan Railroad

 bridge at Grand Rapids,

Date.	Hydrographer.	Stage at Grand Rapids gage.	Discharge.
		Feet.	Secfeet.
September 8, 1899	Geo. W. Bunker	6.69	862
August 31, 1899	do	6.44	897
1891	Fred Morley	5.67	981
July 13, 1898	W. M. Mills	6.29	1,000
June 30, 1899	Geo W. Bunker	6.17	1,098
June 29, 1899	do	6.17	1.270
Do	do	6.17	1.379
June 28, 1899	do	6.19	1,492
June 16, 1899	do	7.09	1.937
June 19, 1899	do	6.39	1,954
1891	Fred Morley	7.32	2 151
1891	do	10.32	5 514
April 22, 1899	Geo W Bunker	11.09	7 368
April 19, 1899	do	13 39	10.570
1891	Fred Morley	14 32	12, 382
April 13 1899	do	16 49	18 527
		10. 10	10,000

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Two gagings of the low-water flow of Thornapple River were made by L. W. Anderson on September 14, 1899, near the mouth of the stream and just above the village of Ada. The velocities were determined by means of both surface and rod floats, which were timed while passing through 100-foot sections. The flow was found to be 155 second-feet, or 0.19 second-foot per square mile from a drainage area of 824 square miles.

Float measurements of Flat River about $7\frac{1}{2}$ miles above its mouth have been made by R. J. M. Danley. Soundings were taken every 10 feet across the channel, and rod floats were put in at the same intervals. The velocity was determined by timing the floats while passing a distance of 200 feet. The drainage area above the point of measurement is 556 square miles, 46 square miles less than at the mouth of the stream.

Discharge measurements of Flat River about 7.5 miles above its mouth.

Date.	Discharge.		
July 16	Second- feet. 215	Secft. per sq. mile.	
July 29. September 5.		0.39 0.40	

Mr. Danley states that these measurements represent extreme low water preceded by a period of six weeks with little or no rain.

Arrangements have been made with L. W. Anderson, C. E., for the continuation of gagings of Grand River at Grand Rapids. A gage has been placed at the Fulton street bridge where observations of the stage of the water are taken twice daily. Current-meter measurements of the flow will be made, from which, with the measurements already available, a rating curve for the Grand Rapids cross section can be prepared.

A station has also been established on Grand River at the Schuyler street bridge in North Lansing. The river freezes over through nearly its entire length above Lansing, and in the spring large quantities of ice are brought down. At the point selected for gaging, however, the river does not freeze over, owing to the presence of a dam an eighth of a mile above.

Two miles above the North Lansing gaging station Grand River receives the drainage from Red Cedar River, on which a gaging station was established in January, 1901. The gage is located at the Grand Trunk Railroad bridge on the grounds of the Michigan Agricultural College. The stream is narrow, with gravel bed and without flood plains; the current is moderate.

The station on Red Cedar River, as well as that at North Lansing on Grand River, is under the immediate direction of Prof. H. K. Vedder, of the Michigan Agricultural College.

The drainage areas above the stations are as follows:

River.	Location.	Area.
Frand River Do Red Cedar River	Fulton street bridge, Grand Rapids North Lansing Michigan Agricultural College	Sq. miles. 4,900 1,238 358

Drainage areas above gaging stations.

The fall and the power in use at the principal dams on the main river and its branches are given in the following table. There is no storage developed on the stream. The dams are of timber, usually provided with logways, though the logging industry on the river is now practically at an end. During the winter months anchor ice is a frequent source of annoyance to water-power users. The present development involves two power canals which run parallel with the river.

Developed water powers on Grand River and its tributaries.

			Number	Effect	or fall.	Rated power of	
Stream.	Location.	Number of dam.	of mills at dam.	Great- est.	Least.	Average.	water wheels re- ported.
Grand River Do Do	Grand Rapids Lyons Three miles above Lyons.	1 2 3	24 3 1	Feet. 15 9	Feet. 6.5 4.0	Feet. 12.5 7.5	Horse- power. 2,000 150
Do Do Do Do	Portland do Grand Ledge do	4 5 6 7	$\frac{1}{2}$ None.	9	6.0	7.5	241 130
Do Do Do Do	North Lansing Eaton Rapids Winfield Jackson		6 2 2	9 9	3.0 5.0	7.0	200 140
Buck Creek Rogue River Do	Grandville Childsdale Rockford	1 1 2	1	18	8.0	13.0	400 418
Porter Creek Thornapple River Do Do	Edgerton Ada Alaska Labarge	1 1 2 3	1 2 2 1	14 8	12.0 4.0	$\begin{array}{c}13.0\\10.0\\6.0\end{array}$	52 32 90
Do Flat River Do	Middleville Lowell Three miles above Lowell.	$\frac{4}{1}$	3 1 1			$\begin{array}{c} 8.0\\ 11.0\end{array}$	297 466
Do Do Do	Alton Belding Greenville	3 4 5	$ \begin{array}{c} 2\\ 1\\ 1 \end{array} $				186
Lookinglass River Red Cedar River - Do	Portland Okemos Williamstown	1 1 2	20202	8	4.0	7.0	203

Water power was originally developed at Grand Rapids in 1836 by the construction of a rubble diverting or wing dam on the limestone ledge at the east side of the stream. In 1851–52 a dam was built across the stream and the width of the east side canal was increased to 60 feet, with the intention of providing slack-water navigation past the Long Rapids at this point. In 1866 W. T. Powers purchased the water privilege on the west side of the stream, and joined with the power users on the east side to build the present timber dam, the crest line of which is 678 feet long. The east side canal is 2,560 feet long and the west side canal 3,750 feet long.

Where the space between the canals and river does not permit of the erection of mills or factories, wheel pits are placed at the river's edge and the power is carried to the mills by telodynamic transmission.

Each canal is entitled to half the flow of the stream. Water privileges on the east side were sold by priority, beginning at the lower end of the canal. The flow in the west side canal, constituting half of the power of the stream, was divided into 66 equal parts or "runs." The net power of one run of stone, at the ordinary stage of the stream and under a head of $12\frac{1}{2}$ feet, has been fixed at 15 horsepower. On this basis the ordinary effective power available at Grand Rapids is estimated at 2,000 horsepower. The power is utilized in the manufacture of furniture, in flour mills, machine, iron, and brass works, and for the generation of electricity. In addition power is transmitted electrically to Grand Rapids from the plant of the Peninsular Electric Company on Flat River, above Lowell. The transmission line is 16 miles long, the tension 10,000 volts.

The foregoing list of water powers does not include a number of rural grist and feed mills on the smaller tributaries, some of them very small, only permitting the mills to run intermittently by holding back the flow as pond storage. Abandoned sites where dams have been washed out are not infrequently found. These were used to supply power for sawmills which have long since ceased to be operative through lack of timber supply.

The fall at Grand Rapids aggregates 18 feet, and the available power could be greatly increased by constructing a new dam, increasing the head, and concentrating the entire flow in one wheel pit, for the generation of electricity. It is estimated that an average of 2,200 horsepower net can be obtained 8 months of the year, from May to December, while during the four spring months a minimum of 3,200 horsepower will be available, with the exception of a few days, when the head will be reduced by backwater to 6 feet or less. The plan contemplates the erection of a 12-foot concrete dam, the construction of a power canal along the stream bed, and the excavation of the tailrace channel $2\frac{1}{2}$ feet below the present bed of the river. It would admit of the filling in of the present power canals and the reclamation of valuable land along the river front.¹

The available power of the main stream is for the most part utilized. It is stated that a site exists between Lyons and Portland where a head of 12 feet could be obtained by the erection of a dam 10 feet

¹ Report on Development of Water Power, Grand Rapids, Michigan. Rae and Monroe, Chicago, 1899.

high. A dam is also contemplated at Delta, 7 miles downstream from Lansing, where a fall of 7 feet is available.

Four miles above Lowell, Flat River forms a bend 5 miles in circumference. The natural difference in elevation of the stream at the two ends of the loop is 11 feet. By building a dam 20 feet high on the upstream side, and carrying the water across the neck of the bow, a head of 30 feet could be obtained, which would yield a minimum of 1,000 horsepower.

On Rogue River, 1 mile below Childsdale, a dam could be erected which would afford a head of 20 feet. Other unimproved privileges are at Fallassburg on Flat River, where a 12-foot head is available at Ada and Cascade on Thornapple River, and at Maple Rapids and other points on Maple River. There are also two abandoned powers on Buck Creek in the vicinity of Grandville, at each of which a head of 12 to 14 feet could be obtained.

Much of the available power on tributaries of Grand River is, however, of little value, owing to irregular flow, limited supply, and remoteness from population centers.

MUSKEGON RIVER, MICHIGAN.

The drainage basin of this stream lies immediately north of that of Grand River. Originally it was covered with pine timber, but now it is almost entirely cleared. Much of the soil is sand and gravel, unfit for profitable cultivation. Large stump-covered areas form a conspicuous feature of the topography. The drainage areas tributary to the stream are given in the following table:

Stream.	Location.	Area.
Muskegon River Clam River Muskegon River Do. Do. Do.	Above Clam River	Sq. miles. 787 307 1,094 1,764 2,352 2,663

Drainage areas o	f Muskegon	River and	tributary.
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In March, 1901, a station was established at the dam of the Newaygo Portland Cement Company. This dam crosses Muskegon River in a deep valley above the village of Newaygo. It is of timber, having framed cribs filled with stone. Its height is 21 feet; it rests on a hardpan foundation, and is considered to be practically water tight. It is provided with a main spillway, with logways, and with four floodways. The floodways are provided with Taintor segmental flood gates, which are operated by a traveling crab. A record is kept of the time and amount of opening of the flood gates and logways, as well as of the depth of water on the crests of the spillways. Ordinarily the flood gates and logways are closed, and the entire flow passes over the main spillway or through the turbines. Water is carried from the pond to the power house by a short headrace separated from the stream channel by a crib breakwater.

The power house contains two pairs of 35-inch Leffel standard turbines on horizontal shafts. The water wheels are connected to electrical generators by endless rope drives. The power will be used for driving machinery in the adjoining cement mills, and the load and consequent discharge of the turbines will be fairly constant. The record kept for the water wheels includes working head, hours run per day, and average width of gate opening for each pair of wheels, as indicated by the Lombard governors.

A gaging of Muskegon River at Big Rapids was made August 27, 1881, by Frederick P. Stearns, civil engineer, and the discharge was found to be 877 second-feet. This amount is taken as the ordinary flow, and is used in partitioning the water power among the several privileges at Big Rapids.

The Newaygo dam is the first one above the mouth of the stream. An effective head of 14 feet is obtained there. Power is also developed at Big Rapids, where there are two dams. The lower dam is a rough timber structure, built with a view to its use in log driving. One hundred and seventy-two horsepower is now in use for the generation of electricity, the head obtained being 8 feet. At the upper dam in Big Rapids power is distributed through two lateral hydraulic canals. The total flow is estimated as equivalent to the discharge through an orifice of 6,758 square inches area under a head of 8 feet, with a coefficient of contraction of 0.7. Each user is entitled to install wheels having a certain number of square inches vent. The head varies from $6\frac{1}{2}$ to 11 feet, the average or ordinary head being 8 or 9 feet. The rated power of the turbines installed is 668 horsepower. It is stated that but 350 horsepower is actually in use. The power utilized at Newaygo and Big Rapids aggregates 1,000 horsepower. Aside from the foregoing, there is no power developed within the drainage basin, except in a small way on certain tributaries.

From the vicinity of Evart to Newaygo, Muskegon River flows between high banks, and has a rapid fall. Levels, which have been run for this purpose, show that within a distance of 10 miles, 5 miles each way from Big Rapids, there is a total fall of 104 feet. Of this 16 feet is now utilized, leaving an available fall of 88 feet. There are favorable sites for the location of dams, so that practically the entire fall could be economically developed. At Rogers's bridge, 6 miles below Big Rapids, surveys have been made for the erection of a dam to give a head of 35 feet.

In connection with power development, good opportunities exist for the conservation of flow by artificial storage. The water-surface areas of the principal lakes of the watershed and of the tributary drainage which they control is given below. Drainage and surface areas of lakes in Muskegon River watershed.

Lake.	Drain- age area.	Water surface.
Muskrat Lake and group Clam Lakes Higgins Lake Houghton Lake (not including Higgins Lake) Higgins and Houghton lakes	Sq. miles. 57 67 67 185 252	$Sq. miles. \\ 8.0 \\ 6.7 \\ 15.0 \\ 31.0 \\ 46.0$

In the upper portion of the watershed there is a total lake area of about 110 square miles. Formerly a lumbermen's dam was maintained for the purpose of flooding logs between Houghton and Higgins lakes, but this has been washed out. A properly constructed dam at this site would flow an area of 15 square miles and would yield a storage of 400,000,000 cubic feet per foot of depth. A lumbermen's dam, built of logs and earth, which still remains about a mile below the foot of Houghton Lake, raises the water level in that lake 4 feet, providing a storage of, in round numbers, 3,350,000,000 cubic feet. Thomas H. Coughlin, superintendent of the Muskegon Booming Company, states that a dam could be constructed at this site which would admit of a total storage 8 feet in depth and would greatly increase the flooded area over that of the present lake.

HURON RIVER, MICHIGAN.

This river receives drainage from a broad, flat basin interspersed with lakes, situated in southeastern Michigan. The inland basin is connected with Lake Erie by a long, narrow valley, in which occurs a large portion of the fall and available power of the stream.¹ A gaging station has been established at Ann Arbor, under the immediate charge of Prof. J. B. Davis, of the University of Michigan. Currentmeter measurements are made from a temporary bridge or by fording. The stream at this point is winding. It flows in a shallow channel, and ordinarily does not overflow its banks. The bed is generally of gravel. The river usually freezes over during the winter, except immediately below the dams. Natural storage in the numerous lakes and marshes regulates the flow to some extent. The character of the watershed has changed somewhat in recent years. Areas of tamarack swamp lands, the soil of which was formerly a quaking bog, have been cleared and drained and are now under cultivation. The drainage area above the mouth of the river is 1,043 square miles; above Ann Arbor it is 841 square miles. A gaging of the bank-full flow of the stream at the Geddes dam, 3 miles below Ann Arbor, was made by Professor Davis, and the estimated discharge was 1,200 second-feet. The Geddes dam has a flat crest and is practically water tight. The

¹A report on the water power of Huron River, by James T. Greenleaf, C. E., was published in the Tenth Census of the United States, Vol. XVI, Water Power, Pt. I, pp. 443-495.

length of the crest is 200 feet and the depth of water on the crest at the time the measurement was made was 1.7 feet.

THUNDER BAY RIVER, MICHIGAN.

Thunder Bay River is joined by two large branches 8 and 10 miles above its mouth, respectively. These branches, as well as the main stream, are further subdivided at short distances upstream, so that the river is of relatively small magnitude, except for a few miles near its mouth, where occurs the outcrop of the Traverse shales. It is in passing over this rock ledge that the most rapid fall of the stream occurs. The drainage area was formerly heavily timbered with Michigan pine. Most of the pine has, however, been cut, but a large amount of small conifers, hard woods, white birch, and cedar remains, so that the watershed may be considered as representing a forested rather than a cleared area. A record of precipitation is kept at Alpena, near the mouth of the stream. The outcrop of the Traverse and St. Clair shales crosses the watershed in a northeast-southwest direction. crossing the river channel a few miles west of Alpena. The surface above the line of this outcrop is almost continuous limestone, composed of calcium carbonate of 96 to 98 per cent purity, small areas being covered with sand or with thin drift deposits.

No water powers of importance have been developed on either of the branches. On the main stream there are two power dams. The lower one, which is at Alpena, was constructed in 1862. It is 1 mile from the head of Thunder Bay, an arm of Lake Huron. The river is navigable to the dam, forming a harbor. The dam and privileges of the river are owned jointly by the Alpena Waterworks Company and the Alpena Booming Company. The water wheels installed have a rated capacity of 864 horsepower under a head of 9 feet. The power is used for pumping the municipal water supply and for the generation of electricity. The second dam is at the mill of the Fletcher Paper Company, 4 miles above Alpena, and 2,000 horsepower is developed from a fall of 17 feet. The only dams above the Fletcher mills are those used for floating logs. Spruce dam, at Long Rapids, gives a head of 7 or 8 feet. At Lower Rapids a head of 20 feet could be obtained by the construction of a dam.

The drainage basin of Thunder Bay River contains thirty lakes, with an average area of about 1 square mile. In addition to these is Hubbard Lake, which has a water surface of 13.4 square miles. A timber dam at the foot of the latter lake produces a storage depth of 5 feet, with an aggregate storage capacity of 1,867,500,000 cubic feet, equivalent to a flow of 68 second-feet for thirty days. A similar dam at the foot of Beaver Lake gives a storage depth of 6 feet. The water from Beaver Lake is used chiefly for driving logs.

The limestone area contains numerous sink holes, often deep and precipitous. Surface water entering these pits disappears with greater

or less rapidity by finding outlets to a lower level through limestone fissures. Such a pocket, known as Sunken Lake, is located near the north branch of Thunder Bay River, and it absorbed the entire flow of that tributary, involving a considerable loss to power users, until, in 1900, a clay puddle dam was constructed across the channel leading from the stream to the sink hole in such a manner as to turn the water down its original channel. Owing to the pervious nature of the rock strata the effective and apparent boundaries of the watershed may differ materially.

The drainage areas tributary to the stream are as follows:

Stroom	Location	A 1100				
stream.	Location.					
		Sa. miles.				
South Branch	Above mouth	454				
North Branch	do	199				
Thunder Bay River	Above mouth of North Branch	580				
Do.	Above mouth of South Branch	789				
Do	At Alpena.	1,267				
Hubbard Lake	(Water surface)	134				
Do	(Drainage area)	148				

- uinage areas o	of Thunder	Bay River	and tributaries
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A gaging station has been established in connection with the dam and mill of the Fletcher Paper Company. The record kept includes the depth flowing over the main dam and logway and the discharge through the turbines. There are four pairs of Trump Model wheels set on horizontal shafts. The water wheels are not run otherwise than at full gate. The dam, which is of timber crib work filled with stone, is on a limestone rock foundation and is 20 feet high and 454 feet long between abutments. A log slide divides the spillway into two sections. The slide has a channel 6 feet in width and is closed by plank flashboards to an elevation of 1 foot above the crest line. The spillway has a vertical face and a crest 4 feet in width, sloping upstream, with a batter of 1 vertical to 5 horizontal. The upstream face of the dam has a batter of about 3 horizontal to 1 vertical. The left section of the spillway is $255\frac{1}{4}$ teet long. The flat crest is covered with sheet iron, slightly rounded at the lip. The right spillway section is 181.7 feet in length, and the crest is faced with planking.

ST. JOSEPH RIVER, MICHIGAN.

St. Joseph River rises at Bunday Hills, in northern Hillsdale County, Michigan. flows southwesterly into Indiana, turns northward at South Bend, recrosses the State line near Bertrand, and debouches into Lake Michigan at St. Joseph. The total area drained is, approximately, 4,586 square miles, of which 2,916 square miles are in Michigan and 1,670 square miles in Indiana. The drainage basin contains more than 400 small lakes, varying in surface area from an eighth of a square mile to 6 square miles. Of these, approximately 100 are in Indiana and 300 in Michigan. No storage is developed on the stream. The drainage areas of the river and its more important tributaries are given in the following table:

	Area.
Above Three Rivers	Sq. miles.
Above month	164
do	178
do	213
Below Three Rivers	1.417
Above Niles	3,616
Above mouth	281
Below mouth of Dowagiac River	3,898
Above mouth of Pawpaw River	4,157
Above mouth	429
Below mouth of Pawpaw River	4,586
	Above Three Rivers Above mouth do do Below Three Rivers Above Niles Above mouth Below mouth of Dowagiac River Above mouth of Pawpaw River Above mouth Below mouth of Pawpaw River

Drainage areas of St. Joseph River and its tributaries.

The drainage basin lies in a completely glaciated region, and is overlain with diversified drift deposits. The current of the river from South Bend to its mouth was formerly reversed, and this valley formed an outlet for the waters of Lake Michigan, which turned to the southwest, through Kankakee River, at South Bend, and thus reached the Mississippi through Illinois River. Leverett states¹ that there is still a well-defined river channel connecting St. Joseph River with the Kankakee, the surface of which, where it leaves the St. Joseph, is but 45 or 50 feet above the present low-water surface of that stream. The watershed of St. Joseph River in Michigan contains relatively little marsh land not artificially drained and relatively little uncleared land. About a third of the lakes are, however, without outlets. The proportion of undrained lakes in Indiana is smaller, and the swamp lands are much more extensive.

Elkhart River, one of the principal Indiana tributaries of the St. Joseph, drains an area of about 500 square miles which contains large lakes and extended swamp areas, with the principal fall occurring in the passage of the stream from marsh to marsh.

St. Joseph River was formerly navigable for boats as far as Elkhart, or perhaps above, and the older dams were provided with locks, long since abandoned and closed. Prof. James Du Shane is of the opinion that at the present time the low-water depth of the river over the rapids is from $1\frac{1}{2}$ to 2 feet. A rise of 5 feet represents ordinary high water, and a rise of 8 feet represents extreme high water. Within the last twenty-two years two freshets have occurred which raised the water in some portions of the river higher than here given. The average width from bank to bank is 400 feet, and the average slope from Elkhart to Berrien Springs is 2.1 feet to the mile.

The first water-power mill in southwestern Michigan was constructed by Eli Ford, in 1827, on Dowagiac Creek, near its confluence with St.

¹ Water resources of Indiana and Ohio, by Frank Leverett: Eighteenth Ann. Rept. U. S. Geol. Survey, Pt. IV, p. 439.

Joseph River, at Niles. This mill, known as the Volante mill, has been in operation since 1828. Power development on St. Joseph River began at a somewhat later date. The dam at Niles was built about 1856. At South Bend the power was developed by the South Bend Manufacturing Company, and was sold in the form of rights to the flow through wheels of a certain number of square inches vent under the available head. The dam is 10 feet high, with lateral power canals on each side. Under an order of the court the water is to be maintained at a stage not lower than 6 inches below the crest of the dam. Nineteen privileges have been granted, alling for a flow of 3,195.5 cubic feet per second under a head of 9.5 feet. Fourteen of these privileges are now in use. The minimum flow of the stream is usually considered to be 1,000 second-feet, but it is stated to have gone considerably lower during the months of July and August, 1895. At Elkhart there is a similar power development, the flow of the stream being divided among eleven mills. The power at Elkhart was originally divided by priority, the amount being specified as so many runs of stone, or "sufficient for the purpose of the mill."

The following table gives the principal facts regarding water power in the St. Joseph River Basin, so far as reported:

					Effecti	ve head	or fall.	Bated
Stream.	Location.	Dam numbe r .	N c a	Number of mills at dam.	Greatest.	Least.	Average.	power of water wheels reported.
St. Joseph River Do Do Do Do	Buchanan Niles South Bend Mishawaka Elkhart.	$ \begin{array}{c} 1 \\ 2 \\ 3 \\ 4 \\ 5 \end{array} $		2 14 3 3	Feet. 12.0 11.0 13.0	Feet.	$Feet. \\ 11.0 \\ 12.0 \\ 9.5 \\ 10.0 \\ 10.0$	Horse- power. 4,018 2,588 1,760 1,920
Do Do Do	Constantine Three Rivers Below Mendon Burlington	6 7 8 9		3	10.0	6.0	8.5	600
Do Do Pawpaw River Do	Tekonsha Watervliet Hartford	$10 \\ 1 \\ 2 \\ 2 \\ 2 \\ 3 \\ 3 \\ 3 \\ 3 \\ 3 \\ 3 \\ 3$		1 1	$\begin{array}{r} 8.0\\ 14.0\end{array}$	6.0 6.0	$\begin{array}{r} 7.0\\ 10.0 \end{array}$	89 600
South Branch of Pawpaw River.	Pawpaw	3 1		1	14.0	12.5	13.5	132
Do Spring Brook Dowagiac Creek	Almena Niles	2 1 1	-	1	17.0		17.0 12.0	108 356
Pokagon Creek South Branch of Dowagiac Creek	Above Niles Summerville Dowagiac	2 1 1		1 1	10.0	8.0	14.5 9.0	715 95
Do. Christiana Creek Elkhart River	Lagrange Elkhartdo	2 1 1			8.5	4.0	7.0	60
Do. Do.	Goshen Benton	23	-	2	17.0	10.0	14.5	700
Rocky River Swan Creek Coldwater River Do	Colon Union City Above Union	$\begin{array}{c}1\\1\\1\\1\\2\end{array}$		1 1 1 1 1	10.5 15.0 10.0 9.0	8.5 11.0 5.0	9.5 14.0 8.0 9.0	297 459 107 52
Do Nottawa Creek	City. Hodunk Athens	3 3		1 1	9.0	6.5	8.0	35

Developed water powers in St. Joseph River Basin.

D

There are a number of undeveloped powers between the present dams, and projects are now formed to utilize them. The power is to be used largely for the generation of electricity for transmission to neighboring towns. A part of it will supplement the power at existing dams. At Berrien Springs, Michigan, a concrete dam 30 feet in height is proposed. This will make available a fall of 20 feet. Eighteen water wheels of a rated capacity of 7,500 horsepower are to be installed. This power is in sec. 18, T. 17 W., R. 6 S., Michigan meridian. At Bertrand, Michigan, a fall of 12 feet could be obtained by the construction of a suitable dam.

Two available sites for dams exist between Mishawaka and Elkhart, Indiana. The former is in sec. 11, T. 38 N., R. 2 E., second principal meridian, where a 12-foot fall is available. The width of the river is about 350 feet. The latter site, called the Twin Branch site, is in sec. 12, T. 37 N., R. 3 E., second principal meridian. A dam 422 feet long is proposed at this point, which would make available a fall of 21 feet.

At Bristol, Indiana, a dam formerly existed, but it was washed out. A site exists in sec. 31, T. 38 N., R. 5 E., second principal meridian, where a fall of 16 feet could be obtained by the construction of a dam 600 feet in length.

At Mottville, Michigan, in sec. 6, T 8 S., R. 5 W., Mic¹, igan meridian, a fall of $9\frac{1}{2}$ feet could be obtained by the construction of a dam 540 feet in length.

An undeveloped water power also exists near Three Rivers, Michigan, in sec. 1, T. 6 S., R. 11 W., where about 9 feet fall could be obtained.

The available power of tributaries of St. Joseph River is of little value, as is indicated by the existence of numerous abandoned sites where dams have been carried away by freshets. At Ligonier, Indiana, a dam formerly existed on Elkhart River, but it was washed out. There are three undeveloped powers on Pawpaw River, in Antwerp Township, Van Buren County, Michigan, with falls of 9 feet, 14 feet, and 9 feet, respectively.

Arrangements have been made with the Berrien Springs Power Company for the maintenance of a record of flow of St. Joseph River at their plant when completed. The record will include discharge over the 500-foot concrete dam, and the run of water wheels, which will be 18 in number, arranged in sets of three pairs each. In the meantime a temporary gaging station has been established at the dam of the Berrien Springs Power Company at Buchanan, Michigau, 10 miles above Berrien Springs. The dam is of timber, of the Beardsley gravity type, with a straight crest approximately 400 feet long. It is 9.83 feet high, and is built on an earth foundation.

In January, 1891, the following gaging of St. Joseph River was made by John F. Meighan at Leepers Bridge, 1 mile below the dam at South Bend:

Discharge measurement of St. Joseph River at Leepers Bridge in January, 1891.

Elevation of water surface above city datum(feet)	7.57
Area of cross section	1,232
Wetted perimeter(lineal feet)	262.91
Hydraulic mean radius	4.686
Slope	0.000378
Coefficient of roughness in Kutter's formula	0.030
Coefficient c in Kutter's formula	65
Mean velocity	2.735
Discharge	3,369

The stated depth of extreme high water on the crest of the Niles dam is 5 feet, indicating a freshet discharge of about 15,000 secondfeet, or 4.5 second-feet per square mile. The extreme high-water flow over the Dowagiac River dam at Niles is stated to be 2 feet depth on the crest of the 120-foot spillway, corresponding to a flow of about 1,200 second-feet, or 4.3 second-feet per square mile, from a drainage area of 281 square miles.

KALAMAZOO RIVER, MICHIGAN.

The details of the hydrography of this stream have been given in an earlier report.¹ The drainage areas of the river and its tributaries are as follows:

Drainage areas of Kalamazoo River and its tributaries.

Stream.	Location.	Area.
North Branch of Kalamazoo River. South Branch of Kalamazoo River. Do. Do. Battle Creek. Kalamazoo River Do. Do. Do. Do. Do. Do. Do.	Albion do Below junction of North and South branches Marshall Above Battle Creek At mouth Below Battle Creek At Plainwell At Allegan Lt mouth	Sq. miles. 138 136 274 443 609 244 847 1, 307 1, 508 2, 064

The accompanying table gives a summary of the developed water powers of the drainage basin. Most of the powers on the main stream are utilized. In 1898–99 a dam giving 23 feet head was built between Allegan and Otsego, to develop 2,000 horsepower for electrical transmission. This plant has the merit of being the first large long-distance transmission plant in the State.² A portion of the fall between this dam and Allegan is still undeveloped, and it is claimed that a head of 20 feet could be obtained by the construction of a dam 2 miles above that city. Above Otsego, on the main river, there are one or two rapids having falls of several feet which are not yet developed.

¹ Report on the run-off and water power of Kalamazoo River, by Robert E. Horton: Water-Supply and Irrigation Paper U.S. Geol. Survey No. 30, pp. 22-38.

² Proc. Mich. Eng. Soc. 1900, pp. 84-91; also Engineering Record, Jan. 13, 1900.

		N .	Number	Effect	Rated power		
Stream.	Location.	of dam.	of mills at dam.	Greatest.	Least.	Average.	of water wheels reported.
Kalamazoo River. DoDo DoDo DoDo DoDo DoDo DoDo DoDo DoDo DoDo DoDo DoDo DoDo Do Do Do Do Comboo Creek Augusta Creek Gull Lake outlet. Do Do Comstock Creek Portage Creek Wabasaco Creek Wabasaco Creek	Allegan Above Allegan Otsego Plainwell Battle Creek do Ceresco Marshall Marengo Albion Newburg Mills Bath Mills Concord Horton Albion North Homer Homer Mosherville Marshall Battle Creek Bellevue Olivet Augusta Galesburg Howkandsburg Yorkville Comsock Kalamazoo Eckford Bedford	$\begin{array}{c} 1\\ 2\\ 3\\ 4\\ 5\\ 6\\ 7\\ 8\\ 9\\ 10\\ 11\\ 12\\ 13\\ 14\\ 15\\ 12\\ 3\\ 4\\ 1\\ 1\\ 2\\ 3\\ 4\\ 1\\ 1\\ 2\\ 3\\ 1\\ 1\\ 1\\ 2\\ 3\\ 1\\ 1\\ 1\\ 2\\ 3\\ 1\\ 1\\ 2\\ 2\\ 3\\ 1\\ 1\\ 2\\ 2\\ 3\\ 1\\ 1\\ 2\\ 2\\ 1\\ 1\\ 2\\ 2\\ 1\\ 1\\ 2\\ 2\\ 1\\ 1\\ 2\\ 2\\ 1\\ 1\\ 2\\ 2\\ 2\\ 1\\ 1\\ 2\\ 2\\ 2\\ 1\\ 2\\ 2\\ 2\\ 1\\ 2\\ 2\\ 2\\ 2\\ 2\\ 2\\ 2\\ 2\\ 2\\ 2\\ 2\\ 2\\ 2\\$		Feet. 12 14 14 11 11 11 11 11 11 11 11 11 11 11 11 11 11 11 11 12 12 12	Feet. 10 12 12 12 12 12 12 11 12 11 12 11 12 11 12 10 11 12 10 10 10	Feet. 23.0 12.0 12.0 9.0 12.0 6.0 13.0 9.0 10.0 10.0 12.0 6.0 12.0 10.0 12.0 10.0 12.0 10.0 11.0 20.0 11.5 11.5	Horse- power, 1,150 2,000 1,725 786 469 200 118
Comstock Creek	Above Comstock	2	1			23.0	35

Developed water powers in Kalamazoo River Basin.

a Undershot water wheel.

It is stated that a dam could be built 1 mile above the mouth of Swan Creek, which enters Kalamazoo River 8 miles below Allegan, and a head of 40 feet be obtained.

During a portion of 1900 a daily record of the river stage was kept at Kalamazoo, the results of which are given on the following page. Earlier records will be found in Water-Supply Paper No. 30, page 36. Arrangements have been made for the maintenance of a gaging record at the electric-power dam at Trowbridge, 6 miles above Allegan. The plant includes four pairs of 45-inch Leffel-Sampson turbines on horizontal shafts. The gate opening and discharge of two pairs are controlled by Lombard governors. The excess of flow not taken by the turbines is discharged over a spillway having three Taintor flood gates, each 20 feet long. The spillways have flat crests 20 feet in width, with slopes of 1 to 1 on the upstream and downstream faces. The discharge on the downstream side is received on a floating apron 20 feet in width, which is anchored to the flood-gate cribs by chains.

Daily gage height, in feet, of Kalamazoo River at foot of Sheldon street. Kalamazoo, Michigan, for 1900.

Day.	Sept.	Day.	Sept.	Day.	Sept.	Day.	Sept.	Day.	Sept.
6 7 8 9 10	$68.45 \\ 68.32 \\ 68.25 \\ 68.15$	11. 12. 13. 14. 15. 15.	$\begin{array}{c} 68.20\\ 68.15\\ 68.00\\ 67.90\\ 68.02 \end{array}$	$ \begin{array}{c} 16 \\ 17 \\ 18 \\ 19 \\ 20 \\ \end{array} $	$\begin{array}{c} 68.05\\ 67.90\\ 67.90\end{array}$	21 22 23 24 25		26 27 28 29 30	67.90

NOTE.—On August 9 the gage height was 68.50 feet.

Daily gage height, in feet, of Kalamazoo River at Gull street, Kalamazoo, Michigan, for 1901.

Day.	Mar.	Day.	Mar.	Day.	Mar.	Day.	Mar.	Day.	Mar.
16 17 18 19	69.86 70.10 70.75	2021212222	$\left\{\begin{array}{c} 71.\ 10\\ 71.\ 72\\ 72.\ 12\\ 71.\ 97\end{array}\right.$	23 24 25	$71.87 \\ 71.66 \\ 71.52$	$26 \dots 27$ 27 28 \dots 28	71.40 71.48	29 30 31	71.27

NOTE.-Gage height on April 1 was 70.04 feet, and on April 12, 68.02 feet.

Daily gage height, in feet, of Kalamazoo River at extension of Paterson street, Kalamazoo, Michigan, for 1900.

Day.	Sept.	Day.	Sept.	Day.	Sept.	Day.	Sept.	Day.	Sept.
$ \begin{array}{c} 1 \\ 2 \\ 3 \\ 4 \\ 5 \\ \end{array} $	$\begin{array}{c} 68.71\\ 68.54\\ 68.47\\ 68.41\\ \end{array}$	$ \begin{array}{c} 6. \\ 7. \\ 8. \\ 9. \\ 10. \\ \end{array} $	$\begin{array}{c} 68.10 \\ 68.23 \\ 68.10 \\ 68.10 \\ 67.99 \end{array}$	$\begin{array}{c} 11 \\ 12 \\ 13 \\ 14 \\ 15 \\ \end{array}$	67.90	$\begin{array}{c} 16 \\ 17 \\ 18 \\ 19 \\ 20 \\ \end{array}$		21 22 23 24	$\begin{array}{c} 68.20\\ 67.98\\ 67.94\\ 68.09 \end{array}$

STREAMS OF NORTHERN PENINSULA OF MICHIGAN.

The streams of the northern peninsula of Michigan are contrasted with those of the southern portion of the State by their steep slopes, rocky channels, and occasional waterfalls. They possess numerous water powers, which are almost wholly undeveloped, and many of which are in close proximity to the mining centers of the iron and copper region. Arrangements are being made for the establishment of a gaging station on one of the larger streams.

On Ontonagon River at Glenns Falls a head of 100 feet could be obtained, which would yield an estimated minimum of 4,500 horsepower. This is in sec. 31, T. 50 N., R. 31 W., about three-fourths of a mile south of the Victoria mine. Ontonagon River is the largest Lake Superior tributary in Michigan. It extends entirely across the northern peninsula, and finds its headwaters in a region of numerous small lakes near the Wisconsin-Michigan line. Its fall is mostly concentrated in the short stretch between the summit of the Michigan Range at Rockland and its entrance to Lake Superior at Ontonagon. Owing to the lack of a map on suitable scale, the drainage area can not at present be estimated.

Dead River, tributary to Lake Superior at Marquette, possesses a fall of 850 feet in a distance of 10 miles.

Much of the southern slope of the upper peninsula drains into Menomine'e River, a tributary of Green Bay. A report on that river was published in the Tenth Census of the United States.¹ Other streams possessing good falls and opportunities for lake storage in the region of their headwaters are the Escanaba, Manistique, Michigamme, and Tahquemenon rivers.

MISSISSIPPI RIVER AT ST. PAUL, MINNESOTA.

Records of gage heights are maintained by the United States Weather Bureau at St. Paul, and are furnished to the Geological Survey. The station is described in Water-Supply Paper No. 36, page 194.

Daily gage height, in feet. of Mississippi River at St. Paul, Minnesota, for 1500.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
$\begin{array}{c} 1 \\ 2 \\ 3 \\ 3 \\ 5 \\ 5 \\ 5 \\ 6 \\ 7 \\ 8 \\ 9 \\ 10 \\ 10 \\ 11 \\ 12 \\ 10 \\ 11 \\ 12 \\ 13 \\ 14 \\ 15 \\ 15 \\ 16 \\ 17 \\ 17 \\ 18 \\ 19 \\ 20 \\ 21 \\ 22 \\ 22 \\ 22 \\ 22 \\ 22 \\ 22$	a 4. 4 a 3. 9 a 3. 8 a 3. 8 a 3. 8	a 6.3	a3.2 a3.7 a3.7 a3.7	$\begin{array}{c} 4 \\ 0 \\ 2 \\ 1 \\ 3 \\ 3 \\ 3 \\ 3 \\ 4 \\ 4 \\ 5 \\ 5 \\ 5 \\ 5 \\ 5 \\ 5 \\ 5 \\ 5$	1-1-22021-1-540-1-520920209-0-6-1-20001-202000 020020000000000000000000	$\begin{array}{c} 209165544488995543111111111111111111$	$\begin{array}{c} 0 & .7 & 0 \\ . & .1 & 0 & 0 & 6 & 9 & 9 & 0 \\ . & .2 & .2 & .2 & .2 & .2 & .2 & .2 $	$\begin{array}{c} 1,1,2,2,2,0\\ 1,1,1,2,2,2,2,3,3,3,4,2,3,3,3,4,4,5,7,0,4,4,4,4,4,4,4,4,4,4,4,4,4,4,4,4,4,4$	$\begin{array}{c} 430875209243875321025799000098\\ 5555555555555555555$	88993563209877433339108865535653 5555666665555555555544444444444	$\begin{array}{c} 4.555.\\ 4.5566.\\ 4.54.56.\\ 4.54.32.\\ 4.4.4.32.\\ 2.2.001.\\ 1.2.2.0.\\ 1.96.38.\\ 2.2.0.\\ 1.96.38.\\ 2.2.0.\\ 1.9.6.38.\\ 2.2.0.\\ 1.9.6.38.\\ 2.2.0.\\ 1.9.6.38.\\ 1.2.2.0.\\ 1.9.6.38.\\ 1.2.2.0.\\ 1.9.6.38.\\ 1.2.2.0.\\ 1.9.6.38.\\ 1.2.2.0.\\ 1.9.6.38.\\ 1.2.2.0.\\ 1.9.6.38.\\ 1.2.2.0.\\ 1.9.6.38.\\ 1.2.2.0.\\ 1.9.6.38.\\ 1.2.2.0.\\ 1.9.6.38.\\ 1.2.2.0.\\ 1.9.6.38.\\ 1.2.2.0.\\ 1.9.6.38.\\ 1.2.2.0.\\ 1.9.6.38.\\ 1.9.6$	$\begin{array}{c} 2.0\\ 2.0\\ 2.0\\ 0\\ 2.2\\ 0\\ 2.2\\ 2.3\\ 3\\ 2.2\\ 2.3\\ 2.2\\ 2.3\\ 2.2\\ 2.3\\ 2.2\\ 2.3\\ 2.2\\ 2.3\\ 2.3$

a Approximate; river frozen.

b River frozen.

WEST GALLATIN RIVER NEAR SALESVILLE, MONTANA.

This station, which was established in July, 1895, is located at the highway bridge crossing the stream about 5 miles south of Salesville. It is described in Water-Supply Paper No. 36, page 195. Results of measurements for 1899 will be found in the Twenty-first Annual

¹ Vol. XV1I, Water Power, Pt. II, pp. 71-81.

MONTANA.

Report, Part IV, page 184. During 1900 the following discharge measurements were made under the direction of Samuel Fortier:

Discharge measurements of West Gallatin River near Salesville, Montana.

	Gage	Dis-	Date.	Gage	Dis-
Date.	height.	charge.		height.	charge.
1900. May 23 Do June 18. June 24	$\begin{array}{c} Feet. \\ 4.86 \\ 5.90 \\ 5.90 \\ 4.72 \\ 4.51 \end{array}$	$\begin{array}{c} Secft. \\ 1,944 \\ 3,727 \\ 3,796 \\ 2,028 \\ 2,039 \end{array}$	1900. July 12 Do August 15 August 25	$\begin{matrix} Feet. \\ 3.\ 61 \\ 3.\ 60 \\ 3.\ 10 \\ 3.\ 15 \end{matrix}$	Secft. 871 842 512 526

Daily gage height, in feet, of West Gallatin River near Salesville, Montana, for 1900.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1	3.40			3.30	4.00	6.15	4.10	3.20	3.00	3.20	3.10	2.80
2			· · · · · •	$\frac{3.40}{3.40}$	$\frac{4.10}{4.25}$	$5.80 \\ 6.40$	$\frac{4.10}{3.90}$	$\frac{3.20}{3.20}$	3.00 3.00	3.20 3.10	$\begin{bmatrix} 3.10 \\ 3.10 \end{bmatrix}$	-2.80 2.85
4				3.40	4.50	6.60	3.70	3.23	3.20	3.20	3.10	2.90
5		3.30		3.50	4.70 5.15	6.65 6.90	$\frac{3.70}{3*70}$	$\frac{3.23}{2.10}$	3.20 3.20	3.20	3.10	3.00
7			3.10	3.80	4.95	6.55	3.70	3.10	3.20	3.20	3.10	3.00
8	3.30	• • • • • •	· · · · · ·	$\frac{3.60}{3.50}$	$5.05 \\ 5.15$	6.25 6.30	$\frac{3.70}{3.70}$	$\frac{3.10}{3.10}$	3.15 3.00	$\frac{3.10}{3.10}$	3.10 3.10	$\begin{bmatrix} 2.90 \\ 2.90 \end{bmatrix}$
10				3.50	5.55	6.15	3.60	3.10	3.00	3.10	3.10	2.90
11. 12		3.00	3 10	$\frac{3.50}{3.50}$	6.05 6.05	$6.45 \\ 5.50$	$\frac{3.60}{3.60}$	$\frac{3.10}{3.10}$	$\frac{3.00}{2.90}$	$\frac{3.10}{3.10}$	3.00	2.90 2.90
13				3.50	5.55	5.55	3.50	3.10	3.00	3.10	3.00	2.90
14 15	3 20		• •	$3.50 \\ 3.50$	$5.30 \\ 5.25$	5.55 5.75	$\frac{3.50}{3.50}$	$\frac{3.10}{3.10}$	3.00 3.10	$\frac{3.10}{3.10}$	3.00 3.00	2.90 2.90
16.				3.60	5.15	5.50	3.40	3.10	3.00	3.10	3.00	2.85
17 18		•••••		$\frac{3.50}{3.60}$	$5.15 \\ 5.20$	5.30 5.15	$\frac{3.40}{3.40}$	3.13	3.00 3.10	$\begin{array}{c} 3.10 \\ 3.10 \end{array}$	$\begin{bmatrix} 3.00 \\ 2.90 \end{bmatrix}$	2.80 2.80
19				3.70	5.00	5.20	3, 40	3.10	3.10	3.10	2.80	-2.80
20 21		3.20	3.10	$\frac{3.85}{4.00}$	5.10 5.15	5.25 5.30	3.40 3.30	3.10 3.10	3.10 3.10	3.10 2.90	$\begin{array}{c} 2.70 \\ 2.70 \end{array}$	2.80
22.	3.20			4.15	5.40	5.20	3.40	3.10	3.00	3.00	2.80	2.80
23 24				$\frac{4.35}{4.05}$	$\frac{5.45}{5.65}$	5.20 5.20	3.30	3.10 3.13	3.20 3.10	3.10 3.10	2.80 2.80	2.80 2.85
25				3.90	5.75	4.70	3.30	3.13	3.10	3.10	2.80	2.85
20 27				4.00	$6.25 \\ 6.75$	4.40	3,30 3.35	$3.20 \\ 3.15$	3.10 3.10	3.10 3.00	$2.80 \\ 2.80$	$2.80 \\ 2.80$
28		3.10	9.96	4.10	6.90	4.20	3.30	3.15	3.20	2.90	2.80	2.80
30	3.20		3. 30	4.10	0.40	4.20	3.20 3.28	3.10 3.10	3.10	$\frac{2.90}{3.00}$	2.80	$2.80 \\ 2.80$
31					6.05		3.30	3.00		3.00		2.78

MIDDLE CREEK NEAR BOZEMAN, MONTANA."

This station, which was established August 3, 1895, is located in Middle Creek Canyon, 9 miles from Bozeman. It is described in Water-Supply Paper No. 36, page 196. Results of measurements for 1899 will be found in the Twenty-first Annual Report, Part IV, page 183. During 1900 the following measurements of discharge were made under the direction of Samuel Fortier:

> May 22: Gage height, 0.57 foot; discharge, 211 second-feet. June 5: Gage height, 0.90 foot; discharge, 366 second-feet. June 18: Gage height, 0.60 foot; discharge, 248 second-feet. June 24: Gage height, 0.60 foot; discharge, 241 second-feet. July 7: Gage height, 0.26 foot; discharge, 104 second-feet. August 15: Gage height, 0.02 foot; discharge, 51 second-feet.

IRR 49-01-5

Daily gage height, in feet, of Middle Creek near Bozeman, Montana, for 1900.

Day.	June.	July.	Aug.	Sept.	Oct.	Day.	June.	July.	Aug.	Sept.	Oet.
1		0.30 .30 .20 .20 .20 .20 .30 .20 .30 .30 .30 .20 .20 .20 .20 .20 .20 .20 .20	$\begin{array}{c} 0.10\\ .10\\ .10\\ .10\\ .10\\ .20\\ .10\\ .10\\ .05\\ .05\\ .04\\ .03\\ .03\\ .02\\ .02\\ .02\\ .02\\ .02\\ .02\\ .02\\ .02$	$\begin{array}{c} 0.00\\ .00\\ .00\\ .00\\ .00\\ .00\\ .00\\ .0$. 0,00 .00 .00 .00 .00 .00 .00 .00 .00 .00	17 18 19 20 21 22 23 24 25 25 26 27 28 28 29 30 31 31	$\begin{array}{c} 0.60\\ .50\\ .60\\ .80\\ .60\\ .90\\ .60\\ .50\\ .50\\ .50\\ .40\\ .30\\ \end{array}$	$\begin{array}{c} 0.20\\ .20\\ .20\\ .20\\ .10\\ .10\\ .10\\ .10\\ .10\\ .10\\ .10\\ .1$	$\begin{array}{c} 0.02\\ .02\\ .02\\ .02\\ .02\\ .02\\ .01\\ .01\\ .01\\ .01\\ .01\\ .01\\ .01\\ .00\\ .00$	$\begin{array}{c} 0.00\\ .00\\ .01\\ .01\\ .01\\ .00\\ .00\\ .00$	

NOTE.—This station was discontinued in 1899, but was reopened on June 18, 1900. It was closed for the winter on October 13.

GALLATIN RIVER AT LOGAN, MONTANA.

This station, which was established August 24, 1893, by F. H. Newell, is located on the bridge of the Northern Pacific Railroad crossing the river at Logan. It is described in Water-Supply Paper No. 36, pages 197 and 198, where will also be found the results of measurements for 1899. During 1900 the following measurements of discharge were made under the direction of Samuel Fortier:

Discharge measurements of Gallatin River at Logan, Montana.

Date.	Gage height.	Dis- charge.	Date.	Gage height.	Dis- ch ar ge.
1900. June 15 June 23 June 28 June 28 July 16	$\begin{array}{c} Feet. \\ 3.91 \\ 2.32 \\ 1.51 \\ 1.22 \\ .40 \end{array}$	$\begin{array}{c} Sec. \cdot feet. \\ 4, 630 \\ 1, 966 \\ 1, 066 \\ 744 \\ 239 \end{array}$	1900. August 13 - September 4	$\begin{matrix} Feet. \\ 0.62 \\ .77 \\ 1.00 \\ 1.00 \end{matrix}$	Secfeet. 349 445 600 596

MONTANA.

Daily gage height, in feet, of Gallatin River at Logan, Montana, for 1900.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1				1.40 1.40	$\frac{2.00}{2.00}$	3, 50 3, 50	1.00	0, 50 50	0.70	0.90	1.00 1.00	$1.10 \\ 1.10$
3	1.20			1.40 1.40	$\frac{2.05}{2.30}$	3.70	.90	. 50	. 80	.90	$1.00 \\ 1.00$	1.10
5				1.40 1.40	$\frac{2.30}{2.50}$	3.75	.80	. 50	. 80	$1.05 \\ 1.10$	$1.00 \\ 1.00$	1.10 1.10 1.10
7		1.50	1.80	1.40 1.40	$\frac{2.80}{2.70}$	3.85 3.60	.80	. 50	.80	$1.10 \\ 1.10$	$1.00 \\ 1.00$	$1.10 \\ 1.10 \\ 1.10$
9 10	1.30			$1.40 \\ 1.40$	$\frac{2.80}{3.05}$	3.40 3.25	70 60	. 60	. 80	$\hat{1}.\hat{0}\hat{0}$ 1.00	$1.00 \\ 1.00$	1.10 1.00
11				$1.40 \\ 1.40$	$3.35 \\ 3.60$	$2.75 \\ 2.50$	60 .50	. 60 . 60	$^{+80}_{-80}$	$1.00 \\ 1.00$	$1.00 \\ 1.00$	$1.00 \\ 1.00$
13. 14		(a)	1.40	$ \begin{array}{c} 1.40 \\ 1.40 \end{array} $	$3.70 \\ 3.25$	$2.50 \\ 2.35$	$.40 \\ .40$. 60 . 60	. 80 . 80	$1.00 \\ 1.00$	$1.00 \\ 1.00$	$1.00 \\ 1.00$
15. 16.				1.50 1.50	3.15 3.00	2.15 2.00	.40 .40	. 60 . 60	. 80 . 80	$1.00 \\ 1.00$	$1.00 \\ 1.00$	$1.00 \\ 1.00$
17 18	1.30	• • • • • • •		1.50 1.60	3.00 3.00	$ \begin{array}{c} 2.00 \\ 1.90 \\ 1.50 \end{array} $. 40	. 60	. 80	$1.00 \\ 1.00 \\ 1.00$	1.00 1.15	1.00 1.00
19 20			1.50	1.60 1.60 1.60	3.00	1.70 1.70 1.70	.40 .40	. 60	. 90	1.00 1.00 1.00	1.35 1.50 1.55	1.00 1.00 1.00
21		(<i>a</i>)	1.50	1.60 1.60 1.80	3.00 3.00 2.00	$1.55 \\ 1.50 \\ 1.50$.40 .40 .40	. 60	. 90	$1.00 \\ 1.00 \\ 1.00$	1.50 1.50 1.40	1.00 1.00 1.00
24	1.50			1.90	$3.00 \\ 3.05 \\ 3.30$	$1.50 \\ 1.50 \\ 1.40$.40	.60	. 90	$1.00 \\ 1.00 \\ 1.00$	1.40 1.30 1.20	1.00
26 27				2.05 2.00	3.40 3.75	$1.40 \\ 1.30$.40 .50	.70	. 90	$1.00 \\ 1.00$	$1.10 \\ 1.10$	1.10
28. 29		1.50	1.50	$2.00 \\ 2.00$	$\frac{4.00}{4.00}$	$1.20 \\ 1.10$. 50 . 50	$.70 \\ .70$. 90 . 90	$1.00 \\ 1.00$	$1.10 \\ 1.10$	1.00
30 31	1.50			2.00	$3.60 \\ 3.70$	1.00	$.50 \\ .50$	$.70 \\ .70$.90	$1.00 \\ 1.00$	1.10	$\begin{pmatrix} (a) \\ (a) \end{pmatrix}$
		1										

a Frozen.

MADISON RIVER NEAR REDBLUFF, MONTANA.

This station, which was established May 2, 1897, is located 4 miles below the Redbluff iron county bridge over the river and $1\frac{1}{2}$ miles below the mouth of Cherry Creek. It is described in Water-Supply Paper No. 37, page 205. Results of measurements for 1899 will be found in the Twenty-first Annual Report, Part IV, page 186. During 1900 the following measurements of discharge were made under the direction of Samuel Fortier. Cherry Creek flows into Madison River between the gage and the point where the river is measured, and its discharge should, therefore, be added to that of the river in order to obtain the total discharge at the gage.

Discharge measurements of Madison River near Redbluff, Montana.

Date.	Gage height.	Dis- charge.	Date.	Gage height.	Dis- charge.
1900. June 8 June 9 June 19 Do Do June 25	Feet. 2.57 2.53 1.92 1.92 1.85	$\begin{array}{c} Secfeet. \\ 4,412 \\ a146 \\ 4,237 \\ 2,715 \\ 2,848 \\ a66 \\ 2,610 \end{array}$	1900. June 25 June 26. July 13 Do August 16 Do	Feet. 1.79 1.40 1.30	Secfeet.

a Cherry Creek.

Daily gage height, in feet, of Madison River near Redbluff, Montana, for 1900.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1			<i>(a)</i>	1.00	2.00	2.70	1.60	1.40	1.40	1.50	1.50	1.40
2		(a)		1.00	2.25	2.50	1.60	1.40	1.40	1.50	1.50	1.40
0	(a)			1.00	2.40	2.80	1.00	1.40	1.40 1 40	1.00 1.50	1.00	1.40
5	(u)			1.30	2.15	2.88	1.50	1 40	1.40 1.40	1.50	1.40	1.40
6				1.30	2.30	2.90	1.50	1.40	1.40	1.50	1.40 1.40	1.40
7				1.40	2.35	2.90	1.50	1.40	1.40	1.50	1.40	1.40
8		(a)	1.00	1.30	2.40	2.80	1.50	1.40	1.40	1.50	1.40	1.40
9				1.30	2.45	2.80	1.50	1.45	1.40	1.50	1.40	1.40
10				1.30	2.50	2.80	1.50	1.50	1.40	1.50	1.40	1.40
11	(α)			1.30	2.62	2.70	1.50	1.50	1.50	1.50	1.40	1.40
12	• • • • • •			1.30	2.70	2.65	1.50	1.50	1.50	1.50	1.40	1.40
13				1.30 1.20	2.80	2.40	1.50	1.40	1.40	1.50	1.40	1.40
14		·····	1.00	1.00	2. 10	2.00 9.90	1.50	1.40	1.40	1.50 1.50	1,40	1.40
18		(u)	1.00	1.00	9.45	2 10	1.50	1,40	1.40	1.50 1.50	1.40	1.40
17				1.40	2 30	2 50	1.50	1 40	1 40	1.50	1.40	1.40
18	(a)			1.50	2.25	1.85	1.50	1.40	1.40	1.50	1.40	1.40
19	()			1.50	2.10	1.80	1.50	1.40	1.40	1.50	1.40	1.40
20				1.50	2.20	1.70	1.50	1.40	1.40	1.50	1.40	1.40
21				1.50	2.23	1.70	1.50	1.40	1.40	1.50	1.40	1.40
22		(<i>a</i>)	1.00	1.60	2.20	1.70	1.50	1.40	1.40	1.50	1.40	1.40
23				1.70	2.25	1.65	1.50	1.40	1.40	1.50	1.40	1.40
24				1.80	2.37	1.60	1.50	1.40	1.40	1.50	1.40	1.40
25	(a)			1.80	2.45	1.60	1.50	1.40	1.40	1.50	1.40	1.40
26				1.80	2.60	1.60	1.50	1.40	1.50	1.50	1.40	1.40
90				1.80	2.80	1.60	1,50	1.40	1,50	1.50	1.40	1.40
80			1.00	1.80	2.90	1.60	1.00	1.40	1.50	1.50	1.40	1.40
90 90			1.00	1.89	3.00	1.00	1.00	1.40	1.50	1.50	1.40	1.40
99				1.8%	9.00	1.00	1.40	1.40	1.50	1.00 1.50	1.40	
01					w. 00		1.40	1.40		1.00		

a Frozen.

JEFFERSON RIVER AT SAPPINGTON, MONTANA.

This station, which was established by Arthur P. Davis in 1894, is located on the bridge of the Northern Pacific Railroad crossing the river at Sappington. It is described in Water-Supply Paper No. 37, pages 206 and 207, where will also be found the results of measurements for 1899. During 1900 the following measurements of discharge were made under the direction of Samuel Fortier:

Discharge measurements of Jefferson River at Sappington, Montana.

Date.	Gage height.	Dis charge.	Date.	Gage height.	Dis- charge.
1900. May 31 June 16 June 23 June 28	$\begin{array}{c} Feet. \\ 5.01 \\ 3.83 \\ 3.46 \\ 3.00 \end{array}$	$\begin{array}{c} Secft. \\ 5,918 \\ 3,593 \\ 3,240 \\ 2,279 \end{array}$	1900. July 16 . August 1 . October 6	Feet. 1.92 1.57 2.45	Secft. 844 589 1,586

Daily gage height, in feet, of Jefferson River at Sappington, Montana, for 1900.

Day.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1 2 3	(a) (a) (a)	$2.80 \\ 2.90 \\ 3.15$	$3.90 \\ 3.90 \\ 4.00$	$5.00 \\ 4.90 \\ 4.80$	$2.70 \\ 2.60 \\ 2.50$	$1.00 \\ 1.60 \\ 1.60 \\ 1.60$	$1.50 \\ 1.50 \\ 1.50$	2.10 2.20 2.25	$2.50 \\ 2.50 \\ 2.50 \\ 2.50$	$2.50 \\ 2.50 \\ 2.50 \\ 2.50$
4 5 6 7	$ \begin{array}{c} (a)\\ (a)\\ (a)\\ (a)\\ (a) \end{array} $	$3.30 \\ 3.40 \\ 3.50 \\ 3.60$	4.05 4.20 4.35 4.55	$\begin{array}{r} 4.90 \\ 5.00 \\ 4.00 \\ 4.90 \end{array}$	$2.50 \\ 2.40 \\ 2.40 \\ 2.40 \\ 2.40$	$1.50 \\ 1.50 \\ 1.50 \\ 1.50 \\ 1.50$	$egin{array}{c} 1.50 \\ 1.60 \\ 1.60 \\ 1.60 \end{array}$	2.33 2.40 2.43 2.40	2.50 2.50 2.40 2.40	$\begin{array}{c} 2.50 \\ 2.60 \\ 2.60 \\ 2.60 \end{array}$
8 9 10 11	(a) (a) 3.00 2.80	$\begin{array}{c} 3.60 \\ 3.60 \\ 3.45 \\ 3.30 \end{array}$	$\begin{array}{r} 4.65 \\ 4.85 \\ 5.05 \\ 5.25 \end{array}$	$\begin{array}{r} 4.90 \\ 4.70 \\ 4.60 \\ 4.50 \end{array}$	2.40 2.30 2.30 2.20	$1.50 \\ $	$1.60 \\ 1.60 \\ 1.70 \\ 1.70 \\ 1.70$	$\begin{array}{c} 2.40 \\ 2.40 \\ 2.40 \\ 2.40 \\ 2.40 \end{array}$	$\begin{array}{c} 2.40 \\ 2.40 \\ 2.40 \\ 2.40 \\ 2.40 \end{array}$	2.60 2.60 2.60 2.60
12 13 14 15	$\begin{array}{c} 2.80 \\ 2.80 \\ 2.70 \\ 2.70 \end{array}$	$\begin{array}{c} 3.20 \\ 3.20 \\ 3.20 \\ 3.20 \\ 3.20 \end{array}$	$5,50 \\ 6,10 \\ 6,40 \\ 6,55$	$\begin{array}{r} 4.20 \\ 4.00 \\ 4.00 \\ 3.90 \end{array}$	$2.20 \\ 2.20 \\ 2.10 \\ 2.00$	$1.50 \\ $	$ \begin{array}{r} 1.70 \\ 1.70 \\ 1.70 \\ 1.70 \\ 1.70 \end{array} $	$2.40 \\ 2.30 \\ 2.30 \\ 2.30 \\ 2.30 $	$\begin{array}{c} 2.40 \\ 2.40 \\ 2.40 \\ 2.40 \\ 2.40 \end{array}$	2.50 2.50 2.50 2.50 2.50
16 17 18 19	$\begin{array}{c} 2.70 \\ 2.60 \\ 2.70 \\ 2.80 \end{array}$	3.30 3.30 3.30 3.30	$ \begin{array}{r} 6.60 \\ 6.45 \\ 6.25 \\ 6.10 \\ \end{array} $	3.80 3.90 4.00 4.10	$ \begin{array}{r} 1.90 \\ 1.80 \\ 1.80 \\ 1.70 \\ 1.70 \\ \end{array} $	$ \begin{array}{r} 1.50 \\ 1$	$ \begin{array}{r} 1.70 \\ 1.70 \\ 1.80 \\ 1.85 \\ \end{array} $	2.30 2.30 2.30 2.20	$\begin{array}{c} 2.40 \\ 2.40 \\ 2.40 \\ 2.40 \\ 2.40 \end{array}$	$\begin{array}{r} 2.50 \\ 2.40 \\ 2.40 \\ 2.40 \\ 2.40 \end{array}$
20 21 22 23	$2.80 \\ 2.90 \\ 2.90 \\ 3.00 \\ 3.00 \\ 3.01 \\ 3.00 \\ $	$\begin{array}{r} 3.40 \\ 3.40 \\ 3.50 \\ 3.60 \end{array}$	5.95 5.80 5.75 5.55	$\begin{array}{r} 4.20 \\ 3.90 \\ 3.65 \\ 3.30 \end{array}$	$ \begin{array}{r} 1.70 \\ 1.70 \\ 1.70 \\ 1.70 \\ 1.70 \\ 1.70 \\ 1$	$ \begin{array}{r} 1.50 \\ $	$ \begin{array}{r} 1.90 \\ 1.90 \\ 1.90 \\ 1.90 \\ 1.90 \\ 1.90 \\ 1$	2.20 2.20 2.20 2.30	2.40 2.40 2.40 2.40 2.40	$\begin{array}{c} 2.40 \\ 2.40 \\ 2.40 \\ 2.40 \\ 2.40 \end{array}$
24 25 26 27	3.10 3.10 3.10 3.05	$3.65 \\ 3.75 \\ 3.80 \\ 3.90$	$5.50 \\ 5.40 \\ 5.35 \\ 5.30 \\ 5.30 \\ 100 \\$	$\begin{array}{c} 3.20 \\ 3.10 \\ 3.00 \\ 2.90 \end{array}$	$ \begin{array}{r} 1.70 \\ 1.70 \\ 1.60 \\ 1.60 \\ 1.60 \\ \end{array} $	$ \begin{array}{r} 1.50 \\ 1.50 \\ 1.50 \\ 1.45 \\ \end{array} $	$ \begin{array}{r} 1.90 \\ 1.90 \\ 2.00 \\ 2.00 \\ 2.00 \\ \end{array} $	2.30 2.30 2.40 2.40	$2.40 \\ 2.40 \\ 2.40 \\ 2.40 \\ 2.40 \\ 2.40 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10 \\ $	$ \begin{array}{r} 2.40 \\ 2.40 \\ 2.40 \\ 2.40 \\ 2.40 \\ 2.40 \\ \end{array} $
28 29 30 31	2.95 2.80 2.70 2.70	3,90 3,90 3,90	$5.30 \\ 5.40 \\ 5.30 \\ 5.15$	$2.85 \\ 2.80 \\ 2.80 \\ 2.80$	$ \begin{array}{r} 1.60 \\ 1.60 \\ 1.60 \\ 1.60 \\ 1.60 \\ \end{array} $	$ \begin{array}{r} 1.45 \\ 1.45 \\ 1.50 \\ 1.50 \\ 1.50 \\ \end{array} $	2.00 2.00 2.00	$\begin{array}{c} z.40\ 2.40\ 2.40\ 2.50 \end{array}$	2.40 2.50 2.50 2.50	2,30 2,30 2,30 2,30 2,30

a The river was frozen from January 1 to March 9, inclusive.

MISSOURI RIVER AT TOWNSEND, MONTANA.

Observations of gage heights are maintained at this place by the Missouri River Commission, and the results are furnished to the Geological Survey by the Corps of Engineers, United States Army. The heights given are the means of two daily readings expressed in feet above the St. Louis directrix, which is 412.73 feet above the mean Gulf level. The figures 3,300 have been omitted from the record, so that it is necessary to add that amount to the daily observations to obtain the elevation of the water surface above the St. Louis datum. A description of this station will be found in Water-Supply Paper No. 37, page 208. Results of measurements for 1899 will be found in the Twenty-first Annual Report, Part IV, page 187. During 1900 the following discharge measurements were made under the direction of Samuel Fortier:

Discharge measurements of Missouri River at Townsend, Montana.

Date.	Gage height.	Dis- charge.	Date.	Gage height.	Dis- charge.
1900. May 28 June 15 June 22 June 29	$\begin{array}{c} Feet. \\ 92.10 \\ 90.65 \\ 90.16 \\ 89.50 \end{array}$	$\begin{array}{c} Secft.\\ 15,982\\ 8,871\\ 7,797\\ 4,524 \end{array}$	1900. July 17 August 14 October 12.	Feet. 88.53 88.30 88.92	Secft. 2, 296 1, 955 3, 419

Daily gage height, in feet, of Missouri River at Townsend, Montana, for 1900.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1	90.8	88.8	92.0	89.2	90.4	91.8	89.2	88.2	a88.2	88.7	88.9	90.5
2	93.0	88.8	90.0	89.4	90.5	91.7	89.1	88.2	88.3	88.7	88.9	90.5
ð	93.0	88.8	90.0	89.0	90.5	91.7	89.0	88.2	88.3	88.8	88.9	90.3
5	92.5	88.8	99.7	89.0	90.0 90.6	91.0 91.8	00.9 88 Q	88.9	88 3	88 8	88 0	90.0
6	92.5	88.8	93.7	89.8	90.7	91.8	88.8	88 2	88 4	88 9	88 9	90.4
7	91.5	88.8	93.7	89.8	90.9	91.7	88.8	88.2	88.4	88.9	88.9	89.5
8	91.4	88.8	93.4	89.8	91.2	91.7	88.8	88.2	88.4	88.9	88.9	89.2
9	89.5	88.8	90.4	89.8	91.4	91.7	88.8	88.2	88.4	88.9	88.9	89.0
10	89.5	88.8	90.5	89.8	91.6	91.5	88.7	88.3	88.4	88.9	88.9	88.9
11	89.4	88.8	90.7	89.7	91.8	91.2	88.7	88.3	88.4	88.9	88.9	88.8
12	89.3	88.8	90.5	89.2	92.2	90.9	88.6	88.2	88.4	88.9	88.9	88.7
13	89.1	89.0	90.3	89.5	92.3	90.7	88.4	88.2	88.4	88.9	88.9	88.6
14	89.1	92.0	89.9	89.0	92.4	90.6	88.3	88.2	88.4	88.9	88.9	88.6
10	89.1	93.4	89.9	89.0	93.4	90.5	00.0	00.2	00.4	88.9	88.9	88.0
17	80 1	0.2 1	80.3	80.8	00.0	90.0 GO 5	88 3	60.2	00.±	88 0	80.0	00.1
19	89 1	02.2	89.3	89.8	92.1	90.5	88.3	88 2	88 4	88.8	89.1	88 A
19	89 1	92.2	89.2	89.8	92 1	90.4	88.3	88 2	88 4	88.8	89 1	88 7
20	89.1	92.3	89.2	89.8	91.9	90.3	88.3	88 2	88 4	88.8	89.1	88.8
21	89.1	92.2	89.3	89.8	91.9	90.2	88.3	88.2	88.4	88.8	89.2	88.9
22	89.1	92.1	89.3	89.9	91.8	90.0	88.3	88.2	88.4	88.8	89.3	88.8
23	89.1	92.1	89.4	90.1	91.7	89.9	88.3	88.2	88.4	88.8	89.6	88.7
24	89.1	92.1	89.4	90.2	91.7	89.8	88.3	88.2	88.4	88.8	89.9	88.7
25	89.1	92.1	89.5	90.3	91.7	89.7	88.3	88.2	88.5	88.8	90.1	88.7
26	89.1	92.1	89.5	90.3	91.7	89.6	88.3	a88.2	88.5	88.8	90.2	88.6
27	89.1	92.1	89.5	90,3	91.8	89.4	88.3	a88.2	88.6	88.8	90.7	88.5
28	89.0	9%.1	89.6	90.3	92.1	89.4	88.3	a88.2	88.6	88.9	90.7	88.4
<i>y</i>	89.0		89.5	90.3	93.3	89.3	88.3	288.2	88.6	88.9	90.7	88.2
SU	00.0		09.0	90.3	02 1	09.0	00.0	488.2	00.0	88.9	90.5	87.9
)1	00.0		00.4		Se. 1		00.0	u00. %		00.9		01.9

a Approximate; no readings received.

CROW CREEK, MONTANA.

Crow Creek, a tributary of Missouri River, is in Jefferson County, Montana. Its headwaters are at an elevation of between 7,000 and 8,000 feet above sea level. It flows in a southeasterly direction for about 25 miles, and empties into Missouri River 33 miles below Toston, at an elevation of about 4,000 feet.

At the foot of the mountains the valley is approximately 12 miles square. About half of it is owned by the residents, and approximately a third of the land owned is being irrigated, though perhaps seantily at times. This leaves without water about 70,000 acres, the greater part of it the choice land of the valley and, according to the farmers who have made efforts in that direction, well adapted to the raising of hay, grain, and fruit crops. The only apparent source of water supply for this vast tract of uncultivated land is small storage reservoirs on Crow Creek, at points along the canyon where the valley widens sufficiently to permit their construction. From the best information obtainable from those familiar with the canyon, the largest of these valleys is from a fourth to a half mile wide and about 2 miles long. On October 13, 1900, the flow of Crow Creek at the mouth of the canyon, 5 miles above Radersburg, Montana, was, by actual measurement, 16 second-feet. On the same date the discharge at the bridge 1 mile below the canyon was also 16 second-feet. The high-water flow lasts from four to six weeks, with an occasional summer flood, and is confined in a channel having an average width of from 25 to 30

feet, with vertical banks of from 4 to 5 feet on either side, and a fall of 58.7 feet to the mile.

MILK RIVER AT HAVRE, MONTANA.

This station, which was established by C. C. Babb on May 15, 1898, is described in Water-Supply Paper No. 37, page 209. Results of measurements for 1899 will be found in the Twenty-first Annual Report, Part IV, page 189. During 1900 the following measurements of discharge were made by C. W. Ling:

Date.	Gage height.	Dis- charge.	Date.	Gage height.	Dis- charge.
1900. A pril 21 A pril 26 Do May 3 May 7 May 11 May 15 May 16 May 16 May 18 May 24 May 31 June 4 June 21 June 21 June 21 June 27 July 10 July 18 July 25 August 3 May 4 May 3 May 4 May 3 May 5 May 4 May 5 May 5 May 5 May 5 May 5 May 5 May 10 May	$\begin{array}{c} Feet. \\ 2,900 \\ 3.00 \\ 3.00 \\ 3.00 \\ 2.70 \\ 2.60 \\ 4.00 \\ 5.20 \\ 4.00 \\ 5.20 \\ 4.00 \\ 5.20 \\ 4.00 \\ 2.40 \\ 2.20 \\ 1.90 \\ 2.20 \\ 1.90 \\ 1.50 \\ 1.40 \end{array}$	$\begin{array}{c} Secff.\\ 242\\ 327\\ 302\\ 314\\ 390\\ 207\\ 250\\ 863\\ 1,651\\ 1,112\\ 185\\ 142\\ 117\\ 108\\ 76\\ 92\\ 300\\ 14\\ 17\end{array}$	1990. August 4 August 11 August 13 August 14 August 20 August 20 August 31 September 4 September 5 September 5 September 8 September 17 September 12 October 2 October 6 October 6 October 18 October 18 October 18 October 27 November 2 November 2 November 10	$\begin{array}{c} Feet. \\ 1, 40 \\ 2, 60 \\ 2, 40 \\ 1, 60 \\ 1, 60 \\ 1, 60 \\ 1, 50 \\ 1, 70 \\ 2, 00 \\ 2, 50 \\ 2, 20 \\ 2, 00 \\ 2, 90 \\ 2, 90 \\ 2, 90 \\ 2, 40 \\ 2, 30 \\ 2, 00 \\ 2, 30 \\ 2, 00 \end{array}$	$\begin{array}{c} Secft.\\ 12\\ 13\\ 182\\ 27\\ 27\\ 27\\ 27\\ 23\\ 48\\ 80\\ 142\\ 50\\ 50\\ 97\\ 84\\ 314\\ 236\\ 35\\ 129\\ 157\\ 129\\ 129\\ 114\\ 96\\ 63\\ 63\\ \end{array}$

Discharge measurements of Milk River at Havre, Montana.

Daily gage height, in feet, of Milk River at Havre, Montana, for 1900.

Day.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1		3.10 3.30	3.10 3.00	2.00 2.00	1.50	1.60 1.50	2.00 2.00	2.30	(a)
3		3.20 3.00	2.90 2.70	$1.90 \\ 1.90$	$1.40 \\ 1.40$	$1.50 \\ 1.50 \\ 1.50$	2.10 2.20	$\frac{2.30}{2.20}$	(a)
5 6.		$\frac{2.90}{2.80}$	2.70 2.70	$1.90 \\ 1.90$	$1.40 \\ 1.40$	$1.70 \\ 1.70$	$\frac{2.40}{3.10}$	2.20 2.20	(a)
7. 8.		$2.70 \\ 2.60$	$2.70 \\ 2.60$	$1.80 \\ 1.80$	$1.40 \\ 1.30$	$1.80 \\ 2.00$	$3.10 \\ 2.90$	$2.20 \\ 2.20$	(a) (a)
9. 10.	3.40	$2.60 \\ 2.50$	$2.60 \\ 2.40$	$1.90 \\ 2.00$	$ \begin{array}{c} 1.30 \\ 1.30 \end{array} $	$2.10 \\ 2.50$	$2.80 \\ 2.70$	$2.20 \\ 2.00$	(a) (a)
11	3.40 3.70	2.40 2.30	2.40 2.40 2.90	$2.10 \\ 1.80 \\ 1.00$	$ \begin{array}{r} 1.40 \\ 2.75 \\ 0.05 \end{array} $	2.40 2.40	2.60 2.60	$1.90 \\ 2.20 \\ 1.00 \\ $	$\begin{pmatrix} a \\ (a) \end{pmatrix}$
13 14	5.60 3.60 2.10	2.40 2.40 2.60	2.30	1.80 1.70 1.70	2.65 2.40 2.90	2.40 2.00 2.00	2.50 2.50	2.40 2.20 2.50	(a) (a)
16. 17	3.30 3.00	4.00	2.30 2.30 2.30	$1.70 \\ 1.70 \\ 1.70$	2.00 2.00 1.90	1.90 1.90	2.00 2.90 3.00	(a)	(a) (a) 1.40
18 19.	3.20 2.90	$4.60 \\ 4.10$	$2.40 \\ 2.20$	$1.70 \\ 1.60$	$1.70 \\ 1.60$	$1.90 \\ 1.90$	$2.90 \\ 2.80$	(a) (a)	$1.40 \\ 1.40 \\ 1.40$
20. 21.	2.90 2.90	$\frac{3.70}{3.60}$	$2.20 \\ 2.20$	$ \begin{array}{r} 1.60 \\ 1.60 \end{array} $	$1.60 \\ 1.50$	$\frac{1.90}{2.00}$	$2.70 \\ 2.70$	(a) (a)	$ \begin{array}{c} 1.40 \\ 1.40 \end{array} $
99 99 99	$2.90 \\ 2.90 \\ 0.10$	3.90 3.60	$2.20 \\ 2.20 \\ 2.10$	$1.60 \\ 1.50$	$1.50 \\ 1.40$	$220 \\ 2.20 \\ 2.10$	2.40 2.40	$\begin{pmatrix} (a) \\ (a) \end{pmatrix}$	(a) = (1.60)
24 25	3.10 3.30	3.40	2.10 2.10 2.00	1.50 1.50 1.50	1.40 1.40 1.40	2.10 2.00	2.30 2.30	(a) (a)	(a) (a)
$\frac{20}{24}$	a. 30 2. 90 3. 10	5.20 3.10 2.90	2.20 2.10 2.10	$1.50 \\ 1.50 \\ 1.60$	1.40 1.40 1.40	2.00 2.00 1.00	2,30 2,30 2,30	(a) (a)	$\begin{pmatrix} (a)\\(a)\\(a) \end{pmatrix}$
29 30.	2.90	$\frac{2.90}{2.90}$	2.10	$1.50 \\ 1.50 \\ 1.50$	1.40 1.40 1.40	1.90 1.90 2.00	$\frac{2.30}{2.30}$ 2.20	(a)	(a)
31		3.00		1.50	1.60		2.20		(a)

YELLOWSTONE RIVER NEAR LIVINGSTON, MONTANA.

This station, which was established May 2, 1897, is located at the highway bridge over the Yellowstone 5 miles south of Livingston. It is described in Water-Supply Paper No. 37, pages 210 and 211, where will also be found the results of measurements for 1899. During 1900 the following measurements were made under the direction of Samuel Fortier:

Discharge measurements of Yellowstone River near Livingston, Montana.

Date.	Gage height.	Dis- charge.	Date.	Gage height.	Dis- charge.
1900. May 25 Do June 14. June 21 June 27	$\begin{array}{c} Feet. \\ 3.08 \\ 3.15 \\ 4.30 \\ 4.08 \\ 3.40 \end{array}$	$\begin{array}{c} Sec.{-}ft.\\ 7,917\\ 8,482\\ 13,552\\ 11,835\\ 9,094 \end{array}$	1900. July 14 August 7 September 29 October 17	$ \begin{array}{c} Feet. \\ 1.76 \\ .75 \\45 \\60 \end{array} $	$\begin{array}{c} Sec.{-}ft. \\ 4,623 \\ 3,160 \\ 1,710 \\ 1,599 \end{array}$

Daily gage height, in feet, of Yellowstone River near Livingston, Montana, for 1900.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
Day. 1	Jan. -0.85	(a) (Mar. (a) (a) (a) (a) (a) (a) (a) (a) (a) (a)	Apr. -1.00 90 70 70 70 20 30 60 60 60 55 60	$\begin{array}{c} \text{May.}\\ 0.30\\ .60\\ .75\\ 1.40\\ 1.75\\ 2.30\\ 2.20\\ 2.15\\ 2.67\\ 3.35\\ 3.73\\ 3.73\\ 3.78\\ 2.28\\ 2.28\\ 2.28\\ 2.28\\ \end{array}$	June. 3.80 4.00 4.20 4.35 4.75 4.35 4.35 4.60 3.955 3.75 3.70 4.25 4.25 4.25 4.20	July. 2.80 2.68 2.55 2.50 2.40 2.30 2.32 2.13 2.10 2.03 1.95 1.88 1.80 1.70 1.63	$\begin{array}{c} {\rm Aug.} \\ 0.95 \\ .90 \\ .88 \\ .80 \\ .75 \\ .75 \\ .70 \\ .65 \\ .50 \\ .50 \\ .50 \\ .45 \\ .45 \\ .40 \end{array}$	Sept. -0.05 05 10 10 10 15 25 25 25 30 33	$\begin{array}{c} \text{Oct.} \\ -0.45 \\43 \\43 \\43 \\45 \\45 \\45 \\45 \\45 \\45 \\60 \\60 \\60 \\60 \\65 \\60 \\60 \end{array}$	Nov. -0.70 70 70 70 70 70 75 88 85 85 85	Dec. -0.95 88 90 100 100 100 100 100
11 19 20 21 22 22 23 24 25 26 27 28 29 28 29 30 31	-0.90	(a) (a) (a) (a) -0.90	-1.00 	$\begin{array}{c} - & .60\\ - & .60\\ - & .50\\ - & .20\\ .00\\ .20\\ .65\\ .40\\ .40\\ .30\\ .30\\ .35\\ \end{array}$	$\begin{array}{c} 2.48\\ 2.40\\ 2.17\\ 2.25\\ 2.38\\ 2.55\\ 2.73\\ 2.90\\ 3.03\\ 3.65\\ 4.20\\ 4.65\\ 4.38\\ 3.98\\ 3.80\end{array}$	4, 13 3, 90 3, 90 3, 90 3, 90 3, 95 3, 95 3, 88 3, 68 3, 68 3, 43 3, 23 3, 68 3, 43 3, 23 3, 10 3, 03	$\begin{array}{c} 1.33\\ 1.53\\ 1.50\\ 1.45\\ 1.40\\ 1.38\\ 1.30\\ 1.25\\ 1.20\\ 1.20\\ 1.20\\ 1.20\\ 1.00\\ 1.05\\ 1.00\\ \end{array}$.30 .30 .25 .25 .20 .20 .20 .20 .20 .20 .15 .15 .05 .00	$\begin{array}{c} - & .35 \\ - & .35 \\ - & .30 \\ - & .30 \\ - & .35 \\ - & .40 \\ - & .40 \\ - & .40 \\ - & .40 \\ - & .40 \\ - & .45 \\ - & .45 \\ - & .45 \\ - & .45 \end{array}$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} - & \cdot & \circ 5 \\ - & \cdot & \circ 5 \\ (a) \\ (a) \\ (a) \\ (a) \\ (a) \\ -1. & 10 \\ -1. & 08 \\ - & \cdot & 90 \\ - & \cdot & 85 \\ - & \cdot & 90 \\ -1. & 00 \\ -1. & 00 \\ \end{array}$	$\begin{array}{c} -1,00\\ -1,00\\ -1,00\\ -1,00\\ -1,00\\ -1,00\\ -1,00\\ -1,10\\ -1,15\\ -1,15\\ -1,35\\ -1,35\\ \end{array}$

a Frozen.

MISCELLANEOUS DISCHARGE MEASUREMENTS IN MONTANA.

During the year the following miscellaneous measurements of streams in Montana were made by Messrs. F. E. and G. H. Matthes:

WYOMING.

Date.	Stream.	Locality.	Hydrographer.	Dis- charge.
1900.				Secft.
une 18	St. Mary River	Main	F. E. Matthes.	2,294
August 6	do	do	G.H. Matthes.	750
)ctober 14	do	do	do	552
une 16	dodo	Outlet of Lower Lake	F.E. Matthes.	750
une 19	North Fork of Milk River.	Bridge at Hall's ranch	do	12
une 21	Middle Fork of MilkRiver	Ford of road to Main	do	7
June 14	South Fork of Milk River.	Paul's ranch	do	31
une 8	Cutbank River	Ford of road to St. Mary	do	488
		Lake.		231
une 9	North Fork of Cutbank	Base of mountains	do	
	River.			390
une 7	Two Medicine River	Outlet of Lower Lake	do	
Iay 23	do	Holy Family Mission	do	1,067
Iay 29	do	Ford 12 miles below Piegan.	do	1,261
1av 28	Badger Creek	Two miles above Piegan	do	562
1av 24	do	Ford at Piegan	do	273
fay 26	Birch Creek	Four miles above Robare	do	387
Do	do	One-half mile above Robare.	do	392

Miscellaneous discharge measurements of streams in Montana.

BIGHORN RIVER NEAR THERMOPOLIS, WYOMING.

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This station, which was established by A. J. Parshall on May 28, 1900, is located about a half mile west of Thermopolis, at the ferry crossing the river. The gage, which consists of a horizontal rod extending out over the water, is fastened to a post set firmly in the bank. On the horizontal stick is attached the wire gage by means of which the heights of the river are recorded. The bench mark is the head of a nail in a stick driven in the ground 1 foot south of the post to which the gage rod is fastened and 2.58 feet below the top of the gage frame. The bench mark is 9.08 feet above gage datum. Discharge measurements have been made from a ferryboat, but during the coming season they will be made from the bridge which has recently been erected. • The channel is straight for a distance above and below the station. Both banks are high and not subject to overflow. The bed of the stream is of gravel, and shifts during only extreme high water. Results of measurements for 1899 will be found in Water-Supply Paper No. 37, page 211. During 1900 the following discharge measurements were made by A. J. Parshall:

> May 28: Gage height, 4.01 feet; discharge, 8,500 second-feet. May 29: Gage height, 5.00 feet; discharge, 10,527 second-feet. May 30: Gage height, 5.40 feet; discharge, 12,187 second-feet. September 13: Gage height, 0.60 foot; discharge, 945 second-feet. September 18: Gage height, 0.45 foot; discharge, 674 second-feet.

Daily gage height, in feet, of Bighorn River near Thermopolis, Wyoming, for 1900.

Day.	June	July.	Aug.	Sept.	Day.	June.	July.	Aug.	Sept.	Day.	June.	July.	Aug.	Sept.
$ \begin{array}{c} 1 \\ 2 \\ 3 \\ 4 \\ 5 \\ 6 \\ 7 \\ 9 \\ 10 \\ 11 \\ \end{array} $	$\begin{array}{r} 4.\ 00\\ 4.\ 30\\ 4.\ 45\\ 5.\ 00\\ 4.\ 85\\ 4.\ 80\\ 5.\ 70\\ 6.\ 60\\ 5.\ 90\\ 5.\ 85\\ 5.\ 45\\ \end{array}$	$\begin{array}{c} 3.40\\ 3.30\\ 3.30\\ 3.20\\ 3.20\\ 3.10\\ 3.20\\ 3.15\\ 3.00\\ 2.80\\ 2.80\end{array}$	$\begin{array}{c} 1.55\\ 1.50\\ 1.50\\ 1.50\\ 1.80\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ \end{array}$	$\begin{array}{c} 1.20\\ 1.20\\ 1.00\\ 1.00\\ 1.00\\ .90\\ .90\\ .90\\ .90\\ .90\\ .70\\ \end{array}$	$\begin{array}{c} 12 \\ 13 \\ 14 \\ 15 \\ 16 \\ 17 \\ 18 \\ 19 \\ 20 \\ 21 \\ 22 \\ 22 \\ \ldots \end{array}$	$\begin{array}{c} 5.\ 20\\ 4.\ 65\\ 4.\ 30\\ 4.\ 10\\ 4.\ 00\\ 3.\ 80\\ 3.\ 60\\ 3.\ 50\\ 3.\ 50\\ 3.\ 50\\ 3.\ 90 \end{array}$	$\begin{array}{c} 2.65\\ 2.55\\ 2.45\\ 2.25\\ 2.20\\ 2.20\\ 2.20\\ 2.10\\ 2.05\\ 1.95\\ 1.60\\ 1.60\\ \end{array}$	$\begin{array}{c} 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.40\\ 1.40\\ 1.30\\ 1.30\\ \end{array}$	0.70 .60 .55 .50	23 24 25 27 27 28 29 30 31	$\begin{array}{c} 4.\ 10\\ 4.\ 45\\ 4.\ 50\\ 5.\ 00\\ 5.\ 25\\ 5.\ 00\\ 4.\ 25\\ 3.\ 50\\ \end{array}$	$\begin{array}{c} 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.60\end{array}$	$\begin{array}{c} 1.\ 40\\ 1.\ 30\\ 1.\ 30\\ 1.\ 30\\ 1.\ 30\\ 1.\ 30\\ 1.\ 20\\ 1.\ 20\\ 1.\ 20\\ 1.\ 20\end{array}$	

CLEAR CREEK NEAR BUFFALO, WYOMING.

This station was established by the State engineer of Wyoming. A measuring flume was erected in order that accurate measurements of discharge might be obtained. Owing to the stability of the station it has not been necessary to make discharge measurements at this place, the computations being made from the rating table established several years ago. The station is described in Water-Supply Paper No. 37, page 212. Results of measurements for 1899 will be found in the Twenty-first Annual Report, Part IV, page 191. Owing to the diversions of water which have taken place within the basin, of late years this station has not been considered as important as formerly, and it was discontinued on March 11, 1900, no measurements of discharge being made during that year.

Daily gage h	eight, in feet. c	of Clear Creek nea	r Buffalo, Wyoming,	for 1900.
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Day.	Jan.	Feb.	Mar.	Day.	Jan.	Feb.	Mar.	Day.	Jan,	Feb.	Mar.
$ \begin{array}{c} 1 \\ 2 \\ 3 \\ 4 \\ 5 \\ - \\ - \\ - \\ - \\ - \\ - \\ - \\ - \\ - \\ -$	$\begin{array}{c} 0, 40 \\ .40 \\ .40 \\ .37 \\ .37 \\ .35 \\ .35 \\ .35 \\ .35 \\ .35 \\ .35 \end{array}$	$\begin{array}{c} 0, 30 \\ .30 \\ .30 \\ .30 \\ .30 \\ .30 \\ .30 \\ .30 \\ .30 \\ .30 \\ .30 \\ .30 \\ .30 \end{array}$	0, 30 . 30 . 30 . 30 . 30 . 30 . 35 	$\begin{array}{c} 12 \\ 13 \\ 14 \\ 15 \\ 16 \\ 17 \\ 18 \\ 19 \\ 20 \\ 21 \\ 22 \\ \end{array}$	0.35 .35 .35 .35 .32 .32 .32 .32 .32 .30 .30 .30	$\begin{array}{c} 0.30 \\ .30 \\ .30 \\ .30 \\ .30 \\ .30 \\ .30 \\ .30 \\ .30 \\ .30 \\ .30 \\ .30 \\ .30 \\ .30 \end{array}$		23. 24. 25 26. 27. 28. 29. 30. 31.	$\begin{array}{c} 0.30\\ .30\\ .30\\ .30\\ .30\\ .30\\ .30\\ .30$	0.30 .30 .30 .30 .30 .30	

BIG SIOUX RIVER NEAR WATERTOWN, SOUTH DAKOTA.

Big Sioux River rises in Grant County, South Dakota, about 30 miles north of Watertown. Its principal headwaters drain lands constituting part of the Sisseton and Wahpeton Indian Reservation. Its general course is southeast, and it empties into Missouri River near Sioux City, Iowa. The river is of interest on account of its water powers, a number of which have been developed, principally at Flandreau, Dell Rapids, and Sioux Falls, South Dakota, and at Akron, Iowa. The gaging station was established by O. V. P. Stout, the gage being put in September 15, 1900, by George W. Carpenter, county surveyor for Codington County. It is located on the farm of L. E. Spicer, about 4 miles above Watertown. The gage consists of an inclined rod securely fastened on the right bank of the stream. The observer is L. E. Spicer. During 1900 the following discharge measurements were made by O. V. P. Stout and G. H. Matthes:

July 17: Discharge, 5 second-feet.July 18: Discharge, 10 second-feet.November 12: Gage height, 1.15 feet; discharge, 7 second-feet.

The measurement of July 18 was not made at the gaging station, but in the town.
Lake Poinsett, which lies almost wholly in Hamlin County, South Dakota, has its outlet in Big Sioux River near Dempster, a short distance above Estelline. Immediately below the outlet of the lake a dam has been constructed on the Big Sioux to maintain the level of the lake within certain limits. A measurement of the inlet to the lake was made July 19, 1900, by O. V. P. Stout, and a discharge of 16.5 second-feet was found.

Big Sioux River at the bridge west of Estelline was also measured by Mr. Stout on July 19, 1900, and a discharge of 16.9 second-feet was found.

Daily gage height, in feet, of Big Sioux River near Watertown, South Dakota, for 1900

Day.	Sept.	Oct.	Nov.	Dec.	Day.	Sept.	Oct.	Nov.	Dec.	Day.	Sept.	Oct.	Nov.	Dec.
1 2 3		1.30	1.25	1.20	$12 \dots 13 \dots 14 \dots$		1.25 1.25	1.15	1.20	23 24 25	1.30 1.30	1.25	1.20 1.20	1.20
4 5 6	• • • • • • • •	1.25	1.25 1.20	1.20	$ \begin{array}{c} 15 \\ 16 \\ 17 \\ 17 \end{array} $	1.40	1.25	1.15	1.20	$ \begin{array}{c} 26 \\ 27 \\ 28 \\ $	1.30	1.25 1.25	1.20	1.15
7 8 9	· · · · · · · · · · · · · · · · · · ·	1.25 1.25	1.15	1.20 1.20	$ \begin{array}{c} 18 \\ 19 \\ 20 \\ 20 \\ 21 \end{array} $	1.30	1.25	1.20 1.20	1.20	$ \begin{array}{c} 29 \\ 30 \\ 31 \\ \ldots \end{array} $	1.30	1.25	1.20	1.15
10		· · · · · · ·	1.15	1.20	21 22 	1.30	1.25	• • • • • • •	1.20					

BIG SIOUX RIVER NEAR SIOUX FALLS, SOUTH DAKOTA.

This gaging station, which was established by O. V. P. Stout on July 21, 1900, is 2 miles west of Sioux Falls. The gage consists of an inclined rod securely fastened to bevel blocks supported on wellbedded cross-ties. The observer is George Beggs. During 1900 the following discharge measurement was made by O. V. P. Stout:

July 21: Gage height, 2.02 feet; discharge, 78 second-feet.

Daily gage height, in feet, of Big Sioux River near Sioux Falls, South Dakota, for 1900.

Day.	Aug.	Sept.	Oct.	Nov.	Day.	Aug.	Sept.	Oct.	Nov.	Day.	Aug.	Sept.	Oct.	Nov.
$ \begin{array}{c} 1 \\ 2 \\ 3 \\ 4 \\ 5 \\ 6 \\ 7 \\ 7 \\ 9 \\ 10 \\ 11 \\ 11 \\ 11 \\ 11 \\ 11 \\ 11 \\ 11$	1.40 1.40	$\begin{array}{c} 1.\ 20\\ 1.\ 20\\ 1.\ 20\\ 1.\ 20\\ 1.\ 10\\ 1.\ 30\\ 1.\ 20\\ 1.\ 20\\ 1.\ 20\\ 1.\ 20\\ 1.\ 30\\ 1.\ 40 \end{array}$	$\begin{array}{c} 1.60\\ 1.80\\ 1.80\\ 1.80\\ 1.80\\ 1.80\\ 1.70\\ 1.70\\ 1.70\\ 1.70\\ 1.70\end{array}$	$\begin{array}{c} 1.80\\ 1.80\\ 1.80\\ 1.80\\ 1.80\\ 1.80\\ 1.80\\ 1.80\\ 1.70\\ 1.70\\ 1.80\\ 1.80\\ 1.80\\ 1.80\\ \end{array}$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 1.40\\ 1.50\\ 1.50\\ 1.40\\ 1.40\\ 1.30\\ 1.40\\ 1.40\\ 1.30\\ 1.30\end{array}$	$\begin{array}{c} 1.40\\ 1.40\\ 1.30\\ 1.50\\ 1.40\\ 1.50\\ 1.50\\ 1.50\\ 1.50\\ 1.40\\ \end{array}$	$\begin{array}{c} 1.\ 70\\ 1.\ 70\\ 1.\ 70\\ 1.\ 70\\ 1.\ 70\\ 1.\ 70\\ 1.\ 70\\ 1.\ 70\\ 1.\ 70\\ 1.\ 90 \end{array}$	$ \begin{array}{c} 1.80\\ 1.80\\ 1.80\\ 1.70\\ 1.70\\ 1.70\\ \hline \\ \hline $	22 23 24 25 25 26 27 28 29 30 31	$\begin{array}{c} 1.30\\ 1.30\\ 1.50\\ 1.40\\ 1.40\\ 1.30\\ 1.30\\ 1.30\\ 1.30\\ 1.30\end{array}$	$\begin{array}{c} 1.\ 40\\ 1.\ 60\\ 1.\ 60\\ 1.\ 60\\ 1.\ 50\\ 1.\ 50\\ 1.\ 70\\ 1.\ 60\\ \end{array}$	$\begin{array}{c} 1.20\\ 1.10\\ 1.10\\ 1.90\\ 1.80\\ 1.80\\ 1.80\\ 1.90\\ 1.90\\ 1.90\end{array}$	

MISCELLANEOUS DISCHARGE MEASUREMENTS OF CHEYENNE RIVER AND ITS TRIBUTARIES.

During the year a number of measurements of Cheyenne River and its tributaries were made by J. T. Stewart, as described in the table on the next page.

Miscellaneous discharge measurements of Cheyenne River and its tributaries.

Date.	Stream.	Locality.	Hydrographer.	Dis- charge.
1900				Sec feet
May 14	Chevenne River	Edgemont S Dak	John T. Stewart	14 6
May 17	do	do	do	10.3
May 29	do	do	do	.5
May 18	do	Above mouth of Cascade Creek	do	12.2
June 12	do	do	do	.7
May 19	do	Above mouth of Fall River	do	39.2
June 4	do	Mouth of Fall River	do	18.7
May 21	do	miles southeast of Buffalo Gap, S. Dak.	ao	47.4
June 5	do	Below mouth of Beaver Creek	do	49.0
May 15	Salt Creek	East of Newcastle, Wyo	do	.2
May 31	do	do	do	.2
May 15	Big Off Creek	B. and M. Kallway bridge		.2
May 29	Little Oil Cueelr	Nomenatio Wre	do	. 05
May 17	do	do	do	.03
May 18	Cascada Creek	At month	do	24 6
June 2	do	do	do	19.9
Do	Hat Creek	do	do	.0
May 19	Fall River	Below Hot Springs, S. Dak	do	24.7
June 4	do	Hot Springs, S. Dak	do	28.6
May 19	do	At mouth	do	33. 3
June 4	do	do	do	24.8
May 26	Iron Creek	Glendale, S. Dak	do	3.8
June 1	Ctooloodo Doomon	Two wiles above I A K wouch	0D	1.0
May 15 May 31	Creek.	Wyo.	do	11.1
May 16	do	At month	do	9.4
May 30		do	do	3.5
May 15	Beaver Creek	Above mouth of Stockade Beaver Creek.	do	.0
May 30	do	do	do	.0
June 5	do	Gap, S. Dak.	do	12.2
May 21	do	At mouth, 7 miles southeast of Buf-	do	1.2
T	1.	falo Gap.	а.	
June 5 Mar 21	Lomo Johnnyr Cucolr	At mouth	do	0.0
may ~1	mane Johnny Creek	Gap.	uo	.0
Do	do	East of Buffalo Gap	do	.0
May 28	French Creek	Custer, S. Dak	do	. 0
May 22	do	Ten miles above Fairburn, S. Dak	do	12.8
June 6	do	Ten miles northeast of Fairburn,	do	4.9
Mar 20	do	S. Dak. Feinburg & Delz	do	9.9
June 7	do	do	do	0. ð 0
May 22	Squaw Creek	Otis S Dak	ob	7 9
June 6	do	do	do	2.8
May 26	Battle Creek	Keystone, S. Dak	do	3.1
June 7	do	do	do	2.3
May 25	do	Hermosa, S. Dak	do	9.1
June 8	do	do.	do	2.3
May 24	Spring Creek	North of Rockerville, S. Dak	do	6.5
June 9 May 22	do	E E and M V Railway bridge S	ao	•
June 9	do	Dak.	do	.4
May 24	Rapid Creek	Five and one-half miles above Rapid	do	48.8
_		City, S. Dak.		
June 8	do	do	do	26.3
May 25	do	Rapid City. S. Dak	do	64.2
June 8	do		do	29.9

NORTH PLATTE RIVER.

This river has its source in the mountains of North Park, in northern Colorado. Upon entering Wyoming the stream passes through a short, narrow canyon, and then flows northerly through the upper Platte Valley, which extends from the State line down to Fort Steele. On August 27, 1900, A. J. Parshall made measurements of the river

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at two points in its upper reaches. The first measurement was made a short distance above the mouth of Grand Encampment Creek and immediately above the mouth of Brush Creek, and a discharge of 176 second-feet was found. The second measurement was made near Saratoga, Wyoming, immediately above the mouth of Spring Creek, and a discharge of 211 second-feet was found.

GRAND ENCAMPMENT CREEK AT PERYAM'S RANCH, WYOMING.

This station, which was established by A. J. Parshall May 16, 1900, is located at the bridge over the river at the ranch of the observer, W. T. Peryam. The rod is vertical, and is fastened to the timbers of the bridge. The channel is straight for a distance above and below the station. The right bank is high and is not subject to overflow, but the left bank is low and overflows at high stages. The bed of the stream is rocky. During 1900 the following measurements were made by A. J. Parshall:

> May 16: Gage height, 2.00 feet; discharge, 2,050 second-feet. June 8: Gage height, 2.00 feet; discharge, 2,184 second-feet. June 21: Gage height, 1.20 feet; discharge, 885 second-feet. July 5: Gage height, 0.60 foot; discharge, 192 second-feet. July 18: Gage height, 0.30 foot; discharge, 39 second-feet.

Daily gage height, in feet, of Grand Encampment Creek at Peryam's ranch, Wyoming, for 1900.

	ise p oi	Day.	may.	June.	July.	Aug.	Sept.
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	0.25 .25 .20 .20 .25 .25 .30 .30 .30 .30 .30 .30 .30 .30 .30 .30	17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 31 31 28 29 29 21 24 25 27 28 29 29 20 21 21 23 24 25 27 28 27 28 29 29 29 21 21 21 23 24 25 27 28 29 27 28 29 29 20 21 21 25 26 27 28 29 29 20 21 21 25 26 27 28 29 20 21 21 21 23 24 25 26 27 28 29 30 31	$\begin{array}{c} 1,90\\ 2,05\\ 1,90\\ 1,70\\ 1,80\\ 1,90\\ 2,30\\ 2,10\\ 2,40\\ 2,50\\ 2,90\\ 3,20\\ 3,00\\ 3,00\\ 3,00\\ 3,00 \end{array}$	$\begin{array}{c} 1.\ 60\\ 1.\ 50\\ 1.\ 50\\ 1.\ 30\\ 1.\ 20\ 1.\ 20\\ 1.\ 20\ 1.\ 1.\ 1.\ 1.\ 1.\ 1.\ 1.\ 1.\ 1.\ 1.$	$\begin{array}{c} 0.40\\ .40\\ .30\\ .30\\ .35\\ .40\\ .40\\ .40\\ .40\\ .45\\ .50\\ .50\end{array}$	$\begin{array}{c} 0.40\\ .40\\ .30\\ .30\\ .30\\ .30\\ .30\\ .30\\ .50\\ .50\\ .50\\ .33\\ .30\\ .27\end{array}$	$\begin{array}{c} 0, 40\\ , 30\\ , 30\\ , 30\\ , 30\\ , 30\\ , 40\\ , 50\\ , 50\\ , 50\\ , 50\\ , 50\\ , 50\\ \end{array}$

LARAMIE RIVER AT WOODS, WYOMING.

This station, which was established in December, 1888, by the Territorial engineer of Wyoming, is located 26 miles from Laramie, and is reached by stage. It is described in Water-Supply Paper No. 37, page 214. Results of measurements for 1899 will be found in the Twenty-first Annual Report, Part IV, page 193. The station was discontinued September 30, 1900. During the year one measurement ment of discharge was made by A. J. Parshall, as follows:

May 4: Gage height, 1.60 feet; discharge, 460 second-feet.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	Ju.	Aug.	Sept.
1				0.70	1.40	4 15	1 40	0.60	0.30
2				. 70	1.40	4.05	1.30	60	30
3				70	1.50	3.90	1 30	60	.30
4				. 80	1.55	3.80	1 20	. 60	- 30
5				. 80	1.60	3.70	1.15	.70	- 30
6				65	1.80	3.60	1 10	70	- 30
7	1 10	1 20	1.30	. 80	2.00	3 45	1.00	65	. 50
8	1. 10	11100	1.00	. 80	2.00	3 45	1.00	60	- 35
9				.00	9.95	3 45	1.00	60	. 50
10				70	2 55	3 45	1.00	60	. 50
11				- 70	2 75	3 40	1.00	50	. 00
12					3.00	3 25		50	. 10
13				- 60	3.00	9 95		- 50	. 00
1.1	1.20	1.90	1.90	00.	9.05	9 75	- 50	- 50	. 40
15	1	1.90	1.40	. 00	9.65	9.65	.00	50	.40
16				- 50	2.05	2 55	.00	. 50	. 40
17				- 60	3.05	9.45	. 80	.50	. 00
18				. 00	3 15	9 45	80	. 10	.00
10				. 00	2.05	9 25	.00	. 10	. 50
20				- 15	2.00	9.95	.00	. 10	. 40
91	1.90	1.90	1.00	1 20	2.05	9 10	.00	. 40	. 40
90 90	1. ~0	1.00	1.00	1.00	9.85	2.10	. 20	. 40	. 40
99 92				1.00	2 15	1 05	- 20	.00	. 40
94 94				1.20 1.10	2.95	1.30	. 20	.00	- 40
95				1.10	2 45	1.00	. 10	. 00	. 10
97				1.00	0.40	1.70	. 10	. 00	- +0
			****	1.00	9.40	1.00	.00	. 30	- 40
64	1 10	1 50	1.00	1.10	0,90	1.00	. 00	. 30	. 40
%0	1.10	1.20	1.00	1.40	4.00	1.30	.00	. 00	- 40
90				1.00	4.10	1.40	. 00	20	. 00
91				1.40	4.20	1.40	.00	. 30	. 50
	• • • • • • • • • •				4.50		, 00	. 30	

Daily gage height, in feet, of Laramie River at Woods, Wyoming, for 1900.

Dai

LARAMIE RIVER NEAR UVA, WYOMING.

This station was established in 1894 by the State engineer of Wyoming. It is described in Water-Supply Paper No. 37, page 216. Results of measurements for 1899 will be found in the Twenty-first Annual Report, Part IV, page 194. The station was discontinued March 31, 1900, and no measurements of discharge were made during the year.

Day.	Jan.	Feb.	Mar.	Day.	Jan.	Feb.	Mar.	Day.	Jan.	Feb.	Mar.
1 2 3		1.6	1.6	12. 13 14	1.4			23 24 25		1.5	2.1
4 5 6	1.6			15 16 17		1.6	2.3	26 27 28	1.5		
8 9 10		1.7	1.8	$ \begin{array}{c} 18 \\ 19 \\ 20 \\ 21 \\ 92 \end{array} $	1.4			30 31			1.9

Daily gage height, in feet, of Laramie River near Uva, Wyoming, for 1900.

NORTH PLATTE RIVER AT ORIN JUNCTION, WYOMING.

This station was established November 1, 1894, by the State engineer of Wyoming. It is described in Water-Supply Paper No. 37, page 217. Results of measurements for 1899 will be found in the Twenty-first Annual Report, Part IV, page 196. The station was discontinued April 1, 1900, and no measurements of discharge were made during the year.

Daily gage height, in feet, of North Platte River at Orin Junction, Wyoming, for 1900.

Day.	Jan.	Feb.	Mar.	Apr.	Day.	Jan.	Feb.	Mar.	Apr.	Day.	Jan.	Feb.	Mar.	Apr.
1				2.3	12			1.3		23		2.2	1.7	
3 4		1.5	2.2		$14 \dots 15 \dots 15 \dots 16$					25 26 27				
6 7					17 18		2.2	2.5		28 29	·····			
8 9 10	(<i>a</i>)	1.5		· · · · · · · · · · · · · · · · · · ·	$ \begin{array}{c} 19 \\ 20 \\ 21 \\ \ldots \end{array} $				· · · · · · · · · · · · · · · · · · ·	30 31	• • • • • • •			
11	•••••				22	<i>(a)</i>	• • • • • • •	• • • • • • •						

a Frozen.

NORTH PLATTE RIVER NEAR GUERNSEY, WYOMING.

This station was established June 14, 1900, by A. J. Parshall. It is located at the county bridge about a half mile northwest of Guernsey. The bridge has eight piers, the sides are planked, and there is uniform flow under each span. The location is an excellent one for accurate measurements. The rod consists of a 4-inch by 4-inch by 12-foot scantling firmly attached to one of the piers of the bridge. As the station was to be a temporary one, a metallic tape, divided into feet and tenths, was securely fastened to the rod. The bench mark is a spike driven in a sleeper of the bridge 1 foot from the rod and at an elevation of 10.04 feet above the zero. The channel is straight for a distance above and below the station. Both banks are high and do not overflow at high stages. The bed of the stream is sandy, but probably does not shift much. The station was discontinued September 15, 1900. During 1900 the following measurements were made by A. J. Parshall:

> June 14: Gage height, 4.40 feet; discharge, 9,792 second-feet. June 26: Gage height, 2.40 feet; discharge, 5,018 second-feet. July 10: Gage height, 0.50 foot; discharge, 1,805 second-feet. July 13: Gage height, 0.25 foot; discharge, 1,376 second-feet. August 2: Gage height, -0.20 foot; discharge, 778 second-feet. August 21: Gage height, -0.70 foot; discharge, 430 second-feet.

Daily gage height, in feet, of North Platte River near Guernsey, Wyoming, for 1900.

Day.	June.	July.	Aug.	Sept.	Day.	June.	July.	Aug.	Sept.
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16		$\begin{array}{c} 1.50\\ 1.30\\ 1.30\\ 1.20\\ 1.00\\ .90\\ .80\\ .50\\ .40\\ .30\\ .25\\ .20\\ .70\\ \end{array}$	$\begin{array}{c} -0.20\\20\\20\\25\\25\\30\\40\\40\\60\\60\\70\\70\\70\\70\\70\end{array}$	$\begin{array}{c} -0.90\\90\\90\\95\\95\\95\\95\\95\\95\\95\\95\\95\\95\\95\\95\\95\\95\\95\\95\\ \end{array}$	17	$\begin{array}{c} 3.40\\ 3.40\\ 3.20\\ 3.00\\ 2.85\\ 2.70\\ 2.50\\ 2.30\\ 2.20\\ 1.90\\ 1.90\\ \end{array}$	$\begin{array}{c} .40\\ 1.10\\ .75\\ .25\\ .10\\ .00\\ .05\\ .10\\ .00\\ .00\\ .10\\ .05\\ .10\\ .10\\ .10\\ .15\\ .10\\ \end{array}$	$\begin{array}{c}70 \\80 \\80 \\70 \\70 \\75 \\80 \\75 \\80 \\90 \\99 \\90 \end{array}$	

NORTH PLATTE RIVER AT GERING, NEBRASKA.

This station, which was established May 29, 1897, is located at the highway bridge at Gering. It is described in Water-Supply Paper No. 37, page 218. Results of measurements for 1899 will be found in the Twenty-first Annual Report, Part IV, page 197. During 1900 the following measurements of discharge were made by R. H. Willis:

Discharge measurements of North Platte River at Gering, Nebraska.

Date.	Gage	Dis-		Gage	Dis-
	height.	charge.	Date.	height.	charge.
1900. April 18 May 11 May 23 May 30 June 12 June 21 June 21 June 22 June 24 June 25 June 25 June 25 June 26 June 26 June 26 June 20 June 21 June 21 Ju	$\begin{array}{c} Feet. \\ 1.67 \\ 1.90 \\ 2.16 \\ 2.46 \\ 2.65 \\ 2.86 \\ 2.24 \\ 1.80 \\ 1.45 \\ 1.55 \end{array}$	$\begin{array}{c} Secft.\\ 5, 251\\ 7, 138\\ 10, 980\\ 10, 909\\ 12, 371\\ 13, 706\\ 9, 231\\ 6, 321\\ 2, 874\\ 3, 947 \end{array}$	1900. August 1. August 10. August 22. August 30. September 11. September 12. October 19. October 30.	$\begin{matrix} Feet. \\ 1.15 \\ 1.02 \\ .93 \\ .84 \\ .96 \\ .85 \\ .32 \\ .35 \\ .45 \end{matrix}$	$\begin{array}{c} Secft.\\ 1,152\\ 848\\ 529\\ 395\\ 385\\ 356\\ 486\\ 486\\ 399\\ 522 \end{array}$

Daily gage height, in feet, of North Platte River at Gering, Nebraska, for 1900.

$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	Day.	Apr.	May.	June.	July.	Aug.	Sept.	Oet.	Nov.
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1		2.25	2.75	1.70	1.00	0.78	0.48	0.35
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	9		2.20	2.80	1.70	1.00	0. 10	35	36
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3		2.25	2.90	1 71	1.02	78		36
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1		2.40	2.98	1.70	1.00	79	.007	.00
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	5		2.35	2.85	1.60	1.01	76	27	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	6		2.35	2.85	1.53	1.00	77	26	40
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	7		2.20	2.82	1.53	. 97	73	27	41
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	8		2.15	2.80	1.44	.98	.76	27	40
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	9		2.15	2.78	1.44	. 95	.75	.27	.42
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	10		2.05		1.40	. 96	. 80	. 26	1.05
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	11		2.15		1.30	. 95	. 85	.25	1.04
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	12		2.16	2.71	1.21	. 93	.87	.23	1.03
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	13		2.30	2.71	1.10	. 90	. 90	.24	1.04
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	14		2.36	2.86	1.12	. 90	. 90	.24	a 1.05
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	15		2.53	2.76	1.29	. 86	. 90	. 23	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	16		2.62	2.56	1.21	. 90	. 85	. 24	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	17		2.65	2.46	1.30	. 90	. 80	. 24	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	18	1.67	2.56	2.29	1.30	. 90	. 80	. 23	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	19	1.60	2.50	2.23	1.56	. 88	. 77	. 32	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	20	1.55	2.45	2.26	1.42	. 88	. 75	. 31	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	21	1.55	2.46	2.19	1.25	. 88	. 75	. 31	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	6)+) M/M	1.60	2.49	2.01	1.30	. 84	. 75	. 30	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	23	1.85	2.40	1.89	1.22	. 82	. 75	. 30	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	24	1.90	2.35	1.89	1.30	. 80	. 75	. 31	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	25	1.83	2.31	1.91	1.40	. 71	. 60	. 31	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	26	1.80	2.29	1.87	1.21	. 73	. 62	. 32	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	27	1.90	2.35	1.81	1.21	. 76	. 60	. 33	
29 2.53 1.76 1.01 74 55 34	28	2.00	2.50	1.80	1.19	. 75	. 61	. 34	
	29	2.00	2.53	1.76	1.01	. 74	. 55	. 34	
30 2.40 2.60 1.70 1.05 $.75$ $.53$ $.36$	30	2.40	2.60	1.70	1.05	. 75	. 53	. 36	
31	31		2.69		1.05	. 75		. 37	

a Closed for winter November 14.

NORTH PLATTE RIVER AT CAMP CLARKE, NEBRASKA.

This station, which was established June 27, 1896, consists of a timber fastened to cross-ties bedded in the bank of the river. It is described in Water-Supply Paper No. 37, page 219. Results of

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measurements for 1899 will be found in the Twenty-first Annual Report, Part IV, page 198. During 1900 the following discharge measurements were made by R. H. Willis:

Discharge measurements of North Platte River at Camp Clarke, Nebraska.

Date.	Gage height.	Dis- charge.	Date.	Gage height.	Dis- charge.
1960. April 19 April 28 May 14 May 25 May 31 June 13 June 29 June 29 July 11 July 20	$\begin{array}{c} Feet. \\ 3.28 \\ 3.71 \\ 4.10 \\ 2.90 \\ 4.08 \\ 4.27 \\ 3.75 \\ 3.35 \\ 2.74 \\ 3.08 \end{array}$	$\begin{array}{c} Secft.\\ 4.928\\ 7,146\\ 11,838\\ 9,131\\ 10,434\\ 11,334\\ 7,695\\ 4,049\\ 2,116\\ 3,654 \end{array}$	1900. July 28 August 11 August 24 August 31 September 12 September 21 October 3 October 31	$\begin{array}{c} Feet. \\ 2.61 \\ 2.20 \\ 2.05 \\ 1.96 \\ 2.08 \\ 2.08 \\ 2.10 \\ 2.18 \\ 2.26 \end{array}$	$\begin{array}{c} Sec.\text{-}ft. \\ 1, 624 \\ 501 \\ 421 \\ 274 \\ 320 \\ 246 \\ 234 \\ 377 \\ 610 \end{array}$

Daily gage height, in feet, of North Platte River at Camp Clarke. Nebraska, for 1900.

$\begin{array}{c ccccccccccccccccccccccccccccccccccc$			to della d				
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 4.10\\ 3.855\\ 3.4.008\\ 3.892\\ 3.899\\ 3.899\\ 4.109\\ 4.127\\ 4.343\\ 3.992\\ 3.899\\ 4.109\\ 4.127\\ 4.4.343\\ 3.992\\ 3.898\\ 3.992\\ 3.8781\\ 4.105\\ 3.982\\ 3.8781\\ 4.115\\ \end{array}$	$\begin{array}{c} 29\\ 4 \\ 4 \\ 4 \\ 4 \\ 4 \\ 4 \\ 4 \\ 4 \\ 4 \\ 4$	31271150659117037162224722378653317883200991120120120120120120120120120120120120120	$\begin{array}{c} 2.253\\ 2.233\\ 2.233\\ 2.220\\ 2.$	$\begin{array}{c} 1.98\\ 1.92\\ 1.956\\ 1.962\\ 1.978\\ 2.080\\ 2.109\\ 1.98\\ 2.080\\ 2.005$	2.105 2.2098 (075) 2.111 2.100 (8.09) 2.111 2.100 (8.09) 2.111 2.100 (8.09) 2.111 2.110 (1.11) 2.110 (1.11) (1.11) (1.11) (1.11) (1.11) (1.11) (1.11	2.23 2.24 2.24 2.24 2.24 2.25 2.26 2.26 2.26 2.28 2.30 <i>a</i> 2.31

 α Closed for winter.

NORTH PLATTE RIVER AT NORTH PLATTE, NEBRASKA.

This station, which was established in 1894, is 3.5 miles above the junction of South Platte River. It is described in Water-Supply Paper No. 37, page 220. Results of measurements for 1899 will be found in the Twenty-first Annual Report, Part IV, page 199. During 1900 one discharge measurement was made by Adna Dobson, as follows:

December 20: Gage height, 2.30 feet; discharge, 1,223 second-feet.

IRR 49-01-6



Daily gage height, in feet, of North Platte River at North Platte, Nebraska, for 1900.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oet.	Nov.	Dec.
1	2.40	2.00	2.70	2.30	3.20	3.45	2.85	1.85	0.80	1.40	1.80	2.10
2	2.35	2.05 2.20	$\frac{2.85}{3.00}$	2.30	$\frac{3.15}{3.35}$	3.50	2.60	1.75 1.60	. 80	1.40 1.40	1.80 1.80	-2.20
4	2.35	$\tilde{2}.\tilde{2}0$	3.10	2.25	3.30	3.65	2.60	1.45	.80	1.40	1.80	2.25
5	2.40	2.25	3.10	2.30	3.35	3.80	2.90	1.50	. 80	1.30	1.70	2.10
6	$\frac{2.50}{2.60}$	2.35	3.10	2.40	$\frac{3.50}{2.50}$	3.85	2.80	1.80	1.80	1.30	1.70	2.30
8	2.00 2.70	2.25	$\frac{2.80}{2.80}$	2.60	3.40	ə. cə 3. 90	2.60	1.95	. 80	1.00 1.30	$1.40 \\ 1.80$	-2.30
9	2.80	2.20	2.80	2.50	3.25	3.80	2.45	1.95	.80	1.30	1.80	2.30
10	2.80	2.30	2.80	2.50	3.20	3.75	2.20	1.65	. 95	1.30	1.70	2.20
1)	2.80	2.40	3.70	2 60	3.20	3.70	2.10	1.00	. 90	1.30 1.40	1.70 1.85	2.25
13	2.90	2.30	2.30	2.65	3.25	3.50	$\frac{2.20}{2.20}$	1.50	. 90	1.40	1.80	2.30
14	2.90	2.30	2.15	2,60	3.30	3.50	2.10	1.45	. 80	1.40	1.85	2.30
15	2.95	2.60	$\frac{2.00}{2.10}$	2.70	$\frac{3.30}{2.20}$	3.55	2.10	$\begin{bmatrix} 1.30 \\ 1.20 \end{bmatrix}$. 80	1.40	1.90	-2.20
10	3.00	2.30	2.80	2.90	3.30	3.60	2.10	1.25	. 90	1.40 1.50	1.60 1.80	2.20
18	3.00	2.35	2.30	2.90	3.45	3.60	2.05	1.15	. 95	1.50	1.75	2.20
19	2.85	2.40	2.10	2.80	3.60	3.45	1.90	1.10	.95	1.50	1.60	2.20
20	2.80	2.50	2.00	2.70	3.60	3.30	2.00	. 95	. 99	1.50	1.70	2.30
22	$\tilde{2}$ 60	2.65	2.50	2.70	3.50 3.50	3.20	$\tilde{2.00}$	$1.49 \\ 1.50$. 90	1.50 1.50	1.95	2.40
23	2.65	2.70	2.40	2.80	3.45	3.10	2.10	1.35	.90	1.50	2.00	2.00
24	2.70	2.80	2.50	2.90	$\frac{3.40}{10}$	$\frac{3.10}{2.10}$	2.35	1.50	.90	1.60	1.95	2.00
20	2.55	2.80	2 40	3.10	3.40 3.35	3.10	2.50	1.40	.90	1.70 1.60	2.20	2.40
27	2.00	2.60	2.40	3.10	3.30	2.90	2.35	1.20	1.00	1.60	2.30	1.85
28	1.70	2.60	2.30	3.05	3.25	2.90	2.00	1.20	1.10	1.60	2.15	1.80
29	1.90		2.30	2.90	$\frac{3.20}{2.20}$	2.80	$\frac{2.00}{2.00}$	1.00	1.10 1.25	1.65 1.70	2.00	1.60
90	2 00		5 20	N. 90	3 10	N. 80	1 00	1.00	1.40	1.75	A. 00	* ~ ~ ~ ~ ~ ~

SOUTH PLATTE RIVER.

The South Platte rises in the high mountain peaks surrounding the basin known as South Park, near the center of the State of Colorado. These mountains vary in altitude from 14,000 feet, in the Park Range, to 9,000 feet, in South Park. From the point where the stream issues from the mountains at Platte Canyon it flows in a northerly direction through Denver to its junction with the Cache la Poudre near Greeley, thence in a northeasterly direction until it leaves the State a short distance to the northeast of Julesburg, and thence in an easterly direction to its junction with the North Platte near North Platte, Nebraska.

The tributaries may be divided into two classes: (1) Those which, like the headwaters of the South Platte, rise in the mountains, and (2) those which drain the plains east of the mountains. The principal tributaries of the first class, in their order down the river, are Bear Creek, Clear Creek, St. Vrain Creek, Boulder and South Boulder creeks, Big Thompson Creek, and Cache la Poudre River. Among those of the second class there may be named, as especially worthy of consideration, Cherry Creek, Lone Tree Creek, Boxelder Creek, Bijou Creek, Beaver Creek, and Pawnee Creek. There are many others of lesser note. The streams of the first class—those flowing from the mountains—resemble the upper reaches of the South Platte in that they furnish a perennial supply of water, which varies, however, with the season, the discharge being great during the flood stages and low

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during the latter part of the summer and in the fall and winter. The streams from the plains, on the other hand, are intermittent in their nature, usually furnishing water only during storms or the melting of snows. In general it may be said that the normal perennial discharge of all of the streams of this division is claimed and used for irrigation, but great quantities of water go to waste during the flood stages and in times of storms. As there is a vast amount of land upon the plains adjacent to the South Platte that might be irrigated if there were a sufficient supply of water, the question of storage becomes one of great importance, and the Geological Survey is now studying this problem, examining such reservoir sites as are considered capable of storing considerable quantities of water. It is hoped that reservoirs will be constructed to prevent the loss of this great amount of water, which, if properly stored, would become one of the greatest assets of the arid region.

An interesting feature of the South Platte Basin is the fact that in all of its valleys there is a great return from seepage, which is increasing from year to year, as may be seen in the tables of seepage measurements of this river published by the State engineer of Colorado. The underground water supply of the plains in this basin is also being studied, and the results of the investigations will be of great interest in determining the possibilities of procuring water from artesian sources for stock purposes and possibly for the irrigation of small tracts of land. The surface flow of the intermittent streams of the plains may be made available for irrigation purposes by the construction of suitable reservoirs, a few of which are now being utilized by corporations and private parties. The most notable projects of this character which have been under way in the basin during the year are the Lake Cheesman dam, which is being constructed by the Denver Union Water Company, C. L. Harrison, chief engineer, and the Bijou Irrigation Company's reservoirs in the neighborhood of Orchard. The Lake Cheesman reservoir is especially noteworthy on account of the great height of its dam (215 feet) and the amount of water to be stored. The dam will be of solid masonry. The reservoir sites of the Bijou Irrigation Company are natural basins, along the rims of which embankments will be constructed, thus storing large quantities of water, which will be conducted from the river through canals. Anv great extension of the irrigated area of this district must depend upon the construction of additional reservoirs and upon improvements in the use and distribution of water. The present system of distribution throughout this section, as in nearly all of the arid region, is very extravagant, in many cases there being several times the number of ditch lines that the most economical use would demand, while much water goes to waste in marshes and swamps which might be drained, and an increased supply thus be made available.

SOUTH FORK OF SOUTH PLATTE RIVER AT LAKE CHEESMAN, COLORADO.

During the year 1900 the engineers in charge of the construction of the dam at Lake Cheesman kept practically continuous records of the gage heights and discharge of Goose Creek and South Platte River above their junction, and also of the combined discharge below the junction, the latter measurements being made below the dam. The accompanying table of discharge measurements at the latter place was obtained through the courtesy of Mr. C. L. Harrison, at present chief engineer of the Denver Union Water Company. The discharge for February is estimated, but it may be considered approximately correct. Discharges for the other months are from actual measurements, which are usually made three times a day, but sometimes oftener. The results may be considered very nearly correct.

SOUTH PLATTE RIVER NEAR PLATTE CANYON, COLORADO.

This station was located about 2 miles above the Colorado and Southern Railroad station at Platte Canvon. It was maintained by the Denver Union Water Company for some time previous to any cooperation on the part of the Survey, which began April 1, 1899. The gage rod was a 2-inch by 2-inch inclined timber on the right-hand side of the stream, the graduations being marked with brass nails. Measurements of discharge were made from the footbridge constructed by the water company at the rod. Readings were taken until June 2, 1900, inclusive, when extremely high water carried away the gage rod, which has not yet been replaced. Only two measurements were made in 1900. The channel at this point is rocky, but the high water changed it materially, so that it will be best for a new location to be selected. A station at this place is of great importance, and one should be maintained with care. A cable should be stretched across the river, with a traveling car, at such a height as to preclude the danger of its being washed away by floods. The figures given in the table show the actual discharge of the river at Platte Canyon before any water is diverted for irrigation or other purpose, except that taken out by the Denver Union Water Company a short distance above the station, for the supply of the city of Denver.

Readings were taken by James Proctor, of Littleton, Colorado, who is in charge of the pumping station of the Denver Union Water Company at that place. While the station was being maintained gage readings were furnished to the officers of the United States Weather Bureau at Denver, who had them published in the papers.

A description of the station was published in Water-Supply Paper No. 37, page 224. The results of measurements for 1899 will be found in the Twenty-first Annual Report, Part IV, page 201. During 1900 the following measurements were made by Λ . L. Fellows:

> March 5: Gage height, -0.40 foot; discharge, 87 second-feet. April 18: Gage height, 1.55 feet; discharge, 467 second-feet.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	Day.	Jan.	Feb.	Mar.	Apr.	May.	June.
$\begin{array}{c} 1 \\ 2 \\ 3 \\ 4 \\ 5 \\ 5 \\ 7 \\ 8 \\ 9 \\ 10 \\ 11 \\ 12 \\ 13 \\ 14 \\ 15 \\ 16 \\ 15 \\ 16 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10$	$\begin{array}{c} 0.3\\ .2\\ .1\\ .1\\ .0\\\\ .435\\\\ .445\\\\ .445\\\\ .445\\\\ .\\ .\\ .\\ .\\ .\\ .\\ .\\ .\\ .\\ .\\ .\\ .$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} -0.5 \\ -0$	$\begin{array}{c} 0.22\\ .22\\ .33\\ .4\\ .66\\ .8\\ .9\\ .7\\ .80\\ 1.1\\ 1.6\\ 1.6\end{array}$	$\begin{array}{c} 4.\widetilde{}.\\ 4.61\\ (b)\\ (b)\\ (b)\\ (b)\\ (b)\\ (b)\\ (b)\\ (b)$	5. 6 5. 6 (<i>a</i>)	$\begin{array}{c} 17 \\ 18 \\ 19 \\ 20 \\ 21 \\ 23 \\ 24 \\ 25 \\ 25 \\ 26 \\ 27 \\ 28 \\ 29 \\ 30 \\ 31 \\ \end{array}$	$ \begin{array}{c} -0.5 \\5 \\4 \\4 \\4 \\3 \\4 \\5 \\4 \\5 \\4 \\5 \\4 \\6 \\ \end{array} $		0.5554933344443333322	$\begin{array}{c} 1.4\\ 1.69\\ 1.96\\ 3.57\\ 8.89\\ 8.82\\ 1.4\\ 5.4\\ 1.8\\ 1.8\\ 1.8\\ 1.8\\ 1.8\\ 1.8\\ 1.8\\ 1.8$	5.5.4455886688922345 5.5.544444444555555	

Daily gage height, in feet, of South Platte River near Platte Canyon, Colorado, for 1900,

a Gage washed away.

b Gage out.

SOUTH PLATTE RIVER AT DENVER, COLORADO.

This station is located at the Fifteenth street bridge in the city of Denver, a short distance below the mouth of Cherry Creek. It was established July 15, 1895, and has been maintained continuously. For a portion of the last year two rods were in use, one on the left bank and the other on the right bank a short distance below the bridge. Both were inclined rods. The rod on the left bank was washed out by the high water of June, 1900, which also removed the sand bar in front of the rod on the right-hand side, making it available at low-water stages, which it had not been before, and since that time the readings have been taken from the latter rod. The bench mark is a cross on the north corner of the top of the east abutment of the Fifteenth street bridge, and is 15.15 feet above gage datum. The river at this point is confined between slag embankments, but owing to the shifting sandy bottom the channel is very changeable, rendering necessary frequent changes in the rating tables. The observations have been made by the water commissioners of water district No. 2, in which Denver is located, W. J. Southland and his successor, S. M. Matlock. During 1900 eleven gagings were made at this point. The daily gage height, with corresponding discharge, was published in the Denver papers by the United States Weather Bureau. A description of the station was published in Water-Supply Paper No. 37, page 225. The results of measurements for 1899 will be found in the Twenty-first Annual Report, Part IV, page 202. During 1900 the following measurements were made by A. L. Fellows and R. W. Hawley:

Discharge measurements of South Platte River at Denver, Colorado.

Date.	Gage heigbt.	Dis- charge.	Date.	Gage height.	Dis- charge.
1906. April 12 April 12 April 16 April 20 April 20 June 11	$\begin{array}{c} Feet. \\ 5.50 \\ 5.90 \\ 7.24 \\ 7.10 \\ 8.32 \\ 8.50 \end{array}$	$\begin{array}{c} Secft.\\ 244\\ 377\\ 1,439\\ 1,395\\ 3,516\\ 3,270 \end{array}$	July 25 1900. August 7	$Feet. \\ 5.45 \\ 5.56 \\ 4.90 \\ 5.50 \\ 5.30 \\ \end{cases}$	<i>Secft.</i> 257 285 90 226 161

Daily gage height, in feet, of South Platte River at Denver, Colorado, for 1900.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1	5.30	5.35	5.25	5.05	9.40	8.75	6.65	5.00	4.75	4.90	5.00	5.00
2	. 5.35	5.45	5.35	5.00	9.40	8.92	6.55	5.10	a 4.75	4.80	5.10	5.10
3	5.35	5.20	5.25	5.10	9.40	8.90	6.35	5.20	a 4.75	4.80	5.10	-5.20
4	5.30	5.25	5.30	5.05	9.40	9.00	6.35	5.40	4.75	4.90	5.40	= 5.20
5	5.25	5.25	5.45	5.30	9.35	8.90	6.30	5.45	4.85	4.90	5.30	-5.20
6	5.35	5.35	5.45	5.50	9.35	8.80	6.30	5.50	4.70	4.85	5.30	-5.30
7	5.35	5.40	5.25	5.60	9.35	8.60	6.30	5.50	4.85	4.70	5.20	5.20
8	5.40	5.30	5.20	5.50	9.40	8.50	6.30	5.55	5.05	4.80	5.30	5.30
9	. 5.35	5.25	5.20	6.00	9.45	8.50	6.20	5.45	4.90	4.90	5.30	5.30
0	5.45	5.25	5.20	5.95	9,40	8.55	6.20	5.45	4.85	4.90	5.30	5.10
1	5.60	5.20	5.30	6.60	9.50	8.55	6.10	5.50	4.95	4.90	5.30	5.20
2	5.40	5.25	5.20	6.45	9.50	8.50	5.70	5.35	5.60	4.90	5.30	5.20
3	. 5.30	5.25	5.40	6.20	9.40	8.45	5.55	5.35	5.60	4.90	5.20	-5.3
4	5.35	5.30	5.40	6.30	9.00	8.40	5.45	5.10	5.35	4.90	5.20	5.3
5	5.45	5.30	5.40	6.65	8.75	8.15	5.40	5.15	5.00	4.90	5.10	-5.3
6	5.40	5.40	5.25	7.35	8.50	8.00	5.40	5.05	5.05	5.20	5.10	5.2
7	. 5.35	5.35	5.30	7.60	8.40	7.95	5.50	4.90	5.20	5.10	5.10	5.2
8	. 5.45	5.40	5.35	6.80	8.48	7.70	5.35	4.95	5.15	5.00	5.20	5.2
9	5.35	5.45	5.25	6.75	8.30	7.60	5.10	4.80	5.25	5.00	5.20	5.3
20	. 5.30	5.50	5.40	7.70	8.40	7.58	5.15	4.95	5.10	5.00	5.20	5.3
21	5.40	5.45	5.30	7.75	8.60	7.35	5.00	4.90	5.10	5.20	5.30	5.4
22	5.30	5.35	5.25	7.95	8.50	7.25	5.00	5.00	5.10	5.20	5.40	5.4
3	5.40	5.25	5.25	8.40	8.50	7.45	5.15	4.95	4.90	5.20	5.40	5.3
24	. 5.35	5.25	5.20	8.40	8.35	7.55	5.15	5.05	4.85	5.10	5.50	5.3
5	. 5.45	5.30	5.30	8.40	8.40	7.55	5.85	5.20	5.00	5.00	5.50	5.2
26	. 5.35	5.35	5.25	8.40	8.30	7.50	5.60	5.10	5.20	5.10	5.50	5.2
27	. 5.25	5.40	5.35	8.05	8.45	7.45	5.55	5.00	5.20	5.10	5.40	5.3
28	. 5.35	5.30	5.40	8.10	8.50	7.25	5.60	4.95	5.20	4.90	5.40	5.4
29	. 5.35		5.35	9.75	8.75	7.05	5.50	4.90	5.00	4.90	5.30	5.4
30	5.40		5.10	9.50	8.70	6.70	5.30	4.80	4.90	4.90	5.20	5.5
31	. 5.30		5.10		, 8.75		5.00	4.70		4.90		5.4

a Estimated.

SOUTH PLATTE RIVER AT ORCHARD, COLORADO.

This station is on the lower part of the South Platte, below all of the mountain drainage tributary to that stream. The gage rod, which is vertical, is fastened to a pile at a wagon bridge about a quarter of a mile southwest of the Union Pacific Railroad station at Orchard. The station was first established in November, 1895, and has been maintained during the greater part of the time since. During the last year the gage rod had to be moved twice, owing to changes in the channel. The left bank of the river is high, but the right bank is low and is likely to overflow. The bed of the stream is sandy and shifting, but the cross section did not change materially during 1900. The station has been of great value in demonstrating the fact that large quantities of water go to waste during floods and during the winter season, a great portion being seepage or return water. As a result of the investigations at this place, a large irrigation enterprise has been undertaken-namely, that of diverting water from the river near Hardin for the purpose of irrigating lands in the vicinity of Fort Morgan, the water to be stored in large reservoirs, which are referred to elsewhere (page 279, Bijou Irrigation Company's reservoirs). The existence of a large flow having been demonstrated, it is now thought best that the station should be changed to a point farther upstream, probably at Kersey, where another large ditch might possibly be taken out. A description of the station was published in Water-Supply Paper No. 37, page 226. The results of measurements for 1899 will be found in the Twenty-first Annual Report, Part IV, page 203. During

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1900 the following measurements were made by A. L. Fellows and R. W. Hawley:

March 7: Gage height, 2.85; discharge, 668 second-feet. April 21: Gage height. 5 feet; discharge, 4,674 second-feet. July 23: Gage height, 1.35 feet; discharge, 156 second-feet. October 27: Gage height, 2.70 feet; discharge, 324 second-feet.

Daily gage height, in feet, of South Platte River at Orchard, Colorado, for 1900.

Day.	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
Day. 2	$\begin{array}{c} \text{Jan.}\\ \hline\\ 4.00\\ 4.00\\ 3.90\\ 3.90\\ 3.90\\ 3.90\\ 3.90\\ 3.90\\ 3.60\\ 3.60\\ 3.60\\ 3.60\\ 3.60\\ 3.60\\ 3.60\\ 3.60\\ 3.60\\ 3.20\\ \end{array}$	Feb. 2.90 2.90 2.90 2.90 2.90 2.90 2.90 2.9	Mar. 3.20 3.30 3.30 2.85	$\begin{array}{c} A \mathrm{pr.} \\ 2.70 \\ 2.90 \\ 3.00 \\ 3.20 \\ 3.30 \\ 3.40 \\ 3.50 \\ 3.60 \\ 3.75 \\ 3.90 \\ 4.00 \\ 4.10 \\ 4.50 \\ 5.00 \\ 6.25 \\ 6.70 \end{array}$	May. 8.50 8.00 8.00 8.00 8.00 7.50 8.00 7.50 8.00 7.50 8.00 7.50 8.00 7.60 6.00	June. 6.50 6.50 6.50 6.30 6.00 5.90 5.70 5.60 5.50 5.40 5.50 5.20 5.20 5.10 4.90 4.80 4.75	July. 2.70 2.50 2.40 2.20 2.10 2.00 2.00 1.90 1.80 1.70 1.60 1.50 1.40 1.35 1.35	Aug. 1.20 1.20 1.15 1.10	Sept. 1.10 1.10 1.10 1.20 1.30	Oct. 2.40 2.50 2.60 2.65 2.70 2.70 2.70 2.70 2.70 2.70 2.70 2.70	Nov. 2.70 2.70 2.75 2.75 2.80 2.80 2.80 2.80 2.80 2.85 2.85 2.90 2.80 2.80 2.80 2.80 2.80 2.80 2.80 2.8	Dec. 2.80 2.80 2.80 2.80 2.80 2.80 2.80 2.8
19	3.00 3.00 2.80 2.90 2.90 2.90 2.90 2.90 2.90 2.90 2.9	3.50 3.50 3.50 3.50 3.40 3.40 3.40 3.40 3.20 3.20 3.20 	12:770 21:270 21:270 21:7700 21:7700 21:7700 21:7700 21:7700 21:7700 21:7700 21:7700 21:77000	$\begin{array}{c} 5.50\\ 5.20\\ 5.00\\ 5.30\\ 6.50\\ 6.40\\ 6.30\\ 6.10\\ 6.00\\ 6.30\\ 7.30\\ \end{array}$	$\begin{array}{c} 5.80\\ 5.80\\ 6.00\\ 7.00\\ 6.00\\ 6.00\\ 6.00\\ 6.00\\ 6.00\\ 6.30\\ 6.30\\ 6.50\\ 6.70\\ 6.80\\ 6.70\end{array}$	$\begin{array}{c} 4.70\\ 4.60\\ 4.50\\ 4.30\\ 4.20\\ 4.00\\ 3.90\\ 3.80\\ 3.70\\ 3.50\\ 2.80\\ \end{array}$	$\begin{array}{c} 1.35\\ 1.35\\ 1.35\\ 1.35\\ 1.35\\ 1.35\\ 1.30\\ 1.30\\ 1.30\\ 1.30\\ 1.30\\ 1.30\\ 1.35\\ 1.40\\ 1.40\\ \end{array}$	$\begin{array}{c} 1.10\\$	1.30 1.30 1.30 1.30 1.30 1.40 1.50 1.65 1.80 1.95 2.10 2.20 2.30	$\begin{array}{c} 2.70\\$	2.80 2.80 2.80 2.80 2.80 2.80 2.80 2.80	2.80 2.80 2.80 2.80 2.80 2.80 2.80 2.80

SOUTH PLATTE RIVER AT JULESBURG, COLORADO.

Although no station has yet been established at this place, one is greatly needed. A rod was attached to the wagon bridge about a mile southeast of the Union Pacific Railroad station at Julesburg, but no one was found who would make the observations, so that no record has been kept. A station here would be of great value, as the bridge referred to is not far from the State line, and a knowledge of the discharge passing from Colorado into Kansas could thus be obtained. The channel is very wide, as it is throughout the lower portion of the river, and on this account the results obtained would necessarily be approximate; but they would nevertheless be valuable. Within the last two years four measurements have been made at this place, as follows:

Discharge measurements of South Platte River at Julesburg, Colorado.

	Secft.
September 14, 1899	. 2
November 12, 1899	1,120
March 8, 1900	2, 291
November 2, 1900	. 76

On December 20, 1900, the South Platte was measured at North Platte, Nebraska, by Adna Dobson, and a discharge of 963 second-feet was found.

BEAR CREEK NEAR MORRISON, COLORADO.

Bear Creek is one of the smaller tributaries of the South Platte, heading in the vicinity of Mount Evans, about 30 miles southwest of Denver, and entering the main stream about 8 miles above that city. Although usually of small volume, the stream drains a considerable portion of very mountainous country, which is subject to more or less violent cloudbursts, so that floods sometimes come down this creek, causing great destruction to property and even the loss of life. All of the normal flow of the stream is used for irrigation, and it is only during high-water stages that a large amount of water passes through it. Records of its flow have been kept for a portion of each irrigation season since April, 1888, with the exception of the years 1892, 1893, and 1894. The present station was established April 16, 1899. It is located just above the little town of Morrison. The gage rod, which is a 2-inch by 4-inch timber placed vertically and marked in feet and tenths, is fastened to the upper side of the dam which diverts water into the mains of the Denver Union Water Company. The bench mark is the top of a granite bowlder about 100 feet above the rod on the left-hand side of the stream, and it is 10.33 feet above the gage datum. As in previous years, the station was maintained through cooperation with the Denver Union Water Company. Owing to the formation of a gravel bar in the summer of 1900, the conditions were for some time radically changed from the normal, and during the month of September no gagings were taken. The observer is S. Hebrew, an employee of the Denver Union Water Company. Tables of gage heights and discharge measurements for 1899 will be found in Water-Supply Paper No. 37, pages 227 and 228. Table of the monthly flow for that year will be found in the Twenty-first Annual Report, Part IV, page 204. During 1900 the following measurements were made by A. L. Fellows:

March 9: Gage height, 1.40 feet; discharge, 17 second-feet. April 14: Gage height, 2.85 feet; discharge, 47 second-feet. April 25: Gage height, 5.80 feet; discharge, 367 second-feet. August 7: Gage height, 3.20 feet; discharge, 63 second-feet. September 6: No gage height taken (conditions abnormal): discharge, 24 second-feet.

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Daily gage heig	ght, in feet, of	^r Bear Creek nea	r Morrison, C	Colorado, f	$or \ 1900.$
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Day.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
1		6.70 6.25	5.95 6.25	4.75	3.55 3.45	2.00	2.60 2.55	1.90 1.85	1.35 1.35
34		6.30	6.55 6.50	4. 55 4. 55	3.30 4.00		2.45 2.40	$1.80 \\ 1.80$	1.45
5		6.20 6.30	6.40 6.10	$\frac{4.35}{4.30}$	$\frac{4.00}{3.75}$		2.35 2.30	$1.70 \\ 1.70$	
7		$6.40 \\ 6.50$	$\begin{array}{c} 6. 25 \\ 6. 25 \end{array}$	$\frac{4.35}{4.30}$	$3.70 \\ 3.60$		$\frac{2.25}{2.30}$	$1.70 \\ 1.60$	
9- 10		$ \begin{array}{r} 6.50 \\ 6.70 \end{array} $	$\begin{array}{c} 6.15 \\ 6.50 \end{array}$	$\frac{4.25}{4.20}$	$3.50 \\ 3.40$		$2.20 \\ 2.20$	$ \begin{array}{r} 1.60 \\ 1.60 \end{array} $	
11		$\begin{array}{c} 6.90 \\ 6.75 \\ \end{array}$	$\begin{array}{c} 6.40 \\ 6.10 \\ 5.05 \end{array}$	4.15 4.10	3.30 3.05		2.20 2.10	$1.60 \\ 1.60 \\ 1.50$	
13. 14. 15.	3.00	6.45 6.20	5.95 5.95 5.95	4.10 4.05 4.00	2.80 2.65 2.45		2.10 2.10 2.00	1.50 1.50 1.50	
16 17	2.95	6.05 5.90	5.85 5.70	4.20	2.35		2.00 2.00 2.00	1.40	
18 19	$3.65 \\ 4.50$	$5.90 \\ 5.90$	$5.70 \\ 5.60$	$\frac{4.05}{4.00}$	$2.20 \\ 2.10$		$\frac{2.00}{2.00}$	$ \begin{array}{c} 1.30 \\ 1.30 \end{array} $	
20 21	$4.80 \\ 5.30$		$5.60 \\ 5.55$	3.90 3.80	$2.20 \\ 2.25$		$1.90 \\ 1.90$	$1.20 \\ 1.20$	
99 99 90 94	5.80	5.95 6.05 6.05	5.55 5.50 5.40	3.75 4.00 4.25	2.30 2.30 2.90		1.90 1.85 1.85	1.20 1.10 1.10	
24 25 26	5.90 6.15		5. 25 5. 25	4. 55 4. 40 4. 25	2.20 2.10 2.10		$1.80 \\ 1.80 \\ 1.70$	1.10 1.20 1.35	
27 28	6.25 6.30	$6.20 \\ 6.10$	$5.15 \\ 5.15$	$4.15 \\ 4.05$	2.10 2.10 2.10		$1.70 \\ 1.70$	$1.40 \\ 1.50$	
29 30	$7.00 \\ 6.90$	$\begin{array}{c} 6.10 \\ 6.05 \end{array}$	$5.05 \\ 4.95$	$\frac{4.00}{3.85}$	$2.05 \\ 2.00$	2.70	$ \begin{array}{r} 1.80 \\ 2.00 \end{array} $	$\begin{array}{c} 1.45\\ 1.40\end{array}$	
31		6.00		3.75	2.00		2.00		

a Gage heights not taken from September 2 to 29, inclusive, on account of dam on stream raising the water.

CLEAR CREEK AT FORKSCREEK, COLORADO.

Clear Creek rises on the eastern slope of the Rocky Mountains, in the vicinity of Gravs and James peaks, about 40 miles west of Denver, and flows easterly, entering the South Platte 6 miles below the center of that city. Like the other streams of this region, for a long distance it flows through mountainous country, the water being used for power purposes and for placer mining. At Golden the creek enters an open and fertile valley, and so large a proportion of the water is diverted, by means of irrigation canals, for the cultivation of the land lying along the stream, that little of the normal flow passes into the South Platte, except that returned by seepage. During the flood stages, however, considerable water enters the main stream. The gaging station is located at the Forkscreek railroad station on the Colorado and Southern Railway, in Clear Creek Canyon, just below the junction of the North and South forks of Clear Creek. It was established May 29, 1899, and has been continued through the irrigation seasons of 1899 and 1900. The gage consists of a weight fastened to a wire running over a pulley at the edge of the embankment upon which the railway station is located. It is referred to bench marks back of the embankment. The stream flows rapidly through this part of the canyon, the channel being rocky and the fall great. Both banks are high and rocky. There is no suitable means for crossing the river at the gaging station, the railway bridge over the stream being constructed at an acute angle. It is possible, however, to seeure fairly good results by means of measurements made at the two bridges above the forks, thus securing data of the flow of each branch as well as the total flow. At low water the stream may be gaged by wading. During the last two years the observer has been C. N. Davis, railway station agent at Forkscreek. He has voluntarily made the readings and sent daily reports to the local forecast official in Denver, who has had them published in the morning papers. A description of the station was published in Water-Supply Paper No. 37, page 228. The results of measurements for 1899 will be found in the Twenty-first Annual Report, Part IV, page 205. During 1900 the following measurements were made by A. L. Fellows:

> March 10: Gage height, 1.60 feet; discharge, 55 second-feet. April 13: Gage height, 1.70 feet; discharge, 73 second-feet. April 24: Gage height, 2.60 feet; discharge, 290 second-feet. August 27: Gage height, 1.78 feet; discharge, 130 second-feet.

Daily gage height, in feet, of Clear Creek at Forkscreek, Colorado, for 1900.

Dar	Mar	Anr	May	June	July	Aug	Sent	Oet	Nor	Dec
Day.	man.	Apr.	may.	o une.	oury.	Aug.	sept.	OCL.	1000	Dec.
1		1.60	2 80	4.40	2 60	9 40	1 70	1.60	1.60	1 55
9		1.60	2 80	4 35	3.50	2 35	1.70	1.60	1.60	1.55
3		1.60	2 80	4 05	3 25	0.05	1 70	1.60	1.60	1.55
4		2.10	2.85	4.20	3.25	2.25	1.70	1.60	1.55	1.55
5		2.10	3.00	4.10	3.20	2.30	1.70	1.60	1.55	
6		2.15	3.25	4.20	3.20	2.25	1.65	1.60	1.55	
7		2.05	3.30	4.35	3.20	2.20	1.60	1.60	1.55	
8		1.85	3.40	4.55	3.10	2.15	1.60	1.60	1.55	
9		1.80	3.55	4.55	3.10	2.10	1. ti0	1.60	1.55	
10	1.65	1.85	3.90	4.45	3.00	2.10	1.70	1.60	1.55	
11	1.70	1.80	4.30	4.05	3.00	2.10	1.65	1.60	1.55	
12	1.65	1.80	4.55	3, 95	2.85	2.10	1.60	1.60	1.55	
13	1.70	1.75	4.20	4.00	2.80	2.00	1.60	1.60	1.55	
14	1.70	1.80	3. 19	3,90	2.75	2.00	1.60	1.70	1.55	
10	1.00	1.80	3.15	3.90	2.10	$\frac{2.00}{1.00}$	1.60	1.65	1. 33	
10	1.60	1.80	0.40	4.05	2.10	1.90	1.00	1.60	1.00	
10	1.00	1.80	3.80	4.00	2.10	1.90	1.00	1.00	1.00	
10	1.00	1.80	0.10	4.00	2.00	1.90	1.50	1.00	1.00	
10	1.00	2.00	3.10	4.00	2 50	1.90	1.50	1.00	1.00	
91	1.60	0.00	3 **	1.00	2.50	1.00	1.50	1.60	1.55	
99	1.60	9 65	3.60	4.00	2.50	1 90	1.50	1.60	1.55	
23	1.60	2.60	3.75	4.00	2.50	1.90	1.50	1 60	1.55	
24	1.60	2.60	3.65	3.90	2 50	1.85	1.50	1.60	1.55	
25	1.60	2.70	4.05	3.85	2.50	1.80	1.60	1.60	1.55	
26	1.60	2.55	4.05	3.80	2.50	1.80	1.60	1.60	1.55	
27	1.60	2.55	4.10	3.60	2.50	1.80	1.60	1.60	1.55	
28	1.60	2.60	4.35	3.60	2.50	1.80	1.60	1.60	1.55	
29	1.60	2.90	4.40	3.60	2.50	1.80	1.60	1.55	1.55	
30	1.60	2.90	4.45	3.70	2.40	1.80	1.60	1.55	1.55	
31	1.60		4.30		2.40	1.75		1.60		

SOUTH BOULDER CREEK NEAR MARSHALL, COLORADO.

South Boulder Creek, a tributary of Boulder Creek, is the next mountain stream of importance north of Clear Creek. The gaging station, which was established in April, 1888, and has been maintained during a portion of each year since, except during 1893 and 1894, is located at the mouth of the canyon from which the stream issues about 3 miles west of the Colorado and Southern Railway station at Marshall. The rod consists of an inclined timber on the

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north bank of the stream near the house of C. E. Barber. Above the station two ditches divert water, namely, the South Boulder and Coal Creek ditch and the Community ditch, and their discharges must be added to the discharge at the station, in order to obtain the total runoff of the basin. The channel of the stream, which is rocky and full of bowlders, does not change materially. Gagings are usually made by wading, but at high water they are made from the footbridge just above the rod. The observer during 1900 was Miss Blanche Barber, who lives near by. A description of the station was published in Water-Supply Paper No. 37, page 229. The results of measurements for 1899 will be found in the Twenty-first Annual Report, Part IV, page 206. During 1900 the following measurements were made by A. L. Fellows:

> July 28: Gage height, 1.40 feet; discharge, 35 second-feet. August 28: Gage height, 1.10 feet; discharge, 10 second-feet.

Daily gage height, in feet, of South Boulder Creek near Marshall, Colorado, for 1900.

Day.	May.	June.	July.	Aug.	Sept.	Day.	May	June.	July.	Aug.	Sept.
1	4.00 4.00 4.00 4.00 4.00 (<i>a</i>)	$\begin{array}{c} 3.45\\ 3.45\\ 3.45\\ 3.40\\ 3.20\\ 3.20\\ 3.20\\ 3.20\\ 3.05\\ 3.00\\ 2.95\\ 2.90\\ 2.90\\ 2.90\\ 2.60\\ 2.70\end{array}$	$\begin{array}{c} 2.40\\ 2.30\\ 2.20\\ 2.25\\ 2.15\\ 2.15\\ 2.16\\ 1.80\\ 1.80\\ 1.80\\ 1.80\\ 1.80\\ 1.85\\ 1.80 \end{array}$	$\begin{array}{c} 1.45\\ 1.50\\ 1.50\\ 1.50\\ 1.60\\ 1.50\\ 1.40\\ 1.40\\ 1.40\\ 1.40\\ 1.40\\ 1.35\\ 1.35\\ 1.35\\ 1.30\\ \end{array}$	$\begin{array}{c} 1.00\\ 1.05\\ 1.00\\ 1.05\\ 1.05\\ 1.05\\ 1.05\\ 1.05\\ 1.05\\ 1.00\\ 1.20\\ 1.10\\ 1.10\\ 1.10\\ 1.00\\ 1.05\\ 1.00\\ \end{array}$	17 18 19 20 21 22 23 24 25 26 27 28 29 30 31		2555 22257 22257 22257 22257 22257 222560 22257 2225 22257 22557 22557 22557 22257 22557 255577 25557 25557 25557 25557 255577 255577 25557 25557 25557 2555	$\begin{array}{c} 1.80\\ 1.75\\ 1.70\\ 1.70\\ 1.70\\ 1.70\\ 1.60\\ 1.55\\ 1.60\\ 1.40\\ 1.40\\ 1.40\\ 1.60\\ \end{array}$	$\begin{array}{c} 1.30\\ 1.30\\ 1.30\\ 1.25\\ 1.30\\ 1.25\\ 1.30\\ 1.25\\ 1.35\\ 1.35\\ 1.30\\ 1.20\\ 1.20\\ 1.10\\ 1.10\\ 1.00\\ \end{array}$	$\begin{array}{c} 1.\ 05\\ 1.\ 10\\ 1.\ 05\\ 1.\ 00\\ 1.\ 05\\ 1.\ 15\\ 1.\ 10\\ 1.\ 15\\ 1.\ 20\\ 1.\ 10\\ 1.\ 10\\ 1.\ 10\\ 1.\ 00\\ \end{array}$

a Regular readings did not begin until June 1.

BOULDER CREEK NEAR BOULDER, COLORADO.

The general character of Boulder Creek, one of the tributaries of St. Vrain Creek, is similar to that of the latter stream. The gaging station is located $1\frac{1}{2}$ miles above the town of Boulder, where the stream issues from the mountains. There are two small irrigation ditches above the station, but the amount of water diverted does not exceed 5 or 6 second-feet, and may, therefore, be disregarded. The channel of the stream contains so many large bowlders that accurate measurements are difficult to obtain, either here or at any other point. During high water measurements are made from the bridge, but at low-water stages the stream can be gaged by wading. The entire normal flow is used for irrigation, but large quantities of water go to waste during the flood season. Plans are being considered for the construction of large reservoirs to store the flood waters for the irrigation of lands now arid. The gage rod is an inclined timber spiked to stakes driven into the bank. The bench mark is the top of a large stone 22 feet west of the gage and 5.72 feet above the zero of the rod. Both banks are high and rocky, and are not subject to overflow. The observer for 1900 was Mrs. Carrie Osgood, who lives near by. A description of the station was published in Water-Supply Paper No. 37, page 231. The results of measurements for 1897, 1898, and 1899 will be found in the Twenty-first Annual Report, Part IV, page 207. During 1900 the following measurements were made by A. L. Fellows:

> April 28: Gage height, 2.10 feet; discharge, 483 second-feet. July 27: Gage height, 1.40 feet; discharge, 220 second-feet. August 28: Gage height, 0.62 foot; discharge, 49 second-feet.

Daily gage height, in feet, of Boulder Creek near Boulder. Colorado, for 1900.

Day.	May.	June.	July.	Aug.	Sept.	Oct.	Day.	May.	June.	July.	Aug.	Sept.	Oct.
$\begin{array}{c} 1 \\ 2 \\ 3 \\ 4 \\ 5 \\ 6 \\ 7 \\ 8 \\ 9 \\ 10 \\ 11 \\ 12 \\ 13 \\ 14 \\ 15 \\ 16 \\ . \end{array}$	55550002557687657688550 01212121212121212121212121212121212121	85555568226821580 81515688226821580 81515688226821580 81515688226821580 815156882268 815156882268 8151580 815156882268 8151580 815156882 8151588 8151588 8151588 8151588 8151588 8151588 8151588 8151588 8151588 8151588 8151588 8151588 8151588 8151588 8151588 8151588 8151588 8151588 815158 81558	$\begin{array}{c} 2.00\\ 1.95\\ 1.95\\ 1.82\\ 1.70\\ 1.60\\ 1.40\\ 1.40\\ 1.40\\ 1.50\\ 1.62\\ 1.52\\ 1.60\\ 1.52\\ 1.60\\ 1.55\\ \end{array}$	$\begin{array}{c} 1.32222\\ 1.12222\\ 1.13220\\ 1.138\\ 1.132\\ 1.088\\ 998\\ 992\\ 990\\ 850\\ 78\end{array}$	$\begin{array}{c} 0, 60 \\ .60 \\ .62 \\ .60 \\ .60 \\ .60 \\ .60 \\ .95 \\ .99 \\ .88 \\ .82 \\ .80 \\ .65 \\ .60 \end{array}$	$\begin{array}{c} 0.455\\ .452\\ .445\\ .445\\ .48\\ .508\\ .480\\ .480\\ .567\\ .70\end{array}$	17 18 19 20 21 23 24 25 26 27 28 29 30 31 31 29 29 20 21 23 23 24 26 27 28 29 29 29 20 20 21 20 21 23 24 26 27 26 27 26 27 26 27 28 29 29 20 29 29 29 20 29 20 20 20 20 21 20 21 23 24 26 29 29 29 20 20 20 20 20 20 20 21 20 20 21 23 24 26 29 30 31	$\begin{array}{c} 255\\ 22215\\ 22215\\ 22215\\ 2222222222222$	2:42 2:42 2:35 2:35 2:38 2:40 2:35 2:38 2:40 2:25 2:30 2:25 2:20 2:20 2:08	$\begin{array}{c} 1.40\\ 1.40\\ 1.38\\ 1.40\\ 1.32\\ 1.35\\ 1.35\\ 1.38\\ 1.38\\ 1.38\\ 1.38\\ 1.25\\ 1.22\\ 1.22\\ 1.22\end{array}$	$\begin{array}{c} 0.75\\ .78\\ .722\\ .703\\ .685\\ .655\\ .723\\ .686\\ .60\\ .60\\ .60\end{array}$	$\begin{array}{c} 0.55\\.55\\.50\\.50\\.48\\.45\\.65\\.65\\.55\\.55\\.55\\.55\\.55\\.55\\.55\\.5$	$\begin{array}{c} 0.\ 62\\ .\ 60\\ .\ 55\\ .\ 55\\ .\ 52\\ .\ 45\\ .\ 43\\ .\ 33\\ .\ 30\\ .\ 35\\ .\ 25\\ .\ 25\\ \end{array}$

ST. VRAIN CREEK NEAR LYONS, COLORADO.

St. Vrain Creek and its tributaries derive their supply of water from the eastern slope of the Front Range, between Longs Peak and James Peak, which are about 30 miles apart. The general trend of the drainage is northeasterly, the St. Vrain flowing into South Platte River about 6 miles below the town of Platteville. The principal tributaries of the stream are the North and South forks and Boulder Creek. Sonth Boulder Creek is a tributary of the latter stream. In their upper portions these creeks flow through mountainous areas where the water is used only for power purposes and for placer mining, but at the foothills each stream emerges into a broad, approximately level valley, devoted entirely to farming, water being furnished by means of irrigation canals leading from the streams. Three stations are maintained on the main stream and its tributaries, namely, at Lyons, on the St. Vrain, at Boulder, on the Boulder, and at Marshall, on the South Boulder. The station at Lyons is about a half mile southeast of the town, and is below the intersection of the North and South forks.

Records of the flow of the creek at or near Lyons have been kept since April, 1888, except during the years 1893 and 1894, but the station was not put in its present condition until May 5, 1899, since when

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records have been kept throughout each irrigation season. The rod is an inclined timber on the left bank of the stream, opposite the Tower Hotel, fastened to pieces of timber driven into the slag embankment. The stream has an excellent channel of gravel and bowlders. and is not likely to change. Measurements have usually been made by wading, but at high water they are made from the bridge about a quarter of a mile below the gage rod. The bench mark is a spike 2 feet from the west side of the trunk of a large cottonwood tree 150 feet north of the rod. Supply ditch diverts water above the station, and its discharge should be added to that of the creek in order to obtain the total run-off of the basin. The observer during the year 1900 was L. H. Dickson, commissioner of the St. Vrain water district, who kept up the readings during the irrigation season. Weekly records of the discharge at this point have been furnished to the Longmont papers. During the greater part of the irrigation season the entire discharge of St. Vrain Creek is utilized, but during the flood period considerable water usually goes to waste. Much of the water is, however, stored in reservoirs, and is used to advantage at low stages of the stream. A description of the station was published in Water-Supply Paper No. 37, page 232. The results of measurements for 1899 will be found in the Twenty-first Annual Report, Part IV, page 208. During 1900 the following measurements were made by A. L. Fellows:

> March 13: Gage height, 2.06 feet; discharge, 35 second-feet. April 27: Gage height, 3.68 feet; discharge, 513 second-feet. July 27: Gage height, 2.70 feet; discharge, 193 second-feet.

Daily gage height, in feet, of St. Vrain Creek near Lyons, Colorado, for 1900.

	Day.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.
1				(10	4 50	0.50		0.15	2.10	2.0"
-1- 9				4.10	4.00	0.00 3.45	0.00	2.15	2.10	2.05
- ñ-				3.00	4.50	2 25	2.50	9.15	2 10	2.05
4				1.00	4.00	2.95	2.50	9 15	2.05	9.05
5				4.00	1 20	3 10	2.50	9.15	2.08	9.05
6				4.10	4.50	3 10	2 55	9 15	2.08	2.05
7				4.15	4.10	3 10	2 50	9 15	2 10	9.05
8			2.90	4.10	1 25	3 10	9 17	5 62		2.05
9		1 90	0.40	4 30	1 40	3.00	9 47	5 53	- 10 - 10	5 05
10		1.90		4 15	4 30	2.95	9 45	0.00	5 10	9.05
11		1.00		4 15	3 90	3.05	9 45	5.75	5 08	* 00
19				4 10	3.85	3.05	2 40	3 70	5 65	9 00
13		2.06		4 10	3.80	3.05	2 35	9 45	5 05	10.00
14		1.00		3 95	3.95	3.05	2.30	2.35	5.05	
15			2.06	3 75	3.80	3.05	2.30	2.25	2.05	
16			1.90	3.65	3.85	3.05	2.30	2 20	2 30	
17		1.85	1.85	3.70	3.85	3.00	2.30	2.15	2.25	
18		1100	1.90	3.70	3.90	2.90	2 25	2.15	2.20	
19.			1.85	3.65	3.95	2.90	2.25	2.12	2.20	
$\overline{20}$			1.90	3.50	4.00	2.80	2.25	2.12	9.95	
21.			1.90	3.60	4.00	2.75	2.25	2.12	2.20	
22		1.90	4.20	3.80	3.95	2.70	2.25	2.10	2.18	
23.			3.80	3.70	4.00	2.70	2.25	2.10	2.15	
24			3.90	3,95	3.90	2.80	2.23	2.08	2.15	
25.			3.80	3.60	3.80	2.75	2.23	2.10	2.15	
26.			3,80	4.00	3.65	2.70	2.20	2.18	2.15	
27.			3.70	4.20	3, 55	2.70	2.17	2.15	2.15	
28.			3.75	4.60	3.55	2.70	2.15	2.18	2.10	
29.			4.80	4.60	3,50	2.70	2.15	2.10	2.10	
30.		1.95	4.30	4.70	3.45	2.65	2.15	2.10	2.10	
31				4.50		2.65	2.15		2.05	

NOTE.-Regular readings did not begin until April 15.

290 OPERATIONS AT RIVER STATIONS, 1900. - PART III. [No. 49.

BIG THOMPSON CREEK NEAR ARKINS, COLORADO.

This stream drains the country immediately north of that drained by the headwaters of St. Vrain Creek, and is one of the largest tributaries of South Platte River, into which it empties about 4 miles above the town of Evans. Little Thompson Creek is an important tributary of Big Thompson Creek, and the country drained by these two streams makes up irrigation district No. 4. The junction of these creeks is near the lower end of the district, a short distance above the point where their combined waters enter the South Platte.

Records of the flow of this stream were begun in April, 1888, and have been maintained for a portion of each year since, with the exception of the years 1893 and 1894. The station was established at its present location on April 1, 1899. The only diversion above the gaging station is Handy ditch, a record of the gage heights of which is kept by the water commissioner of that district, J. M. Wolaver, who has also kept the records of Big Thompson Creek at this point during the year 1900. It is necessary to include the discharge of Handy ditch in order to obtain the total run-off of the basin. The rod is a vertical 2-inch by 4-inch timber fastened to the downstream side of the right-hand end of the wagon bridge on the ranch of John Chasteen. The bench mark is 25 feet south of the gage, and is a nail in the root of a cottonwood stump, the head of the nail being 9.35 feet above the zero of gage. The channel of the stream is lined with bowlders and is very rough, but, not being likely to change, it furnishes a good point for obtaining accurate measurements. A permanent station could be located here to advantage. Like the other tributaries of the South Platte, nearly all of the normal flow of Big Thompson and Little Thompson creeks is used for irrigation, and during the high-water stages the greater part of the volume is diverted into large reservoirs, from which it is used to advantage later in the season. A description of the station was published in Water-Supply Paper No. 37, page 233. The results of measurements for 1899 will be found in the Twenty-first Annual Report, Part IV, page 209. During 1900 the following measurements were made by A. L. Fellows:

> April 26: Gage height, 1.91 feet; discharge, 512 second-feet. July 26: Gage height, 1.35 feet: discharge, 322 second-feet.

Daily gage height, in feet, of Big Thompson Creek near Arkins, Colorado, for 1900.

Day.	Apr.	May.	June.	July.	Aug.	Sept.	Day.	Apr.	May.	June.	July.	Aug.	Sept.
1 2 3 4 5 6 9 10 11 12 13 14 14 16 11 12 13 14 14 13 14 14 15 15 16 17 10 11 12 13 14 15 15 10 11 12 13 14 15 15 15 16 17 17 17 18 19 11 12 11 14 14 15 16 17	$\begin{array}{c} 0.20\\ .20\\ .30\\ .50\\ .60\\ .60\\ .90\\ .90\\ 1.00\\ 1.00\\ 1.10\\ 1.90\\ 1.90\\ 1.90\\ \end{array}$	$\begin{array}{c} 3,50\\ 3,40\\ 3,40\\ 3,40\\ 2,80\\ 2,60\\ 2,60\\ 2,60\\ 2,60\\ 2,60\\ 2,80\\ 3,10\\ 3,10\\ 3,00\\ 2,90\\ 2,90\\ 2,90\\ 2,90\\ 2,90\end{array}$	$\begin{array}{c} 3.50\\ 3.60\\ 3.40\\ 3.20\\ 2.90\\ 3.00\\ 3.40\\ 3.50\\ 3.50\\ 3.00\\ 3.00\\ 2.90\\ 3.00\\$	$\begin{array}{c} 2.00\\ 1.80\\ 1.80\\ 1.70\\ 1.70\\ 1.70\\ 1.70\\ 1.80\\ 1.80\\ 1.70\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.60\\ 1.70\\ 1.70\\ 1.60\\ 1.60\\ 1.60\\ 1.70\\ 1.70\\ 1.60\\ 1.60\\ 1.70\\$	$\begin{array}{c} 1.10\\ 1.10\\ 1.10\\ 1.10\\ 1.10\\ 1.10\\ 1.10\\ 1.00\\ 1.00\\ .90\\ .80\\ .80\\ .80\\ .80\\ .80\\ .80\\ .80\\ .8$	$\begin{array}{c} 0.\ 70\\ .$	17 18 19 20 21 22 23 24 25 26 27 28 29 20 21 23 24 25 26 27 28 29 20 21 23 24 25 26 27 27 27 27 27 27 27 27 27 27	$\begin{array}{c} 1.60\\ 1.60\\ 2.00\\ 2.20\\ 1.90\\ 1.80\\ 1.80\\ 1.80\\ 1.80\\ 1.90\\ 2.10\\ 3.60\\ 3.50\\ \end{array}$	$\begin{array}{c} 2.70\\ 2.80\\ 2.80\\ 2.60\\ 2.65\\ 2.75\\ 2.75\\ 2.80\\ 3.10\\ 3.30\\ 3.50\\ 3.60\\ 3.70\\ 3.50\end{array}$	$\begin{array}{c} 2,90\\ 2,80\\ 2,80\\ 2,80\\ 2,80\\ 2,80\\ 2,80\\ 2,80\\ 2,80\\ 2,80\\ 2,60\\ 2,60\\ 2,50\\ 2,40\\ 2,30\\ \end{array}$	$\begin{array}{c} 1.50\\ 1.40\\ 1.40\\ 1.20\\ 1.20\\ 1.20\\ 1.30\\ 1.30\\ 1.20\\ 1.30\\ 1.20\\ 1.30\\ 1.20\\ 1.30\\ 1.10\\ \end{array}$	$\begin{array}{c} 0.80\\ .80\\ .80\\ .80\\ .80\\ .80\\ .80\\ .70\\ .70\\ .70\\ .70\\ .70\\ .70\\ .70\\ .7$	0.60 .60 .60 .60 .60 .60 .60 .60

Daily gage height, in feet, of Handy ditch near Arkins, Colorado, for 1900.

Day.	June.	July.	Aug.	Sept.	Day.	June.	July.	Aug.	Sept.	Day.	June.	July.	Aug.	Sept.
1 2 3 4 5 6 7 9 10 11		$\begin{array}{c} 1.20\\ 1.20\\ 1.20\\ 1.20\\ .80\\ .80\\ .72\\ .72\\ .72\\ .72\\ .72\end{array}$	$\begin{array}{c} 0.40 \\ .40 \\ .40 \\ .40 \\ .40 \\ .40 \\ .40 \\ .45 \\ .45 \\ .40 \\ .40 \end{array}$	$\begin{array}{c} 0.32\\ .30\\ .30\\ .30\\ .30\\ .30\\ .30\\ .30\\ .30$	$\begin{array}{c} 12 \\ 13 \\ 14 \\ 15 \\ 16 \\ 17 \\ 18 \\ 20 \\ 21 \\ 22 \\ 22 \\ \ldots \end{array}$	2.20 2.20 2.20 2.20 2.20 2.20 2.20 2.20	0. 72 22 22 22 22 22 22 22 22 22 22 22 22		$\begin{array}{c} 0.30\\ .30\\ .30\\ .30\\ .30\\ .30\\ .30\\ .30$	23 24 25 26 27 27 28 29 30 31	$\begin{array}{c} 2.20\\ 2.20\\ 2.20\\ 2.20\\ 2.20\\ 1.20\\ 1.20\\ 1.20\\ 1.20\\ \end{array}$	$\begin{array}{c} 0.40 \\ .40 \\ .40 \\ .40 \\ .40 \\ .40 \\ .40 \\ .40 \\ .40 \\ .40 \end{array}$	0.33232323232	. 30 . 30 . 30 . 30 . 30 . 30 . 30

CACHE LA POUDRE RIVER NEAR FORT COLLINS, COLORADO.

This stream is the northernmost of the large tributaries of the South Platte which issue from the east front of the Rocky Mountains. During the irrigating season its discharge is augmented by the supply diverted from the headwaters of Laramie River, which lie immediately to the west of the headwaters of the Cache la Poudre, the diversion being made through Sky Line canal. Measurements of the discharge of the Cache la Poudre Basin, therefore, include some of the Laramie waters. Practically the entire flow of the Cache la Poudre is used for irrigation purposes, even the greater part of the flood waters being stored for use later in the season. It is along the valley of the Cache la Poudre that the earliest and best irrigation of the State has been carried on.

The gaging station, which was established in 1884, is about 15 miles above Fort Collins. Since its establishment it has been maintained under the direction of Prof. L. G. Carpenter, of the Colorado State Agricultural College. The records are from the figures published by Professor Carpenter in the daily papers. The figures of daily discharge for the years 1895 to 1899, inclusive, will be found in Water-Supply Paper No. 37, pages 235 to 237.

Day.	Apr.	May.	June,	July.	Aug.	Sept.	Oct.
1		2,551	3,951	1,360	369	204	140
i) N		2,508	3,938	1,276	355	199	137
3		2,447	4,080	1,176	341	160	122
4		2,251	3,600	1,042	374	143	122
5		2,461	3,104	958	460	133	122
6		2,354	3,602	871	435	126	122
7		2,447	4,376	853	392	124	1.22
8		2,486	4,227	827	315	137	1.22
9		2,586	4,193	795	299	183	122
10		2,777	4,180	752	292	260	141
11		3,012	3,224	705	276	255	141
12		2,992	2,978	666	260	151	141
13		2,811	2,813	641	247	157	141
14		2,652	3,001	625	235	156	141
15		2,411	2,797	597	214	144	141
16		2,049	2,968	599	218	138	141
17		2,143	2,923	576	218	133	
18	427	2,258	2,622		218	126	
19	556	2,095	2,189	525	214	118	
20	823	2,271	2,567	0.0	212	113	
21	1,108	2,582	2,013	481	210	122	
//////////////////////////////////////	1,004	2, 525	2,441	460	248	1:2:3	
23	1,240	2,490	2,400	1/0	195	121	
64	1,200	2,884	2, 329	400	200	121	
40	1, 200	2,959	2,140	/0/ ~10	198	120	
20	1, 10+	0.640	1,000	419	~10 919	141	
64	1,204	0,001	1,010	509	÷1÷	111	
40	1,004	4,071	1,074	558	201	140	
59 90	9 520	4,000	1,040	592	100	140	
90	a, 000	4, 110	1,040	508	204	141	
		1,204		300	~0±		
Mean	1,376	2,808	2,942	721	265	149	132

Daily discharge, in second-fect, of Cache la Poudre River near Fort Collins, Colorado, for 1900.

[Continued in Water-Supply Paper No. 50, where will be found tables of computations of seepage on numerous streams in Colorado.]

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Sixteenth Annual Report of the United States Geological Survey, 1894-95, Part II. Papers of an economic character, 1895; octavo, 598 pp.

Contains a paper on the public lands and their water supply, by F. H. Newell, illustrated by a large map showing the relative extent and location of the vacant public lands; also a report on the water resources of a portion of the Great Plains, by Robert Hay.

A geological reconnoissance of northwestern Wyoming, by George H. Eldridge, 1894; octavo, 72 pp. Bulletin No. 119 of the United States Geological Survey; price, 10 cents.

Contains a description of the geologic structure of portions of the Bighorn Range and Bighorn Basin, especially with reference to the coal fields, and remarks upon the water supply and agricultural possibilities.

Report of progress of the division of hydrography for the calendar years 1893 and 1894, by F. H. Newell, 1895; octavo, 176 pp. Bulletin No. 131 of the United States Geological Survey; price, 15 cents.

Contains results of stream measurements at various points, mainly within the arid region, and records of wells in a number of counties in western Nebraska, western Kansas, and eastern Colorado.

1896.

Seventeenth Annual Report of the United States Geological Survey, 1895-96, Part II, Economic geology and hydrography, 1896; octavo, 864 pp.

Contains papers on "The underground water of the Arkansas Valley in eastern Colo-rado," by G. K. Gilbert; "The water resources of Illinois," by Frank Leverett, and "Pre-liminary report on the artesian waters of a portion of the Dakotas," by N. H. Darton.

Artesian-well prospects in the Atlantic Coastal Plain region. by N. H. Darton, 1896; octavo, 230 pp., 19 plates. Bulletin No. 138 of the United States Geo-logical Survey; price, 20 cents.

Gives a description of the geologic conditions of the coastal region from Long Island, N. Y., to Georgia, and contains data relating to many of the deep wells.

Report of progress of the division of hydrography for the calendar year 1895, by F. H. Newell, hydrographer in charge, 1896; octavo, 356 pp. Bulletin No. 140 of the United States Geological Survey; price, 25 cents.

Contains a description of the instruments and methods employed in measuring streams and the results of hydrographic investigations in various parts of the United States.

1897.

Eighteenth Annual Report of the United States Geological Survey, 1896-97, Part IV, Hydrography, 1897; octavo, 756 pp.

Contains a "Report of progress of stream measurements for the calendar year 1896," by Arthur P. Davis; "The water resources of Indiana and Ohio," by Frank Leverett; "New developments in well boring and irrigation in South Dakota," by N. H. Darton, and "Res-ervoirs for irrigation," by J. D. Schuyler.

1899.

Nineteenth Annual Report of the United States Geological Survey, 1897-98, Part IV, Hydrography, 1899; octavo, 814 pp.

Contains a "Report of progress of stream measurements for the calendar year 1898," by F. H. Neweil and others; "The rock waters of Ohio," by Edward Orton, and "Preliminary report on the geology and water resources of Nebraska west of the one hundred and third meridian," by N. H. Darton. Part II of the Nineteenth Annual contains a paper on "Principles and conditions of the movements of ground water," by F. H. King, and one on "Theoretical investigation of the motion of ground waters," by C. S. Slichter.

1900.

Twentieth Annual Report of the United States Geological Survey, 1898–99, Part IV, Hydrography, 1900; octavo, 660 pp.

Contains a "Report of progress of stream measurements for the calendar year 1898," by F. H. Newell, and "Hydrography of Nicaragua," by A. P. Davis.

1901.

Twenty-first Annual Report of the United States Geological Survey, 1899-1900, Part IV, Hydrography, 1900; octavo, 768 pp.

Contains a "Report of progress of stream measurements for the calendar year 1899," by F.H. Newell; "Preliminary description of the geology and water resources of the southern half of the Black Hills and adjoining regions in South Dakota and Wyoming," by N. H. Darton; and "The High Plains and their utilization," by W.D.Johnson.

Bulletins can be obtained only by prepayment of cost, as noted above. Money should be transmitted by postal money order or express order, payable to the Director of the United States Geological Survey. Postage stamps, checks, and drafts can not be accepted. Correspondence should be addressed to

The Director, U. S. Geol. Survey, Washington, D. C.

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WATER-SUPPLY AND IRRIGATION PAPERS.

1. Pumping water for irrigation, by Herbert M. Wilson, 1896.

2. Irrigation near Phœnix, Arizona, by Arthur P. Davis, 1897.

3. Sewage irrigation, by George W. Rafter, 1897.

4. A reconnoissance in southeastern Washington, by Israel C. Russell, 1897.

5. Irrigation practice on the Great Plains, by E. B. Cowgill, 1897.

6. Underground waters of southwestern Kansas, by Erasmus Haworth, 1897.

7. Seepage waters of northern Utah, by Samuel Fortier, 1897.

8. Windmills for irrigation, by E. C. Murphy, 1897.

9. Irrigation near Greeley, Colorado, by David Boyd, 1897.

10. Irrigation in Mesilla Valley, New Mexico, by F. C. Barker, 1898.

11. River heights for 1896, by Arthur P. Davis, 1897.

12. Underground waters of southeastern Nebraska, by N. H. Darton, 1898.

13. Irrigation systems in Texas, by W. F. Hutson, 1898.

14. New tests of pumps and water lifts used in irrigation, by O. P. Hood, 1898.

15, 16. Operations at river stations, 1897, Parts I, II, 1898.

17. Irrigation near Bakersfield, California, by C. E. Grunsky, 1898.

18. Irrigation near Fresno, California, by C. E. Grunsky, 1898.

19. Irrigation near Merced, California, by C. E. Grunsky, 1899.

20. Experiments with windmills, by Thomas O. Perry, 1899.

21. Wells of northern Indiana, by Frank Leverett, 1899.

22. Sewage irrigation, Part II, by George W. Rafter, 1899.

23. Water-right problems of Bighorn Mountains, by Elwood Mead, 1899.

24, 25. Water resources of the State of New York, Parts I, II, by G.W. Rafter, 1899.

26. Wells of southern Indiana (continuation of No. 21), by Frank Leverett, 1899.

27, 28. Operations at river stations, 1898, Parts I, II, 1899.

29. Wells and windmills in Nebraska, by Erwin Hinckley Barbour, 1899.

30. Water resources of the Lower Peninsula of Michigan, by Alfred C. Lane, 1899.

31. Lower Michigan mineral waters, by Alfred C. Lane, 1899.

32. Water resources of Puerto Rico, by H. M. Wilson, 1900.

33. Storage of water on Gila River, Arizona, by J. B. Lippincott, 1900.

34. Geology and water resources of southeastern S. Dak., by J. E. Todd, 1900.

35-39. Operations at river stations, 1899, Parts I-V, 1900.

40. The Austin dam, by Thomas U. Taylor, 1900.

41, 42. The windmill: its efficiency and use, Parts I, II, by E. C. Murphy, 1901.

43. Conveyance of water in irrigation canals, etc., by Samuel Fortier, 1901.

44. Profiles of rivers, by Henry Gannett, 1901.

45. Water storage on Cache Creek, California, by Albert E. Chandler, 1901.

46. Reconn. of Kern and Yuba rivers, Cal., by F. H. Olmsted and M. Manson, 1901. 47-52. Operations at river stations, 1900, Parts I-VI, 1901.

Other papers are in various stages of preparation. Provision has been made for printing these by the following clause in the sundry civil act making appropriations for the year 1896–97:

Provided, That hereafter the reports of the Geological Survey in relation to the gaging of streams and to the methods of utilizing the water resources may be printed in octavo form, not to exceed 100 pages in length and 5,000 copies in number; 1,000 copies of which shall be for the official use of the Geological Survey, 1,500 copies shall be delivered to the Senate, and 2,500 copies shall be delivered to the House of Representatives, for distribution. (Approved, June 11, 1896; Stat. L., vol. 29, p. 453.)

The endeavor is made to send these pamphlets to persons who have rendered assistance in their preparation through replies to schedules or who have furnished data. Requests made for a certain paper and stating a reason for asking for it are granted whenever practicable, but it is impossible to comply with general demands, such as to have all of the series sent.

Application for these papers should be made either to members of Congress or to

THE DIRECTOR, UNITED STATES GEOLOGICAL SURVEY, WASHINGTON, D. C.

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